



## SUSITNA HYDROELECTRIC PROJECT

January 8, 1982  
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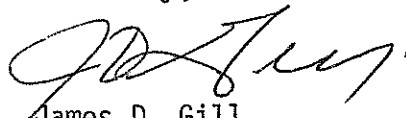
Dear Mr. Yanagawa:

I am enclosing for your review the following reports prepared by the Alaska Department of Fish and Game for the Susitna Hydroelectric Project:

1. Final Draft Report, Adult Anadromous Fisheries Project
2. Resident and Juvenile Anadromous Fish Investigations on the Lower Susitna River
3. Aquatic Habitat Investigations

These reports are provided for your information only, they are not part of our formal Agency Coordination Program. Comments are not requested but will certainly be accepted.

Sincerely,

  
James D. Gill  
Resident Manager

JDG/ja

Encl: as

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ALASKA POWER AUTHORITY

SUSITNA HYDROELECTRIC PROJECT

TASK 2 - SURVEYS AND SITE FACILITIES

SUBTASK 2.10  
ACCESS PLANNING STUDY

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Anchorage, Alaska



ALASKA POWER AUTHORITY  
SUSITNA HYDROELECTRIC PROJECT  
ACCESS PLANNING STUDY

TABLE OF CONTENTS

LIST OF TABLES

LIST OF FIGURES

1 - INTRODUCTION

- 1.1 The Study Area
- 1.2 Study Description
- 1.3 Objectives and Scope of Study
- 1.4 Plan Formulation and Selection Process
- 1.5 Organization of Report

2 - SUMMARY

- 2.1 Scope of Work
- 2.2 Previous Studies
- 2.3 Project Design
- 2.4 Project Schedule
- 2.5 Logistics Requirements
- 2.6 Project Parameters
- 2.7 Alternative Segments
- 2.8 Alternative Access Plans

3 - SCOPE OF WORK

- 3.1 Corridor Selection
- 3.2 Modal Split Analysis
- 3.3 Access Plan Development

4 - PREVIOUS STUDIES

- 4.1 U.S. Army Corps of Engineers - 1975 and 1979
- 4.2 Others

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5 - PROJECT DESIGN

- 5.1 The Dams and Related Facilities
- 5.2 The Construction Camps
- 5.3 The Permanent Village
- 5.4 Air Strip
- 5.5 Project Access

6 - PROJECT SCHEDULE

- 6.1 Power Demand Growth
- 6.2 Generating Facility Schedule
- 6.3 Access Facility Schedule Constraints

7 - LOGISTICS REQUIREMENTS

- 7.1 Construction Equipment, Materials and Supplies
- 7.2 Support Requirements
- 7.3 Permanent Village
- 7.4 Summary of Freight Movements
- 7.5 Personnel Movements

8 - ACCESS ROUTE DESIGN PARAMETERS

- 8.1 Roadway Parameters
- 8.2 Railroad Parameters

9 - CORRIDOR SELECTION

- 9.1 Methodology
- 9.2 Discussion of Alternative Segments
  - A. Description
  - B. Line and Grade
  - C. Drainage Features
  - D. Bridges
  - E. Soils
  - F. Environmental

H. Segment Suitability

9.3 Corridor Summary

10 - ACCESS PLANS

10.1 Supply Sources and Shipping Options

10.2 Alaska Ports

10.3 Modal Options

10.4 Access Plans

A. Ports

B. Modal Split

C. Segments Included

D. Cost Estimates

E. Advantages/Disadvantages

11 - CONCLUSIONS AND RECOMMENDATIONS

12 - APPENDICES

A. Preliminary Design Development

B. Proposed Alternative Segments

C. Alternative Comparison - Grade, Curvature and  
Distance

D. Terrain Unit Mapping

E. Environmental Concerns

F. Cost Estimates

## LIST OF TABLES

<u>Table</u>	<u>Page</u>
2.1 Major Quantities in the Dams	2-2
2.2 Average Weekly Freight Movements	2-3
2.3 Approved Roadway Design Parameters	2-4
2.4 Approved Railroad Design Parameters	2-4
2.5 Linehaul Rates in Dollars/Ton-mile	2-7
7.1 Major Quantities in the Dams	7-2
7.2 Construction Fleet	7-3
7.3 Required Diesel Fuel Requirements for Construction	7-4
7.4 Required Diesel Fuel Flow Rates	7-4
7.5 Required Material Flow Rates	7-5
7.6 Summary of Required Average Material Flow Rates	7-7
8.1 Original Proposed Design Criteria	8-2
8.2 Approved Roadway Design Parameters	8-4
8.3 Approved Railroad Design Parameters	8-4
10.1 Mileage from Ports to Railhead or Project	10-6
10.2 Across the Dock Handling Costs	10-7
10.3 Linehaul Rates in Dollar/Ton-Mile	10-8
10.4 Maintenance Factors	10-9
10.5 Basic Corridor Segments	10-9
C.1 Summary of Alignment Parameters	C-1
C.2 Combination of Alignment Parameters	C-2
F.2.1 Across the Dock Handling Costs	F-2
F.2.2 Linehaul Rates in Dollars/Ton Mile	F-2
F.4.1 Railhead Cost Estimate	F-8
F.7.1 Culverts	F-34

<u>Table</u>	<u>Page</u>
F.8.1 Access Construction Estimates - Segment A-1	F-37
F.8.2 Access Construction Estimates - Segment A-2	F-38
F.8.3 Access Construction Estimates - Corridor 1	F-39
F.8.4 Access Construction Estimates - Segment B-1	F-40
F.8.5 Access Construction Estimates - Segment B-2	F-41
F.8.6 Access Construction Estimates - Segment B-3	F-42
F.8.7 Access Construction Estimates - Corridor 2	F-43
F.8.8 Access Construction Estimates - Corridor 3	F-44
F.8.9 Access Construction Estimates - Segment R-1	F-45
F.8.10 Access Construction Estimates - Segment R-2	F-46
F.8.11 Access Construction Estimates - Segment Railroad	F-47
F.8.12 Access D&C Costs - Corridor 1	F-48
F.8.13 Access D&C Costs - Corridor 2	F-49
F.8.14 Access D&C Costs - Corridor 3	F-50
F.8.15 Access D&C Costs - Railroad	F-51
F.9.1 Maintenance Costs	F-52
F.10.1 Watana Logistic Breakdown	F-54
F.10.2 Devil Canyon Logistic Breakdown	F-55
F.10.3 Roadhaul Segment Costs	F-56
F.10.4 Logistics Total	F-57

## LIST OF FIGURES

<u>Figure</u>	<u>Page</u>
1.1 Location Map	1-9
1.2 Access Study Logic Diagram	1-10
2.1 Project Access Location Alternatives	2-5
8.1 Typical Road Cross Section	8-3
8.2 Typical Railroad Cross Section	8-5
9.1 Susitna Access Corridor - Segments 1A, AB	9-8
9.2 Susitna Access Corridor - Segments 1C, 1D, 1E, 1F	9-16
9.3 Susitna Access Corridor - Segments 2A, 2B	9-21
9.4 Susitna Access Corridor - Segments 2C, 2D, 2E	9-27
9.5 Susitna Access Corridor - Segments 2F, 2G, 2H	9-32
9.6 Susitna Access Corridor - Segments 2I, 2J, JK	9-38
9.7 Susitna Access Corridor - Segments 2L	9-41
9.8 Susitna Access Corridor - Segments 2R	9-44
9.9 Susitna Access Corridor - Segments 2RR	9-46
9.10 Susitna Access Corridor - Segments 3A, 3B, 3C	9-52
9.11 Project Access Location Alternatives	9-55
9.12 Susitna Access Corridor Borrow Areas	9-56
10.1 Access Plan #1	10-12
10.2 Access Plan #2	10-15
10.3 Access Plan #3	10-18
10.4 Access Plan #4	10-21
10.5 Access Plan #5	10-24
10.6 Access Plan #6	10-26
10.7 Access Plan #7	10-30
10.8 Access Plan #8	10-33

<u>Figure</u>	<u>Page</u>
A.1 Watana Dam Plan	A-5
A.2 Devil Canyon Dam Plan	A-6
A.3 Preliminary Watana Schedule	A-7
A.4 Preliminary Devil Canyon Schedule	A-8
B.0 Access Corridors - Index Map	B-2
B.1 Access Corridors - Alignments	B-3
B.2 Access Corridors - Alignments	B-4
B.3 Access Corridors - Alignments	B-5
B.4 Access Corridors - Alignments	B-6
B.6 Access Corridors - Alignments	B-7
B.7 Access Corridors - Alignments	B-8
B.8 Access Corridors - Alignments	B-9
B.9 Access Corridors - Alignments	B-10
B.14 Access Corridors - Alignments	B-11
B.15 Access Corridors - Alignments	B-12
B.16 Access Corridors - Alignments	B-13
B.17 Access Corridors - Alignments	B-14
B.18 Access Corridors - Alignments	B-15
B.19 Access Corridors - Alignments	B-16
B.20 Access Corridors - Alignments	B-17
B.21 Access Corridors - Alignments	B-18
D.0 Terrain Unit Properties and Engineering Interpretation	D-2
D.1 Access Corridors - Terrain Unit Maps	D-3
D.2 Access Corridors - Terrain Unit Maps	D-4
D.3 Access Corridors - Terrain Unit Maps	D-5
D.4 Access Corridors - Terrain Unit Maps	D-6
D.6 Access Corridors - Terrain Unit Maps	D-7
D.7 Access Corridors - Terrain Unit Maps	D-8
D.8 Access Corridors - Terrain Unit Maps	D-9
D.9 Access Corridors - Terrain Unit Maps	D-10

D.14	Access Corridors - Terrain Unit Maps	D-11
D.15	Access Corridors - Terrain Unit Maps	D-12
D.16	Access Corridors - Terrain Unit Maps	D-13
D.17	Access Corridors - Terrain Unit Maps	D-14
D.18	Access Corridors - Terrain Unit Maps	D-15
D.19	Access Corridors - Terrain Unit Maps	D-16
D.20	Access Corridors - Terrain Unit Maps	D-17
D.21	Access Corridors - Terrain Unit Maps	D-18
E.1.1	Access Corridors - Index Map	E-2
E.1.2	Access Corridors - Environmental Conflicts	E-3
E.1.3	Access Corridors - Environmental Conflicts	E-4
E.1.4	Access Corridors - Environmental Conflicts	E-5
E.1.5	Access Corridors - Environmental Conflicts	E-6
E.1.6	Access Corridors - Environmental Conflicts	E-7
E.1.7	Access Corridors - Environmental Conflicts	E-8
E.1.8	Access Corridors - Environmental Conflicts	E-9
E.1.9	Access Corridors - Environmental Conflicts	E-10
E.1.10	Access Corridors - Environmental Conflicts	E-11
E.1.11	Access Corridors - Environmental Conflicts	E-12
E.1.12	Access Corridors - Environmental Conflicts	E-13
E.1.13	Access Corridors - Environmental Conflicts	E-14
E.1.14	Access Corridors - Environmental Conflicts	E-15
F.4.1	Typical Plan - Rail to Truck Transfer Facility	F-4
F.5.1	Indian River Bridge	F-11
F.5.2	Susitna River Bridge	F-12
F.5.3	1160' Bridge South of Devil Canyon	F-13
F.5.4	Fog Creek Bridge	F-14
F.5.5	1000' Bridge Southeast of Devil Canyon	F-15
F.5.6	Susitna River Bridge at Devil Canyon	F-16



Figure

Page

F.6.1 Typical Road Section - 0-10% cross-slope	F-18
F.6.2 Typical Road Section - 15% cross-slope	F-19
F.6.3 Typical Road Section - 25% cross-slope	F-20
F.6.4 Typical Road Section - 30% cross-slope	F-21
F.6.5 Typical Road Section - 35% cross-slope	F-22
F.6.6 Typical Road Section - 40% cross-slope	F-23
F.6.7 Typical Road Section - 45% cross-slope	F-24
F.6.8 Typical Road Section - 50% cross-slope	F-25
F.6.9 Typical Railroad Section 0 to 10% cross-slope	F-26
F.6.10 Typical Railroad Section 15% cross-slope	F-27
F.6.11 Typical Railroad Section 25% cross-slope	F-28
F.6.12 Typical Railroad Section 30% cross-slope	F-29
F.6.13 Typical Railroad Section 35% cross-slope	F-30
F.6.14 Typical Railroad Section 40% cross-slope	F-31
F.6.15 Typical Railroad Section 45% cross-slope	F-32
F.6.16 Typical Railroad Section 50% cross-slope	F-33

## INTRODUCTION

SUSITNA HYDROELECTRIC PROJECT  
ACCESS PLANNING  
REPORT

1 - INTRODUCTION

The Susitna Hydroelectric Project has, for many years, been considered a viable source of "clean" energy for Central Alaska. The project has been viewed as including one or more dams on the upper Susitna River. Extensive preliminary work has been done on the project by various government agencies. In an effort to expedite the project, the State of Alaska through the Alaska Power Authority, in late 1979, initiated the necessary feasibility studies and preparation of the necessary FERC (Federal Energy Regulatory Commission) license application. Access to the project is a part of those studies.

1.1 - The Study Area

The location of the project is approximately 120 air miles north of Anchorage (see Figure 1.1). The dams, as proposed, would be upstream from Talkeetna laying between the Parks Highway and the Denali Highway. This area is remote, with no existing access. The quantities of materials and supplies required for construction of the project and for the maintenance of the construction camps are of such a magnitude as to require major transportation facilities to serve the project site.

1.2 - Study Description

The Access Planning Study involved the selection of potential highway and railroad alignments that would serve the dam sites

selected for detailed study. The process involved aerial reconnaissance of the potential corridors, definition of the parameters which control the horizontal and vertical alignment and the selection and analysis of alternative alignments which serve the needs of the entire project.

### 1.3 - Objectives And Scope of Study

The objectives of the Access Planning Study are as follows:

- (a) To define an access route location or combination of route locations that will serve the supply needs of the hydroelectric project with a minimum of environmental impact.
- (b) To determine a reasonable combination of transportation modes which will provide a cost effective system of supply.
- (c) To define an access plan that will meet the overall scheduling requirements of the hydroelectric project.

The Scope of the Study includes the definition and analysis of routes within three general corridors. Corridor 1 is located on the north side of the Susitna River from the Parks Highway to the Watana site. Corridor 2 is on the south side of the Susitna River between the same general termini. Both corridors were required to serve both Devil Canyon and Watana Dam site. The third corridor connects the Watana Dam site with the Denali Highway to the north. Both road and railroad access are to be considered.

The study must examine the corridors and generate preliminary route locations and cost estimates. The costs estimates will include the costs of constructing the access, maintaining the facility and moving material over the route. The environmental impacts of the various alignments are to be addressed under Task 7, however a

continuous flow of input from the environmental studies will be provided to aid in studying the alignments.

Engineering, Soils, Cost and Environmental information will be combined to develop alternate access plans that satisfy the stated objectives. This report will present those alternate plans.

#### 1.4 - PLAN FORMULATION AND SELECTION PROCESS

There are a number of important factors to be considered in developing and analysing transportation facility plans. The locations of the dams, of course, dictate terminal points common to all access plans. The number and size of loads of material and supplies together with the volume of traffic to be generated by the construction camp population dictate the design parameters appropriate to the facility. The terrain, soils and environmental concerns control and limit the possible location for the facility. All of these factors will be considered.

##### (a) Planning Methodology

The planning process for transportation facilities of this magnitude is one of a series of iterations in which proposals are developed, tested, revised and tested again until a plan emerges that serves the desired function in a cost effective and environmentally sound manner. Following this pattern design parameters were developed then potential alignments were selected that appeared to serve the project needs. A number of alternative alignments were identified for further consideration. During the process of evaluating the engineering considerations of the alternatives some were eliminated and some sections of others were revised so that

all remaining sections conformed to the required design parameters. The information on the remaining sections was then given to the geological team and the environmental team for additional input. Consideration of this input has resulted in elimination of additional sections and changes in some of those remaining. The various available port facilities and transportation modal options were identified and then combined with the remaining possible alignments to form possible access plans. Each plan was then analyzed to determine how well the project objectives were satisfied. Any advantages or disadvantages were identified and the estimated costs for construction, maintenance and logistics were developed.

(b) Economic Analysis

Each access plan has four major cost factors associated with it. Each of the cost factors were considered and used in comparing the alternate access plans and determining the cost-effectiveness of the various plans.

- ° Construction cost estimates were prepared for each alternative. These estimates were very preliminary and valid only for comparison and determining the order of cost magnitude. More refined cost estimates are not possible or necessary at this stage of the work. Detailed cost estimates are not possible due to the lack of micro-scale data. The estimates prepared are, however, correct with regard to order of magnitude and, because of the assumptions, for comparison purposes.
- ° Maintenance cost estimates were developed for the

various plans. These costs covered only maintenance on the facility constructed. Maintenance costs on existing facilities that may be attributable to the project would be difficult to identify and the difference between plans would be insignificant.

- ° Logistics costs as used herein are the costs associated with moving material, supplies and equipment to the site. Port costs, freight rates for various modes, and the transportation modal split combine to generate significant cost variations when comparing access plans. Each plan was evaluated by estimating the transportation costs for major material items to be moved to the site.
- ° Schedule costs were discussed in terms of time delays that would result from selecting any of the alternate plans. Dollar costs were not estimated for any such delays because the complexities of such estimates go far beyond the scope of this work. It is intuitively obvious, however, that with a project of the magnitude of the Susitna Hydroelectric Project any delays from the planned schedule will have major construction cost ramifications due to inflation and social cost ramifications resulting from the inability to meet the demand for power.

#### 1.5 - Organization of Report

The objective of the report is to present a series of alternative access plans which serve the needs of the Susitna Hydroelectric project. The report does not include a single recommended plan.

The body of the report contains a discussion of the pertinent features. Detailed technical information is contained in a series of appendices. The report is organized as follows.

Section 1. Introduction

Section 2. Summary

The section contains a complete Summary of the report.

Section 3. Scope of Work

This section outlines the Scope of Work associated with the results presented with this document.

Section 4. Previous Studies

This section briefly summarizes the access information available in previous Susitna Basin Studies done by others.

Section 5. Project Design

This Section briefly describes the Susitna Hydroelectric Project in a way that sets the stage for the remainder of the access analysis.

Section 6. Project Schedule

This section discusses the overall planned schedule for the Susitna Hydroelectric Project and identifies the scheduling requirements for construction of the access facilities.



## Section 7. Logistics Requirements

This section presents the estimated quantities of the major items of equipment, materials and supplies that must be transported to the site during the course of construction, including the supplies necessary for the construction camp. Any particular constraints affecting the mobilization and/or movement of material for access construction are also discussed.

## Section 8. Access Design Parameters

This section discusses the specifics of the basic design parameters for both road and railroad construction. The parameters discussed include curvature, maximum grades, horizontal and vertical clearance requirements, load requirements and surfacing requirements.

## Section 9. Corridor Selection

This section discusses the process by which the suggested corridors were selected for study and includes a discussion of each of the alignment segments originally investigated.

## Section 10. Access Plans

This section presents a series of alternate access plans including a discussion of the pros and cons of the various available ports, shipping options, and land transportation modes. Cost estimates for each plan are developed which include construction, maintenance and logistics costs.

## Section 11. Conclusions and Recommendations

Conclusions and recommendations are not a part of this report because additional environmental data is to be considered along

with the data presented here. A final recommendation is expected to result from that analysis combined with the results of this study.

## APPENDICIES

- Appendix A Preliminary Design Development
- Appendix B Proposed Alternative Segments
- Appendix C Alternative Comparison - Grade, Curvature  
and Distance
- Appendix D Terrain Unit Maps
- Appendix E Environmental Concerns
- Appendix F Alternative Plans

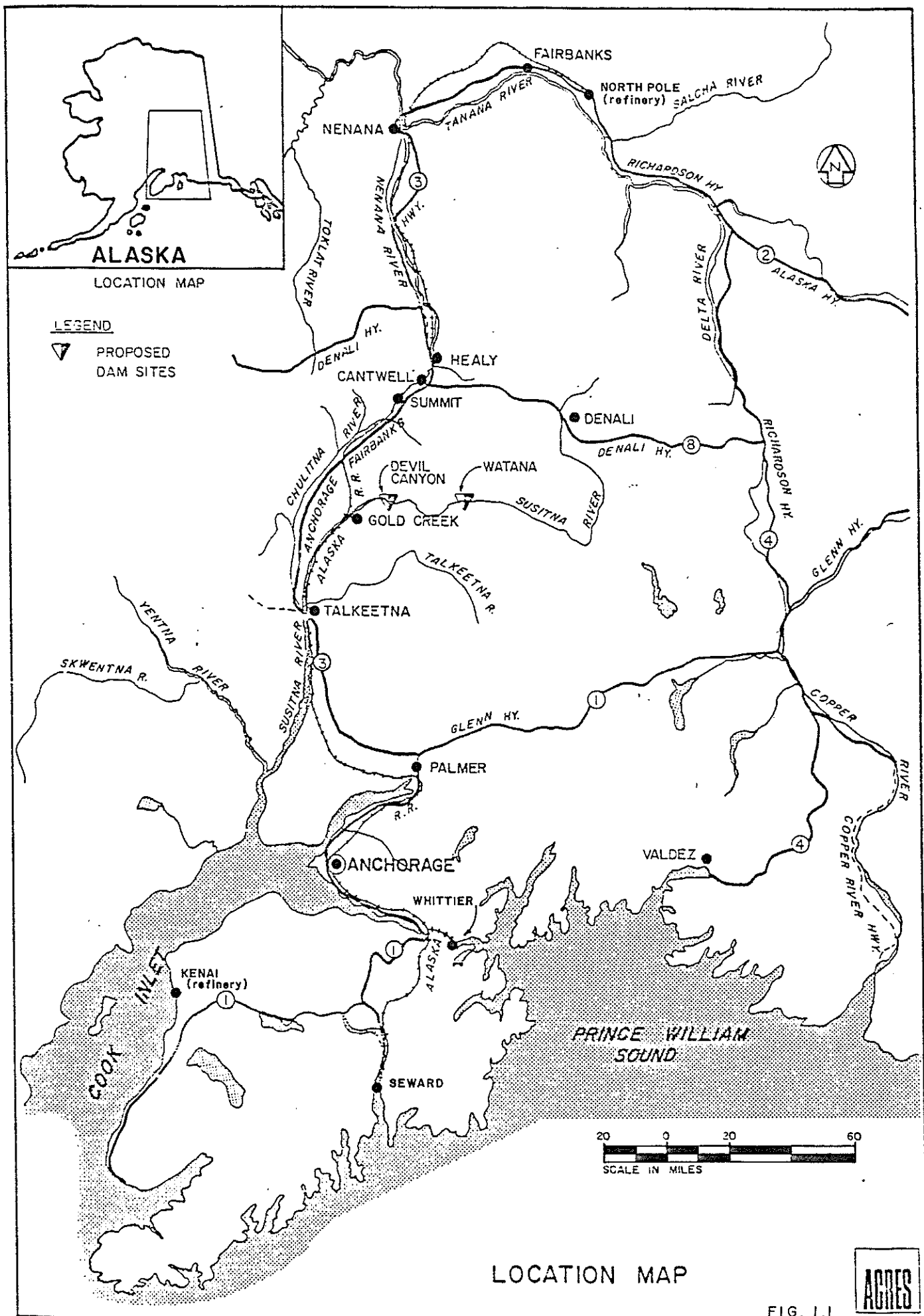
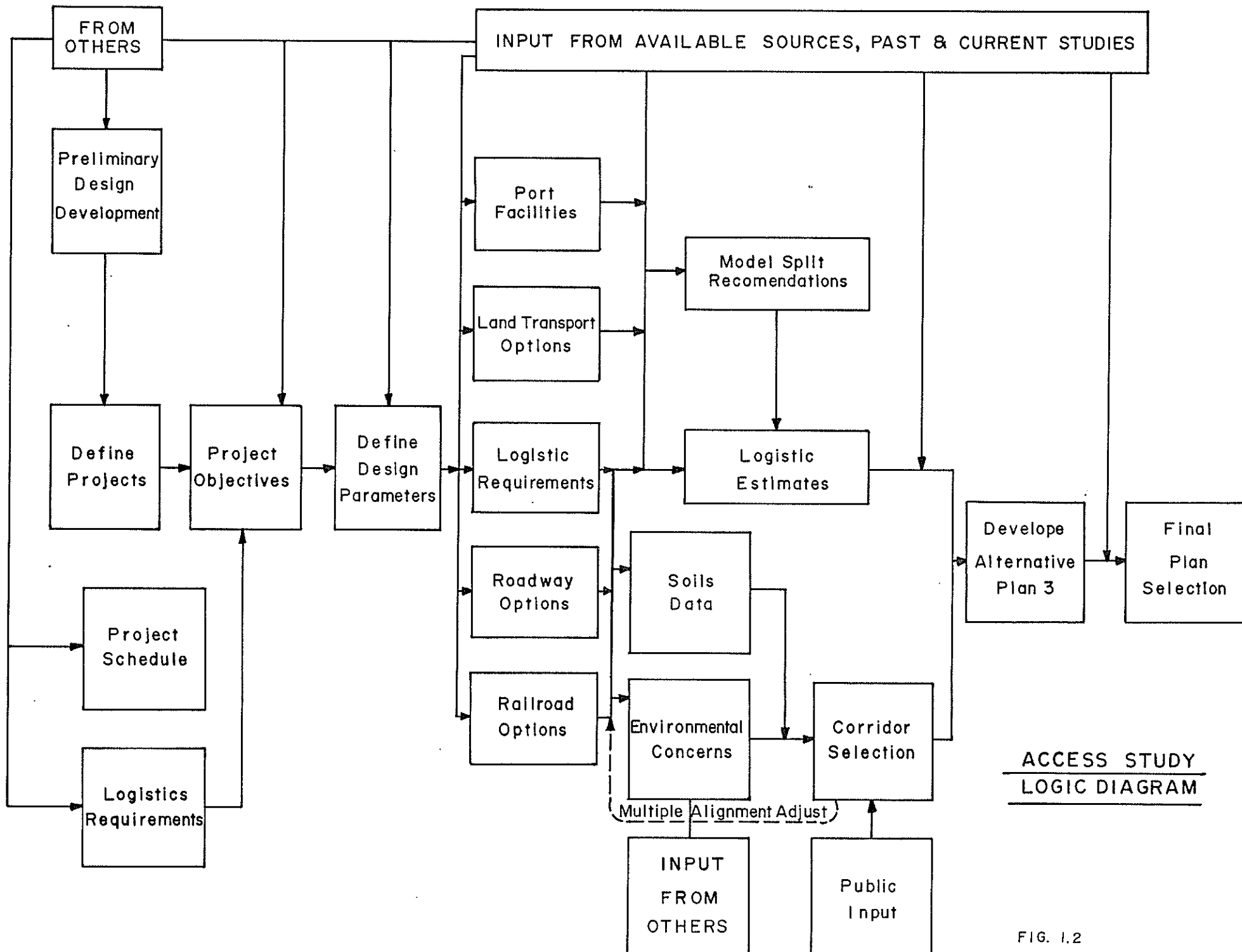


FIG. 1.1





ACCESS STUDY  
LOGIC DIAGRAM

## SUMMARY

## 2 - Summary

This summary is intended to provide a brief overview of the access study, its methods and results.

### 2.1 - Scope of Work

The scope of work for the Susitna Access Study was defined in general terms in the original Plan of Study (POS) for the Susitna Hydroelectric Project. The POS required that three corridors be examined and the both road and rail options be included. The access plan was required to serve both Watana and Devil Canyon Dams and be able to satisfy the desired project schedule.

### 2.2 - Previous Studies

Previous studies of the Susitna Hydroelectric project were reviewed to determine the extent of work that had been done relative to access. Very little had been done. The Corps of Engineers had carried the access question the furthest and their 1975 reports included a roadway that followed closely the alignment described as Plan 1 from Parks Highway to Watana on the south side of the river via Gold Creek.

### 2.3 - Project Design

Preliminary design of the hydroelectric project provided input to the access study. The quantities of materials to be imported to the project site and the size of the work crews were considered in estimating the costs of transportation and in selecting the ports and land transportation modal splits suggested in the various plans.

Watana  
1993  
Devil Canyon -  
2000

#### 2.4 - Project Schedule

The overall schedule for the Susitna Hydroelectric project has been set based on projected power requirements in the region. These studies show that power from Watana Dam is needed first with power on line required in 1993. A period of eight years is projected to build the facility. This requires initial construction in 1985. The Federal Energy Regulatory Commissions license is anticipated in late 1984 on early 1985. Construction of access facilities cannot predate the FERC license therefore an access plan was desired that would allow mobilization and resupply activities to occur in 1985. This meant a plan providing access to Watana that could be made passable in one construction season. The estimated construction time for Devil Canyon is seven years with construction projected to begin in 1993.

#### 2.5 - Logistics Requirements

The primary requirements for imported material and supplies were provided by other tasks. The volumes of materials were combined with planned construction schedules to project required average rates of flow for supplies.

TABLE 2.1


#### Major Quantities in the Dams

	<u>Watana</u>	<u>Devil Canyon</u>
Excavation (Rock & Earth)	22,000,000 c.y.	5,000,000 c.y.
Fill	76,000,000 c.y.	1,335,000 c.y.
Construction Equipment	16,000 ton	5,000 ton
Explosives	20,000 ton	3,000 ton
Cement	350,000 ton	650,000 ton
Reinforcing Steel	33,000 ton	22,000 ton
Rock Bolts	12,500 ton	3,000 ton
Steel Support & Liners	3,600 ton	2,200 ton
Mechanical, Structural & Electrical Equipment	15,000 ton	13,500 ton
Fuel	75,000,000 gal.	17,000,000 gal.

Camp populations were estimated at 4,500 persons for Watana and 3,100 persons for Devil Canyon. Past experience shows that camps of this size require 13 pounds of food and supplies per occupant and 1.1 gallons of fuel oil per occupant on a daily basis.\* These quantities where combined with the construction schedules to develop the following average material flow requirements for the project.

\* Data provided by Arctic Hosts, Inc., Anchorage Alaska.

TABLE 2.2  
SUMMARY OF REQUIRED AVERAGE MATERIAL FLOW RATES

	<u>Watana Dam</u>	<u>Devil Canyon Dam</u>
Trucks	90	110
Contingency & Misc.	<u>18</u>	<u>22</u>
 Total	108 Truck Loads/week	132 Truck Loads/week
Rail Cars	39	44
Contingency & Misc.	<u>8</u>	<u>9</u>
Total	47 Rail Car Loads/week	53 Rail Car Loads/week

## 2.6 - Project Parameters

The required freight movements and the size and weight of transformers and other major components were used to establish parameters for line, grade and load requirements for both railway and roadway options. These parameters were then used to identify potential access routes and are based on standards published by The American Association of State Highway and Transportation Officials (AASHTO) and the American Railway Engineering Association (AREA).



TABLE 2.3

APPROVED ROADWAY DESIGN PARAMETERS

Design Speed	60 mph
Maximum Grade	6%
Maximum Curvature	5%
Design Loading (Construction Period)	80 Kip Axle & 200 Kip total
Design Loading (After Construction)	HS-20

*APSC grade  
ID-1216*

TABLE 2.4

APPROVED RAILROAD DESIGN PARAMETERS

Maximum Grade	2.5%
Maximum Curvature	10°
Loading	E-72.

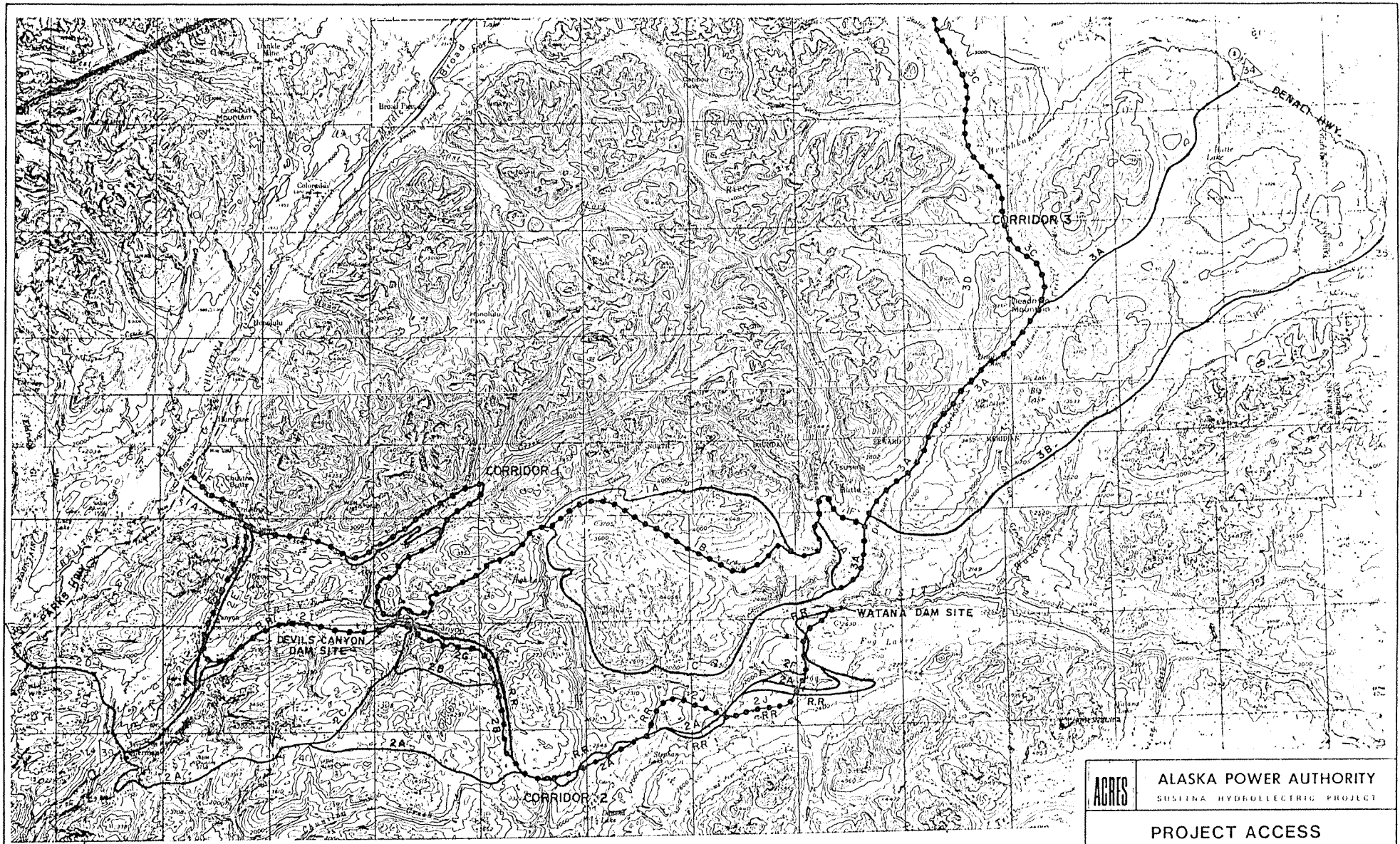
2.7 - Alternatives Segments

The design parameters were used to define a series of alternative alignment segments that could be mixed and matched to define alternate access routes meeting project requirements. The segments as originally defined were given to the soils and environmental teams for their input. That input, along with engineering considerations was used to eliminate some segments and modify others. The remaining segments were combined to establish preferred routes in each corridor. These corridor alignments are shown on Figure 2.1.

2.8 - Alternative Access Plans

Alternative access plans were developed. Each plan included recommended Alaskan ports, line haul mode, location of transfer points and delivery mode.

FIG. 2.1



REV

—●—●—●— PREFERRED ROUTE IN EACH CORRIDOR  
— OTHER ALTERNATES INVESTIGATED



ACRES	ALASKA POWER AUTHORITY SUSTINA HYDROELECTRIC PROJECT
	PROJECT ACCESS LOCATION ALTERNATIVES
SCALE: 1" = 1 MILE	

The sea ports checked include the following:

Anchorage  
Seward  
Whittier  
Valdez

Anchorage is the preferred port for those items suitable for shipment in conventional containers and trucks. The port has the apparent adequate capacity and the best facilities of the four. The drawback in Anchorage is a lack of capabilities for roll-on roll-off rail shipment. Anchorage does, at times, have an ice problem.

Seward is unable to compete directly with Anchorage in facilities or capacity. Seward is suitable for an overflow port as there is equipment available to handle container cargo and there is direct rail and highway access. Seward is an ice free port.

Whittier is unique in that there is roll-on roll-off rail capability. Because of freight rates and handling charges Whittier is the obvious choice for arrival of all materials that can be shipped by rail car.

Valdez has a considerable capacity and is expanding its port facilities. Valdez has been eliminated from major consideration for a number of reasons that would contribute to increases in project cost.

- ° Lack of Rail Service
- ° Highest Wharfage and Handling Costs of Any of the Four
- ° Longest Truck Haul to the Project

Anchorage and Whittier are the ports selected and are common to all plans.

Line haul rates were collected from the Alaska Railroad and several trucking firms. A comparison of line haul rates is shown below.

TABLE 2.5  
LINE HAUL RATES IN DOLLARS/TON-MILE

<u>Item</u>	<u>Rail</u>	<u>Truck</u>
Equipment	0.1878	0.2069
Steel	0.2577	0.2069
Cement	0.1565	0.2069
Fuel	0.1450	0.2069
General Cargo	0.1262	0.2069
Explosives	0.6267	0.2069

While certain items may move by truck with lower costs, the mix of items and quantities make it clear that the overall most cost effective line haul mode is rail. For this reason all plans contemplate rail haul to the maximum extent practicable.

A total of seven access plans have been outlined. There are no plans including the segments around Portage Creek as the engineering, soils and environmental problems have combined to make the Portage Creek drainage very undesirable.

Plan 1 serves both Devil Canyon and Watana Dam by road south of the Susitna River. This plan includes a rail head at Gold Creek and road access to the Parks Highway. This plan encounters significant amounts of critical wildlife habitat around Stephan and Fog Lakes. There are some extensive areas of deep organic soils and soils containing massive ice near Stephan Lake. There are major schedule constraints involving two major bridges and extensive rock construction. The schedule constraints are such

that the construction of Watana could be delayed by as much as three years.

Plan 2 is the railroad alternative to Plan 1. Plan 2 also does not satisfy the requirement of being able to allow resupply of construction activities at Watana in one construction season.

Plan 3 serves Watana by road from the Denali Highway east of Cantwell. A railhead is called for at Cantwell. Access to the Devil Canyon Dam is by road with a railhead at Gold Creek. This plan meets all primary objectives of the study but does not include a direct connection between Watana and Devil Canyon. The roadway from Denali Highway can be made usable for construction equipment and resupply in one construction season allowing access to Devil Canyon to be constructed as required.

Plan 4 is similar to Plan 3 except that access to Devil Canyon is to be by rail rather than road.

Plan 5 uses all roadway connecting with the Parks Highway and a railhead at Gold Creek. The south side of the river is followed to Devil Canyon. At this point the plan calls for a high bridge over the Susitna River and utilization of the north side alignment between Devil Canyon and Watana. This plan avoids the majority of the identified environmentally critical areas of all three corridors. There is a major time constraint however. The high bridge at Devil Canyon would have to be a suspension bridge approximately 2600 feet long. Such a bridge would require a three year construction period thus delaying construction of Watana by at least that much.

Plan 6 is the same as Plan 4 except that a road is included between Watana and Devil Canyon for the exclusive use of the maintenance and operations personnel. This plan satisfies all major objectives of the study.

Plan 7 is the same as Plan 3 except that a road is included between Watana and Devil Canyon for the exclusive use of the maintenance and operations personnel. This plan satisfies all major objectives of the study.

The final choice of access plan will be made after additional input from the remainder of the study team can be evaluated.

SCOPE OF WORK

### 3 - SCOPE OF WORK

The Scope of Work discussed in this Section includes the development and selection of corridor alignments, an analysis of modal split options and selection of alternative access plans designed to provide a cost effective access system that will satisfy the project requirements while meeting the project schedule.

Further details of the Scope of Work may be found in Acres' Plan of Study (POS).

#### 3.1 - Corridor Selection

The initial step in selecting the corridors was definition of the parameters that control line and grade. Preliminary estimates of the size and weight of the critical components were made and the width, grade and curvature parameters were selected to allow movement of those components

After the controlling parameters were defined, possible alignments were identified using 1:63,360 scale contour maps. A number of alternate segments were identified for further analysis. Potential corridors were to be identified on both sides of the Susitna River from the Parks Highway to Watana and, from Watana north to the Denali Highway. At least one corridor was to include a potential for rail service to both Dam sites.

The alternative segments were grouped into possible total routes. The possible routes were compared with regard to alignment, gradient, soil conditions, environmental constraints and other considerations to determine the most favorable alignment within each corridor.



### 3.2 Modal Split Analysis

The modal split analysis was necessary to suggest the optimum mix of transportation modes and the most advantageous transfer point between modes.

Potential seaports and the cargo handling capability of the respective ports are of prime importance. It was necessary to determine if roll-on roll-off rail barge service was possible or if material must come by barge and be transferred to rail and/or truck.

Freight rates for the railroad and for truck haul were checked to determine the most economical way to ship various items within the State of Alaska.

The estimated quantities of the major items were supplied from other tasks. Using these quantities and the rate information a variety of modal mix options were examined to determine the cost effectiveness of the apparent options.

### 3.3 Access Plan Development

This effort is a mix and match exercise in which the various combinations of potential corridor segments and modal split options are tested to compare cost effectiveness of the over all plan and the degree to which overall project time schedules are served. The cost effectiveness of the various plans are based on combined costs of construction, maintenance and logistics over the construction life of the project. The degree to which the overall time schedule can be satisfied is based on two factors, estimated construction time for the access facility and whether the plan will allow initial work on the dams to begin as planned.

PREVIOUS STUDIES

#### 4 - PREVIOUS STUDIES

The studies done by the various agencies that have looked at the Susitna Hydroelectric project have presented much information on the many alternative power development plans. These same studies have included very little data on access to the project. Generally, construction of a road is presumed and little else is mentioned.

##### 4.1. U.S. Corps of Engineers

The 1975 report prepared by the Corps of Engineers incorporated a road access that corresponds very closely with one of the corridors defined in the study. That access proposal began at the Parks Highway near Chulitna Station, parallels the Alaska railroad south and east to a crossing of the Susitna river then proceeds up the south side of the river to Devil Canyon and on the the Watana site via the north end of Stephan Lake and the west end of Fog Lakes. The facility contemplated was a 24-foot wide roadway designed for 30 miles per hour. A rail head was planned at Gold Creek also.

##### 4.2 Others

Other studies done on the Susitna Hydroelectric project over the years mentioned access only in passing and and did not develop access plans.

## PROJECT DESIGN

## 5 - PROJECT DESIGN

The Susitna Hydroelectric Project is developing as a two dam system. The total system will include, in addition to the dams themselves, all associated on-site power generating facilities, and transmission facilities. A large construction camp with all of the required support facilities will be needed during construction, at each dam, and a permanent village for the operating and maintenance staff will be necessary after construction is complete. An airstrip and other access facilities over which all of the equipment, personnel and supplies will reach the project site must be provided as early in the project as possible.

### 5.1 - The Dams and Related Facilities

- (a) The Watana Dam is projected to be a large earth and rockfill structure involving placement of approximately 76 million cubic yards of zone type embankment that will come largely from borrow areas near the site. The dam is to be located on the main stream of the Susitna River a short distance above the mouth of Tsusena Creek. During construction, the river is to be diverted through tunnels which will be gated and used for other purposes after completion of the work. The Power house is planned to be underground while the spillways are to be surface structures configured to prevent nitrogen saturation of downstream waters. Staging areas for construction activities are available on both sides of the river at the Watana Site.
- (b) The Devil Canyon Dam is projected to be a concrete arch structure set in the section of the Susitna River known as Devil Canyon. To achieve planned pool elevation, a low saddle dam will be required south of the main dam. River

diversion will again be through tunnels during the construction period and the power house for this structure will also be underground. Construction activities will probably be staged from the south side at Devil Canyon because of the terrain.

- (c) The Transmission Lines are proposed for the north side of the river from Watana west to a connection with the Anchorage-Fairbanks intertie near Chulitna Pass. The final location of the transmission corridor has not been selected as of this time.

#### 5.2 - Construction Camps

A Construction Camp is expected to be located near the Watana site and probably on the north side of the river. Manpower requirements based on quantities of materials and projected construction schedule show a need for up to 4,500 persons during the peak of construction activities at Watana. Current plans call for a construction camp at each of the dams. There is a shortage of land suitable for a camp near the Devil Canyon site, however, there is one site near the south end. Manpower projections for Devil Canyon construction indicates a peak population of 3,100 persons.

#### 5.3 - Permanent Village

The size and complexity of the overall system will require a full time maintenance and operations staff. Projections show that this staff including their dependents will require a permanent village of approximately 45 dwelling units plus support buildings.

for both?

#### 5.4 - Airstrip

Over-all project development, the size of the work force involved and the remote nature of the site indicate that an airstrip will be desirable for a wide variety of reasons including the movement of personnel and a need of rapid emergency evacuation capability. To that end, a runway site has been located on the north side of the Susitna River near the proposed site for the Watana construction camp. It is expected that the airstrip will be constructed very early in the project. The proposed facility would be adequate for aircraft up to and including a C-130. The location study for the airstrip has been done as a part of another task.

#### 5.5 - Project Access

Providing access into a remote area such as the upper Susitna, while small in comparison to the total project, is a major undertaking in itself. Massive quantities of material, supplies, equipment and fuel must be moved to the project site in an uninterrupted flow. Estimates of the amounts of the principal materials to be imported to the site and used in construction of the dams and related facilities are included in Appendix A. The movement of materials in such quantities requires a railroad or a high type of highway comparable to rural highways throughout the country. The access to the project is the topic of this study.

PROJECT SCHEDULE



## 6 - PROJECT SCHEDULE

The Susitna Hydroelectric project is intended to provide electrical power to the Alaska Railbelt region. The time frame for providing the required generating capacity has been determined as a result of Task 6 "Design Development".

### 6.1 - Power Demand Growth

The load and demand growth projections presented in the Task 6 "Design Development" report indicate that more electrical power will be required by the year 2000 than can be generated by the Susitna Hydroelectric Project alone. The demand over and above that which Susitna can satisfy will have to be provided from other sources, quite probably fossil fuel fired steam generators. The demand growth curves indicate that power from the Watana Dam is needed in 1993 and power from Devil Canyon Dam is needed by 2000. The Watana generating capacity can be installed in stages with the initial 400 megawatts available in 1993 and the second 400 megawatts on line in 1996.

### 6.2 - Generating Facility Schedule

Construction periods for Watana Dam and Devil Canyon Dam are projected as eight years and seven years respectively. If power from Watana is needed in 1993 and an eight-year period is required to construct the dam then construction must begin in 1985. Power from Devil Canyon is needed in 2000. Backing up seven years indicates that construction must begin in 1993. The construction schedules currently show access construction beginning January 1985 with work on the diversion tunnels beginning during the second quarter of 1985 and on the cofferdams and main abutments of Watana in the third quarter of 1985.

### 6.3 - Access Facility Schedule Constraints

Access is an integral part of the total project and as such is subject to FERC approval for construction. Current project schedules are based on FERC licensing in late 1984. Access construction is currently planned to begin in very early 1985, as soon as possible following FERC licensing. If access construction is to begin in 1985 and construction activities on the dam are to begin in mid to late 1985 then it is necessary that an access facility be provided that can be passable for heavy equipment, explosives and fuel supplies sometime during the 1985 construction season. Any access plan that cannot be brought to rough grade and kept passable in a single construction season will require one of two schedule adjustments, access construction prior to FERC licensing or delay in work on the Watana Dam.

LOGISTICS REQUIREMENTS

## 7 - LOGISTICS REQUIREMENTS

The dams and associated facilities are of a size that require vast quantities of equipment, materials, supplies and personnel for construction. Because of the remote location, a base camp must be provided that will resemble a small town complete with all essential services near each dam site. A permanent village must also be provided for the operations and maintenance personnel who will be stationed at the project when construction is completed.

The principle logistics requirements include the equipment, materials and supplies necessary for the dams and related facilities including the camp and permanent village, the food and other items necessary to provide for the crew during construction and the logistics requirements for construction of the access facilities. The requirements for the dams and related facilities and the camp supply needs will be discussed here. Logistic requirements for the alternate access plans will not be discussed in detail. Logistic requirements at access construction will vary with location, length, and bridge requirements. Significant constraints of access construction will be identified however, the cost of this element of logistics will be included in the estimated construction costs.

### 7.1 - Construction Equipment, Materials and Supplies

The following estimates of equipment, materials and supplies are presented as a basis for the cost estimates to be generated as a part of analyzing and comparing the various access plans to be presented.

The major quantities to be incorporated into the project are shown in Table 7.1.

Table 7.1 Major Quantities in the Dams

	<u>Watana</u>	<u>Devil Canyon</u>
Excavation (Rock & Earth	22,000,000 c.y.	5,000,000 c.y.
Fill	76,000,000 c.y.	1,335,000 c.y.
Construction Equipment	16,000 ton	5,000 ton
Explosives	20,000 ton	3,000 ton
Cement	350,000 ton	650,000 ton
Reinforcing Steel	33,000 ton	22,000 ton
Rock Bolts	12,500 ton	3,000 ton
Steel Support & Liners	3,600 ton	2,200 ton
Mechanical, Structural		
Electrical Equipment	15,000 ton	13,500 ton
Fuel	75,000,000 gal.	17,000,000 gal.

Additional items that will be required for each dam include: Tires, Equipment Parts, and miscellaneous lumber and building material. Actual estimated quantities are not available and are largely a function of the contractor's operation.

For a comparison of transportation costs only the easily identified major items will be listed individually. These items will allow comparisons of the relative differences in transportation costs when reviewing alternative plans.

In order to estimate quantities of fuel, tires and parts required at each site, estimates of equipment fleets with average unit fuel consumption figures were made. See Table 7.2.

The fuel consumption rates shown in Table 7.2 are estimates based on Alaskan General Contractors experience with similar equipment.

Table 7.2 Construction Fleet

<u>Equipment</u>	<u>Fuel Per Unit (1 gallon/hr.)</u>	<u># Units *</u>	
		<u>Watana</u>	<u>Devil Canyon</u>
40 C.Y. End Dumps	21	40	6
8 C.Y. Loaders	15.5	10	5
Motor Patrols (Cat 14)	6.5	8	4
D-9	17	30	5
D-7	8	10	3
Cranes	10	2	4
Rock Crusher	20	1	2
Screening Plant	10	1	2
Concrete Plant	10	1	2
Mixer Trucks	10	3	3
Fork Lifts	5	6	6
Dump Trucks	10	10	2
Compactors	8	6	2
Power Generator	20	2	2
Miscellaneous	7	20	15
Pickups and other Gasoline Vehicles	2	60	30

	<u>Watana</u>	<u>Devil Canyon</u>
By Rail: Flat car loads	133	66
By Road: Truck loads	67	31
self driven units	143	62
Total Units	210	93

---

\* The number of units represents the anticipated number of pieces necessary based on the materials needed to be moved, amount of time per machine to move them and the total time frame provided to complete the task. When this input was not available it is a result of estimates from previous project experience.

Table 7.3

## WEEKLY DIESEL FUEL REQUIREMENTS FOR CONSTRUCTION

<u>Equipment Type</u>	<u>Watana gallons/week</u>	<u>Devil Canyon gallons/week</u>
End Dumps	94,080	14,100
Loaders	17,360	8,680
Motor Patrols	5,820	2,900
D-9	57,120	9,520
D-7	8,960	2,700
Cranes	2,240	4,480
Crushers	2,240	4,480
Screening Plant	1,120	2,240
Concrete Plant	1,120	2,240
Mixer Trucks	3,360	3,360
Fork Lifts	3,360	3,360
Dump Trucks	11,200	2,240
Compactors	5,380	1,790
Power Generator	4,480	4,480
Miscellaneous Vehicles	15,680	11,760
<b>** Total Gallons per week</b>	<b>227,700</b>	<b>78,330</b>

\* Assume 24 hours per day and seven days per week. An assumption has been made that 1/3 of the equipment will be down for service and maintenance at all times this provides for 112 hours/week base.

\*\* This is an estimated average fuel flowage during the major portion of the activity. Actual flowage may vary significantly.

Table 7.4

## REQUIRED DIESEL FUEL

	<u>Watana</u>	<u>Devil Canyon</u>
<u>Diesel Fuel</u>	227,700 Gal./wk.	78,330 Gal./wk.
<u>Truck Loads</u>		
@ 7,500 Gal./load ***	30 Loads/wk.	10.4 Loads/wk.
<u>Rail Car Loads</u>		
@ 20,000 Gal/load ***	11 Loads/wk.	4 Loads/wk.

\*\*\* Sizes of loads are typical of what is currently available.

TABLE 7.5  
REQUIRED MATERIAL FLOW RATES

	<u>Watana</u>	<u>Devil Canyon</u>
<u>Gasoline</u>	20,160 Gal./wk.	10,000 Gal./wk.
Truck Loads	3 Loads/wk.	1.3 Loads/wk.
@ 7,500 Gal./load		
Rail Car Loads	1 Load/wk.	0.5 Load/wk.
@ 20,000 Gal./load		
 <u>Time Requirement***</u>	 7 yrs.	 6 yrs.
<u>Cement</u>	350,000 ton	650,000 ton
Quantity per week	1154 ton/wk.	2,500 ton/wk.
Truck Loads @ 30 ton/Load*	38.5 Loads/wk.	83.3 Loads/wk.
Rail Car Loads @ 75 ton/Load*	15.4 Load/wk.	33.3 Load/wk.
 <u>Steel (all)</u>	 49,100 ton	 27,200 ton
Quantity per week	162 ton/wk.	105 ton/wk.
Truck @ 30 ton	5.4 Loads/wk.	3.5 Loads/wk.
Rail Car Loads @ 75 ton	2.2 Loads/wk.	1.4 Load/wk.
 <u>Explosives</u>	 20,000 ton	 3,000 ton
Quantity per week	66 ton/wk	11.5 ton/wk
Truck loads @ 30 ton	2.2 load/wk	0.4 load/wk
Rail Carloads @ 75 ton	0.9 load /wk	0.15 load/wk
 <u>Mechanical, Structural</u>	 15,000 ton	 13,500 ton
<u>Electrical</u>		
Quantity per week	49.5 ton/wk	52 ton/wk
Truck loads @ 30 ton	1.6 load/wk	1.7 load/wk
Railcars loads @ 75 ton	0.7 load/wk	0.7 load/wk
 <u>Tires and Parts **</u>	 2 Loads/wk.	 2 Loads/wk.
Truck loads		
 Subtotal Trucks Loads/wk.	 52.7	 92.2
Subtotal Rail Cars Loads/wk.	22.2	38.1

\* Sizes of loads are typical of what is currently available.

\*\* This Figure represents a rough estimate of truck/rail car loads of materials that will be needed for maintenance of construction equipment.

\*\*\* Assumed deliveries over 10 months per year activity and 1 year less than total construction time. The schedules show startup period of about one year before the peak activity levels are approached.



## 7.2 - Support Requirements

Supplies and fuel for the base camps must flow steadily and smoothly. It has been estimated the construction camp population will be approximately 4,500 for Watana and 3,100 for Devil Canyon. A camp operation report together with information from experienced arctic work camp contractors indicates a camp of 3,000-5,000 people would require approximately thirteen (13) pounds of food and supplies per person per day and fuel for power and heat at 1.1 gallons per person per day. These figures convert to the following delivery rates:

### Camp Supplies

$$\frac{4500 \text{ persons}}{2000 \text{ lb./ton}} \times \frac{13 \text{ lb.}}{\text{man-day}} \times \frac{7 \text{ days}}{\text{week}} = 204.8 \text{ tons/week (Watana)}$$

$$\frac{3100 \text{ persons}}{2000 \text{ lb./ton}} \times \frac{13 \text{ lb.}}{\text{man-day}} \times \frac{7 \text{ days}}{\text{week}} = 141.1 \text{ tons/week (Devil Canyon)}$$

	<u>Watana</u>	<u>Devil Canyon</u>
Truck Loads @ 30 tons each =	6.8 load/wk	4.7 load/wk
Rail Cars @ 75 tons each =	2.7 load/wk	1.9 load/wk

### Camp Fuel

$$\frac{4500 \text{ persons}}{1} \times \frac{1.1 \text{ gal.}}{\text{day}} \times \frac{7 \text{ days}}{\text{week}} = 35,000 \text{ gal./week (Watana)}$$

$$\frac{3100 \text{ persons}}{1} \times \frac{1.1 \text{ gal.}}{\text{day}} \times \frac{7 \text{ days}}{\text{week}} = 24,000 \text{ gal./week (Devil Canyon)}$$

Truck Loads @ 7,500 gallons = 5 loads per week for Watana; 3½ per week for Devil Canyon.

Rail Car Loads @ 20,000 gallons = 2 loads per week for Watana; 1¼ per week for Devil Canyon.

### 7.3. - Permanent Village

The permanent Village is estimated as 45 dwelling units. It is expected that construction of the village will occur over a period of two years at an average of two truck loads of materials per dwelling unit.

### 7.4 - Summary of Freight Movements

The following summary of freight movements is intended to show the order of magnitude for transport requirements on the access facility.

Table 7.6  
SUMMARY OF REQUIRED AVERAGE MATERIAL FLOW RATES

	<u>Watana Dam</u>	<u>Devils Canyon Dam</u>
Trucks	95	111
Contingency & Misc.	<u>19</u>	<u>22</u>
Total	114 Trucks Loads/week	133 Truck Loads/week
Rail Cars	38	45
Contingency & Misc.	<u>8</u>	<u>9</u>
Total	46 Rail Cars Loads/week	54 Rail Cars Loads/week

Note: Total includes Tables 7.4, 7.5, camp supplies and camp fuel. Total does not include initial mobilization of construction equipment or materials for permanent village.

## 7.5 - Personnel Movements

In addition to the requirements for moving freight the workers themselves must be moved to the site. There are at least four options for accomplishing the movement of personnel depending on the nature of the access facility provided and the types of controls put on the construction personnel. Construction crews and support personnel will be working 7 days per week and three shifts per day. Even with this kind of schedule large numbers of people will be off shift at any one time. It would seem appropriate that these people have some way of leaving the area. Options include the following:

1. An aircraft shuttle
2. A rail shuttle if rail only is provided
3. A bus shuttle
4. Private vehicles

An aircraft shuttle could be used for the movement of personnel to the construction camp. Transportation costs would be high and the mode is extremely vulnerable to weather limitations.

Several of the access plans outlined herein include options for access to all or part of the project by rail only. The camp populations are such that a steady flow of personnel to and from camp may be expected. If only ten percent of the population travels on a given day, the total person trips will be in the range of 300 to 500 daily.

*where is  
this  
figure?*

Rail coaches normally seat 50 to 80 persons. If access to either dam is limited to rail only, then a regularly scheduled shuttle train of an engine and two to four passenger cars will be needed to provide the required service. This service combined with the freight haul requirements will necessitate additional rail sidings and a much more complex communication system on the rails.

If roads are provided as primary access to the job site, a bus shuttle could be provided for personnel movements. This would best be handled by commercial carrier. The cost could be borne either by the individual or the project.

The use of private vehicle would be the simplest method to administer. It would also allow the workers the greatest flexibility. If only 10% of the population travels on a given day, traffic volumes on the access road could exceed 500 vehicles per day. Traffic volumes at this level normally warrant a paved surface rather than a gravel surface.

For the purpose of comparison, in this report, logistics costs will not include passenger transportation.

ACCESS ROUTE  
DESIGN PARAMETERS

## 8. - ACCESS ROUTE DESIGN PARAMETERS

The plan of study for the Susitna Project calls for the analysis of three general routes and two transportation modes to provide access to the proposed dam sites from port facilities or instate sources of supply. Consideration must be given to using road, railroad or a combination of both to serve the project.

The alternate routes to be studied were required to accomodate the following:

- Serve all dam sites that might be proven feasible by other portions of the overall study.
- Corridors had to be included on the North and South sides of the Susitna River with connections to the Alaska Railroad near Gold Creek, to the Parks Highway and to the Denali Highway.

In order to be able to make a valid comparison between alternatives a basis for that comparison must be established, with this thought in mind, proposed design ciriteria were developed.

### 8.1 - Roadway Parameters

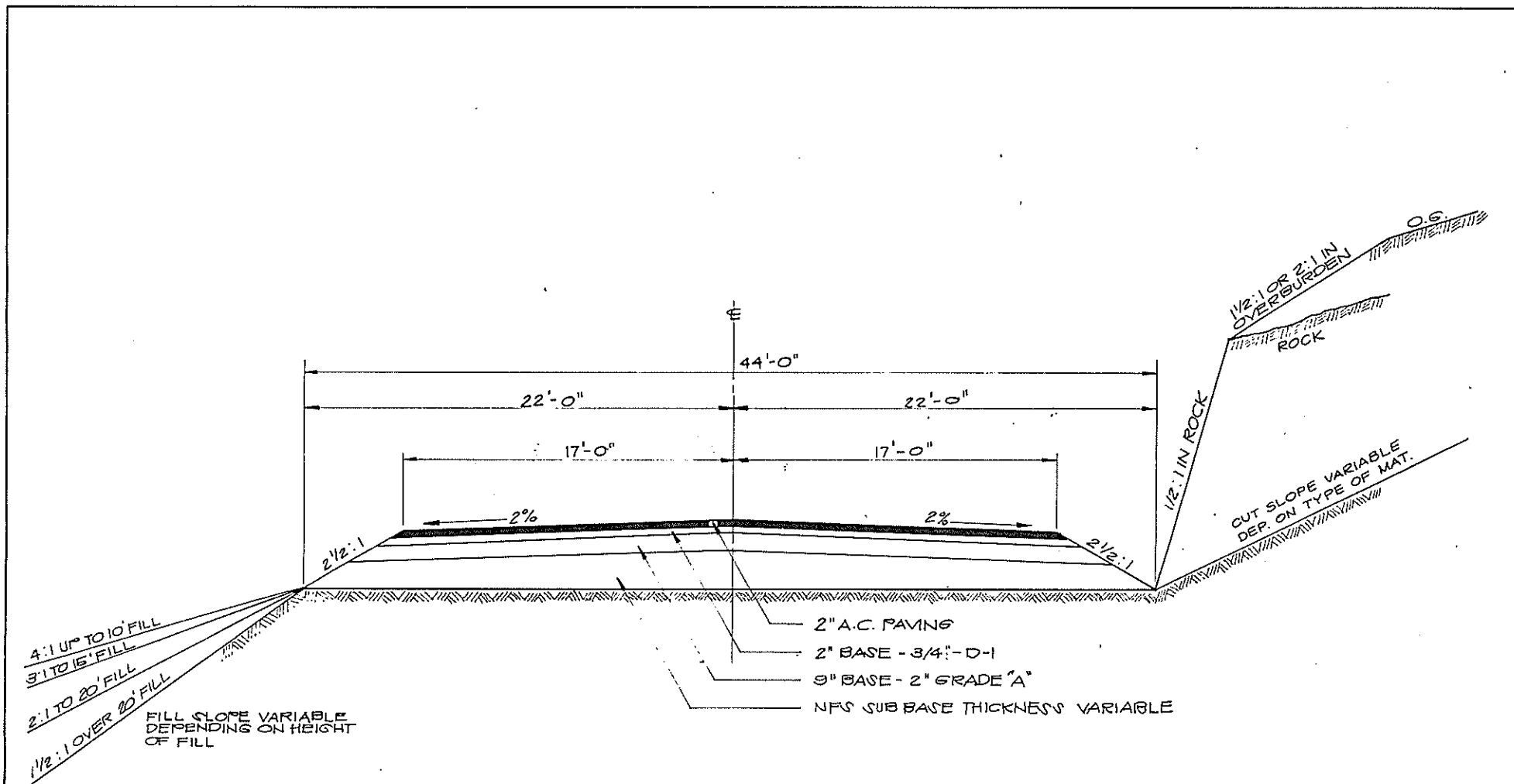
Originally the access road was envisioned as a low volume service road. The road was to be adequate for moving the necessary amounts of material and personnel but not necessarily in conformance will all requirement for a major public highway. As a result the original proposed design parameters were for a 30 mile per hour design with a 30 foot top width.

TABLE 8.1  
ORIGINAL PROPOSED DESIGN CRITERIA

	<u>Road</u>
Design Speed	30 mph
Maximum Grade	10%
Maximum Curvature	19°
Design Loading	HS-20

Design criteria such as these are used to establish guidelines for design. The designer normally attempts to provide horizontal and vertical alignment that is better than the minimum alignment such limits would provide. In order to maintain schedule, work began on a number of possible alignments prior to approval of the proposed criteria. While the corridor definition work was in progress information on certain primary dam components was developed that required flatter grades and curves. Satisfying these criteria would provide a roadway that would essentially conform to a 50-60 mile per hour design speed. Subsequent work confirmed the need for roadway design criteria for 60 mile per hour design speed. The relatively high roadway design parameters are required because of the size and weight of certain components of the dams that must be manufactured and imported to the site. The approved roadway design parameters are given in Table 8.2. With acceptance of the design parameters, a typical cross section was developed and is depicted in Figure 8.1.

Projected traffic volumes suggest that asphalt pavement should be provided if personnel access to the construction camps is by private auto.



**TYPICAL ROAD CROSS SECTION**



FIG. 8.1

REV.	
DATE	INTL

ACRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
	SUSITNA ACCESS ROAD	
TYPICAL CROSS SECTION		
REV.	DWN CKD	RE VG



TABLE 8.2  
APPROVED ROADWAY DESIGN PARAMETERS

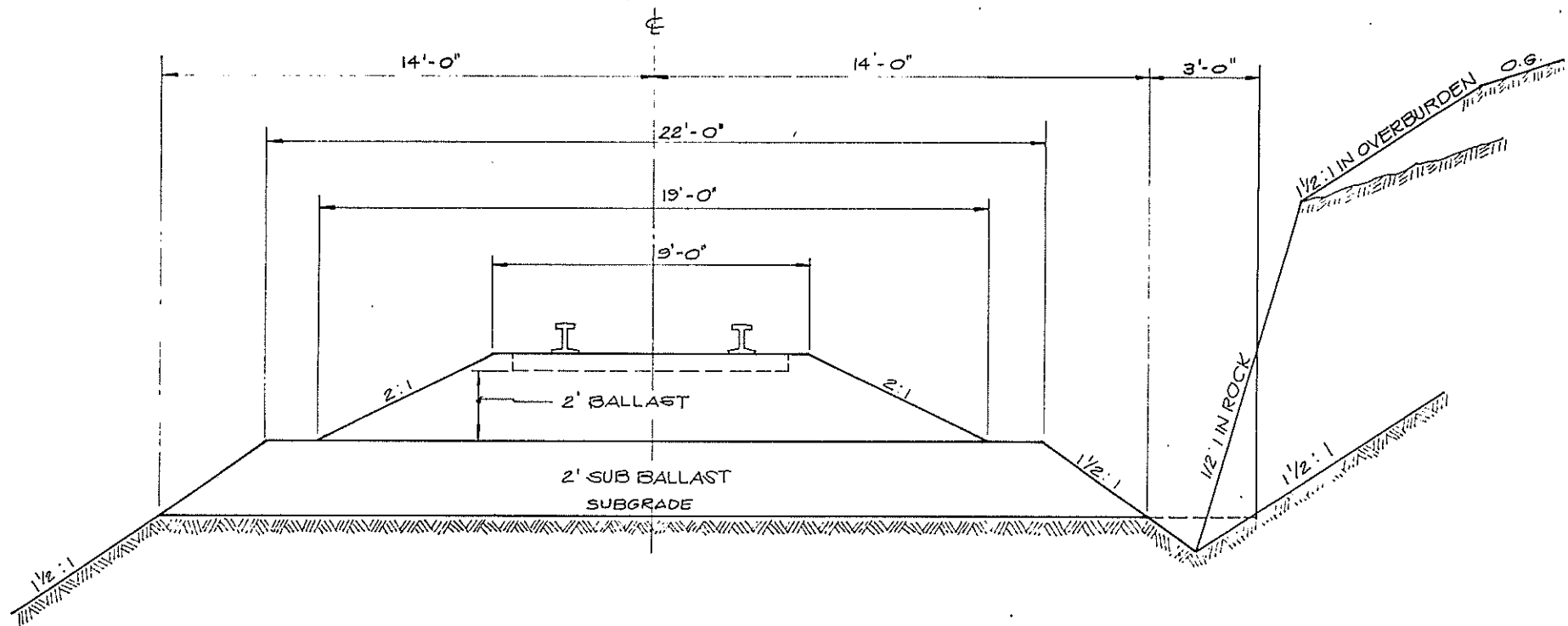
Design Speed	60 mph
Maximum Grade	6%
Maximum Curvature	5°
Design Loading (Construction Period)	80 Kip Axle & 200 Kip total
Design Loading (After Construction)	HS-20

### 8.2 - Rail Road Parameters

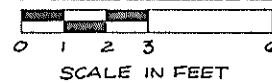
The volume of bulk materials to be moved to the Susitna project during the fifteen year period of construction make consideration of rail service mandatory. The principle concern with using the Alaska railroad was the load capacity of existing trackage and bridges. Horizontal and verticle clearances governing the overall size of loads that can be moved by rail are controlled by existing facilities. The existiting facilities conform to the American Railway Engineering Association (AREA) standards. The Engineering office for the Alaska Railroad states that the ARR is currently rated as an E-50 railroad. They are in the process of up grading to E-80 facilities. The Chief Engineer for the ARR recommended using an E-72 loading for railway planning. Input from the railroad engineering staff and AREA standards suggest the following design parameters would be appropriate.

TABLE 8.3  
APPROVED RAILROAD DESIGN PARAMETERS

Maximum Grade	2.5%
Maximum Curvature	10°
Loading	E-72.*



**TYPICAL RAILROAD CROSS SECTION**



REV	DATE	INTL

ACRES	ALASKA POWER AUTHORITY
	SUSITNA HYDROELECTRIC PROJECT
	<b>SUSITNA ACCESS RAILROAD TYPICAL CROSS SECTION</b>
DWM	DWM REL

FIG. 8

## CORRIDOR SELECTION

## 9.0 - CORRIDOR SELECTION

The general locations for the potential access corridors were defined in the POS. The next step in the process was the determination of where within these general corridors facilities could be built that would conform to the required design parameters. To that end, a series of alternate segments were identified and then evaluated. This section documents the process by which this segment selection was done and the results of the evaluation.

### 9.1 - Methodology

The Susitna Hydroelectric Project is located on a section of the Susitna River that is remote wilderness. Earlier studies by government agencies had generated some contour mapping in the vicinity of the proposed dam sites. The only other available contour information was USGS mapping on a one-inch (1") equals one (1) mile scale with one-hundred foot (100') contour intervals. To aid the project team in selecting possible routes, a low level helicopter flight was made in late March, 1980. A mosaic was then made of the USGS mapping from Gold Creek and the Parks Highway through the Watana site and out to the Denali Highway north of Watana. Using the preliminary design parameters and information gained from the overflight of the project area, a number of possible alignments were laid out on the map mosaic.

The various alternatives were split into convenient segments. Some of these segments were unique while others could be common to two (2) or more alternatives. Each segment was analyzed for grades on a section by section basis. Each curve was checked for degree of curve and deflection angle. Each curve and each identifiable gradient section were then tabulated. The various segments considered were combined to provide a total of

thirty-six (36) possible alignment alternatives that could conceivably be constructed to provide access to one or both of the principle dam sites. The various combinations of segments making up potential access route alignments were compared. The alignments identified as being the most attractive within each of the three (3) general corridors required by the plan of study was selected for further work. A low level reconnaissance flight with part of the environmental team was made April 30, 1980 to review the proposed corridor alignments prior to the photographic flights. Valuable input for future analysis was gained, and there was nothing identified that would force a major line change at this early stage of the work.

On May 5, 1980 the proposed corridor alignments were approved for photographic flights.

For the purpose of analysis the proposed general corridors are identified as follows:

- Corridor 1      On the north side of the Susitna River between the Parks Highway and the Watana Camp.
- Corridor 2      On the south side of the Susitna River between the Parks Highway and Watana Dam site. This corridor is being studied for railroad possibilities as well as road.
- Corridor 3      Connecting Watana Camp with the Denali Highway to the north.

## 9.2 - Discussion of Alternative

A number of alternative segments were considered within each of these three (3) general corridors. The alternative segments within

the respective corridors are discussed below and shown in Appendix B.

(a) Segment 1-A

(i) Description

This segment begins near MP 156 on the Parks Highway in the vicinity of Chulitna Pass. The line runs south east through Chulitna Pass crossing the rail road near summit lake, then proceeds easterly across Indian River and on to the Portage Creek Canyon. The line travels northeasterly for several miles while desending into a crossing of Portage Creek then south westerly while climbing out of Portage Creek to the north side of the Devil Canyon Dam Site. From Devil Canyon the line proceeds north easterly crossing into the upper reaches of Devil Creek then easterly through a 4,000-foot high pass and follows a drainage to a crossing of Tsusena Creek then south to the north side of the Watana Dam Site. Over-all length of the line is sixty four and seven tenths miles. The segment is shown on Figure 9.1.

(ii) Line and Grade

Segment 1-A is well within the desired limits with regard to alinement and grade with the exception of the portion through Portage Creek and near Devil Canyon. The terrain in Portage Creek Canyon is very difficult. Providing an alignment through Portage Creek Canyon that conforms with the design parameters will require very heavy earthwork and several small to medium length bridges across the side drainages.

(iii) Drainage Features

Most of the drainages along 1-A carry flows which can be passed through standard culverts quite satisfactorily. Bridges or multiplate pipe will be required for Indian River, Portage Creek, Devil Creek and Tsusena Creek.

(iv) Bridges

As stated, at least four bridges are expected. The Indian River bridge is a 440-foot long three span structure whose configuration is dictated more by the shape of the crossing than by the quantity of water in the river. The Portage Creek bridge will be a two or three span structure approximately 200 feet long. The Devil Creek bridge will be a simple one span structure less than 100 feet long. The Tsusena Creek bridge is expected to be a 260-foot three span structure similar to the Portage Creek bridge. Any construction within the Portage Creek Canyon will require additional structures in the under 200-foot class at several side drainages.

(v) Soils

Much of the alignment for segment 1-A from the Parks Highway to Devil Canyon traverses frozen soils, generally basal till with moderate side slopes. Drill holes indicate permanent ice beginning at depths of around fifteen feet. The material consists of gravels, sands and silts. Properly handled the material can be used to construct road bed, however the silts and sands will erode readily unless protected. The material is generally frost susceptible due to the silt content which will require a substantial non-frost susceptible subbase layer in the road bed. The soil is very susceptible to thaw settlement making it necessary to severely

limit the depth of excavation and then requiring extensive borrow areas to provide roadway embankment.

There are extensive organics in the section of line from the Parks Highway through Chulitna Pass. This material is ten to twenty feet deep and will be difficult to build on. The remainder of the segment encounters occasional small areas of organic soils. With the exception of the crossings of Portage and Tsusena Creeks these areas of organics can be avoided.

The Portage Creek Canyon section traverses very steep cross slopes. Because of the frozen soils any road-way construction in the area could result in major erosion and thaw settlement problems at deep cuts will be unavoidable.

The section of 1-A from Devil Canyon to Watana traverses soils with shallow to exposed bedrock. Most of this section traverse relatively gentle cross-slopes. These conditions will allow road bed construction without undue problems with erosion and thaw settlement. Borrow sources are available close by the alignment.

(vi) Environmental Concerns

Portions of Segment 1-A have significant potential environmental problems. The section between the Parks Highway and Chulitna Pass traverses an obvious wetland area and encroaches on the Denali State park. Both Indian River and Portage Creek are anadromous fish streams. Indian River could be crossed without a serious conflict with the fish, however the potential for erosion that would result from construction in the Portage Creek Canyon may well pose a threat to the Portage Creek fish runs. The lower Portage Creek area has been identified as a potential raptor area and



most of Portage Creek is known furbearer habitat. The alignment between Devil Canyon and Watana does not encroach on any environmentally sensitive areas.

(vii) Segment Suitability

Segment 1-A is actually a full length alternate alignment. The section from the Parks Highway to Devil Canyon is not considered suitable for access construction. This section has numerous construction, soils and environmental problems. The section from Devil Canyon to Watana remains viable.

(b) Segment 1-B

(i) Description

Segment 1-B is an alternate to a portion of 1-A between Devil Creek and Tsusena Creek. The segment begins just west of Devil Creek and drops into the Devil Creek drainage, crossing the creek, and swings north and east past Mama Bear Lake, then south easterly through a wide pass at 3,400-foot elevation, then proceeds easterly to rejoin segment 1-A before reaching Tsusena Creek. See Figure 9.1.

This alignment lies south of 1-A and utilizes a broader, lower pass which should be easier to keep open during and after snow storms. The cross slopes are gentle to moderate with the steepest being as the line climbs out of Devil Creek.

This segment is 16.2 miles in length

(ii) Line and Grade

Alignment and grade on this segment are well within the required parameters.

(iii) Drainage Features

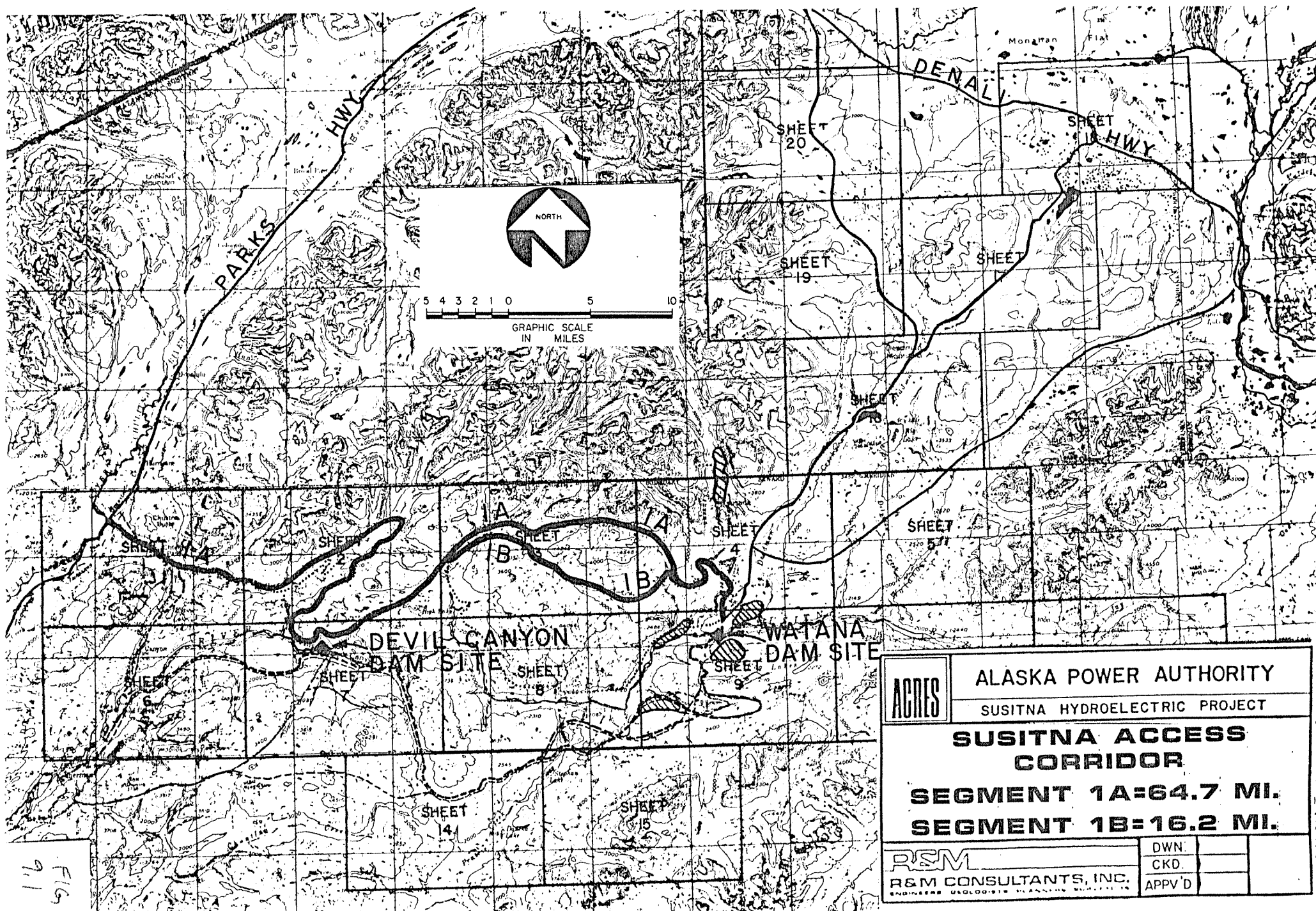
Segment 1-B encounters no major or complicated drainage features. Cross culverts will be required at intervals. The only major stream crossing is Devil Creek.

(iv) Bridges

The only Bridge on this segment is expected to be the Devil Creek crossing. This bridge will be a simple two hundred foot structure, probably with three spans.

(v) Soils

Some frozen Basal till with shallow bedrock occurs as the line drops into Devil Creek. Cross slopes are such that heavy cuts should not be required. Erosion and thaw settlement problems should be kept to a minimum. The crossing of Devil Creek is on thawed soils generally Ablation tills and flood plain deposits which are good soils for road bed construction. Climbing out of Devil Creek, the line crosses good soils with bedrock at or near the surface. Frozen soils are not encountered until the east end of Mama Bear Lake. The remainder of the alignment is sporadically frozen soils however the terrain has gentle to moderate slopes which will allow road bed construction without heavy cuts.



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<b>SEGMENT 1A=64.7 MI.</b>			
<b>SEGMENT 1B=16.2 MI.</b>			
<b>R&amp;M</b>		DWN	
<b>R&amp;M CONSULTANTS, INC.</b>		CKD	
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FIG 9.1

(vi) Environmental Concerns

This segment does not appear to cross any environmentally sensitive areas. The alignment is generally at or above the tree line and conflicts with wildlife appear to be minimal. Where erodible soils are encountered, slopes are flat enough that a minimum of soil will be exposed thereby keeping the potential for erosion down.

(vii) Segment Suitability

Segment 1-B is a viable alternate. It does exhibit some advantage over 1-A in that the pass is lower and such that snow control should be easier.

(c) Segment 1-C

(i) Description

This segment leaves 1-B at Devil Creek and descends Devil Creek to the Susitna River then up the Susitna River crossing Tsusena Creek near its mouth and climbing to the north end of the Watana Dam. This alignment was intended to provide a water level access along the Devil Canyon reservoir. See Figure 9.2.

The segment is 27.5 miles in length.

(ii) Line and Grade

This segment can be constructed to meet 30 mph design speed but cannot meet the desired parameters. There are two sections where grades approaching eight percent cannot be avoided.

(iii) Drainage Features

This segment is generally side hill construction with numerous stream crossings. With the exception of Devil Creek and Tsusena Creek, culverts should handle the drainage concerns with no more than normal considerations.

(iv) Bridges

Two bridges are positively identified at Devil Creek and at Tsusena Creek. Both bridges would be in the one hundred fifty to two hundred foot category with two or three spans.

(v) Soils

This alignment crosses generally good soils with some scattered frozen materials near Watana Camp. The portion of Alternate 1-C along the Susitna River is mostly in frozen materials composed of solifluction deposits which are composed of saturated soil material and rock debris especially subject to frost creep or down slope movement. In addition there are large slide scar areas crossed and one apparently active landslide area (see Appendix D). The unfrozen and organic soils at the surface are covering sections of permafrost and these soils are prone to frost heave and thaw settlement. Since the majority of the slopes face the south, thawing is more likely giving lower bearing strengths and very low slope stability as evidence by the existing slide scars.

(vi) Environmental Concerns

There are a number of potential environmental concerns with this alignment. Erosion from cut and fill slopes in frozen soils and existing slides would be a major problem. The timbered side hills are important moose and black bear habitat. The most important habitat area is near the mouth of Tsusena Creek.

(vii) Segment Suitability

This segment is not very suitable; poor soils conditions, the inability to meet grade requirements, and the encroachments on wildlife habitat make this segment unattractive. In addition, the alignment encroaches on a borrow area needed for construction of Watana Dam (Borrow Area C) and crosses a portion of the construction area.

(d) Segment 1-D

This alignment is a shorter steeper crossing of Portage Creek. The alignment uses switch backs, steep grades and sharp curves to minimize the amount of damage in the Portage Creek Canyon. See Figure 9.2.

The segment is 9.0 miles in length.

(ii) Line and Grade

Vertical and horizontal alignment violate the desired parameters. There is no possibility of constructing an acceptable alignment on this segment.

(iii) Drainage Features

There are no significant drainage features on this alignment. Ditches and cross culverts would be standard type construction.

(iv) Bridge

A bridge would be required at Portage Creek very similar to the segment 1-A Portage Creek Bridge; a three span structure approximately 200 feet long.

(v) Soils

This segment traverses some very steep ground completely characterized by frozen soils which are highly subject to erosion, thaw settlement and frost heave.

(vi) Environmental Concerns

Portage Creek is an anadromous fish stream and there is concern that erosion of cut and fill slopes would be detrimental. In addition the alignment traverses known furbearer habitat and potential raptor nesting areas.

(vii) Segments Suitability

This segment is not suitable for further consideration.

(e) Segment 1-E

(i) Description

This segment is an alternate crossing of Tsusena Creek

upstream from the 1-A crossing and connects with 3-A near Deadman Creek. See Figure 9.2.

This segment is 7.5 miles long.

(ii) Line and Grade

While longer than the 1-A crossing, this segment crosses Tsusena Creek with easier grades and good horizontal alignment.

(iii) Drainage Features

There are no significant drainage features on this segment. Normal ditch and culvert construction will serve.

(iv) Bridges

A bridge will be required over Tsusena Creek. The bridge will be a simple two span structure of about 150 feet in length.

(v) Soils

This segment crosses generally thawed soils exhibiting good road building characteristics.

(vi) Environmental Concerns

The crossing is far enough up Tsusena Creek to avoid the most critical moose habitat. The soils are such that the erosion possibilities are low, making this an attractive option.



(vii) Segment Suitability

This is a good segment much more suitable than 1-A in the Tsusena Creek drainage. The bridge crossing is good and cross slopes are moderate.

(f) Segment 1-F

(i) Description

This segment is an alternate to the section of 1-A from Parks Highway through Chulitna Pass. This segment crosses the railroad track closer to the highway and traverses the base of Chulitna Butte against the railroad tracks connecting with 1-A east of Summit Lake. See Figure 9.2.

This segment is 4.1 miles long.

(ii) Line and Grade

This segment conforms with the preferred design parameters although is not as straight and flat as the comparable sections of 1-A.

(iii) Drainage Features

No major drainages features are encountered. There are a few small streams crossed which can be handled with culverts. The line does avoid the wetland area traversed by 1-A.

(iv) Bridges

This segment does not include any bridges.

(v) Soils

This section crosses frozen basal till and organic soils just as 1-A does, however, the extent of organics is much smaller. 1-F is further up slope and on moderate cross-slopes. The terrain is generally suitable for fill type construction often used to bridge organics and insulate frozen soils. As with other areas of the project there is some 10-15 feet of unfrozen soil over the permafrost; at least a portion of which can be worked in normal fashion provided due care is used with regard to erosion, thaw settlement and frost heave.

(vi) Environmental Concerns

The first two miles of the line encroach on a corner of Denali state park essentially parallel to the rail road. This alignment may require the taking of some dwelling units in the Chulitna Pass area. No critical habitats area appear to be impacted.

(vii) Segment Suitability

This segment essentially parallels the railroad and in so doing should have minimal added environmental impact. The wetland area in the pass is avoided and, while frozen and organic soils are a factor, they can be dealt with. This segment is preferable to the corresponding section of 1-A.



(g) Segment 2-A

(i) Description

This segment begins at Sherman on the Alaska railroad south of Gold Creek. The alignment climbs the river bluffs via switchbacks to the higher ground near the head of Gold Creek. From there the line runs generally east on the high ground to the divide above Prairie Creek. The line then descends along a ridge and passes just north of Stephan Lake then proceeds easterly to a crossing of Fog Creek and north to the Watana Dam site past the west end of Fog Lakes. See Figure 9.3.

This alignment is 56.7 miles long.

(ii) Line and Grade

This alignment conforms quite well with the design parameters except for the climb from Sherman to the head of Gold Creek. This section is switchbacks using grades to ten percent and very sharp curves.

(iii) Drainage Features

Drainage features along this route are routine. The only problem areas being the west area near Stephan Lake and near Fog Lake where flat, boggy and frozen ground will be difficult to drain.

(iv) Bridges

The only Bridge involved with this alignment is the crossing of Fog Creek. This is a major bridge. The canyon is fairly

deep with near vertical rock walls. The length of the crossing is approximately 600 feet. The probable structure type is a continuous deck truss that can utilize cantilever type construction techniques. This bridge will take eighteen to twenty four months to construct and will require a passable road over which to transport materials. This bridge could be a major schedule constraint.

(v) Soils

This alignment traverses a variety of soils. The climb through the switchbacks from Sherman is in an area of frozen Basal till over bedrock. The steep terrain will require heavy cuts and fills which will not be suitable. The Basal till is erodable and subject to frost heave and thaw settlements all of which would be major problem in the switch back area.

The section from the head of Gold Creek to the Prairie Creek divide crosses sporadically frozen soils and colluvial deposits mixed with bedrock. The material is generally acceptable for roadbed construction provided proper care is exercised with regard to frost susceptibility and erosion control. Scattered pockets of shallow organics exist that could be largely avoided.

From Prairie Creek divide to Watana the soils are Lusterines over frozen tills with pockets of organics and some bedrock near Fog Creek. The soils are acceptable for roadbed construction provided that consideration is given to frost susceptibility, and thaw settlement and erosion. The soils near the end of Stephan Lake show evidence of massive ice. This area should be avoided if possible.

(vi) Environmental Concerns

The environmental concerns along this alignment are in the Stephan Lake - Fog Lakes area. These areas are prime habitats for variety of big game animals, waterfowl, and fur bearers. There is a potential for raptor use in the Fog Creek area. These same areas have been identified as having archeological sites of potential significance. There is a concern that public access to these area will have detrimental effects on big game populations and on the archeaological sites.

(vii) Segment Suitability

The portion from Sherman to the Prairie Creek divide is not considered as suitable because of difficult line and grade restrictions above Sherman and the fact that this line does not directly serve Devil Canyon.

The portion from the Prairie Creek divide to Watana is suitable for construction although there are some unavoidable environmental concerns. A portion of the line passes through borrow area H designated for use in construction Watana Dam. Some re-routing would be required to avoid the massive ice near Stephan Lake.

(h) Segment 2-B

(i) Description

This segment begins in at the south side of the Devil Canyon Dam site and travels south, up Cheechako Creek, about two miles before turning east and crossing the creek. The line then continues south easterly for about five miles while

climbing to the top of a deep gorge. At this point the segment turns southerly following the top edge of the gorge to its head and join 2-A at the Prairie Creek divide. See Figure 9.3.

This segment is 13.6 miles in length.

(ii) Line and Grade

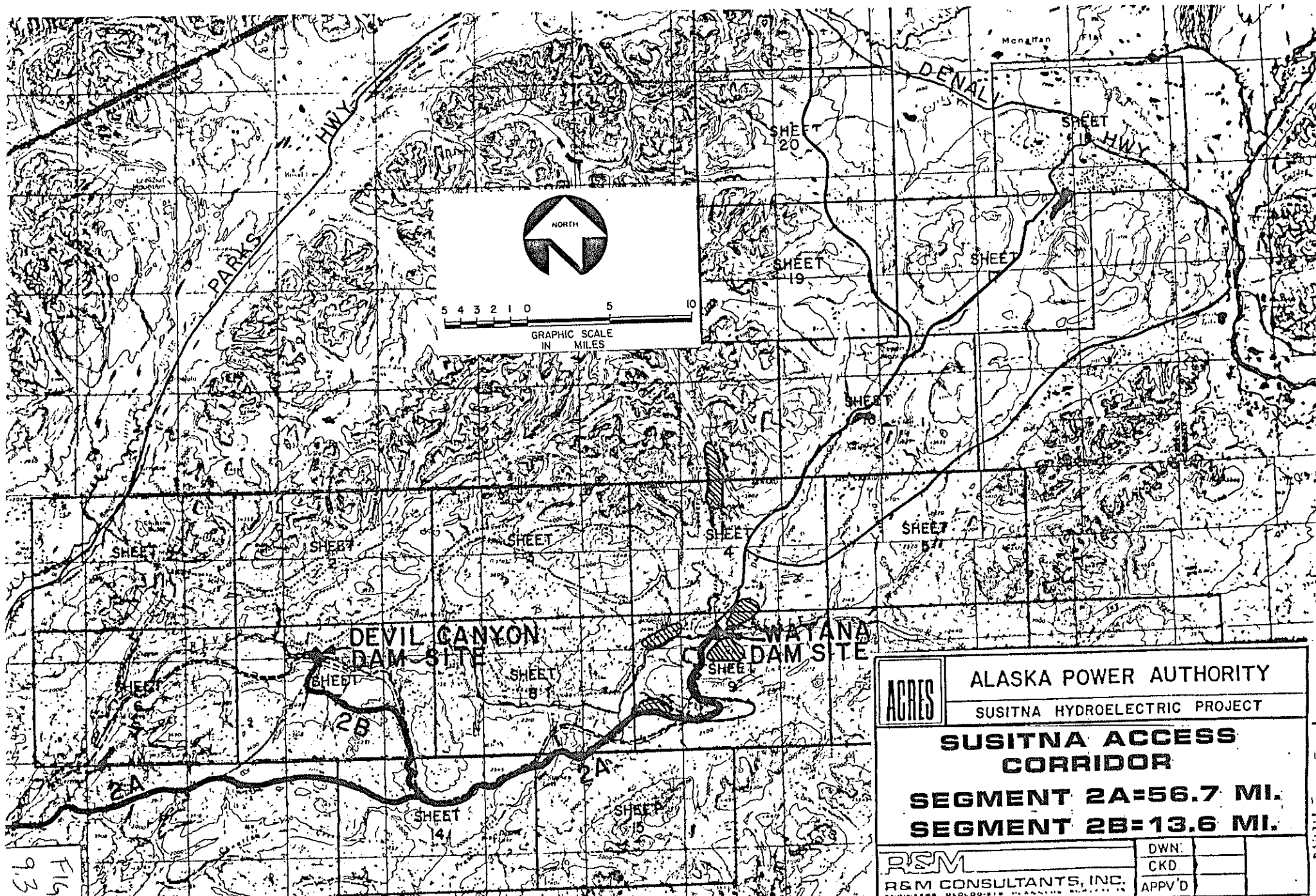
The horizontal alignment on this segment is acceptable. It is not possible to bring the portion south of Devil Canyon into conformance with the required gradient criteria. 7% to 10% grades would be required for about two miles.

(iii) Drainage Features

This alignment is located on high ground with little or no drainages involved. The one exception is a three mile reach that follows a small stream. The line appears to be above the stream far enough to avoid direct conflicts and should be no problem.

(iv) Bridges

One Bridge will be required crossing Cheechako Creek. This will be over a deep rock gorge. It will be curved and will require long spans and some tall towers for the intermediate supports. Because the bridge will be on a curve it will likely be a steel box girder structure. A second, more conventional bridge may also be required across a tributary of Cheechako Creek.



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<b>SEGMENT 2A=56.7 MI.</b>			
<b>SEGMENT 2B=13.6 MI.</b>			
<b>RSM</b>		<b>DWN:</b>	
<b>R&amp;M CONSULTANTS, INC.</b>		<b>CKD</b>	
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93  
F16



(v) Soils

The soils are Basal till over bedrock - generally frozen along the first part of the line and bedrock or colluvium over bedrock along the remainder. The frozen till is on variable cross slopes much of it steep enough to require large fills to avoid cuts in frozen soils. Extensive borrow may be required to provide material for the fills.

(vi) Environmental Concerns

Portions of this segment traverse areas used by caribou as winter range because the wind keeps the ridge tops blown of snow. No other environmental conflicts have been identified.

(vii) Segment Suitability

The westerly section of 2-B near Devil Canyon is not suitable in that excessive grades cannot be avoided. The easterly end along the deep gorge approaching the Prairie Creek divide is highly suitable in that soils are rock, grades and alignment satisfactory.

(i) Segment 2-C

(i) Description

This segment runs south from 2-B near Devil Canyon up the Cheechako Creek drainage to join 2-A. This was intended to be the side connection to serve Devil Canyon from 2-A. See Figure 9.4.

This segment is 7.5 miles long.

(ii) Line and Grade

The horizontal alignment on this segment is satisfactory however grades exceed the desired maximum with no way of improving it. Over four miles of the line would be in the 7% to 9% range.

(iii) Drainage Features

There are no special drainage features along the segment. Several cross drainages exist; however standard ditches and culverts will serve.

(iv) Bridge

There are no bridges on this segment.

(v) Soils

This segment crosses unfrozen colluvial deposits and bedrock generally acceptable for normal roadway construction with proper attention to erosion control and frost classification of materials.

(vi) Environmental Concerns

There have been no significant environmental conflicts identified along this alignment.

(vii) Segment Suitability

This segment is not considered suitable because of excessive grades.

(j) Segment 2-D

(i) Description

This section begins at Sherman, crosses the Susitna River and cuts through a pass inside Denali State Park to connect with the Parks Highway. See Figure 9.4.

This segment is 10.7 miles long.

(ii) Line and Grade

All of this segment conforms to the requirements for horizontal and verticale alignment. The grades do approach 6% however.

(iii) Drainage Features

This segment is located nearly in the bottom of drainages and may generate some conflicts with the streams. In addition there is a wet area in the pass west of the river which may result in surface drainage problems.

(iv) Bridges

A major bridge over the Susitna River will be required. The bridge will be a mulitspan structure, probably welded plate girders, and approximately 1,000 feet long.

(vi) Soils

The soils along this corridor have not been mapped. The material immediately north has been mapped and is frozen basil till over bedrock with some pockets of organics interspersed.

(vi) Environmental Concerns

This segment cuts directly through Denali State Park. Some wetlands are involved and while not verified the vegetation is typical of other areas that have been identified as Moose habitat.

(vii) Segment Suitability

This segment is not considered viable because it passes through Denali State Park and would disrupt the Park without demonstrating an off setting distinct advantage.

(k) Segment 2-E

(i) Descriptions

This segment connects 2A and 2D at Sherman with 1-A at Chulitna Pass. The line generally parallels the railroad and was looked at as an alternative to 2-D in connecting with the Parks Highway. From Sherman to Gold Creek the alignment runs between the railroad and the base of the mountain. In two locations it is squeezed into some difficult side hill construction. After crossing the Susitna River the line stays back from the bluff above Indian River to avoid some side hill construction. See Figure 9.4.

The length of the line is 15.6 miles.

(ii) Line and Grade

Horizontal and vertical alignment conform with the desired parameters.

(iii) Drainage Features

There are no special drainage considerations on this segment normal ditches and culverts will serve.

(iv) Bridges

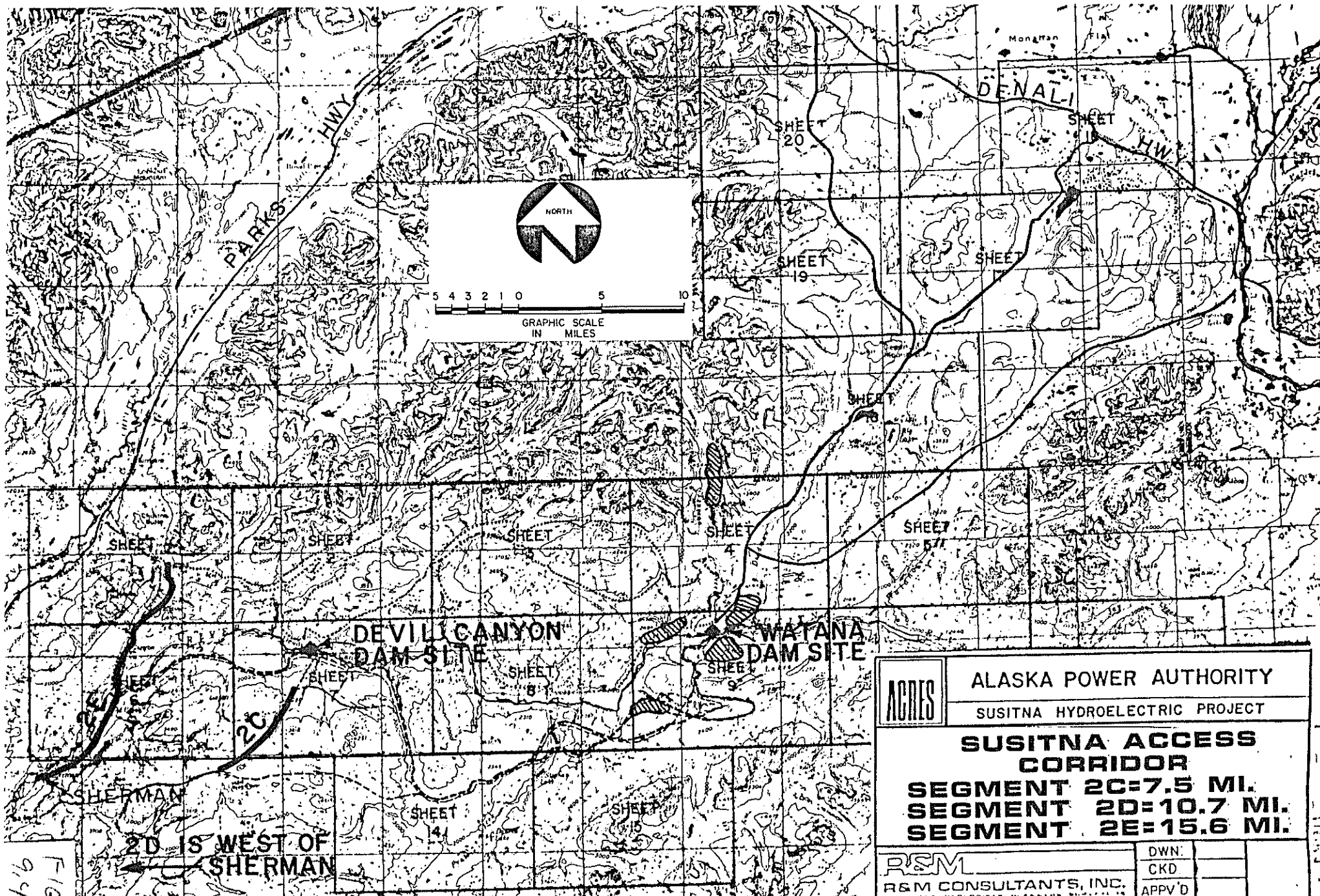
There are a total of three bridges identified on this segment. The main stream Susitna River Bridge is located immediately upstream of the Railroad Bridge. The first of two bridges over Indian River is just upstream from the Susitna River and will be an approximately 400-foot, three span structure. The second bridge over Indian River is near Chulitna Pass this will also be an approximately 400-foot, three span struction.

(v) Soils

This segment has a variety of soil types. The portion south of the Susitna River crossing is largely alluvial and flood plain deposits exhibiting good road building characteristics. This material is unfrozen and normal care with erosion contol and frost heave will result in a quality facility. The section north of the Susitna River crosses frozen Basal till and, some floodplain deposits near the stream crossings.

(vi) Environmental Concerns

The principle environmental concerns for the segment result from potential impacts on the Susitna and Indian Rivers. In each case there is a potential for equipment working in the streams. The impacts should be temporary in nature and not adversely effect the fish populations.



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<b>SEGMENT 2C=7.5 MI.</b>		
<b>SEGMENT 2D=10.7 MI.</b>		
<b>SEGMENT 2E=15.6 MI.</b>		
<b>R&amp;M</b>	<b>DWN</b>	
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The segment does border a State land disposal area known as the "Indian River Remote" disposal.

(vii) Segment Suitability

The entire segment is suitable for construction. Only portions of it may be used depending on the final access plan accepted.

(i) Segment 2-F

(i) Description

Segment 2F is a road alignment developed to shorten the distance traveled by 2A in crossing Fog Creek. The segment uses a bridge and somewhat steeper grade to effect a nearly straight crossing rather than a long switch back. See Figure 9.5.

This segment is 3.9 miles long.

(ii) Line and Grade

This segment does conform to the desired parameters for horizontal and vertical alignment. Grades do approach the 6% maximum. The horizontal alignment can allow safe truck operations on the alignment and need not be designed at the maximum curvature.

(iii) Drainage Features

The segment does not encounter major drainage features other than Fog Creek. A bridge will be required for Fog Creek while other drainage considerations can be treated satisfactorily with normal ditches and culverts.

(iv) Bridges

A major bridge is required on this segment at Fog Creek the structure crosses a deep rocky gorge. The structure type suggested is a deck truss because of the propable span arrangement and height of intermediate support towers. Structures of this type require considerable length of time to assemble. One and one half to two years is probable.

(v) Soils

The soils are Lusterines over frozen Basal tills south of Fog Creek and frozen Basal tills over bedrock north of Fog Creek. There is bedrock at or near the surface at Fog Creek. The south side of Fog Creek is a designated borrow source for Watana Dam.

(vi) Environmental Concerns

The entire area traversed by the segment has been identified as Moose and Caribou habitat. Fog Creek has been identified as potential raptor habitat.

(vii) Segment Suitability

The segment is considered suitable for construction with one exception. The alignment does pass through one of the borrow sources for Watana Dam. For this reason segment 2-J was selected and 2-F dropped from further consideration.



(m) Segment 2-G

(i) Description

Segment 2-G begins at Devil Canyon Dam on the south side and follows the side hill upstream while climbing to join segment 2B as both lines turn south away from the Susitna along the top of a deep gorge. This segment is an alternate to 2-B that can conform with design parameters. See Figure 9.5.

Over all length of the segment is 7.7 miles.

(ii) Line and Grade

This segment has acceptable line and grade. The segment was designed to bypass the grade problems of segment 2-B.

(iii) Drainage Features

Standard culverts and ditches will serve all known drainage considerations for this segment.

(iv) Bridges

This segment includes a major structure over Cheechako Creek just after leaving Devil Canyon. This structure would be a three span deck truss over a deep narrow gorge. This type of structure will require one and one half to two years to construct.

(v) Soils

Soils on the segment are varied. Portions of the line cross frozen Basil till with bedrock near the surface, exposed

bedrock, and bedrock under Colluvium. Cross slopes are generally steep. This segment will require extensive rock excavation resulting in slow construction.

(vi) Environmental Concerns

The segment passes along the Susitna River banks which have been identified as potential raptor habitat. Extensive side hill construction on fairly steep terrain increases the potential for erosion and slides.

(vii) Segment Suitability

This segment is suitable for construction should south side road access be selected. There are some scheduling constraints however because of the bridges and the extent of construction in rock.

(n) Segment 2-H

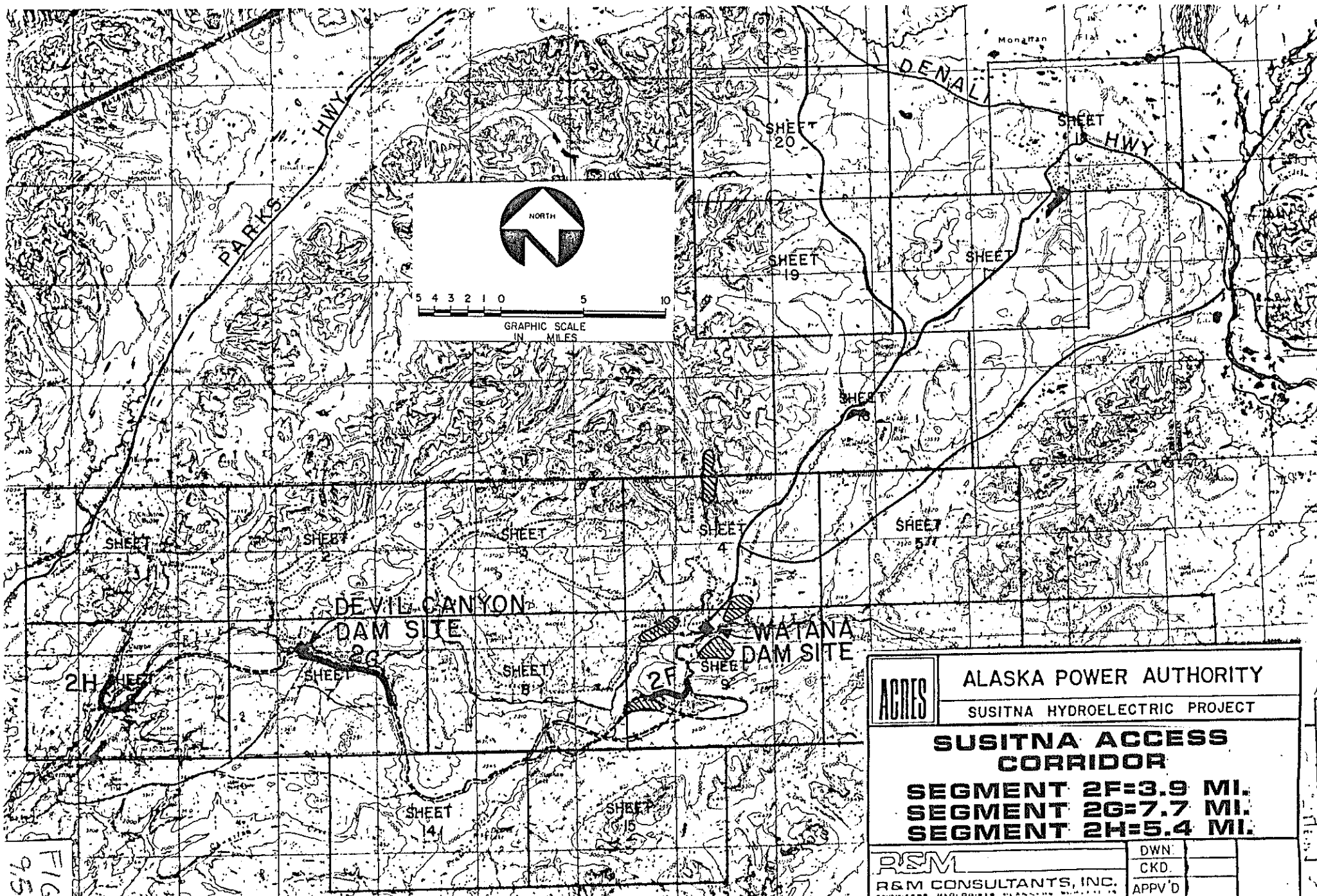
(i) Description

This segment leaves 2-E at Indian River and closely parallels the railroad south across the Susitna River then turns north easterly to connect with 2-I about two miles upstream from Gold Creek. This segment would be one logical route if road access were provided from the Park Highway while providing a rail head at Gold Creek. See Figure 9.5.

This segment is 5.4 miles long.

(ii) Line and Grade

The horizontal and vertical alignments for this segment will meet desired parameters.



(iii) Drainage Features

The only drainage features of note on this segment are Indian River and the Susitna River.

(iv) Bridges

Bridges required on this segment would be similar in configuration to those required at the Susitna River and the first Indian River crossing of Segment 2E. The location will vary from the 2-E location, however the general design would be similar.

(v) Soils

The soils encountered along 2-H are largely floodplain and terrace deposits with portions located on frozen Basil till.

(vi) Environmental Concerns

Both the Susitna River and Indian River are anadromous streams at the proposed crossing. Bridge construction would have to be done in a manner approved by the responsible agencies. No other significant environmental concerns have been identified.

(vii) Segment Suitability

This segment is suitable for construction. All or part may be used depending on the final access plan adopted.

(o) Segment 2-1

(i) Description

This segment is located on the south side of the Susitna River slowly ascending in elevation to reach the south end of Devil Canyon Dam. The segment begins about 2 miles above Gold Creek. See Figure 9.6.

The segment is 11.4 miles long.

(ii) Line and Grade

This segment has very good horizontal and vertical alignment generally providing an alignment that will be better than the required minimums would provide.

(iii) Drainage Features

Several drainages cross this segment. Some of these may require large culverts such as multiplate or pipe arches of a type common to highway construction. A portion of the alignment follows a small drainage, care must be taken to protect this stream.

(iv) Bridges

It does not appear that any bridges will be required on this segment. There are two drainages where final design may dictate a small bridge however nothing that would be a significant schedule constraint.

(v) Soils

Nearly all of this segment traverses frozen Basal till on side slopes varying from flat to moderately steep. Care must be taken not to cut so deep as to disturb the thermal regime without insulation or other special features to protect the underlying conditions. Large quantities of borrow will be required for this section because of the frozen soils.

(vi) Environmental Concern

No major environmental concerns have been identified along this segment. There are small wetland areas that must be considered in final design.

(viii) Segment Suitability

This segment is suitable for construction of roadway. Access to Devil Canyon from Gold Creek could be provided fairly rapidly via this segment.

(p) Segment 2-J

(i) Description

This segment provides an alternative to 2A around Stephan Lake and the borrow area near Fog Creek. The alignment moves north of 2A as it passes Stephan Lake to avoid some wetland and bad soil areas then crosses 2A and runs south and east of 2A joining 2F north of Fog Creek. See Figure 9.6.

The segment is 12.2 miles long.

(ii) Line area Grade

This segment has good line and grade its entire length. There are some maximum (6%) grades at Fog Creek.

(iii) Drainage Features

This alignment crosses several small drainages of the type normally handled with culverts. There appears to be no significant drainage problems.

(iv) Bridges

There is a major bridge over Fog Creek. This bridge would be similar to the structure required on 2-F, multispans, and approximately 500 feet in length. It may be possible to use a welded plate girder structure rather than a truss. If so, some six to twelve months could be saved on the construction schedule when compared to the bridges on 2-F. This bridge will still require a year to build.

(v) Soils

The soils along this segment are largely Lusterines over frozen Basal tills. These soils are sensitive and require care in designing slopes, ditches and other features to avoid erosion, frost heave and thaw settlement. Cross slopes are generally gentle to moderate thus allowing cuts to be kept to a minimum.

(vi) Environmental Concerns

The entire segment traverses quality wildlife habitat. Moose, Bear, Caribou, Raptors, and Furbearers use this area. The

segment does stay further from Stephan Lake, other than that the impacts would be comparable to 2A.

(vii) Segment Suitability

The segment is suitable for construction. It has two advantages over 2A in that it is further from Stephen Lake and the associated environmental concerns and it skirts the edge of borrow area H for Watana Dam.

(q) Segment 2-K

(i) Description

This segment was proposed as a shorter alternative to a portion of 2-H. The segment leaves 2E as the south side of the Susitna River and turns sharply east climbing to join 2H on top of a bluff. See Figure 9.6.

This segment is only 0.9 miles long.

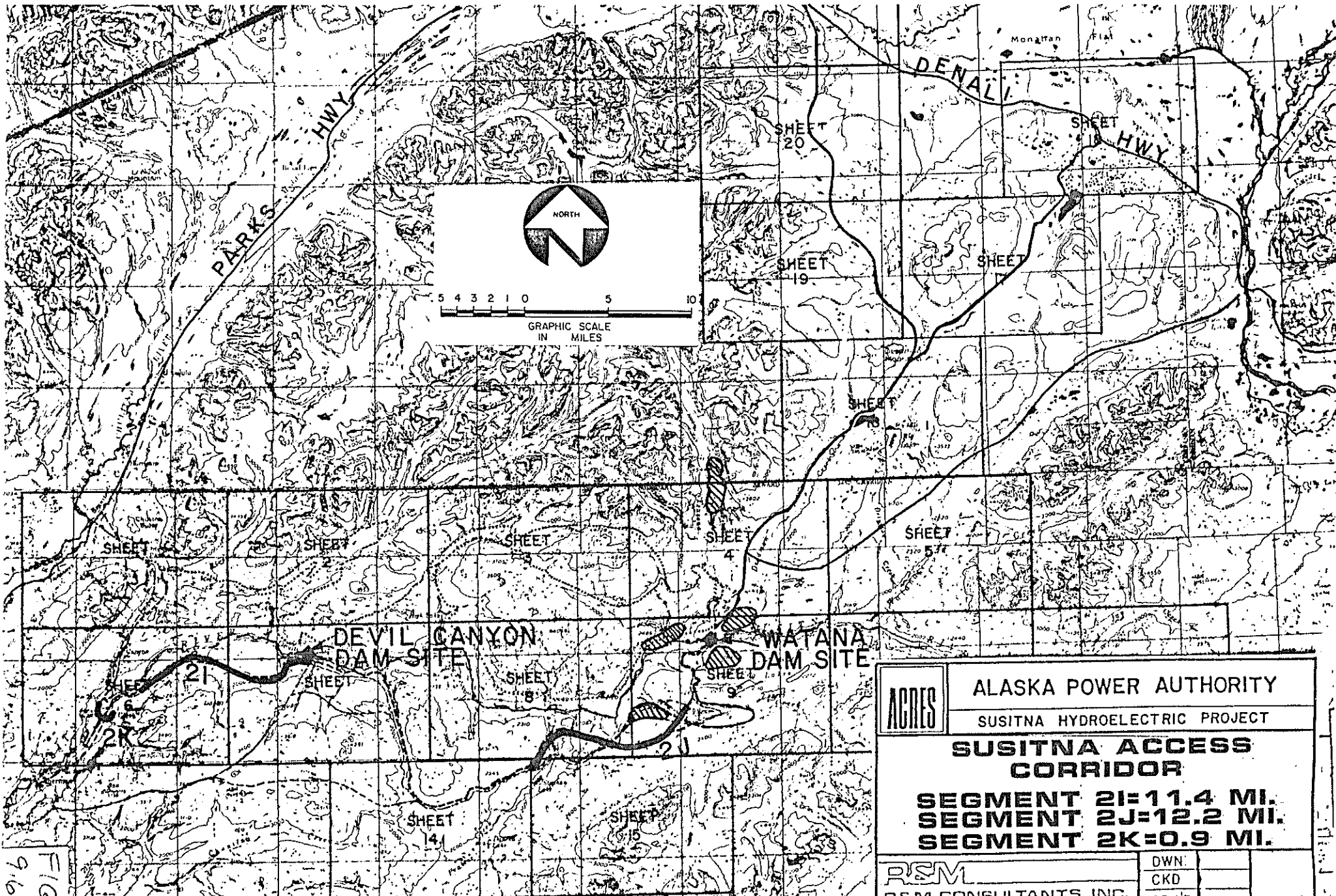
(ii) Line and Grade

This segment conforms to the required parameters however maximum curvature and gradients are involved.

(iii) Drainage Features

No significant drainage features are encountered by this segment.





<b>ACRES</b>	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
	<b>SUSITNA ACCESS CORRIDOR</b>	
<b>SEGMENT 2I=11.4 MI.</b>		
<b>SEGMENT 2J=12.2 MI.</b>		
<b>SEGMENT 2K=0.9 MI.</b>		
<b>RSM</b>	DWN	
<b>RSM CONSULTANTS, INC.</b>	CKD	

FIG 9.6

(iv) Bridges

No bridges are involved on this segment.

(v) Soils

The soils crossed are flood plain deposits and frozen Basal tills. Much of the alignment would require high fills constructed of borrow. Some cuts in frozen material are also likely as the line joins 2-H on top of the bluff.

(vi) Environmental Concerns

No major environmental conflicts appear along this segment.

(vii) Segment Suitability

The segment is suitable but not desirable due to the use of maximum curves and grades and the requirement for high fills.

(r) Segment 2-L

(i) Description

This segment is parallel to 2E connecting 1-A at Chulitna Pass with 2-I east of Gold Creek. Portions are coincident with 2E. The primary purpose of this alternate is to provide a line that has less potential for conflict with a State of Alaska Land disposal tract. Another potential Susitna River crossing is identified that allows the alignment to avoid going over or around a short, high bluff. See Figure 9.7.

This line is 8.7 miles long.

(ii) Line and Grade

The horizontal and verticle alignments for segement 2-L satisfy all requirements.

(iii) Drainage Features

No abnormal drainage features are encountered. There are several small cross drainages suitable for conventional culverts.

(iv) Bridges

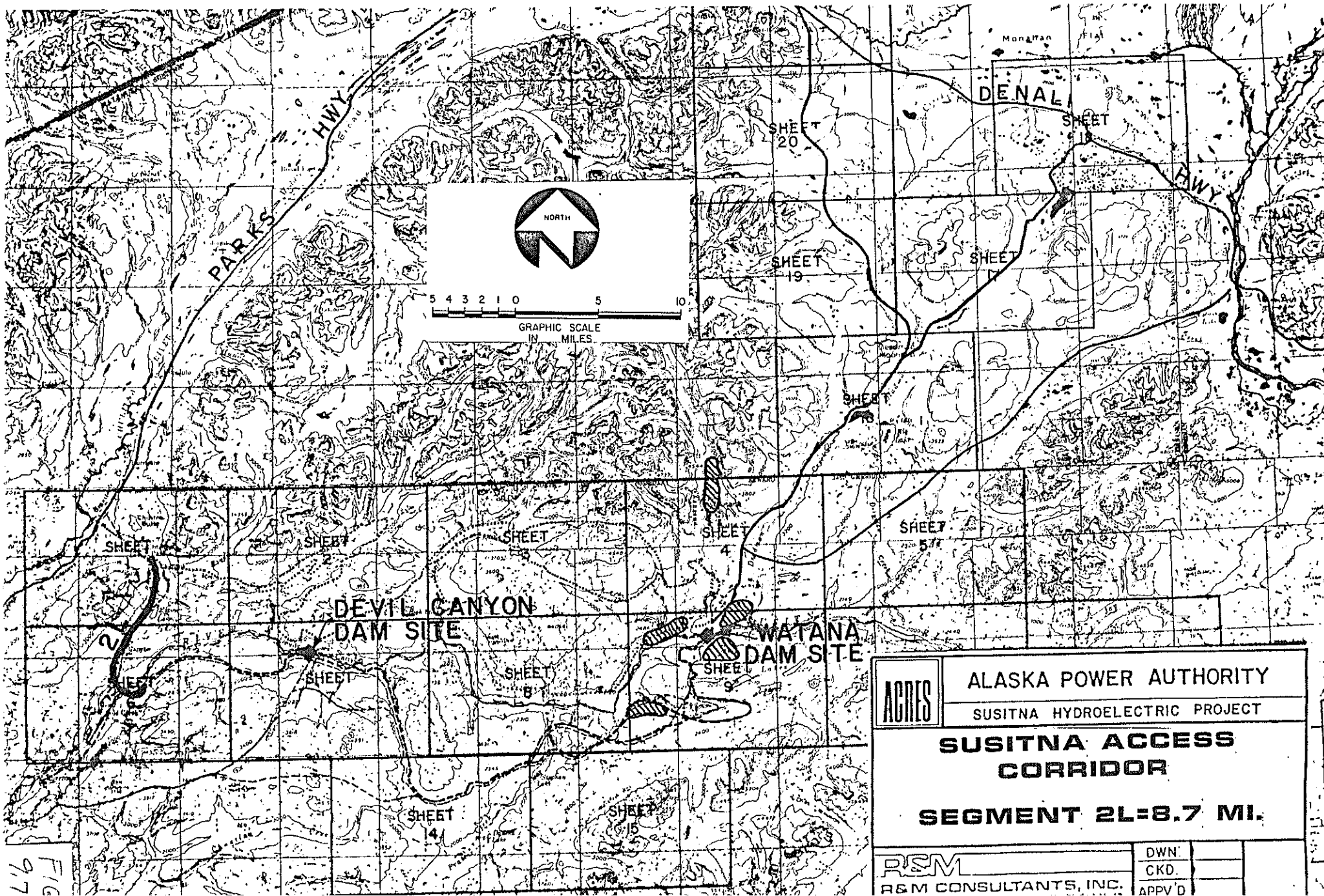
The Susitna River must be crossed. This structure can be a mulitspan continuous welded plate girder structure. The over all length is such that approximately two years will be needed to construct this structure. This segment also requires one bridge over Indian River. This would be a three span continuous welded plate girder structure about 400-foot in length.

(v) Soils

The soils traversed by the segment are predominately frozen Basal till. Care must be taken to avoid disturbing the thermal balance. The side slopes are moderate. The line is intended to stay along the break just on the top of a bluff along Indian River.

(vi) Environmental Concerns

There are salmon using Indian River, therefore care should be taken to minimize erosion. There is private property close to the line. Property owners have expressed a negative feeling about having any access facility near them.



<b>ACRES</b>	ALASKA POWER AUTHORITY		
	SUSITNA HYDROELECTRIC PROJECT		
	<b>SUSITNA ACCESS CORRIDOR</b>		
	<b>SEGMENT 2L=8.7 MI.</b>		
<b>R&amp;M</b>		DWN'	
R&M CONSULTANTS, INC.		CKD.	
		APPV'D	

FIG  
9.7

(vii) Segment Suitability

The segment is suitable for construction and would be preferable to the corresponding section of 2E. It reduces the possibility of any potential encroachment on private property. The line requires one less crossing of Indian River than does 2-E, and provides a good crossing of the Susitna while eliminating the need to build over or around a bluff on the south side of the Susitna River.

(s) Segment 2-R

(i) Description

This segment is the principle rail alternative identified for the project. The alignment is within corridor 2 on the south side of the Susitna. The line would begin at the railroad at Gold Creek traversing a short section of steep terrain at water level then becoming coincident with Segment 2-I all the way to Devil Canyon. From Devil Canyon 2-R traverses the side hill above the Susitna River parallel to and below segment 2-G turning south and requiring a full bench cut up the side of a steep gorge to the Prairie Creek divide above Stephan Lake. From this point the segment is essentially coincident with Segment 2-A all the way to Watana Dam except for a few sections that require wider swings to maintain the acceptable grades. See Figure 9.8.

The line is 57.7 miles long.

(ii) Line and Grade

The line conforms with the desired parameters for railroad construction. The ruling grade is approximately 2.5% which

we are advised is comparable to some mainline sections on the Alaska Railroad.

(iii) Drainage Features

Drainage features along the route include the same small streams and wet areas encountered by the roadway segments. Culverts will handle most cross drainages although a few will be large enough to require multiplate or pipe arch type structures. There are some wetland areas that must be considered also, particularly near Stephan Lake.

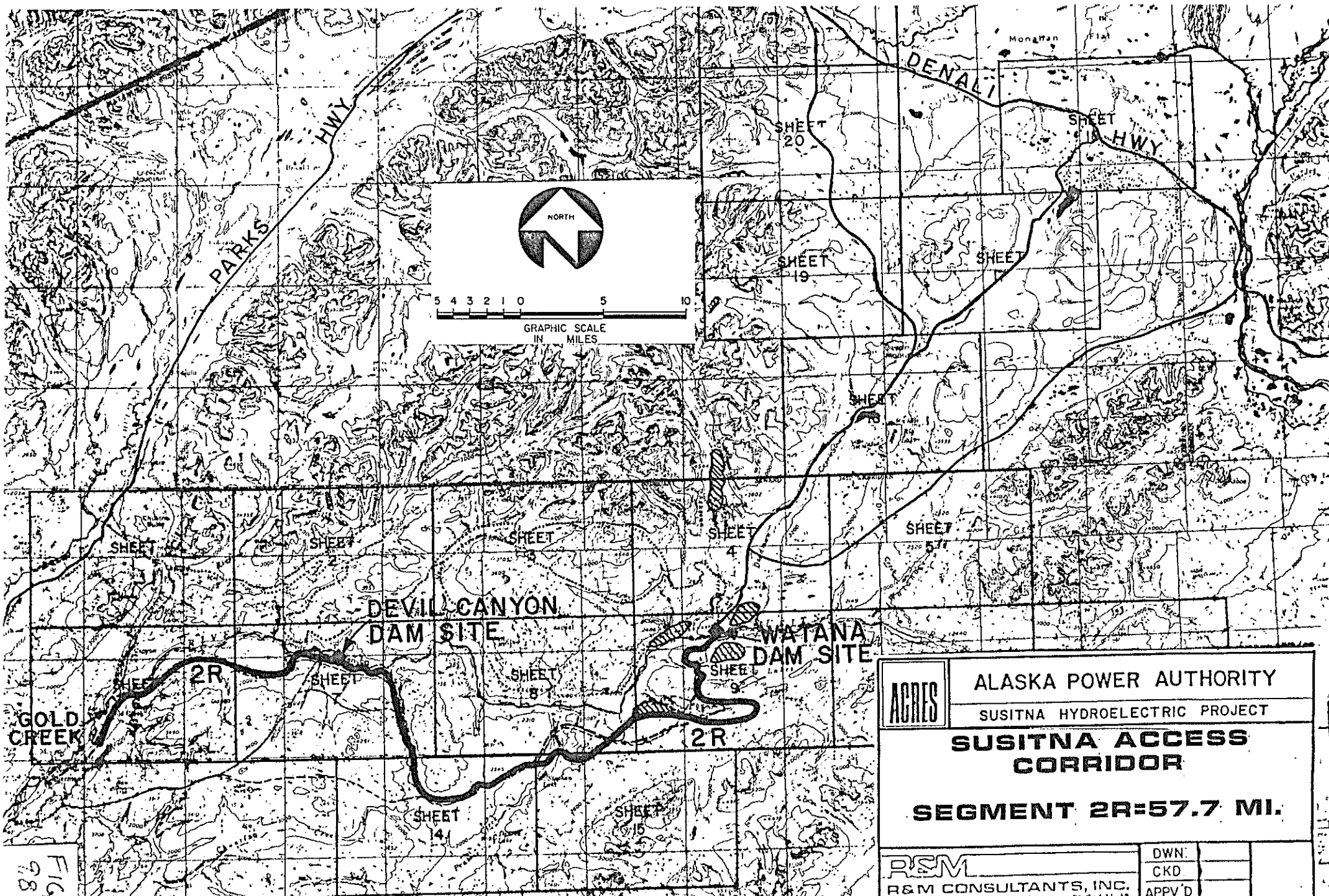
(iv) Bridge

The railroad alignment required only one major bridge. That is across Cheechako Creek just upstream from Devil Canyon. This will probably be a Deck Truss requiring three spans. This type of structure will require about two years to build and no rail service could be provided with any sort of bypass.

(v) Soils

This alignment crosses the same general soil type as other segments described. Much of the alignment is on frozen soils that tend to be subject to erosion, frost heave, and thaw settlement with a few sections of deep organic soils and one section between Devil Canyon and Stephan Lake having very heavy rock work.

This line also crosses the massive ice area near Stephan Lake.



<b>ACRES</b>	<b>ALASKA POWER AUTHORITY</b>	
	<b>SUSITNA HYDROELECTRIC PROJECT</b>	
	<b>SUSITNA ACCESS CORRIDOR</b>	
	<b>SEGMENT 2R=57.7 MI.</b>	
<b>R&amp;M</b>		<b>DWN:</b>
<b>R&amp;M CONSULTANTS, INC.</b>		<b>CKD</b>
		<b>APPV'D</b>

FIG 98

(vi) Environment Concerns

The Environmental concerns for the railroad are the same as for the roadway. The primary area of environmental concern is near Stephan and Fog Lakes 2-R does encroach on the borrow area H for Watana Dam.

(vii) Segment Suitability

If Railroad is chosen for access this segment is quite suitable. There are however certain schedule constraints to be considered. The Cheehako Creek bridge is a two year construction project. The portion of road bed from Devil Canyon to the Prairie Creek divide is, to a large extent, a rock excavation project requiring extensive blasting. This section alone will take a construction season. The terrain south of the Susitna makes winter mobilization very difficult if not impossible. Summer supply would require extensive roads and resulting environmental damage. It appears that construction of rail access to Watana would require three to four years.

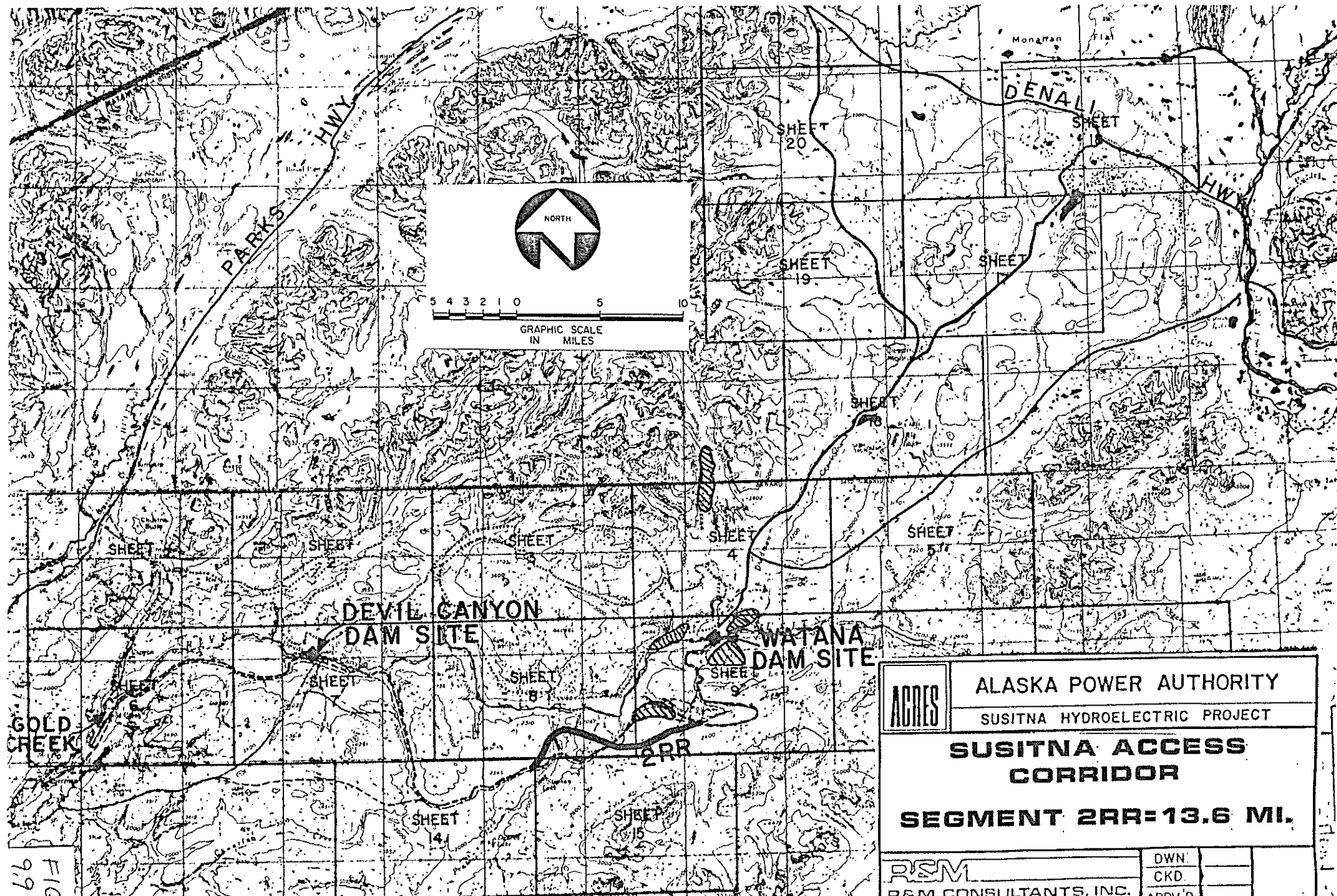
(t) Segment 2-RR

(i) Description

This segment is an alternate railroad alignment in the Stephan Lake area which avoids the worst soils conditions of Segment 2-R in this vicinity. See Figure 9.9.

Length of the segment is 13.6 miles.





99  
FIG

(ii) Line and Grades

The alignment conforms to the required parameters for line and grade with no distinct advantage over 2-R.

(iii) Drainage Features

There are no unique or special drainage features on this segment. Standard drainage practice will serve adequately.

(iv) Bridges

No Bridges are required on this segment.

(v) Soils

The soils are predominately frozen Basal till or Lusterines over frozen Basal till. These materials require care in design and construction. They are common to all segments however.

(vi) Environmental Concerns

All environmental conflicts have been identified. They are essentially the same as for 2-R.

(vii) Segment Suitability

This segment does have some advantage over 2-R in that it avoids the worst of the organic soils near Stephan Lake and avoids borrow area H as designated for construction of Watana Dam.

(u) Segment 3-A

(i) Description

Segment 3-A begins at Watana Dam on the north side of the river. The alignment proceeds north easterly to Deadman Creek then ascends Deadman Creek on an easy grade past Deadman Lake, continuing onto Butte Lake and connecting with the Denali Highway some 40 miles east of Cantwell. See Figure 9.10.

The line is 38.5 miles long.

(ii) Line and Grade

The horizontal and vertical alignment of this segment are excellent.

(iii) Drainage Feature

All streams and intermitent drainages on this alignment could be served by culverts of varying sizes.

(iv) Bridges

There are no bridges on this alignment

(v) Soils

The soils traversed along this alignment are unfrozen till, frozen Solifluction deposits, flood plain deposits, alluvial fans and Lusterines. The cross slope, with few exceptions are gentle enough so that major cuts and fills can be avoided. This will keep the disturbance of erodible and/or frozen soils

to a minimum. The needed borrow areas to provide embankment over frozen soils will be much less than for other segments discussed so far.

(vi) Environment Concerns

The environmental concerns identified to include archaeological finds near Deadman and Butte Lakes. A known Bald Eagle nest tree, and the fact that much of the line traverses areas sometimes used by the Nelchina Caribou herd as calving grounds and summer range.

(vi) Segment Suitability

This segment is suitable for roadway construction. The terrain is gentle enough that by using multiple contracts and winter mobilization this entire alignment could be made possible in a single construction season, thereby minimizing any potential schedule impact on construction of Watana Dam.

(v) Segment 3-B

(i) Description

This segment leaves 3-A at Deadman Creek and proceeds east into the Watana Creek drainage. The line proceeds up Watana Creek to its head then follows Butte Creek northeasterly to an intersection with the Denali Highway at the Susitna River. See Figure 9.10.

This line is 36.6 miles long.

(ii) Line and Grade

All desired parameters for line and grade are satisfied.

(iii) Drainage Features

No abnormal drainage feature are encountered although crossings of Deadman Creek and Butte Creek are required. These will necessitate small bridges or large pipe structures.

(iv) Bridges

At this time no bridges are planned. The crossing of Deadman and Butte Creek could be accomplished using Pipe arch structures that are much faster and more economical than bridges.

(v) Soils

The soils along this alignment are similar to thoses encountered along 3-A except that more wet ground is encountered as the Denali Highway is approached. The soils along this line were not mapped in detail.

(vi) Environmental Concern

This alignment also serves known Caribou calving grounds.

(vii) Segment Suitability

This segment has been detemined to be less suitable that 3A or 3C for the following reasons.

- ° The crossings of Deadman and Butte Creeks

- ° Intersects Denali Highway furtherst from the potentail railhead at Cantwell, thereby increasing haul distance and the length of Denali Highway to be maintained.

(u) Segment 3-C

(i) Description

This segment leaves 3-A north of Deadman Lake and travels northerly to intersect the Denali Highway west of Seattle Creek some 25 miles east of Cantwell. See Figure 9.10.

This segment is 23.4 miles long.

(ii) Line and Grade

The line and grade for this line are excellent comparing favorably with 3-A.

(iii) Drainage Features

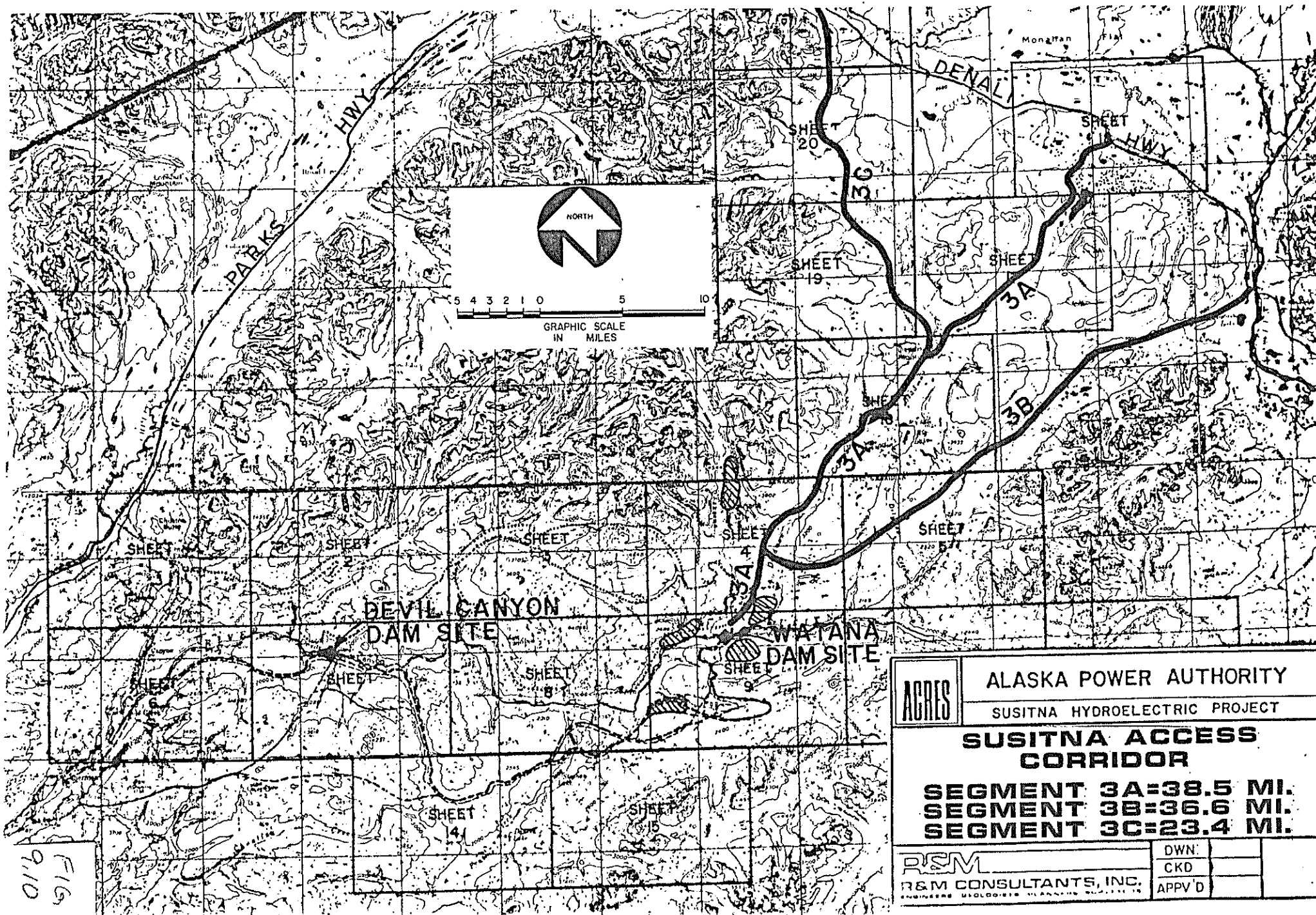
Drainage for the alignment will be by roadside ditches and standard culverts.

(iv) Bridges

No Bridges are required on the alignment.

(v) Soils

This segment shows the largest amounts of unfrozen materials of any line investigated. Because of terrain and soil types nearly all of this alignment can be constructed with side borrow techniques requiring a minimum of disturbance away from the alignment.



ACRES	ALASKA POWER AUTHORITY		
	SUSITNA HYDROELECTRIC PROJECT		
<b>SUSITNA ACCESS CORRIDOR</b>			
<b>SEGMENT 3A=38.5 MI.</b>			
<b>SEGMENT 3B=36.6 MI.</b>			
<b>SEGMENT 3C=23.4 MI.</b>			
R&M R&M CONSULTANTS, INC. ENGINEERS GEOLOGISTS PLANNING SURVEYORS	DWN		
	CKD		
	APPV'D		

FIG  
9.10

(vi) Environmental Considerations

This line avoids most of the area identified as caribou calving area. Summer caribou range is traversed, however little other environmental impact is identifiable from construction activities.

(vii) Segment Suitability

This segment appears to be quite suitable for implementation. It largely avoids the principle environmental concern pertaining to caribou calving. It can be made passable in a single construction season and it requires the least maintenance on the Denali Highway.

9.3 - Corridor Summary

With the various segments identified and estimates made of grades and curvature a series of probable combinations were developed and compared. The criteria used to compare the alternative combinations are as follows:

- ° Overall length to be constructed;
- ° Average grade;
- ° Average deflection per mile.

The tabulation of the comparison is included in Appendix A.

The alternatives identified as being most favorable based on length, alignment and grade are as follows:



For Corridor 1. Parks Highway to Watana Dam site - North side  
Segments 1-A and 1-B.

Overall	72.50 Miles
Average Grade	2.4%
Deflection Per Mile	7°06'±

This Corridor will be identified as Alternate A in further studies.

For Corridor 2. Parks Highway to Watana Dam Site - South Side  
Segments 1-E, 2-L, 2-I, 2-G, 2-B, 2-A, 2-F

Overall	62.03 Miles
Average Grade	2.2%
Deflection Per Mile	7.°50'±

This Corridor will be identified as Alternate B in further studies.

For Corridor 3. Watana Dam to Denali Highway  
Segment 3-A and 3-C

Overall	44.32 Miles
Average Grade	1.3%
Deflection Per Mile	1°30'±

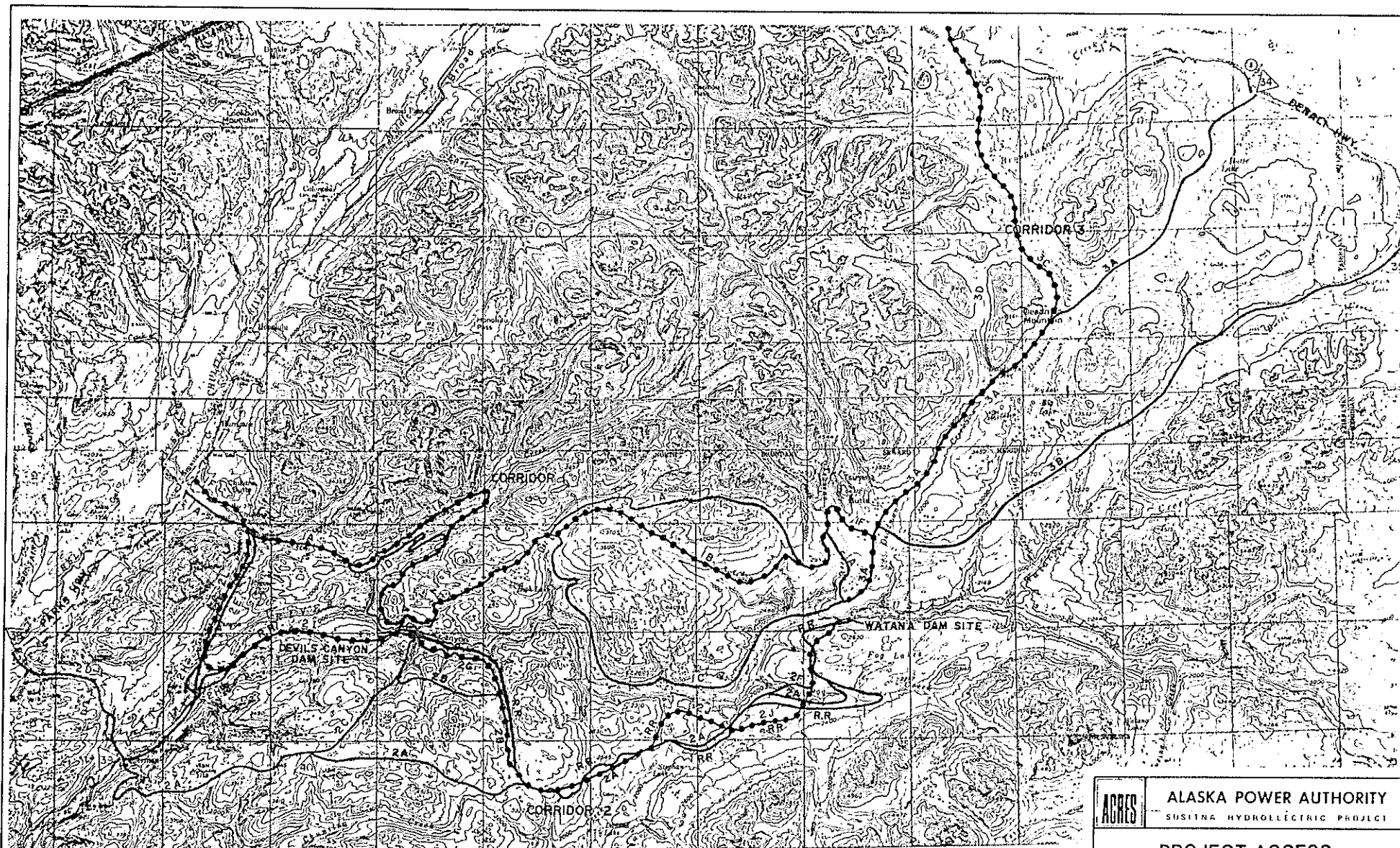
This Corridor will be identified as Alternate C in further studies.

For Railroad. Use 2-R and 2-RR on the south side of the river  
from Gold Creek to Watana Dam site. This closely follows the  
preferred road alignment for Corridor 2.



Overall	57.86 Miles
Average Grade	1.5%
Deflection Per Mile	5°11'±

This line will be identified as Alternate R in further studies.

Fig 9.11



REV

 PREFERRED ROUTE IN EACH CORRIDOR  
 OTHER ALTERNATES INVESTIGATED



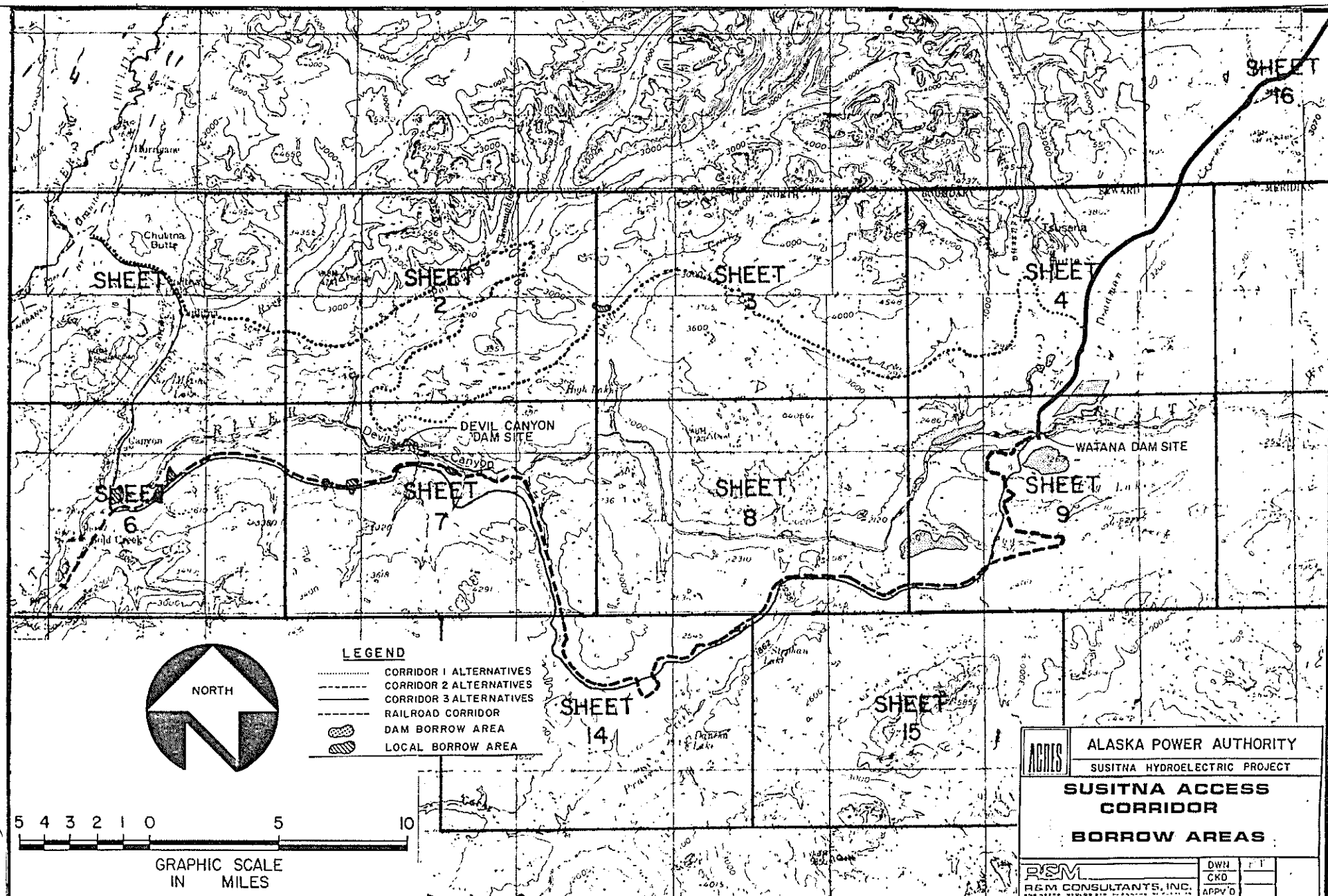
ACRES

ALASKA POWER AUTHORITY  
SUSITNA HYDROELECTRIC PROJECT

PROJECT ACCESS  
LOCATION ALTERNATIVES

RPM

SCALE: 1" = 1 MILE



1651-1

## ACCESS PLANS

## 10 - ACCESS PLANS

The Access plan selected should provide a cost effective method of serving the total requirements of the project, including construction schedule, provide a facility that can serve the ultimate recreational uses following construction, provide for maintenance of the facilities, and control or minimize the impact on the environment.

### 10.1 - Supply Sources and Shipping Options

Nearly all material supplies and equipment that will be required for construction of the Susitna project will have to be brought in from outside Alaska. The major exception to this is fuel which is available from two separate in state sources.

For this reason an assumption has been made that all such items other than explosives will be shipped from Seattle, Washington. Explosive will be shipped through Prince Rupert B.C. It is felt that this is reasonable in that sources of supply and transportation within the Continental United States will be identical for all alternatives and that differences in shipping costs will result from Port of Entry in to Alaska and differences in modal split and route traveled within the state.

Sources of fuel within the state are the refineries at Kenai and at North Pole, Alaska. Transport from Kenai would be via product pipe line to Anchorage and rail or truck from Anchorage. Transport from North Pole would be via rail or truck.

Shipping options include a variety of transportation modes. There is no direct rail connection to Alaska therefore all items brought in from elsewhere must come by sea or air. Air Transport will not be addressed because of the costs involved and the limitation on quantities. Ships and barges will be most likely be used to bring

most items to Alaska. Trucks could be used, however the rate disparity between sea and trucking makes trucking very unattractive. The barges offer some options with regard to connecting land transportation modes.

- Roll-on Roll-off Rail Cars
- Roll-on Roll-off Trucks
- Containers
- Pallatized Cargo
- Bulk Cargo

The type and quantities of materials and supplies required by the project are such that the roll-on roll-off modes and containers are the obvious choice because of the reduced need for storage and handling.

Once the materials are in Alaska the shipping options are reduced to rail or truck. Rail can offer bulk car load transport or piggy back from the dock to the project rail head. Trucks are capable of moving everything from either the dock or the project railhead.

## 10.2 - Alaska Ports

The sea ports within Alaska that could serve the project are:

- Anchorage
- Seward
- Whitter
- Valdez

### (a) Anchorage

(i) Facilities

- Petroleum Terminal - 612 feet long with multiple manifolds and electric hose handling hoists.
- General Cargo Terminal #1 - 600 feet long - 47 feet wide. Live load 600 pounds per square inch, Containers.
- General Cargo Terminal #2 - 610 feet long - 69 feet wide containers and Bulk Cement.
- General Cargo Terminals #3 - 898 feet long - Roll-on Roll-off trucks and containers.
- 35 feet of water MLLW as the dock face.
- Cranes
  - 2 - 40 Ton Level Luffing Gantry
  - 1 - 7½ Ton Level Luffing Gantry
  - 2 - 27½ Ton Container Cranes
- Transit Shed - 52,950 square feet - 22-foot ceiling - heated - Rail and truck access.
- Staging and Storage Areas
  - A - 4.6 acres
  - B - 6.4 acres
  - C - 6.7 acres

(ii) Limitations

- Cook Inlet does form heavy ice floes during the winter months. Tidal fluctuations keep the ice broken up, however there are periodic problems for shipping due to winter ice.

- There is no provision for roll-on roll-off rail.

(b) Seward

(i) Facilities

- One general cargo dock capable of handling a single ship.
- A single 40 ton level luffing gantry.
- Truck and rail service to the dock.
- 20 acres open storage.

(ii) Limitations

- No covered storage
- Limited capacity
- No movement of explosive allowed

(c) Whittier

(i) Facilities

- Single dock with roll-on roll-off rail capacity
- Rail switchyard for storing cars from barge and making up train.

(ii) Limitation

- No truck access

(d) Valdez

(i) Facilities

- 600' x 60' wooden dock



- 33-foot of water MLLW at the dock face
- 1 - 150 ton crawler crane
- 1 - 100 ton fork lift
- 2 - 30 ton fork lifts
- 3 - 9 ton fork lifts
- 5 - 3 ton fork lifts
- 200 acre open storage area four miles from dock
- 12,000 square foot warehouse at dock
- Two private barge docks having 0- to 1-foot of water at MLLW. Both were used during the Trans-Alaska pipe line construction.
- New dock under construction is a floating dock 700' x 100' with live load capacity of 1,000 lb./sq.ft. and served by two 150 ton crawler cranes. Work should be completed in 1982.

(ii) Limitations

- No railroad access

(e) Comparisons

Anchorage is closest to the project and has the greatest flexibility. Winter ice and the lack of roll-on roll-off rail capability notwithstanding Anchorage is a viable sea port for the project.

Seward is a longer haul than Anchorage and does not have the capacity of Anchorage however it is an ice free port and could be used nicely as an alternate should ice conditions or volume of traffic become such that there would be delays in reaching Anchorage. For this reason Seward is not considered further except as an alternate if needed. It must be noted that explosives cannot flow through Seward.

Whitter is a viable port for all items that can be shipped via rail car load lots. The roll-on roll-off rail barge capability is very attractive for bulk items and heavy equipment. Whitter is an ice free port so that material can flow year round.

Valdez apparently will have the capacity to handle the material flow however this is the longest truck haul and there is no rail access to Valdez. The lack of rail access and the length of truck haul combine to effectively eliminate Valdez from consideration as a viable sea port to serve the Susitna Project.

TABLE 10.1  
Mileage from Ports to Rail Head or Project

Rail Haul to	Anchorage	Seward	Whitter	Valdez*
Gold Creek	149 mi	262	211	NA
Devil Canyon	165 mi	278	227	-
Cantwell	205 mi	318	267	NA
Watana via Devil Canyon	207 mi	320	269	-
Truck Haul to				
Gold Creek, via B-1	180	307	NA	
Devil Canyon	193	320	NA	393 mi
Cantwell	212	339	NA	
Watana via Devil Canyon, B-3	229	356	NA	
Watana via Denali Highway	277	404	NA	349 mi
Watana via Devil Canyon, A-2	234	361	NA	

\* The road mileage from Valdez is shown via Denali Highway and Richardson Highway and Corridor 3.

The access plans must include the ports through which materials should flow. For comparison purposes shipping rates through the possible ports were requested. Table 10.2 below includes "across the dock" costs including handling as derived from the data supplied by port offices and shippers.

TABLE 10.2  
ACROSS THE DOCK HANDLING COSTS

Material From Seattle (6)	Cost in \$/Ton			
	(1) To Anchorage	(2) To Seward	(4) To Whittier	(1) To Valdez
Reinforcing Steel	72.00	72.00	55.00	86.00
Structural Steel	85.40	85.40	55.00	125.00
Cement	66.00	66.00	(3) 55.00	80.00
General Cargo	80.00	80.00	55.00	110.00
Equipment	160.00	160.00	120.00	191.00
Explosives	89.00	Not Allowed	55.00	115.00

- 1 Quoted by Pacific Western.
- 2 Information not received - Estimated equal to Anchorage.
- 3 Rate for 140,000 lb Hopper Cars - Rates for Bags 100.00/ton as per ARR.
- 4 Rates derived from quotation by ARR.
- 5 Includes Stevedoring at all ports.
- 6 Explosives must flow through Prince Rupert, B.C.

### 10.3 - Surface Transportation Modal Options

There are two obvious modes of transportation available to serve the project, Truck and Rail. The project may be served by either one or a combination of both. In order to compare the two modes the respective rates are presented in ton-mile figures. In this way length of haul may be considered in the analysis.

TABLE 10.3  
LINE HAUL RATES IN \$/TON-MILE

<u>Item</u>	<u>Rail*</u>	<u>Truck**</u>
Equipment	0.1878	0.2069
Steel	0.2577	0.2069
Cement	0.1565	0.2069
Fuel	0.1450	0.2069
General Cargo	0.1262	0.2069
Explosives	0.6267	0.2069

\* From price per 100 Lb. rates quoted by ARR.

\*\* One rate for all quoted by three separate truck lines.  
The cost shown is an average of three rates.

The modal alternates that seem most probable include the following:

- ° Truck from port to the site.
- ° Rail from port to the site.
- ° Rail to Gold Creek or Cantwell and truck from the rail head to the site.

#### 10.4 - Access Plans

To this point three alternative Corridors have been defined. Estimates have been made of the amounts of materials required at each site and freight handling costs have been identified for the available transportation modes and ports. The three major costs pertaining to access are logistics, construction and maintenance. Estimated construction costs are outlined. Maintenance costs will not be estimated in detail. Instead, an estimate of the relative

difference in difficulty of maintenance will be applied to an average maintenance figure of \$10,000 per mile per year. Alaska Department of Transportation and Public Facilities records show an average annual maintenance cost of \$10,000 per mile for primary highways.

TABLE 10.4  
MAINTENANCE FACTORS

	Section	Maintenance Factor*
A-1	Parks Highway to Portage Creek	1.0
	Portage Creek - Devil Canyon	1.4
A-2	Devil Canyon - Watana	1.0
B-1	Parks Highway to Gold Creek	1.0
B-2	Gold Creek to Devil Canyon	1.2
B-3	Gold Creek to Stephan Lake	1.3
	Stephan Lake to Watana	1.0
C	Denali Highway to Watana	0.8
R-1	Gold Creek to Devil Canyon	0.5
R-2	Devil Canyon to Stephan Lake	0.7
	Stephan Lake to Fog Creek	0.6

\* Based on author's past experience.

The alternate corridors identified herein are split into sections for further analysis. Those sections are as follows:

TABLE 10.5  
BASIC CORRIDOR SEGMENTS

<u>Section</u>	<u>Description</u>
A-1	Parks Highway to Devil Canyon (north side)
A-2	Devil Canyon to Watana (north side)
B-1	Parks Highway to Gold Creek
B-2	Gold Creek to Devil Canyon (south side)
B-3	Devil Canyon to Watana (south side)
C	Denali Highway to Watana
R-1	Gold Creek to Devil Canyon
R-2	Devil Canyon to Watana

The access plans outlined below are made of combinations of the above listed corridor segments.

(a) Plan I

(i) Description

Access Plan I is a basic roadway plan beginning at the Parks Highway and serving both Devil Canyon and Watana dams from the south side of the river. See Figure 10.1.

(ii) Sea Ports

There are two sea ports that appear logical for serving the project. Anchorage and Whittier. These are common to all access plans. Seward is available as an emergency backup to Anchorage. All items that can be shipped in carload lots should enter the State through Whittier because of the rail barge facility. Information provided by railroad officials indicates that this facility can handle any rail load that can be shipped on main line trackage in the continental United

States and fit on the barge. Other cargo should be containerized for shipment through Anchorage because of port capacity and available area for short term storage.

(iii) Modal Split

The split in transportation modes is consistent through all plans. Based on ton mile freight costs, the railroad should be used to as near the project as practical for all items except explosives. Therefore the rail mode should be used for all items to a rail head at Gold Creek. For Plan I, a rail head should be provided at Gold Creek with truck haul from Gold Creek to the work site.

(iv) Sections Included

The corridor sections included in Plan I include B-1, B-2, and B-3.

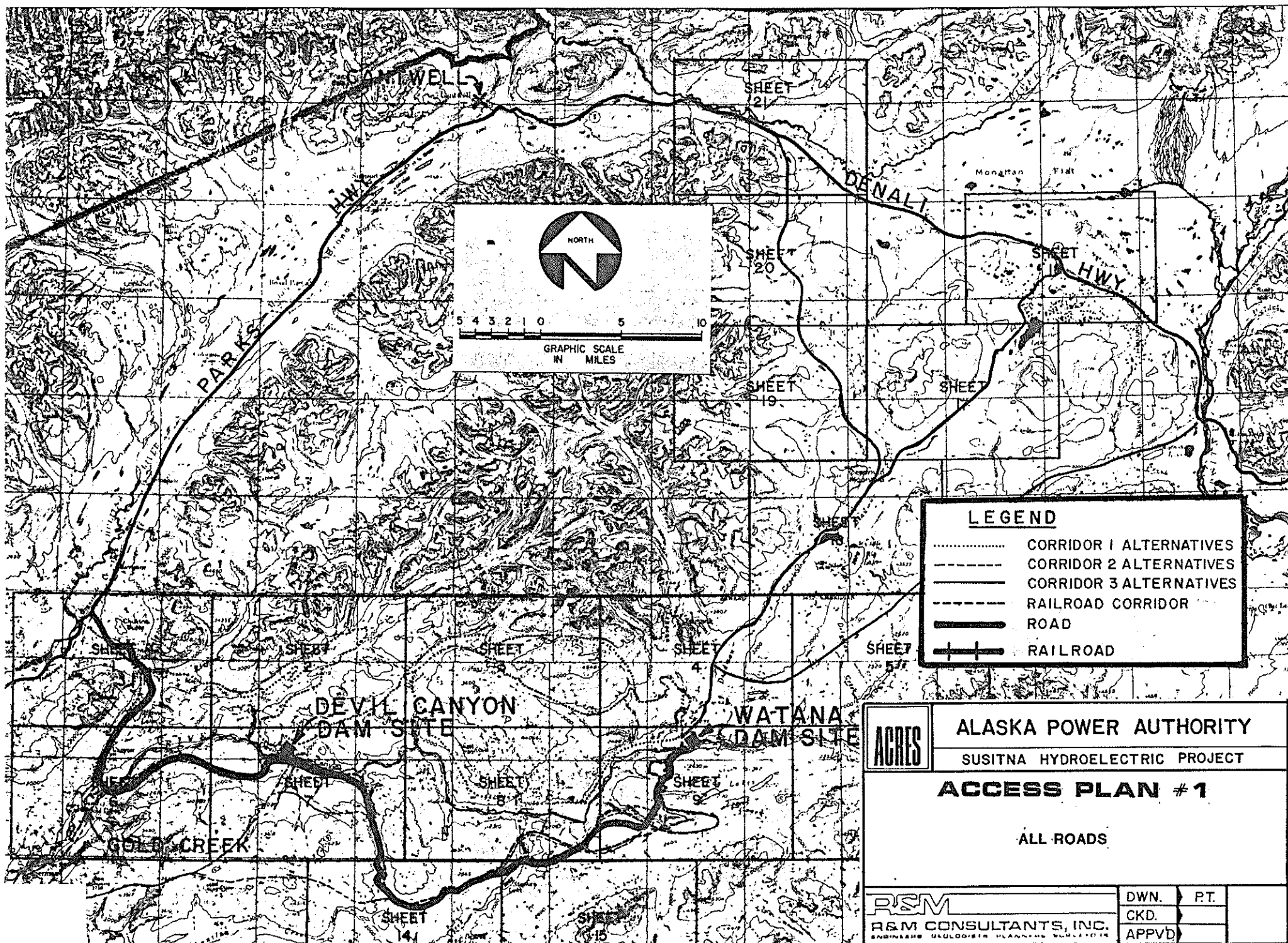
(v) Cost Estimates

The estimated cost of Plan I in 1982 dollars is outlined below:

Construction (D&C)	\$158,140,152
Maintenance	7,996,640
Logistics	<u>214,438,346</u>
TOTAL	380,575,138

(vi) Advantages/Disadvantages

This plan has the advantages of being the shortest haul to serve the project and a further advantage of requiring just a single rail head at Gold Creek while utilizing the same section from Gold Creek to Devil Canyon throughout the construction of both dams.



<b>ACRES</b>	<b>ALASKA POWER AUTHORITY</b>	
	SUSITNA HYDROELECTRIC PROJECT	
	<b>ACCESS PLAN #1</b>	
ALL ROADS		
<b>R&amp;M</b> R&M CONSULTANTS, INC. ENGINEERS GEOLOGISTS PLANNERS SURVEYORS	DWN.	P.T.
	CKD.	
	APPVD	



Disadvantages deal primarily with schedule constraints and potential environmental impacts. The plan includes a major bridge above Cheechako Creek that will take 18-24 months to construct with about twelve miles of heavy rock construction immediately beyond. The rock work will be slow work and there is no easy access around Cheechako Creek to allow the rock work to proceed coincident with the bridge. In addition, a similar but shorter bridge is required at Fog Creek. The Fog Creek bridge will require approximately 18 months to construct. These time constraints combined with the length of facility to be constructed will require an overall construction period of nearly four years. The terrain is such that construction of multiple sections simultaneously would not be practical. Recent soils investigations have revealed massive ice at or near the surface with up to 20 feet of organic soils in the area north of Stephan Lake.

(b) Plan 2

(i) Description

This plan is the railroad alternative to serve both dams. A spur track would be constructed beginning at Gold Creek and following the south side of the river to Watana Dam. There would be no roadway involved with this plan. See Figure 10.2.

(ii) Sea Ports

Anchorage and Whittier would be the obvious sea ports for this plan. The rail barge capabilities of Whittier would be vital to this plan.

(iii) Modal Split

Transportation would be essentially single mode with all material being transported from the dock to the job site by rail. The movement of personnel would be by rail or by air. The volumes of personnel would probably dictate passenger train service. This service has not been included in the cost estimates.

(iv) Section Included

This plan includes Sections R-1 and R-2.

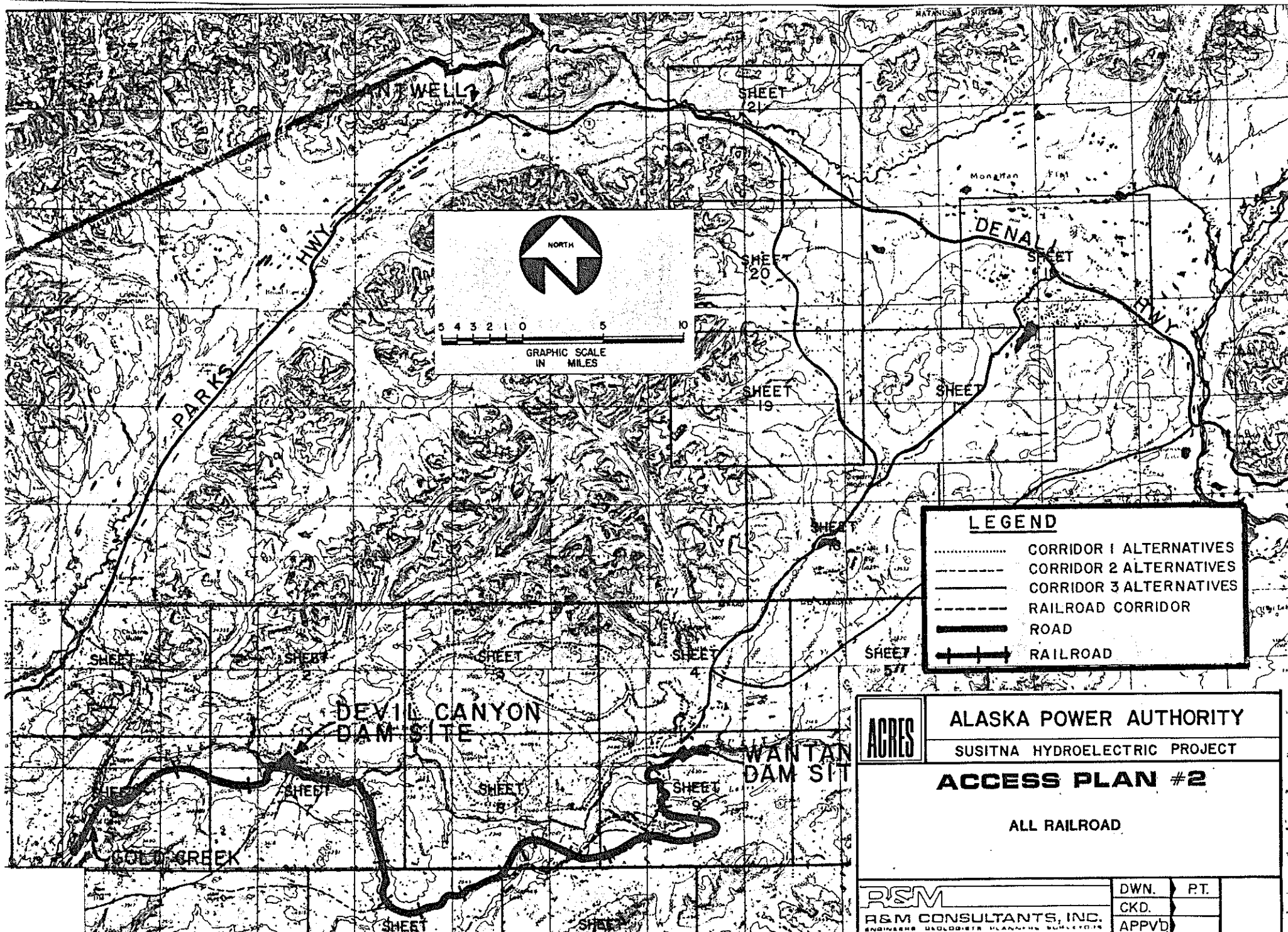
(v) Cost Estimates

The estimated cost of Plan 2 in 1982 dollars is outlined below:

Construction (D&C)	139,786,755
Maintanance	3,549,670
Logistics	<u>213,620,014</u>
TOTAL	356,956,439

(vi) Advantages/Disadvantages

- ° This plan appears to be the least total cost alternate for serving the project.
- ° This plan essentially eliminates concern about the impact of public access to the project area.
- ° The rail line could be used as a transportation facility to aid in potential mineral resources along part of the route.
- ° Least cost to maintain
- ° Least Logistics cost



# **LEGEND**

- ..... CORRIDOR 1 ALTERNATIVES
- CORRIDOR 2 ALTERNATIVES
- CORRIDOR 3 ALTERNATIVES
- RAILROAD CORRIDOR
- ROAD
- +++++ RAILROAD

**ACRES**

**ALASKA POWER AUTHORITY**

SUSITNA HYDROELECTRIC PROJECT

## **ACCESS PLAN #2**

ALL RAILROAD

**RSM**  
**R&M CONSULTANTS, INC.**  
 ENGINEERS GEOLOGISTS PLANNERS SURVEYORS

DWN.	P.T.
CKD.	
APPVD	

- ° A significant disadvantage is that the line must be built lineally rather than in simultaneous sections.
- ° Another disadvantage is the major bridge at Cheechako Creek. This also is an 18-24 month construction project.
- ° The section of heavy rock construction is even more severe than for Plan I because grades hold the line down further on the slope in the critical section.
- ° The ice and organic soils problems near Stephan Lake would have more impact on the railroad than on a roadway.
- ° As with Plan I, construction time would be three to four years.

(c) Plan 3

(i) Description

This plan uses a combination of rail and truck. Construction of Watana Dam would be served from a rail head at Cantwell by truck across the Denali highway and along Alternate C. Construction of Devil Canyon dam would be served by truck from a rail head at Gold Creek with road access to Parks Highway. This plan does not include a connection between the two dams. See Figure 10.3.

(ii) Sea Ports

Common to all plans are Anchorage and Whittier.

(iii) Modal Split

This plan requires rail heads at Gold Creek and at Cantwell. Materials would move from port to rail head via rail road, be

transferred to trucks at the rail head and be hauled to the work site by truck. The movements of construction workers would be via private auto direct to the construction camp.

(iv) Section Included

This plan includes Sections B-1, B-2 and C

(v) Cost Estimates

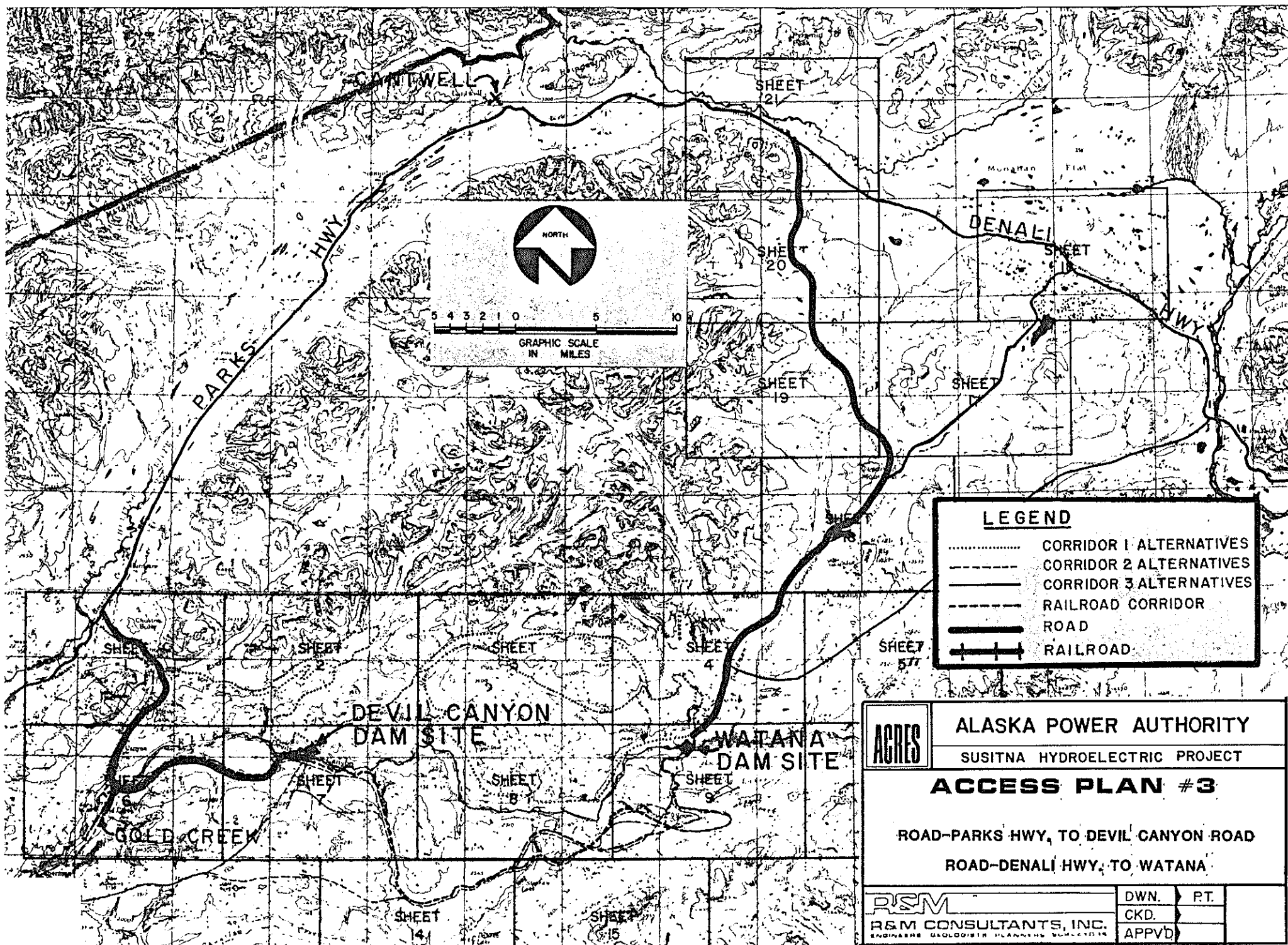
This plan is estimated to cost as follows:

Construction (D&C)	156,509,746
Maintanance	6,142,720
Logistics	<u>228,050,607</u>
 TOTAL	 390,703,073

(vi) Advantages/Disadvantages

The advantages of the plan are:

- ° It utilizes Section C which is the only approach to Watana that could be completed sufficiently in one season to allow resupply of construction activities at Watana.
- ° Personnel access via private auto.
- ° No major bridges necessary for movement of construction materials.
- ° Segments B-1 and B-2 including the Susitna River Bridge could be built during the period of construction for Watana thereby eliminating the time constraints.



The disadvantages of the plan are:

- ° Potential environmental impacts resulting from public access to additional portions of the Nelchina Caribou Range.
- ° Lack of direct access between dams for maintenance and operations staff.

(d) Plan 4

(i) Description

This plan serves Watana by truck from a rail head at Cantwell and Devils Canyon by rail from Gold Creek. In the plan there is no connection between dams.

(ii) Sea Ports

The same sea ports are common to all plans. They are Anchorage and Whittier.

(iii) Modal Split

This plan would require rail service to Cantwell via existing trackage with construction of a rail head at Cantwell and truck service from Cantwell to Watana.

Devil Canyon would be served by rail only from Gold Creek with the second rail head at the Devil Canyon dam site.

All material would flow by rail to the rail head. Personnel access for Watana would be via private vehicle while rail shuttle service, probably from Hurricane, would be required for Devil Canyon.

(iv) Section Included

This plan would require construction of Sections C and R-1

(v) Cost Estimates

The estimated cost of Plan 4 in 1982 dollars is outlined below:

Construction (D&C)	124,129,310
Maintenance	4,750,630
Logistics	<u>228,004,342</u>
 TOTAL	 356,884,282

(vi) Advantages/Disadvantages

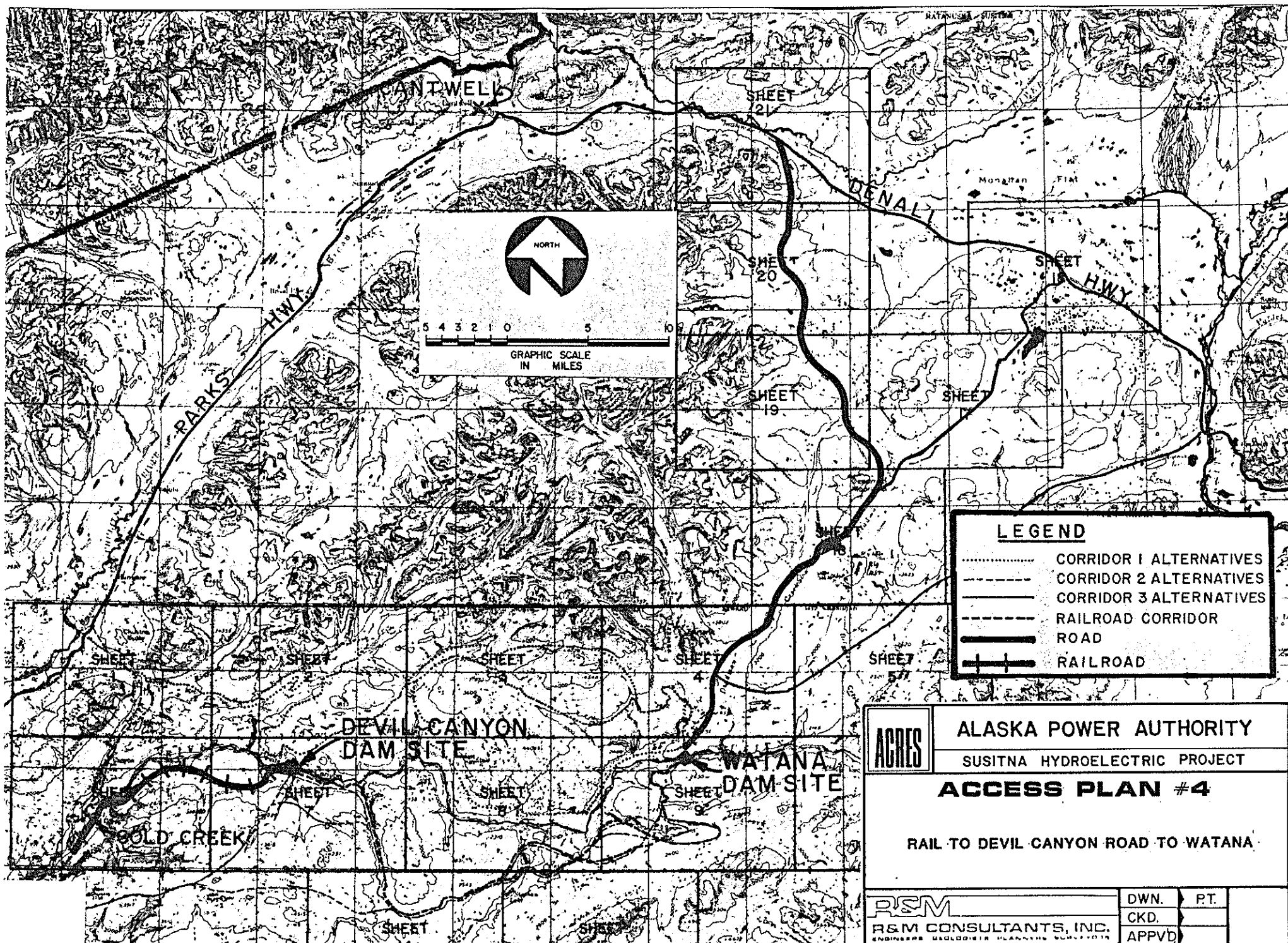
The advantages of this plan include:

- Good compliance with required project schedule.
- Sections C to serve Watana can be constructed sufficiently to allow resupply in one season using multiple simultaneous contracts for shortened sections with primary mobilization via winter snow road.
- No major bridges.

The disadvantages include:

- Potential impact from public access.
- Need for rail shuttle to move personnel into Devil Canyon.
- No direct connection between dams for maintenance and operations staff.





(e) Plan 5

(i) Description

This plan serves both dams by truck from a rail head at Gold Creek. The south side of the river is used to Devil Canyon with a major bridge downstream from the damsite, then the north side is used to Watana. A road way connection to the Parks Highway is included.

(ii) Sea Ports

This plan utilized Anchorage and Whittier as do the other plans presented.

(iii) Modal Split

Rail haul to Gold Creek with a subsequent truck haul to the work site. Personnel would access the camps via private auto.

(iv) Sections Included

The Sections that would be included in this plan are B-1, B-2, and A-2 with bridges over the Susitna River.

(v) Cost Estimates

The estimated costs of this plan are outlined below:

High Susitna Bridge (D&C)	13,260,000
Construction (D&C)	128,420,452
Maintanance	7,504,800
Logistics	<u>215,571,641</u>
 TOTAL	 364,756,893

\* High Bridge Cost: 2,600 ft. x 34 ft. x \$150/sq. ft.

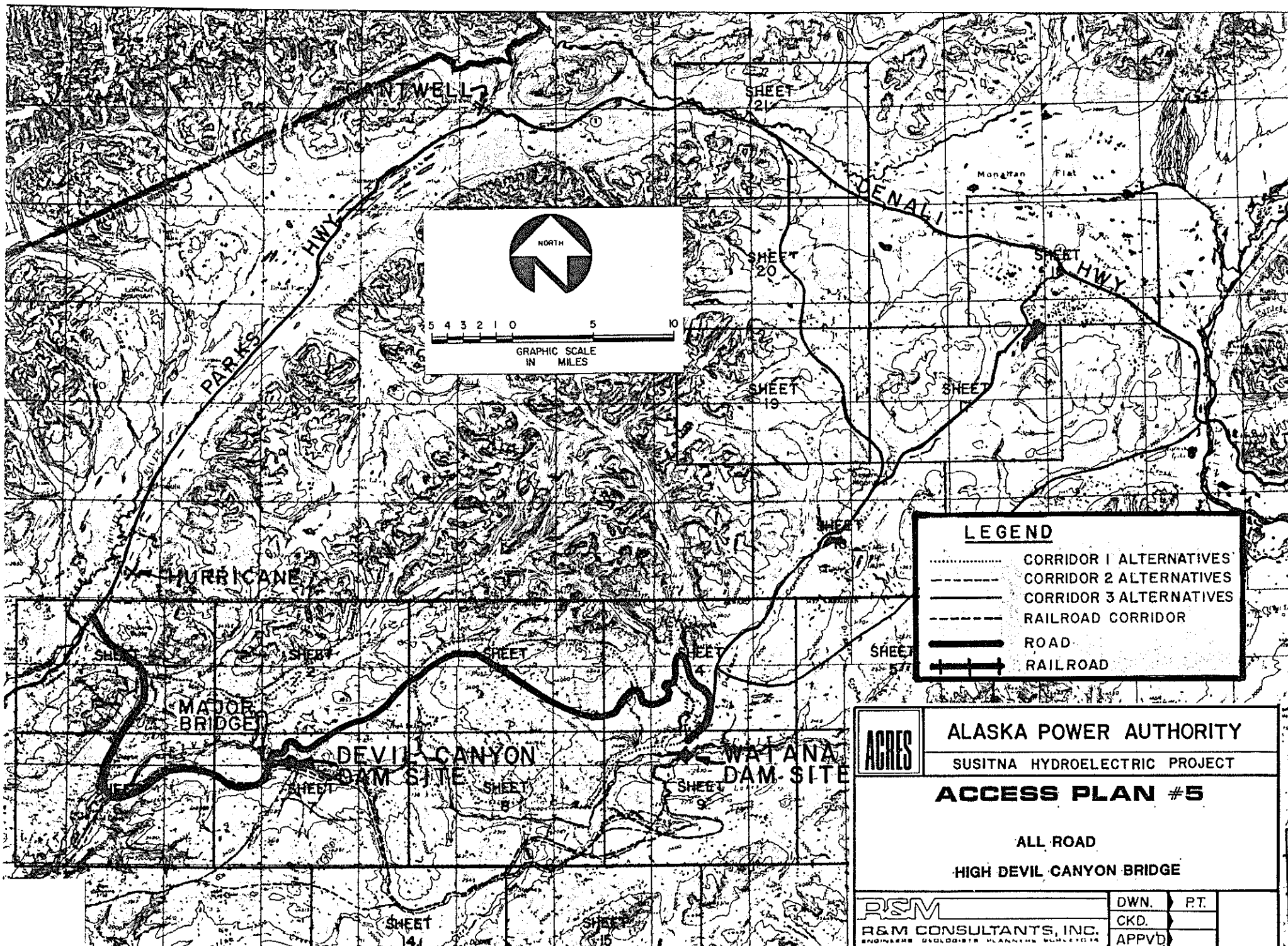
(vi) Advantages/Disadvantages

The advantages of this plan are:

- The segments involved encounter the apparent minimum of environmental conflicts.
- Personnel access is via private auto.

The disadvantages include:

- A requirement for total construction of the access prior to being able to resupply construction at Watana.
- The requirement to construct a high bridge over the Susitna below Devil Canyon. This would be a suspension bridge and would require two to three years to construct thus preventing work beyond until the bridge could be crossed.
- The time from the construction of this plan would be three to four years with the associated negative impacts on total project schedule.



### LEGEND

- ..... CORRIDOR 1 ALTERNATIVES
- CORRIDOR 2 ALTERNATIVES
- CORRIDOR 3 ALTERNATIVES
- RAILROAD CORRIDOR
- ROAD
- +—— RAILROAD

**ACRES**

**ALASKA POWER AUTHORITY**

SUSITNA HYDROELECTRIC PROJECT

**ACCESS PLAN #5**

ALL ROAD

HIGH DEVIL CANYON BRIDGE

**R&M**  
R&M CONSULTANTS, INC.  
ENGINEERS GEOLOGISTS PLANNERS SURVEYORS

DWN.	P.T.
CKD.	
APPVD	

(f) Plan 6

(i) Description

This plan is essentially the same as Plan 4 except that a secondary road is provided along the north side between the dams for use by the maintenance and operations staff. This plan would use the top of Devil Canyon Dam for a crossing rather than constructing a bridge.

(ii) Sea Port

As with all plans, the sea ports will be Anchorage and Whittier.

(iii) Modal Split

This plan contemplates rail haul to Cantwell with truck haul from Cantwell to Watana and direct rail haul to Devil Canyon via Gold Creek. Personnel access to Watana by private auto and Devil Canyon by rail shuttle.

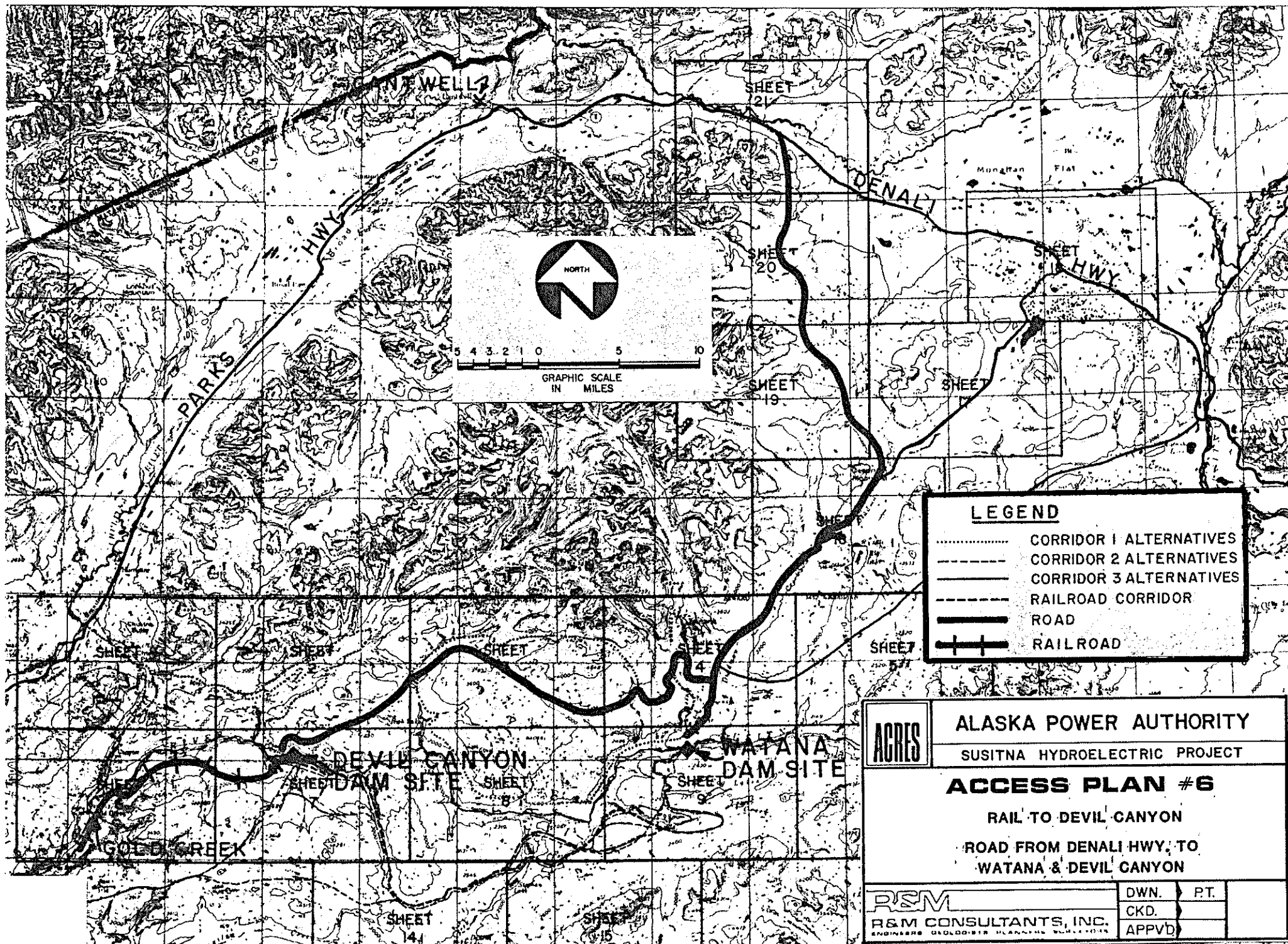
(iv) Section Included

The Sections included are A-2, R-1 and C

(v) Cost Estimates

The estimated cost of the plan is outlined below:

Construction (D&C)	183,240,606
Maintanance	7,638,130
Logistics	<u>228,004,342</u>
TOTAL	418,883,078



(vi) Advantages/Disadvantages

The advantages of the plan include:

- ° Good compliance with the required project schedule.
- ° Section C to serve Watana can be constructed to a point that would allow resupply in one construction season using multiple simultaneous contracts over short sections with primary mobilization over winter snow roads.
- ° No major bridges involved.
- ° Direct access between dams for maintenance and operations staff.

The disadvantages of the plan include:

- ° The potential impact from increased public access.
- ° The need for a rail shuttle to bring personnel to the Devil Canyon site.

(g) Plan 7

(i) Description

This plan serves Watana by truck from a rail head at Cantwell, Devil Canyon by truck from a rail head at Gold Creek with a road connection to the Parks Highway and a road connection between dams north of the river. This plan would use the crest of Devil Canyon for a crossing rather than constructing a bridge.

(ii) Sea Ports

Anchorage and Whittier are the logical sea ports for this plan.

(iii) Modal Split

All freight would travel by rail to the appropriate rail head then by truck to the work sites. Personnel travel would be by private vehicle.

(iv) Section Included

The Sections include B-1, B-2, A-2, C with rail head construction at Gold Creek and Cantwell.

(v) Cost Estimates

The estimated cost of this plan is outlined below:

Construction (D&C)	215,621,042
Maintanance	9,030,220
Logistics	<u>228,050,607</u>
TOTAL	452,701,869

(vi) Advantages/Disadvantages

The advantages of this plan include:

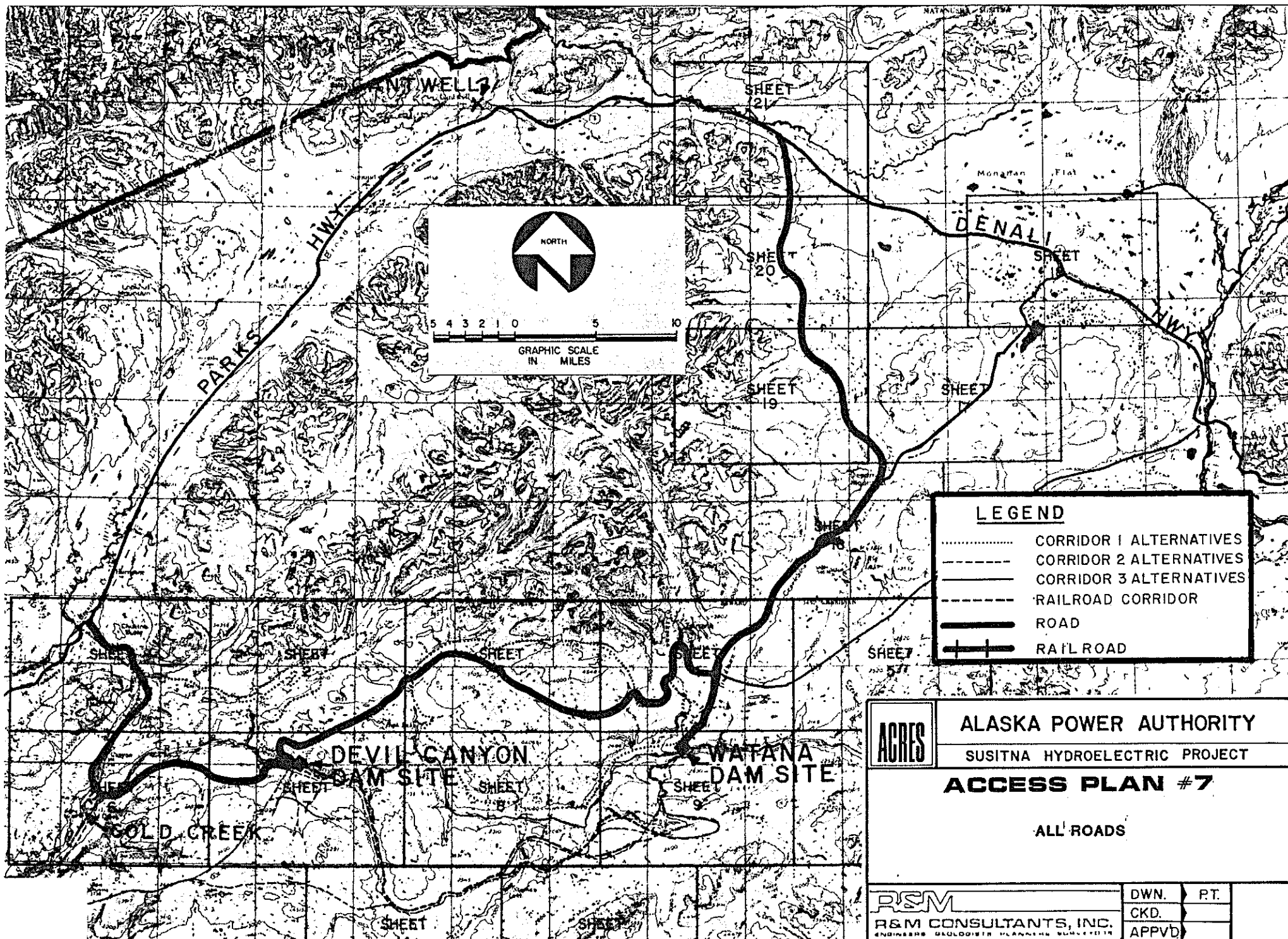
- ° Good compliance with the required project schedule.
- ° Section C to serve Watana can be constructed in one season sufficient to allow resupply.



- ° The only major bridge is over the Susitna River at Gold Creek and is not on the project critical path.
- ° Direct access between dams for the maintenance and operations staff.
- ° All personnel access via private auto.

The disadvantages of this plan include:

- ° The potential impacts from public access.



(h) Plan 8

(i) Description

This plan is essentially the same as Plan 5, except that there is no road connection between the Parks Highway and Gold Creek. The plan serves both dams by truck from a rail head at Gold Creek. The south side of the river is used to Devil Canyon with a major bridge downstream from the damsite, then the north side is used to Watana. All truck tractors will initially have to be ferried to Gold Creek by train, than they will be able to shuttle between Gold Creek and the damsites.

(ii) Sea Ports

This plan utilized Anchorage and Whittier as do the other plans presented.

(iii) Modal Split

Rail haul to Gold Creek with a subsequent truck haul to the work site. Personnel would access the camps via train to Gold Creek, than bus shuttle on the road, or by air.

(iv) Sections Included

The Sections that would be included in this plan are B-2 and A-2 with one bridge over the Susitna River.

(v) Cost Estimates

The estimated costs of this plan are outlined below:

High Susitna Bridge	13,260,000
Construction	78,327,742
Maintanance	5,103,300
Logistics	<u>215,571,641</u>
TOTAL	312,262,683

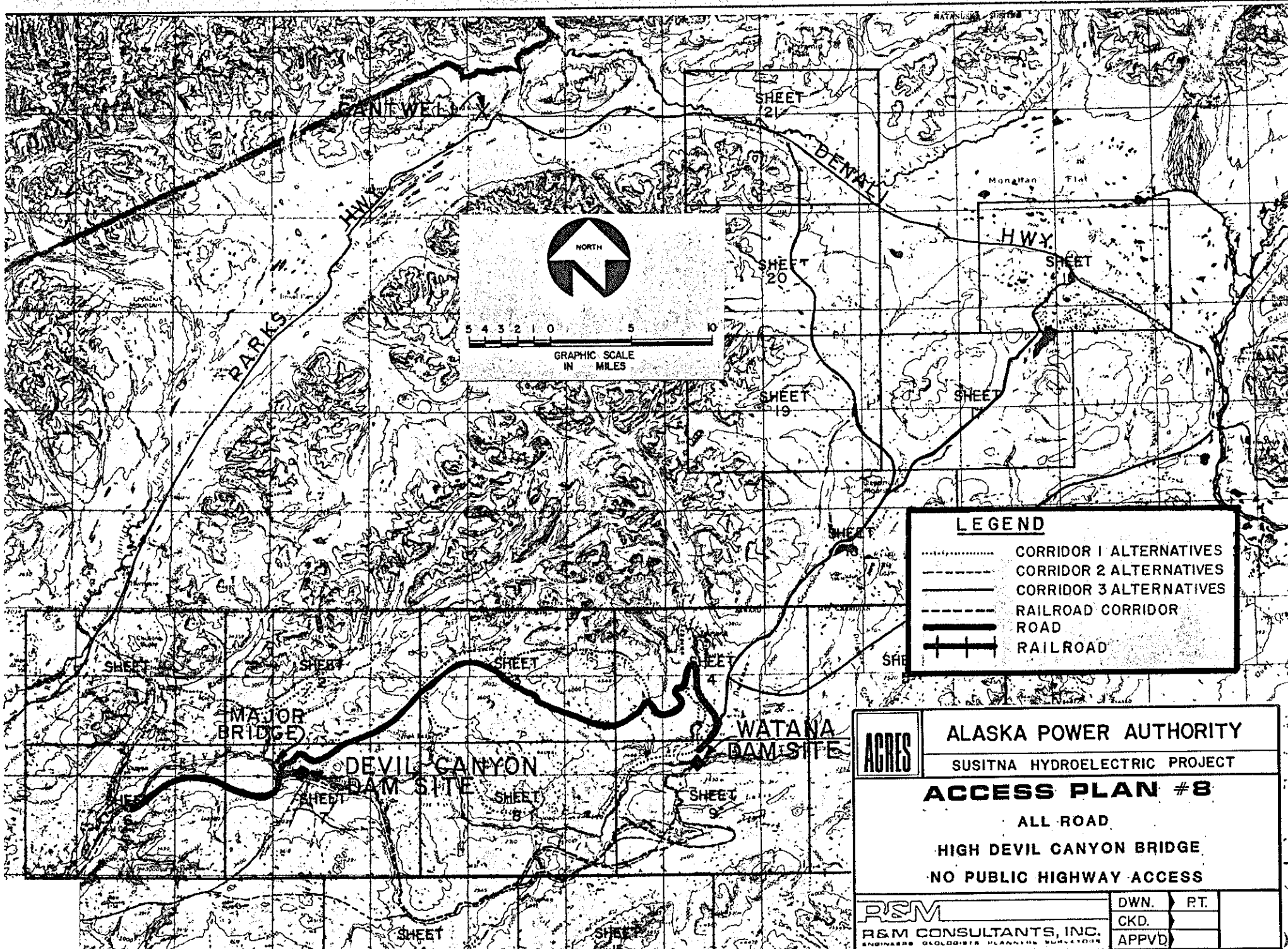
(vi) Advantages/Disadvantages

The advantages of this plan are:

- The segments involved encounter the apparent minimum of environmental conflicts.
- Public access is restricted.
- Lowest design and construction cost
- Lowest overall costs.

The disadvantages include:

- A requirement for total construction of the access prior to being able to resupply construction at Watana.
- The requirement to construct a high bridge over the Susitna below Devil Canyon. This would be a suspension bridge and would require two to three years to construct thus preventing work beyond until the bridge could be crossed.
- The time from the construction of this plan would be three to four years with the associated negative impacts on total project schedule.
- Need to provide transportation for personnel access.



CONCLUSIONS  
AND  
RECOMMENDATIONS

## 11 - Conclusions and Recommendations

No final conclusions or recommendations are made at this time. Additional input is required from other project team members before a final plan selection can be made.

## APPENDIX A

### PRELIMINARY DESIGN DEVELOPMENT



## Appendix A - Preliminary Design Development

The Susitna Hydroelectric project includes two large dams. These structures are located in remote wilderness however the size of the structures are such that major transportation facilities are required to serve the project and small communities are needed to house the construction crews.

In order to demonstrate the magnitude of the planned development plan views of the dams are included as are the projected construction schedules. Correspondence is included that identifies the major quantity requirements and crew requirements. This data has been used in the development and analysis of the various access plans.

August 20, 1981  
P5700.11.10  
T.1078

R&M Consultants Inc.  
P.O. Box 6087  
5024 Cordova Street  
Anchorage, Alaska 99503

Attention: Mr. N. Gutcher

Dear Mr. Gutcher:

Susitna Hydroelectric Project  
Estimate of Total Weights

As discussed with you on August 10, we have made an initial estimate of the total weights of various major items needed for construction of the Susitna development. These quantities should be used in completing the logistics portion of your access road report and are as follows:

	<u>Watana</u>	<u>Devil Canyon</u>
Installed Mechanical, Structural & Electrical Equipment	15,000 ton	13,500 ton
Construction Equipment	16,000 ton	5,000 ton
Explosives	20,000 ton	3,000 ton
Cement	350,000 ton	650,000 ton
Reinforcing Steel	33,000 ton	22,000 ton
Rock Bolts	12,500 ton	3,000 ton
Steel Support & Liners	3,600 ton	2,200 ton
Fuel	75 million gallons	17 million gallons

MOORE AMERICAN INCORPORATED

Mr. N. Gutcher  
R&M Consultants Inc.

August 20, 1981  
Page 2

Please forward your completed report to us by September 15. If you have any questions or need further information please contact either Tom Gwozdek or myself at this office.

Sincerely,

*Dennis Meilhede*

D. Meilhede

DM/ljr

cc: J. Lawrence  
J. Hayden  
J. Gill  
F. Toth

052211

September 4, 1981  
P5700.11.10  
T.1132

R&M Consultants  
P.O. Box 6037  
5024 Cordova Street  
Anchorage, AK 99503

Attention: Mr. N. Gutcher

Dear Mr. Gutcher:

Susitna Hydroelectric Project  
Project Schedule

As you requested, enclosed please find the following:

1. Preliminary Schedule Watana - July 1981
2. Preliminary Schedule Devil Canyon - July 1981
3. Most Recent Layout-Watana (reduced Dylar)
4. Most Recent Layout-Devil Canyon (reduced Dylar)

As we discussed, these items reflect the present level of development of the Susitna Project and can be used in completion of your access road logistics study. Finalized layouts and schedules are, of course, impossible to provide at this time. Similarly, our present estimate for peak camp size is 4,500 units at Watana and 3,100 units at Devil Canyon.

If you have any further questions, please call.

Sincerely,

*Dennis Meilhede*

Dennis Meilhede

DM:db

Enclosures

cc: J. Lawrence  
J. Hayden  
T. Gwozdek

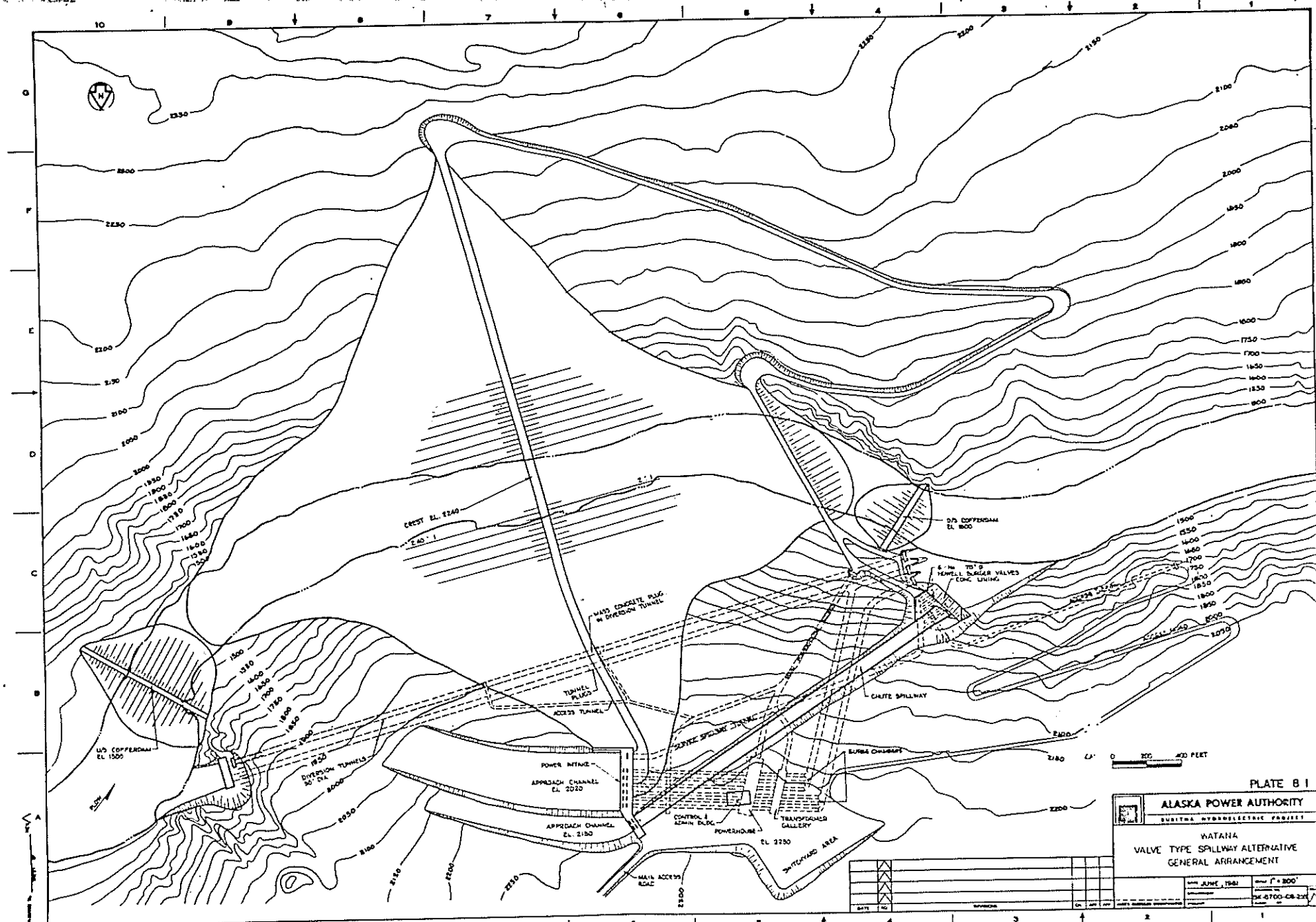
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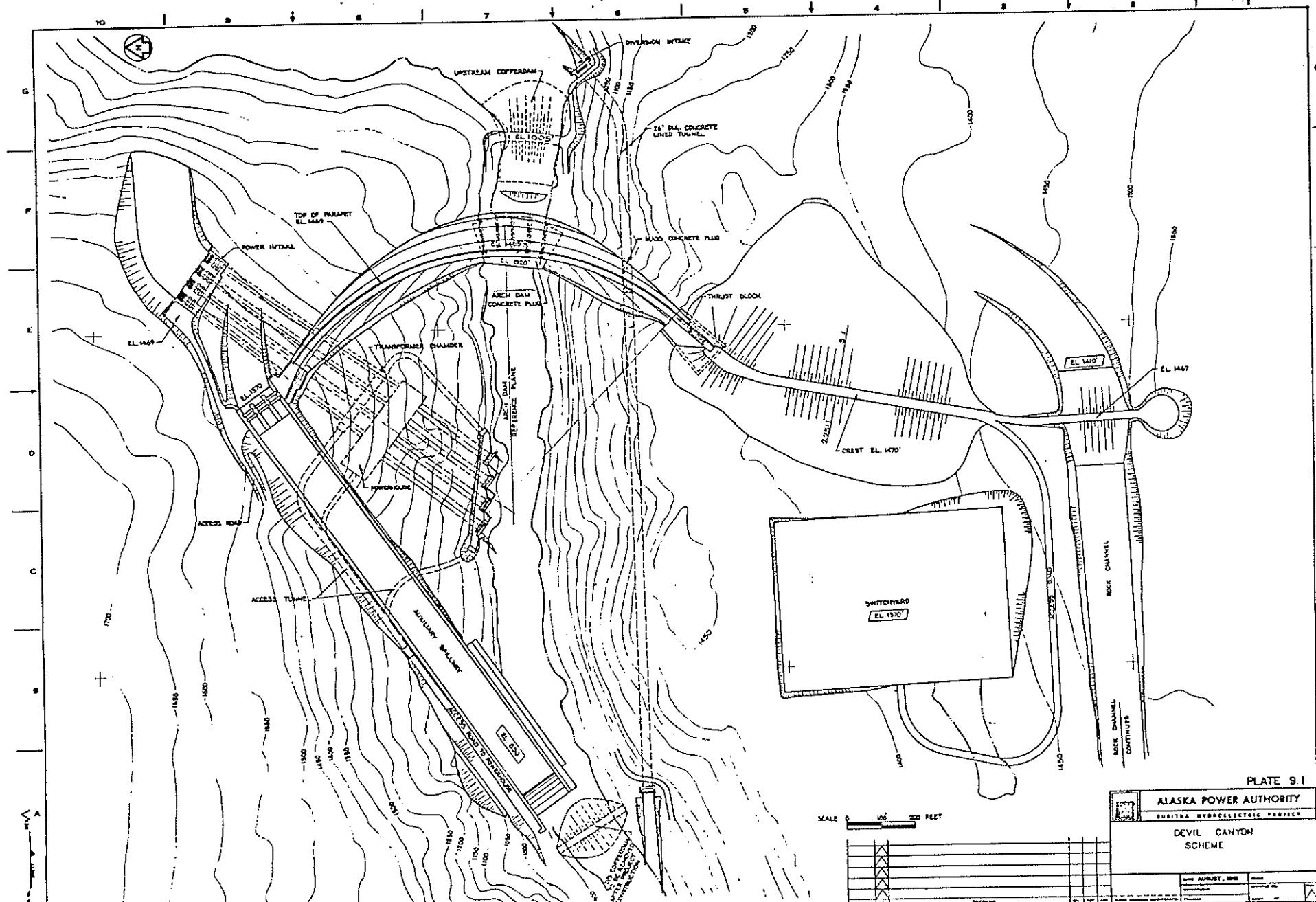
Consulting Engineers

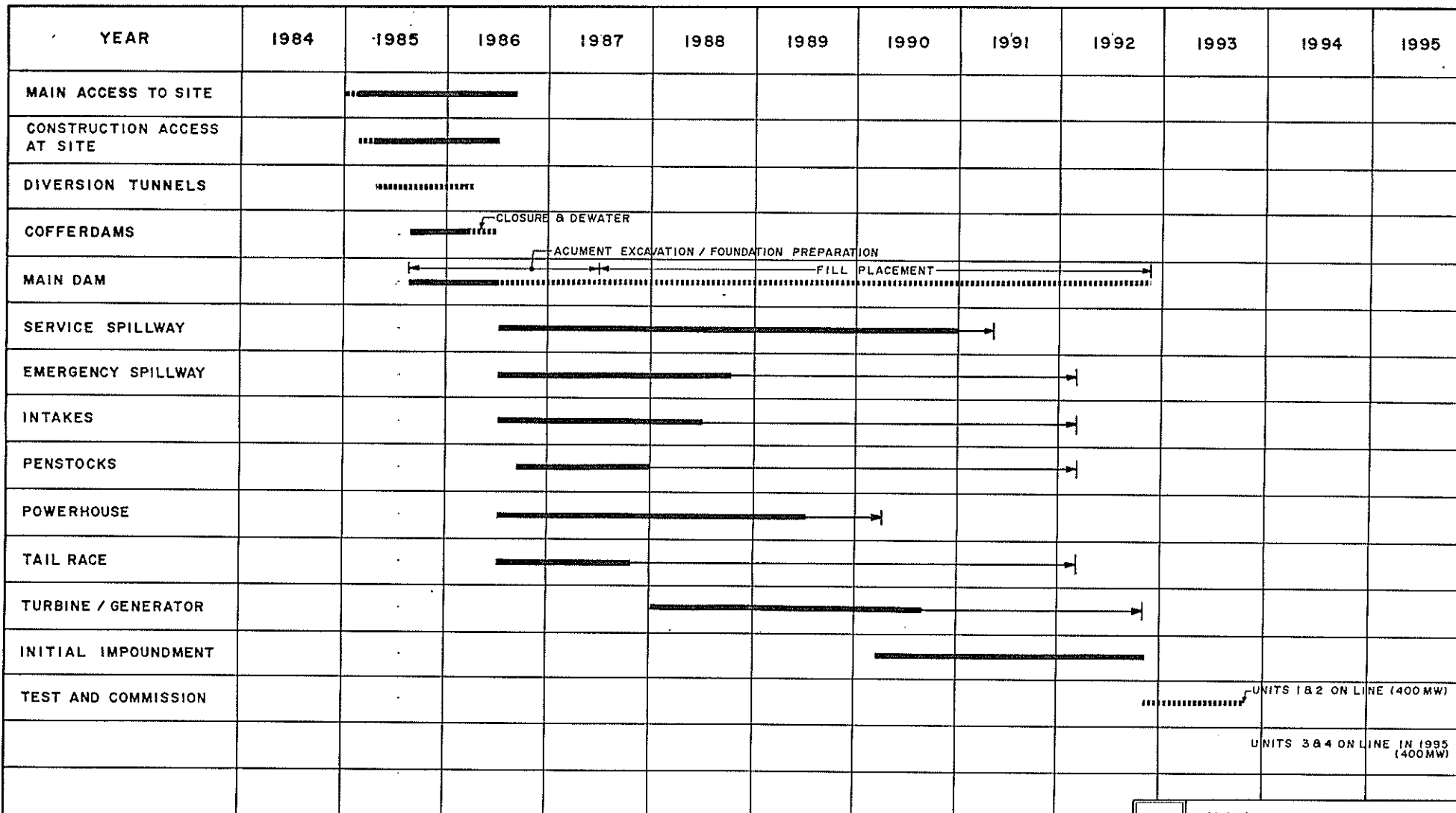
The Liberty Bank Building, Main at Court  
Buffalo, New York 14202

Telephone 716-853-7525

Telex 91-6423 ACRES BUF







**LEGEND**

■■■■■■■■■■ CRITICAL ACTIVITIES  
 ██████████ OTHER ACTIVITIES

SEASONAL LIMITATIONS (400 MW)

**KEY**



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ALASKA POWER AUTHORITY  
SUSITNA HYDROELECTRIC PROJECT

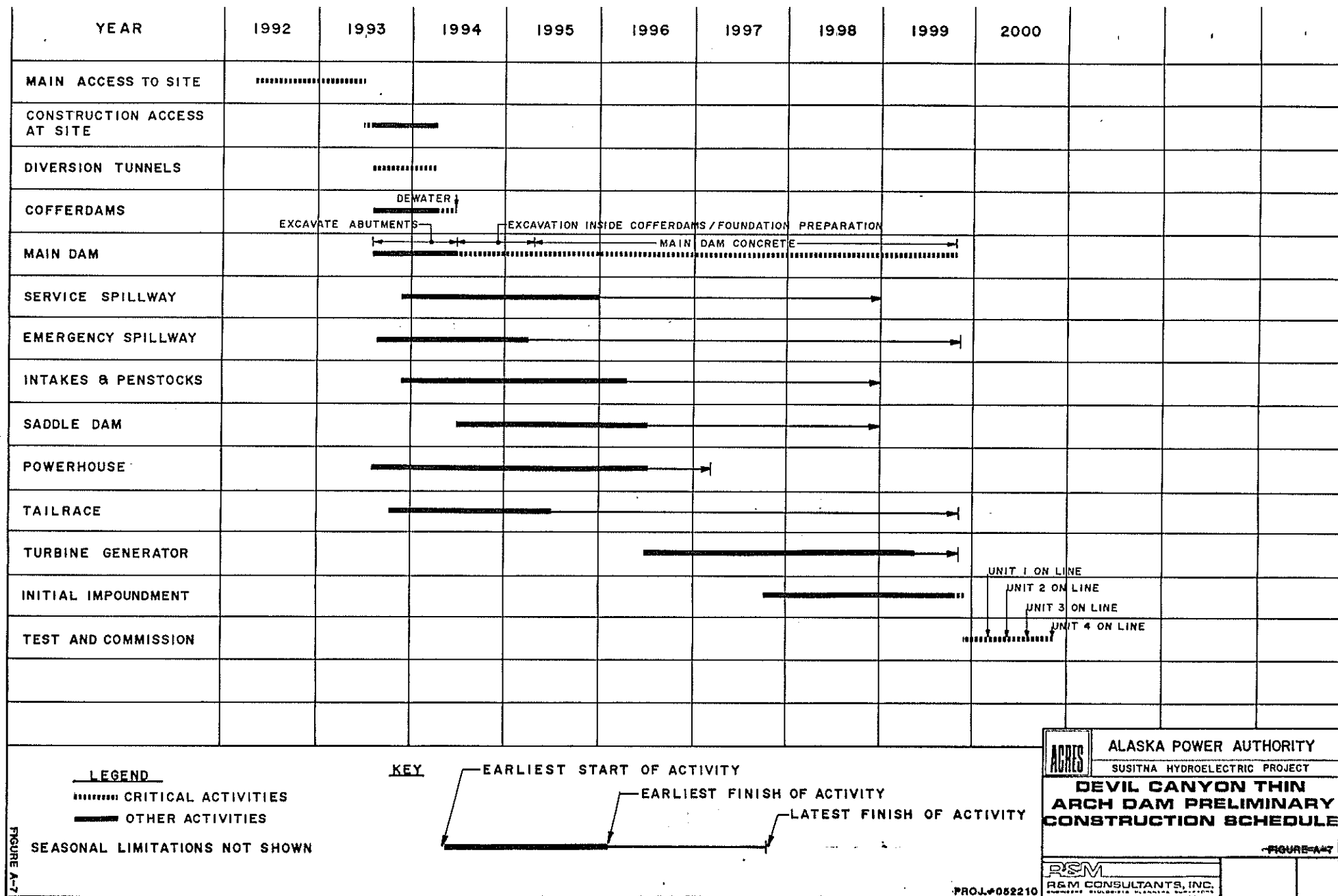
WATANA FILL DAM  
 PRELIMINARY SCHEDULE

RSM

RSM CONSULTANTS, INC.

FIGURE A-8

FIG A-8



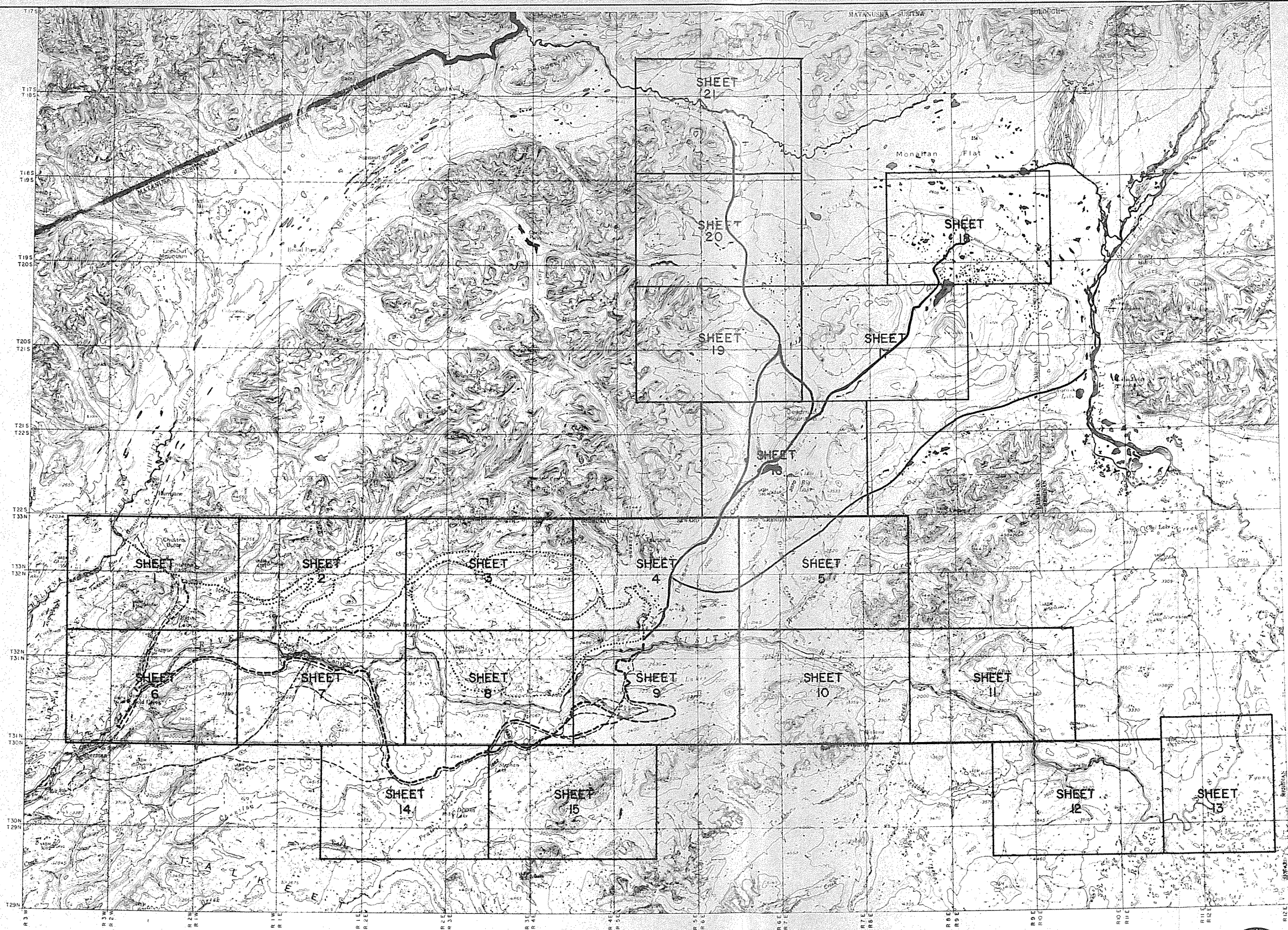


## APPENDIX B

### PROPOSED ALTERNATIVES SEGMENTS

## Appendix B Proposed Alternative Segements

Appendix B consist of a set of map showing each of the alternatives alignment segments studied during the course of the work.

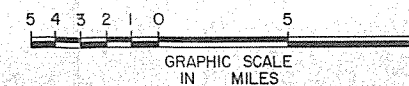


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- CORRIDOR 3 ALTERNATIVES
- RAILROAD CORRIDOR

**NOTE**

SHEETS NO. 1, 5, 10, 11, 12, & 13  
ARE OMITTED. NO ACCESS  
CORRIDORS ARE CONTAINED  
THEREIN.



**R&M CONSULTANTS, INC.**  
ENGINEERS GEOLOGISTS PLANNERS SURVEYORS

PREPARED FOR :  
ACRES AMERICAN, INC.

**INDEX MAP**

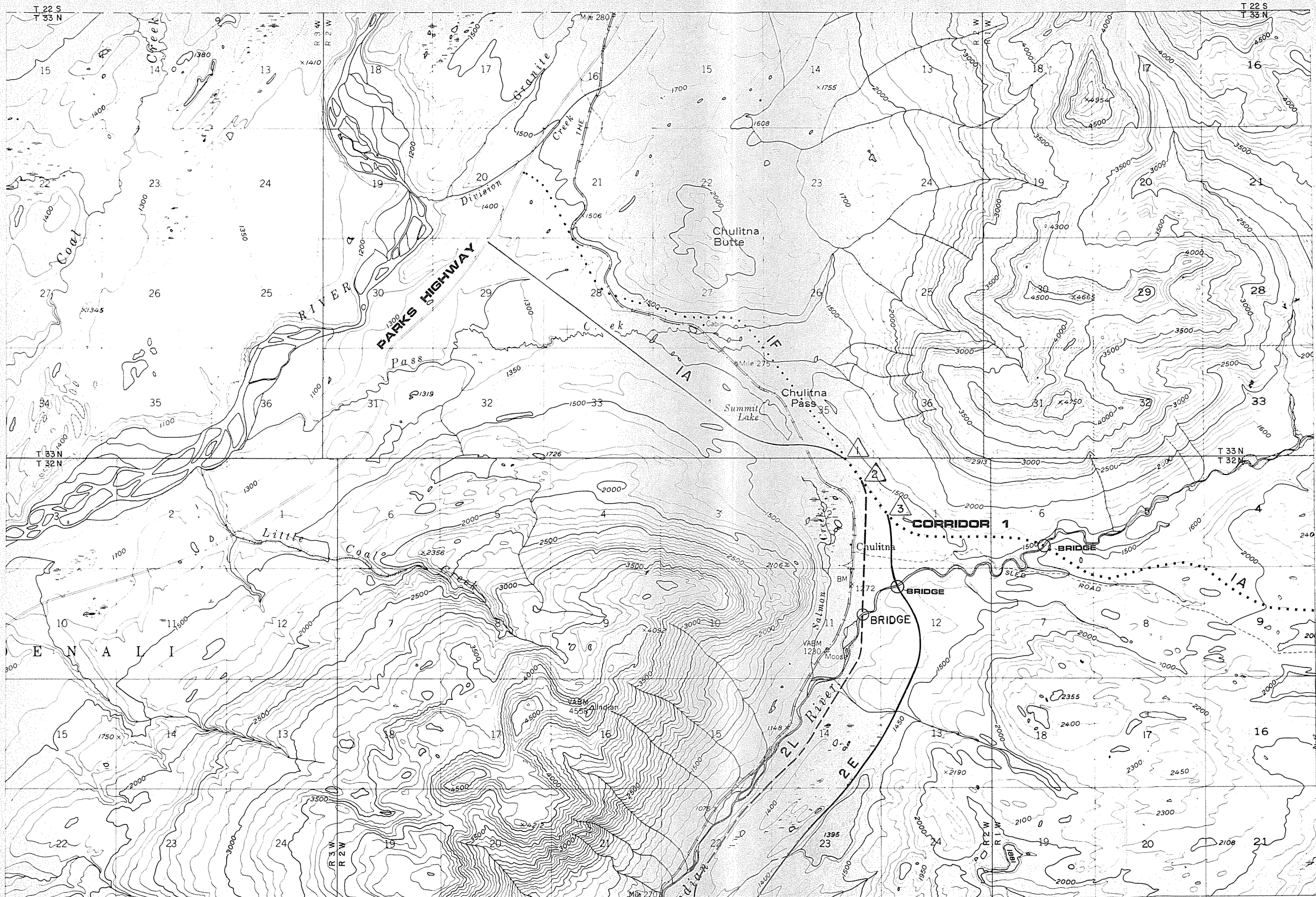
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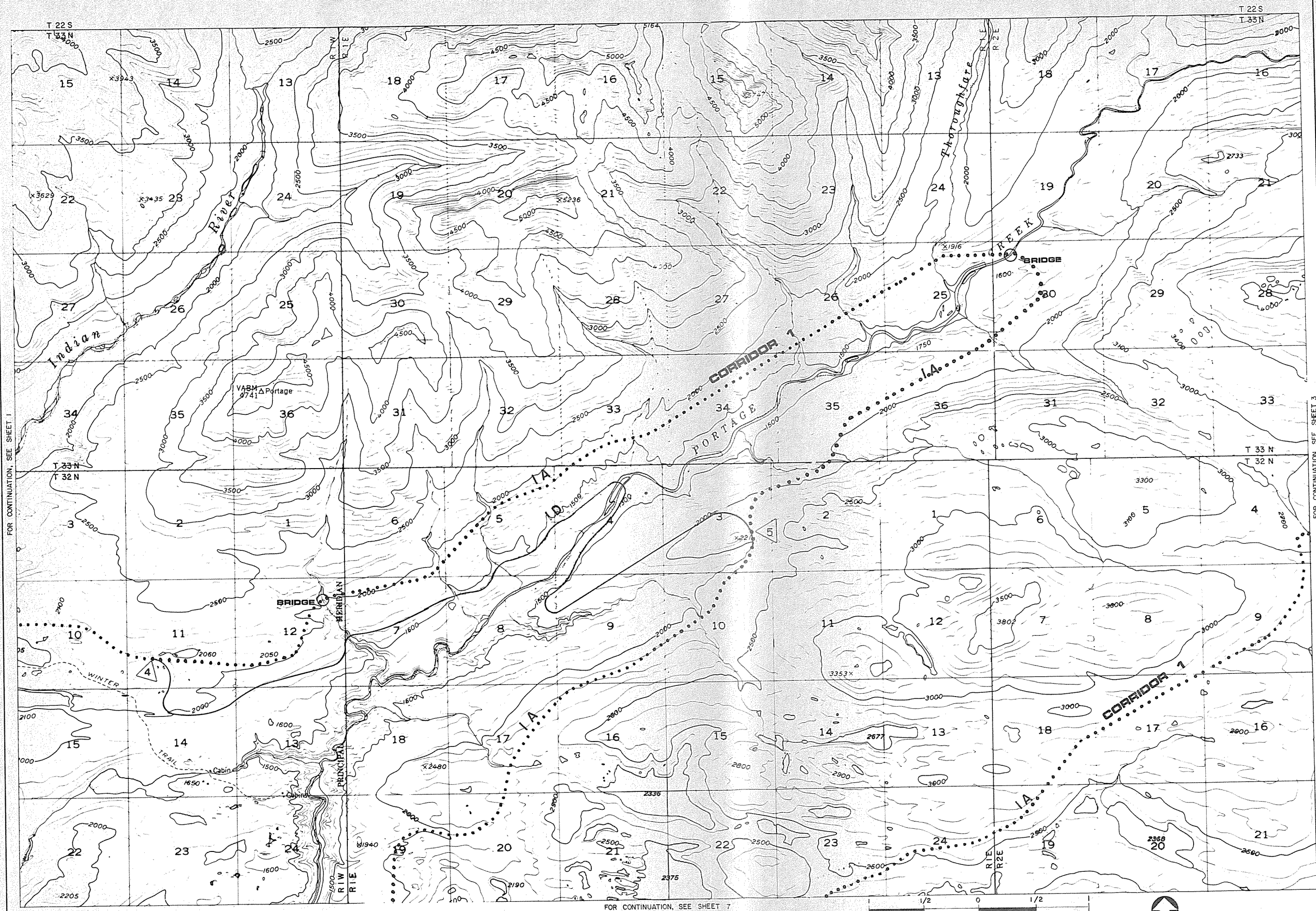
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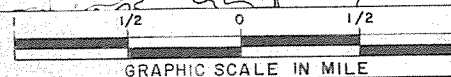
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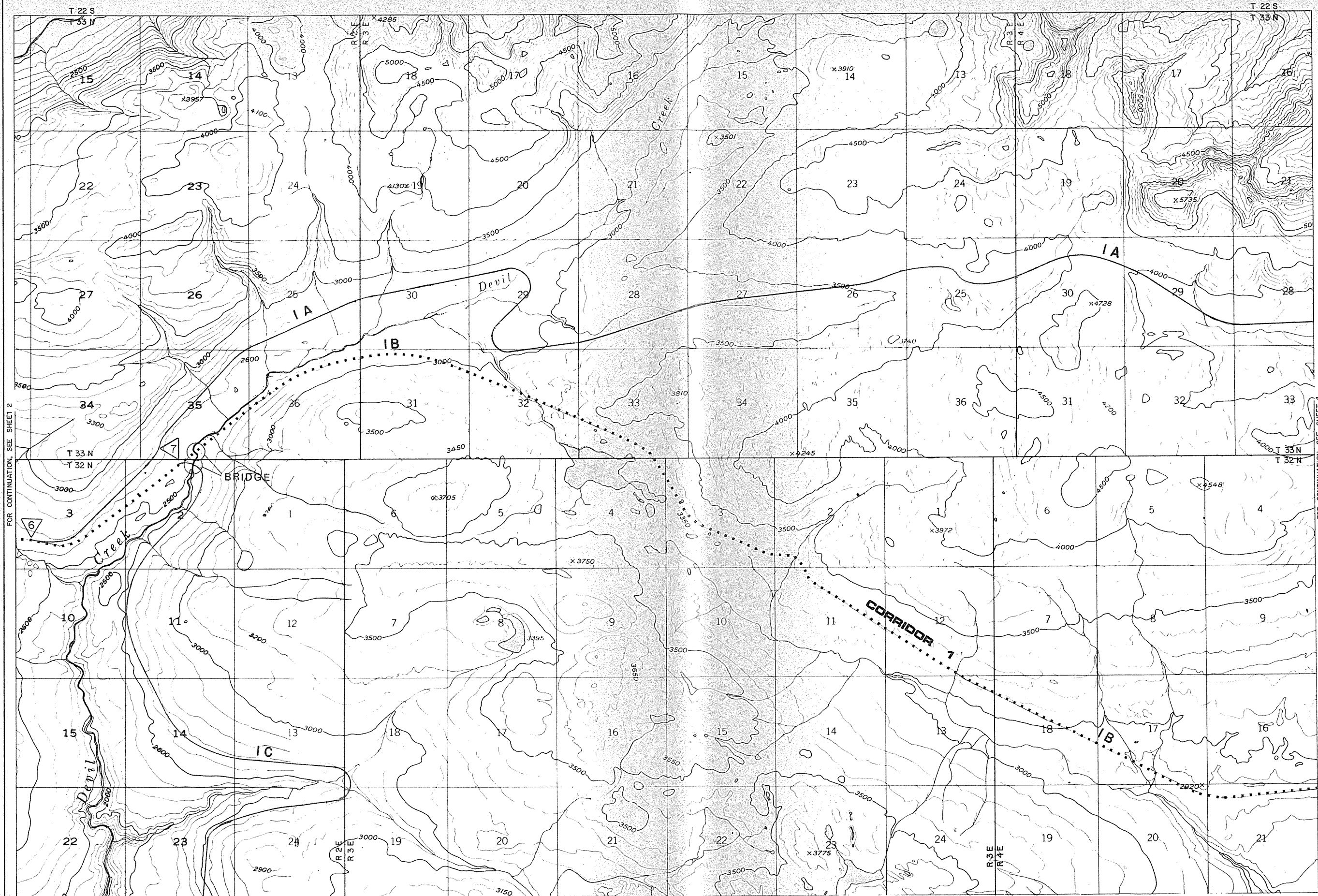
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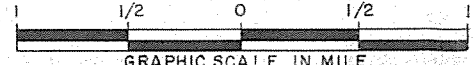




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FOR CONTINUATION, SEE SHEET 8



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**R&M**

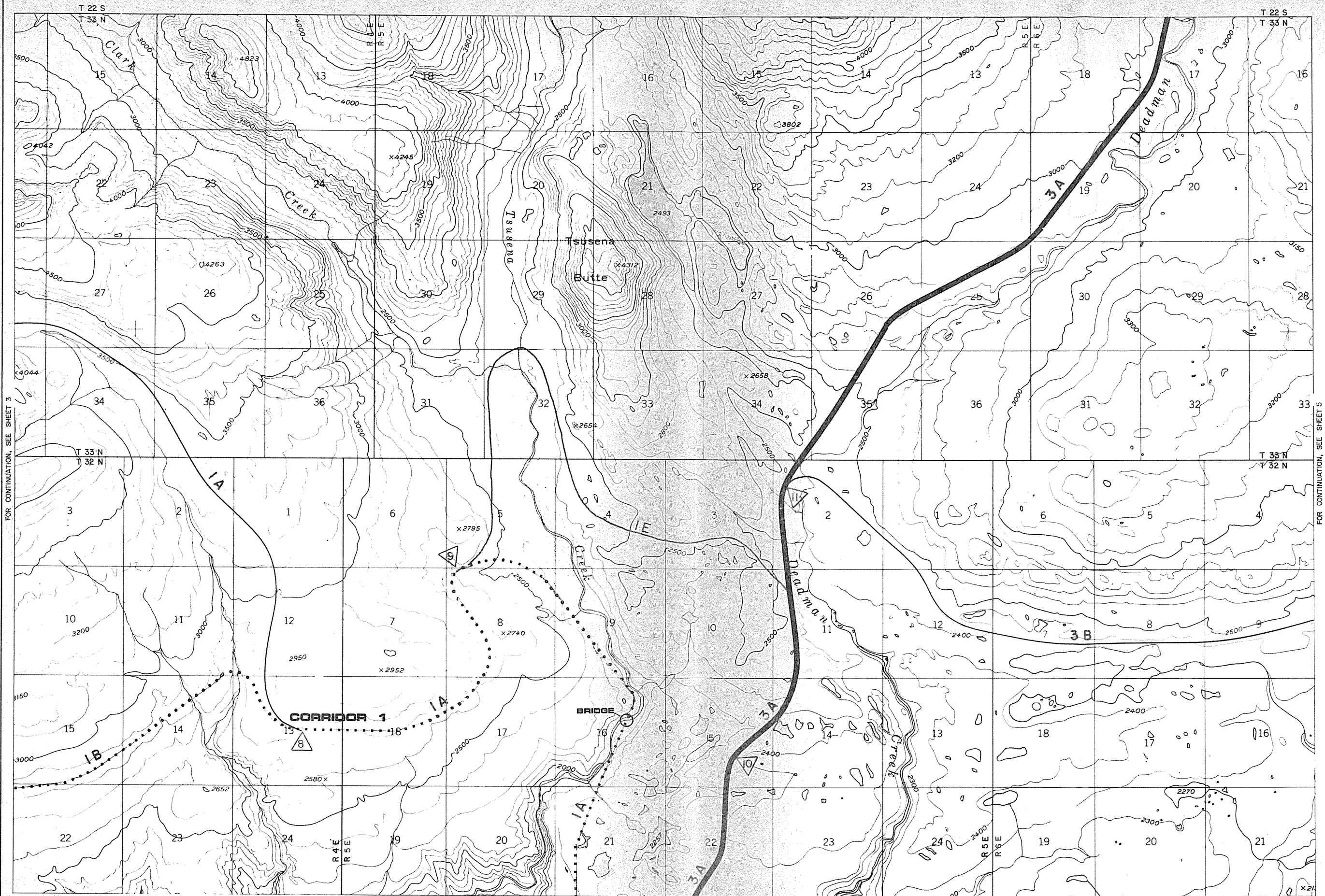
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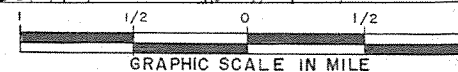
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FOR CONTINUATION, SEE SHEET 5

FOR CONTINUATION, SEE SHEET 9



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SUSITNA HYDROELECTRIC PROJECT

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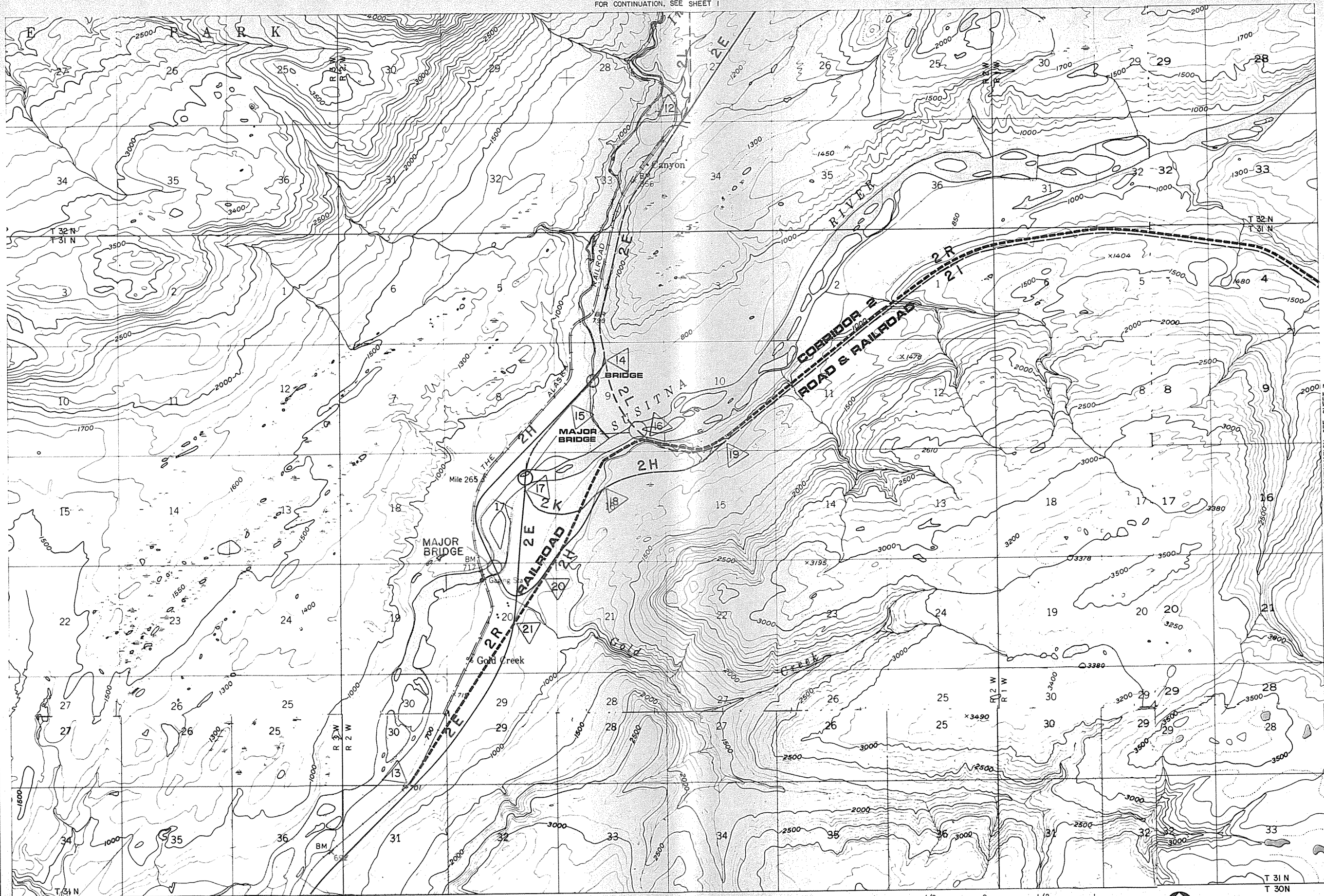
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FOR CONTINUATION, SEE SHEET 1



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SUSITNA HYDROELECTRIC PROJECT

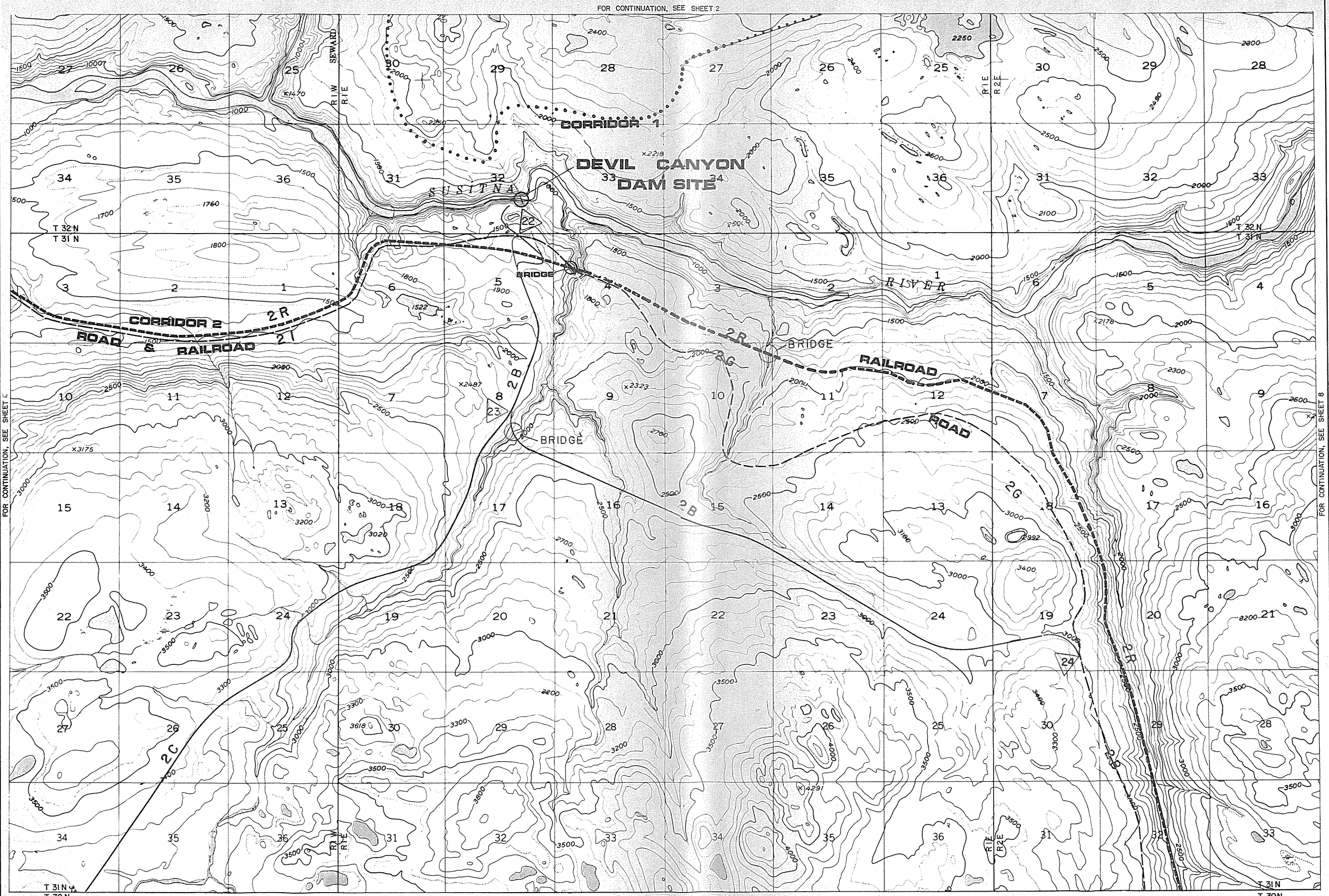
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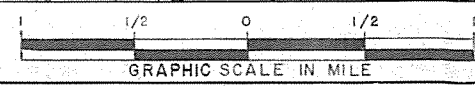


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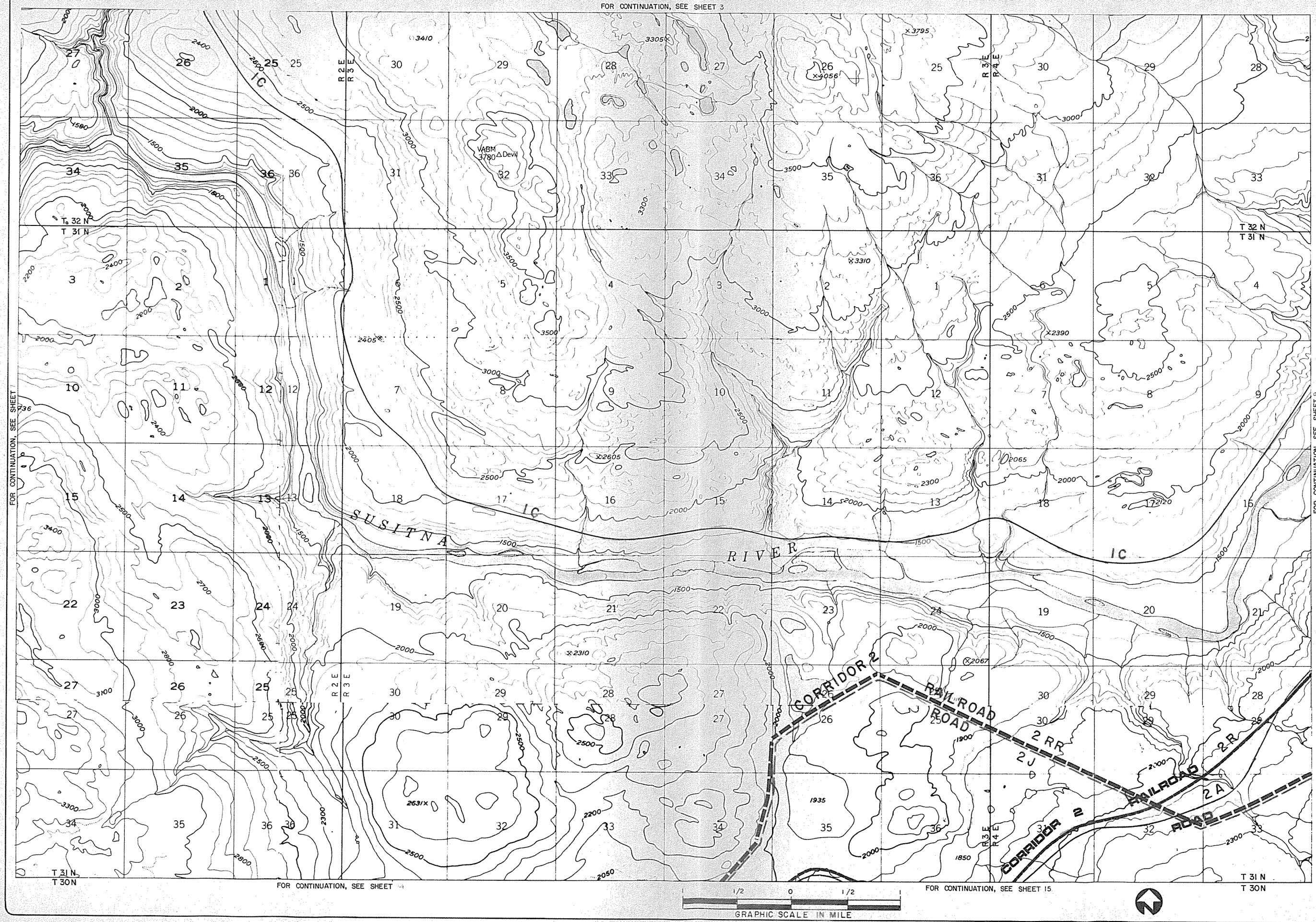
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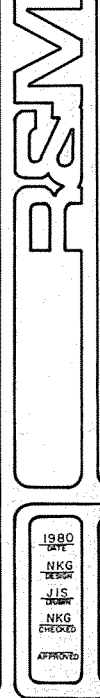


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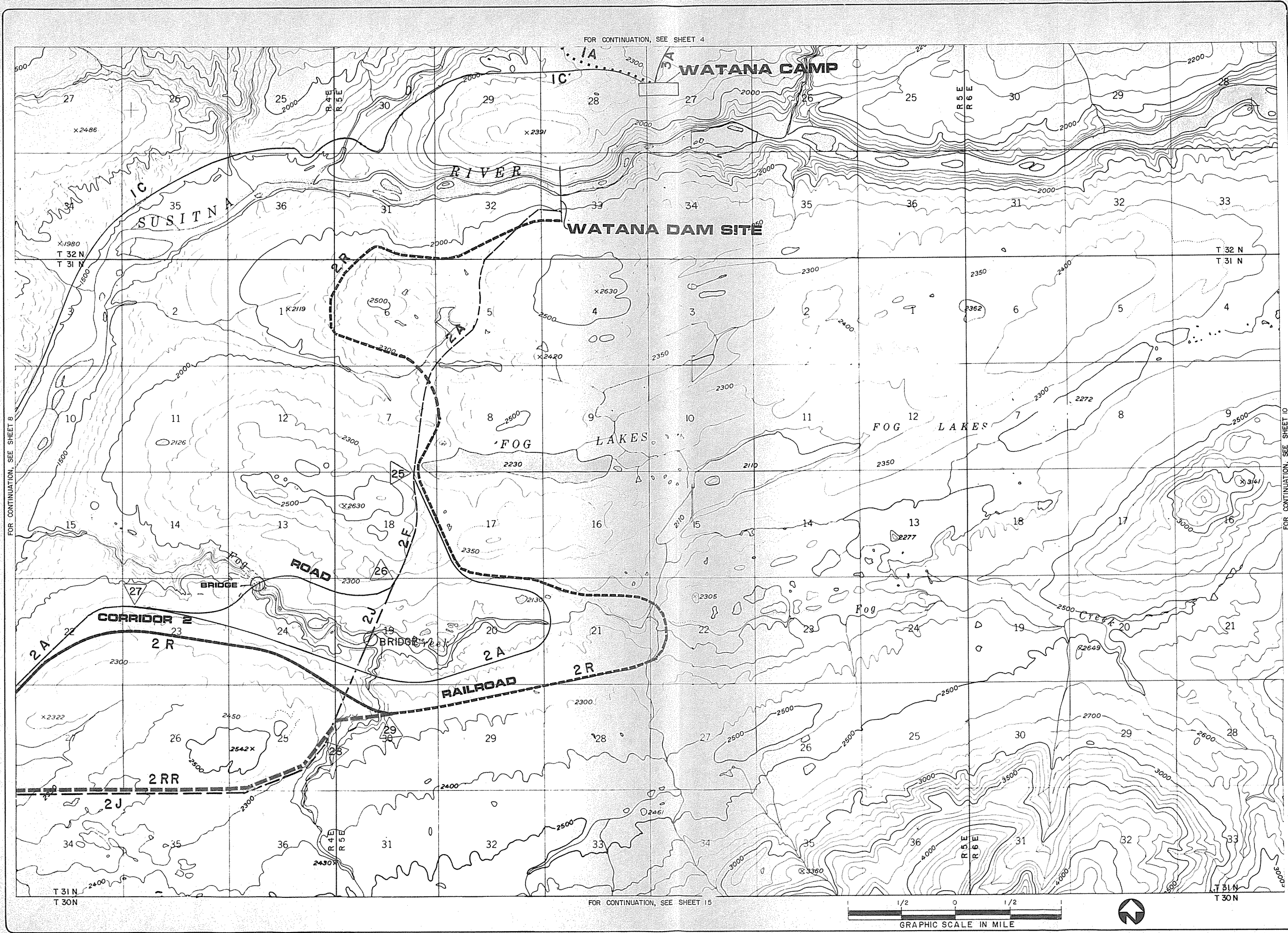
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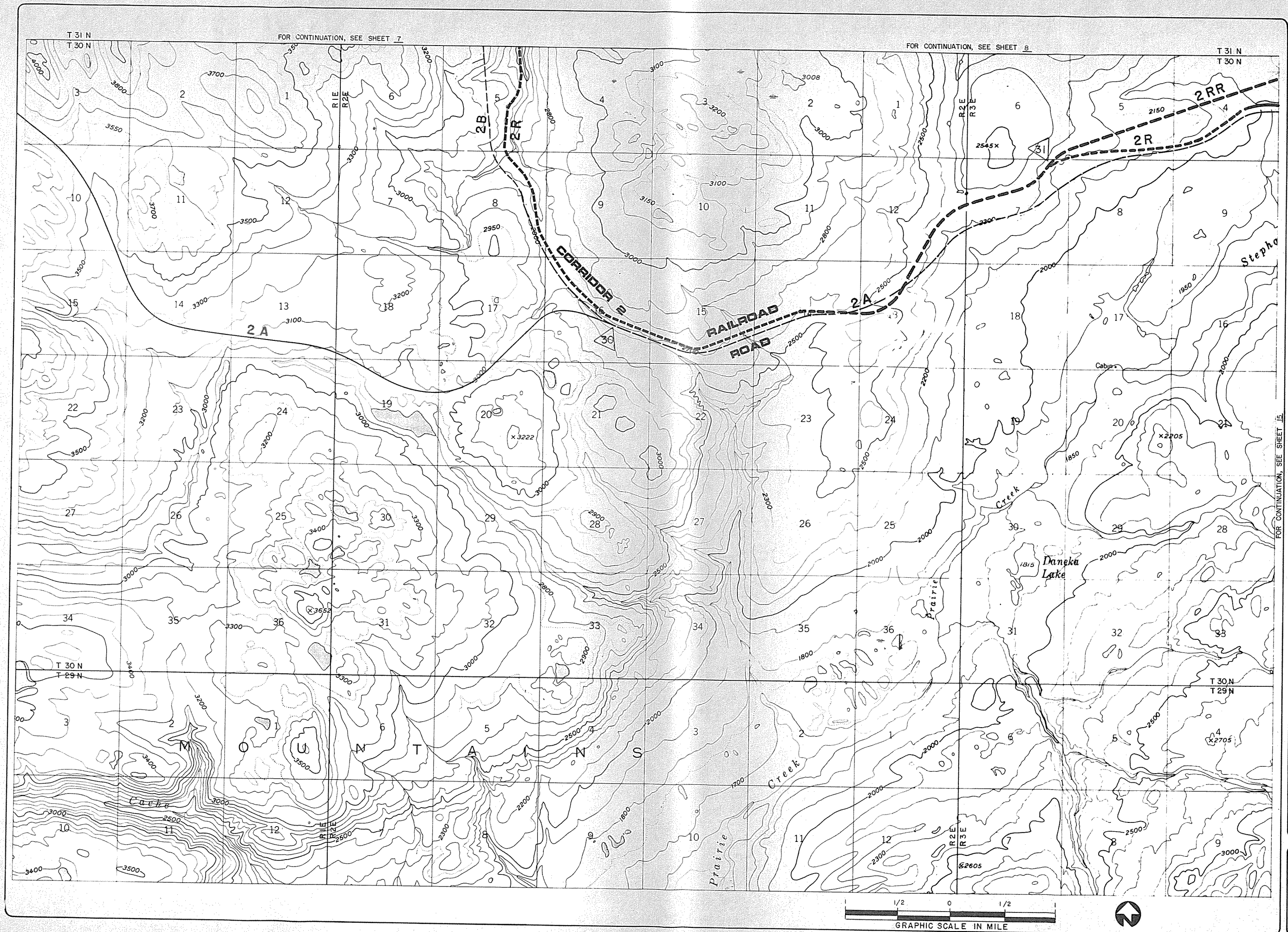
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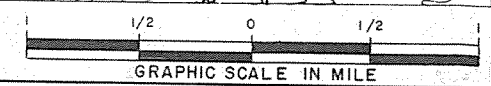
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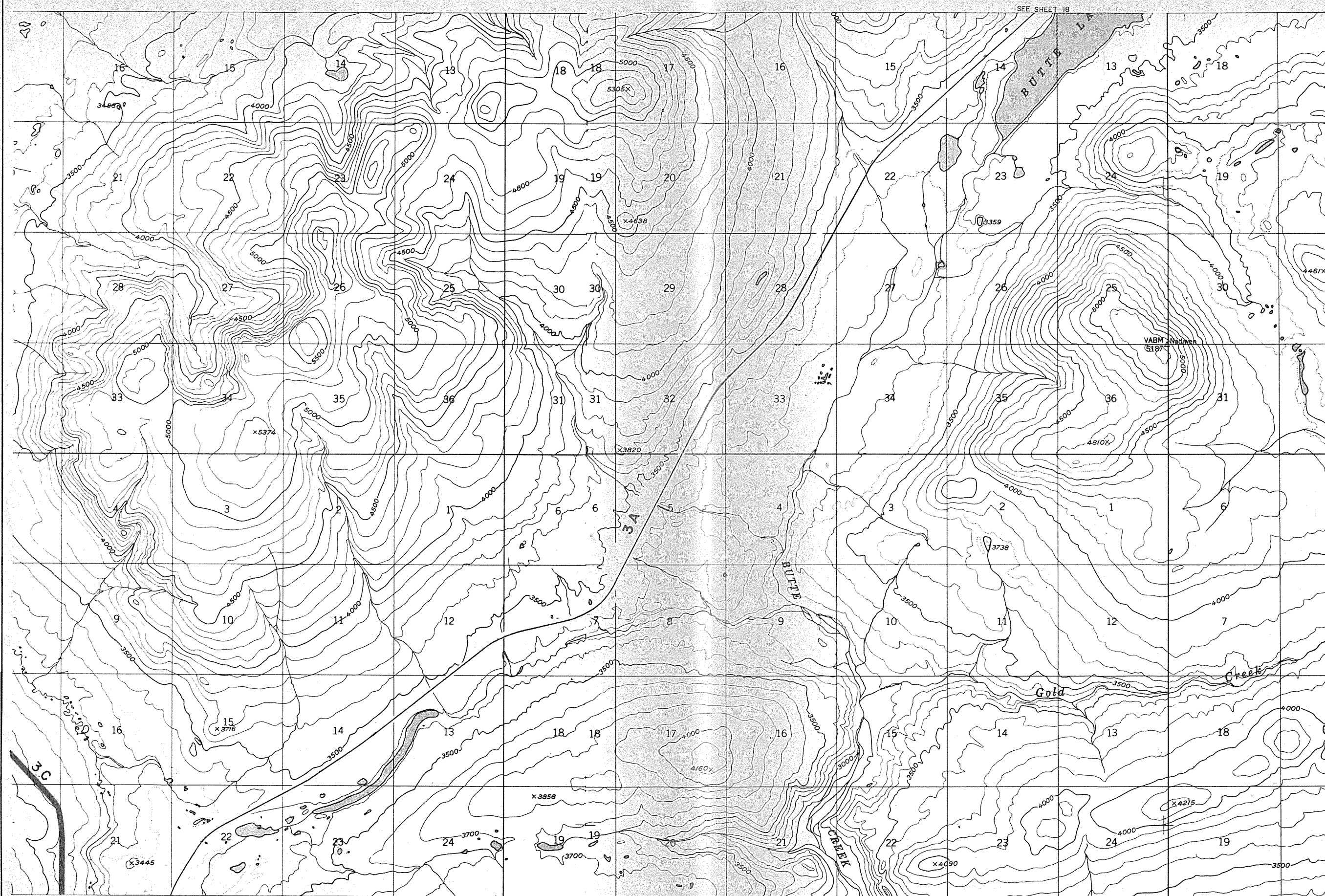








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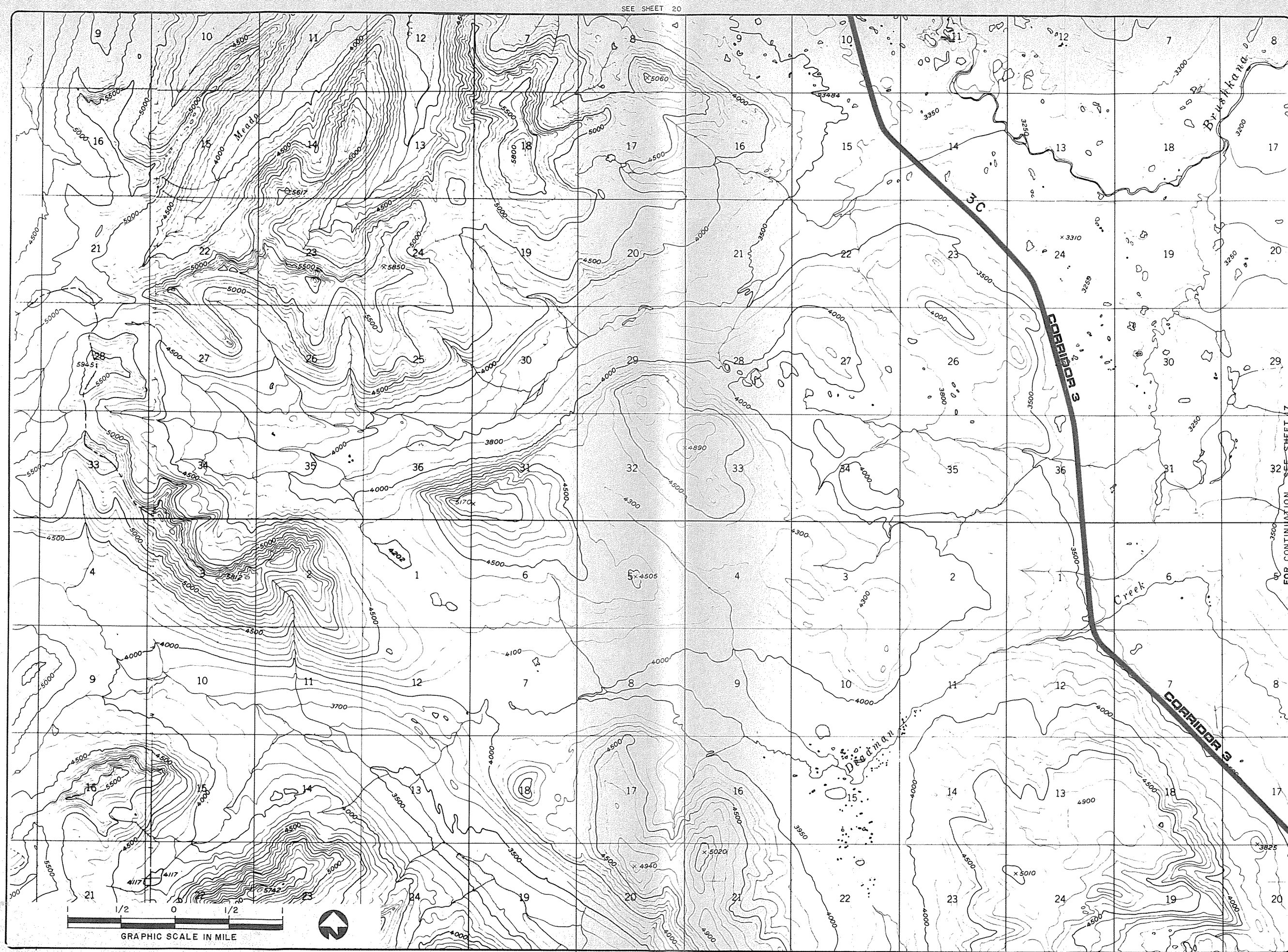
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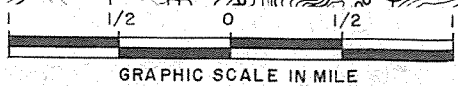







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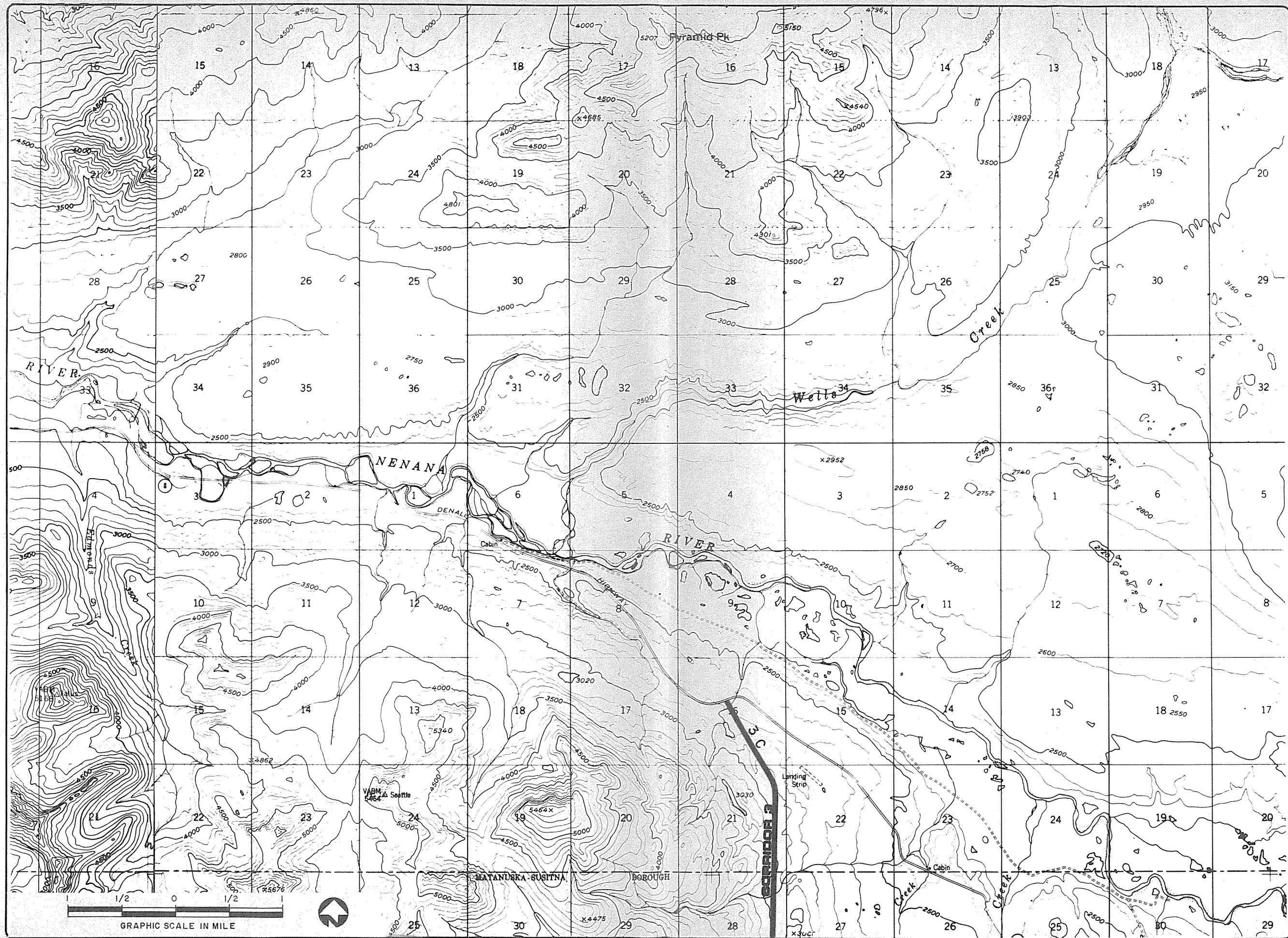
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APPENDIX C

ALTERNATIVE COMPARISON

APPENDIX C  
COMPARISON OF ALTERNATIVE SEGMENTS  
GRADE, CURVATURE AND DISTANCE

Appendix C lists the length, average grade and sum of deflection angles for each segment studied and each potential combination of segments. This tabulation was used to select the combination that make up the preferred alignment within each corridor.

TABLE C.1, Summary of Alignment parameters

	<u>Distance (Miles)</u>	<u>Average Grade %</u>	<u>Sum of Deflections</u>
Segment 1-A	64.7 Miles	2.51%	492° 34'
Segment 1-B	16.2 Miles	1.91%	57° 10'
Segment 1-C	27.5 Miles	2.10%	163° 37'
Segment 1-D	9.0 Miles	4.19%	125° 57'
Segment 1-E	7.5 Miles	3.82%	282° 38'
Segment 1-F	4.1 Miles	2.24%	138° 51'
Segment 2-A	56.7 Miles	2.72%	154° 29'
Segment 2-B	13.6 Miles	3.32%	79° 08'
Segment 2-C	7.5 Miles	5.08%	26° 16'
Segment 2-D	10.7 Miles	3.32%	16° 48'
Segment 2-E	15.6 Miles	2.09%	35° 16'
Segment 2-F	3.9 Miles	2.09%	22° 16'
Segment 2-G	7.7 Miles	4.49%	152° 30'
Segment 2-H	5.4 Miles	1.91%	24° 00'
Segment 2-I	11.4 Miles	1.13%	18° 30'
Segment 2-J	12.2 Miles	3.78%	268° 48'
Segment 2-K	0.9 Miles	5.9%	120° 00'
Segment 2-L	8.7 Miles	2.1%	34° 28'
Segment 3-A	38.5 Miles	1.26%	59° 16'
Segment 3-B	38.5 Miles		
Segment 3-C	23.4 Miles	1.18%	84° 12'

	<u>Distance (Miles)</u>	<u>Average Grade %</u>	<u>Sum of Deflections</u>
Railroad (2-R)	57.7 Miles	1.48%	299° 59'
Railroad 2-RR	13.6 Miles		

## C.2 - Combinations of Alignment Parameters

### North of Susitna River Access Roads (Corridors 1 and 3)

		<u>Distance (Miles)</u>	<u>Average Grade</u>	<u>Defl. Mile</u>	<u>Sum of Deflections</u>
1.	Segment 1-A - Watana Camp to Parks Hwy. N. Jct.	68.6 Mi.	2.51%	7° 10.82'	492° 34.15
2.	Segment 1-A, 1-B - Watana Camp to Parks Hwy.	64.8 Mi.	2.37%	7° 05.66'	460° 17.07
3.	Segment 1-A, 1-C - Watana Camp to Parks Hwy.	68.08 Mi.	2.35%	7° 59.86'	544° 29.10
4.	Segment 1-A, 1-D - Watana Camp to Parks Hwy.	64.27 Mi.	2.70%	8° 29.59'	545° 51.13
5.	Segment 1-A, 1-B, 1-D - Watana Camp to Parks Hwy.	60.55 Mi.	2.58%	8° 28.90'	513° 34.04
6.	Segment 1-A, 1-C, 1-D - Watana Camp to Parks Hwy.	63.75 Mi.	2.54%	9° 22.61'	597° 46.07
7.	Segment 1-A, 3-A - Devil Canyon to Denali Hwy.	77.50 Mi.	1.83%	5° 07.09'	396° 39.52
8.	Segment 1-A, 1-B, 3-A - Devil Canyon to Denali Hwy.	73.16 Mi.	1.67%	4° 56.29'	364° 22.94
9.	Segment 1-A, 1-C, 3-A - Devil Canyon to Denali Hwy.	76.73 Mi.	2.22%	5° 49.63'	448° 34.47
10.	Segment 3-A - Watana Camp to Denali Hwy.	39.09 Mi.	1.26%	1° 30.96'	59° 15.72
11.	Segment 3-B - Watana Camp to Denali Hwy.	41.98 Mi.	1.15%	2° 13.15'	93° 09.49
12.	Segment 1-A, 3-B - Devil Canyon to Denali Hwy.	80.39 Mi.	1.73%	5° 21.36'	430° 33.79
13.	Segment 1-A, 1-B, 3-B - Devil Canyon to Denali Hwy.	76.68 Mi.	1.58%	5° 11.64'	398° 16.71
14.	Segment 1-A, 1-C, 3-B - Devil Canyon to Denali Hwy.	79.86 Mi.	1.59%	6° 02.49'	482° 28.74
34.	Segment 1-A, 1-B, 1-E, 1-F Watana to Park Highway	69.98 Mi.	2.21%	7°09'	538° 24'
36.	Segment 3A, 3C	51. Mi	1.48%	1°24'	49° 18'

South of Susitna River (Corridor 2)

	<u>Distance (Miles)</u>	<u>Average Grade</u>	<u>Defl. Mile</u>	<u>Sum of Deflections</u>
15. Segment 2-A - Watana to Sherman	56.6 Mi.	2.72%	2° 43.77'	154° 29.53
16. Segment 2-A, 2-D - Watana to Parks Hwy.	67.15 Mi.	2.81%	2° 33.05'	171° 17.37
17. Segment 2-A, 2-E, 1-A - Watana to Parks Hwy.	76.51 Mi.	2.52%	2° 33.11'	195° 14.77
18. Segment 2-A, 2-F - Watana to Sherman	54.79 Mi.	2.81%	3° 00.09'	164° 26.93
19. Segment 2-A, 2-F, 2-D - Watana to Parks Hwy.	65.34 Mi.	2.89%	2° 46.43'	181° 14.77
20. Segment 2-A, 2-F, 2-E - Watana To Gold Creek	74.69 Mi.	2.58%	2° 44.84'	205° 12.17
21. Segment 2-A, 2-B, 2-C - Watana to Sherman	59.47 Mi.	3.26%	4° 02.91'	240° 45.96
22. Segment 2-A, 2-F, 2-B, 2-C - Watana to Sherman	57.66 Mi.	3.36%	3° 57.73'	228° 27.48
23. Segment 2-A, 2-B, 2-C, 2-D - Watana to Parks Hwy.	70.02 Mi.	3.85%	3° 40.71'	257° 33.80
24. Segment 2-A, 2-F, 2-B, 2-C, 2-E, 1-A - Watana to Parks Hwy.	77.56 Mi.	3.00%	3° 28.26'	269° 12.72
25. Segment 2-A, 2-B, 2-G, 2-I, 2-H - Watana to Gold Creek	51.66 Mi.	2.38%	5° 32.25'	286° 04.2'
26. Segment 2-A, 2-B, 2-G, 2-I, 2-H, 2-E, 2-D - Watana to Parks Hwy.	68.50 Mi.	2.09%	4° 04.18'	278° 46.48
27. Segment 2-A, 2-B, 2-G, 2-I, 2-H, 2-E, 1-A - Watana to Parks Hwy. N. Jct.	68.25 Mi.	2.17%	4° 36.27'	314° 15.28



South of Susitna River (Corridor 2)  
(Continued)

		<u>Distance (Miles)</u>	<u>Average Grade</u>	<u>Defl. Mile</u>	<u>Sum of Deflections</u>
28.	Railroad 2-R, Watana to Gold Creek	58.01 Mi.	1.48%	5° 10.27'	299° 58.86'
29.	Segment 2-A, 2-B, 2-C, 2-E, Watana to Parks Hwy.	79.37 Mi.	2.93%	3° 32.82'	281° 31.2'
30.	Segment 2-A, 2-F, 2-B, 2-G, 2-D - Watana to Parks Hwy. S. Jct.	68.21 Mi.	3.35%	3° 35.74'	245° 15.32'
31.	Segment 2-A, 2-F, 2-B, 2-G, 2-I, 2-H - Watana to Gold Creek	49.23 Mi.	2.33%	5° 56.30'	296° 1.6'
32.	Segment 2-A, 2-F, 2-B, 2-G, 2-I, 2-H, 2-E, 2-D - Watana to Parks Hwy. S. Jct.	66.69 Mi.	2.41%	4° 54.59'	327° 26.39'
33.	Segment 2-A, 2-F, 2-B, 2-G, 2-I, 2-H, 2-E, 2-I Watana to Parks Hwy.	66.44 Mi.	2.22%	4° 50.79'	324° 12.18'
35.	Segment 1-F, 2-L, 2-I 2-G, 2-B, 2-A, 2-J	68.5 Mi.	2.10%	4° 06'	284° 58'

Combinations beyond these include a variety of segments that are minor adjustments and do not significantly impact length grade or curvature.

The Combinations selected for each corridor are:

Corridor 1	Combination 34
Corridor 2	Combination 35
Corridor 3	Combination 36

APPENDIX D

TERRAIN UNIT MAPPING



#### Appendix D - Terrain Unit Maps

This appendix includes the terrain unit analysis for the access alternatives.

This data identifies the surface geology and tabulates the engineering characteristics of the various soils. The alternative segments studied are plotted on the Terrain Unit Maps. The soil types and characteristics have been taken into account in developing the construction cost estimates for the alternate plans.

TERRAIN UNIT PROPERTIES AND ENGINEERING INTERPRETATION

TERRAIN UNIT SYMBOL	TERRAIN UNIT NAME	TOPOGRAPHY AND AREAL INTERPRETATION	SOIL STRATIGRAPHY	SLOPE CLASSIFICATION	PROBABLE UNIFIED SOIL TYPES	DRAINAGE AND PERMEABILITY IN UNFROZEN SOILS	EROSION POTENTIAL	GROUND WATER TABLE	PROBABLE PERMAFROST DISTRIBUTION	FROST HEAVE POTENTIAL	THAW SETTLEMENT POTENTIAL	BEARING STRENGTH	SLOPE STABILITY	SUITABILITY AS SOURCE OF BORROW
Bxu	Unweathered, consolidated bedrock	Cliffs in river canyon, rounded knobs on broad valley floor and mountain peaks.		Moderate to Near-Vertical	-	-	Low	Deep		Nil	Nil	Very High	Moderate to High	Fine - Poor Coarse - Good
C	Colluvial deposits	Prodominantly found at the base of steeper bedrock slopes as coalescing cones and fans and rock glaciers.	Angular frost cracked, blocks of rock, some silt and sand.	Moderate to Steep	GP, GW, GM, SW, SM	Good/High	Moderate to High	Deep	Sporadic at Low Elevation. Discontinuous at High Elevations	Low to High	Low to Moderate	Low to Moderate	Low to Moderate	Fine - Poor Coarse - Variable
Cl	Landslide deposits	Hummocky unconsolidated deposits most common along the Susitna River and its major tributaries	Silty gravels, silty sands and sandy silts; possible crude contorted layers.	Moderate to Steep	GM, SM, ML	Poor/Low	High	Shallow (perched)	Active - Unfrozen Inactive - Frozen	High	High where Frozen	Low	Low	Poor
Cs-f	Solifluction deposits	Relatively smooth to lobate topography created by the flow of materials subjected to frequent freeze/thaw cycles.	Silty sand and sandy silt showing contorted layering.	Gently to Steeping Sloping	SW, SM, ML	Frozen	High	Shallow (perched)	Continuous	High	High	High	Low	Poor
Ffg	Granular alluvial fan	Low cone shaped deposits formed where high gradient streams flow onto flat surfaces.	Rounded cobbles and gravel with sand and some silt, some sorting and layering of materials.	Moderate	GW, SW	Good/High	Moderate	Shallow	Unfrozen	Low	Low	High	High	Fine - Poor Coarse - Good
Fp	Floodplain deposits	Flat plains, slightly above and adjacent to the present Susitna River and its major tributaries.	Rounded cobbles, gravel and sand sorted and layered, with or without silt cover.	Flat to Gentle	GW, GP, SW, SP, SM	Good/High	High	Very Shallow	Unfrozen	Generally Low, High for Surface Cover	Low	Surficial Silts Low. Sands and Gravels High	High	Fine - Poor Coarse - Good.
Fpt	Terrace	Flat surface remnants of former floodplain deposits isolated above present floodplain.	Rounded cobbles, gravel and sand with some silt covered by a thin silt layers. Sorted and layered.	Flat to Gentle	GW, GP, SW, SP, SM, ML	Good/High	Low	Deep	Unfrozen	Generally Low, High for Surface Cover	Low	High	Low to Moderate	Fine - Poor Coarse - Good
GfO	Outwash deposits	Bottoms of U-shaped tributary valleys and adjacent to Susitna area.	Rounded & striated cobbles, gravel, and sand, crudely sorted and layered.	Gentle	GW, SW	Good/High	Moderate	Shallow to Deep	Unfrozen	Low	Low	High	Low to High	Fine - Poor Coarse - Excellent
GFe	Esker deposits	Rounded to sharp crested sinuous ridges in upper Susitna area.	Rounded & striated cobbles, gravel, and sand. Crudely to well sorted and layered.	Steep Local Slopes	GW, SW	Good/High	Moderate	Deep	Unfrozen	Low	Low	High	Moderate	Fine - Poor Coarse - Excellent
GfK	Kame deposits	Rounded to sharp-crested, Hummocky hills.	Rounded & striated cobbles, gravel, and sand. Crudely sorted and layered.	Steep Local Slopes	GW, SW	Good/High	Moderate	Deep	Unfrozen	Low	Low	High	Moderate	Fine - Poor Coarse - Excellent
Gta	Ablation till	Tributary valley side walls and valley bottoms in general, between Tsusena and Deadman Creek Hummocky rolling surface, numerous channels.	Rounded and striated cobbles, gravel and sand, no sorting or layering. Boulder-cobble lag covering surface.	Gentle to Steep	GW, GM, SW, SM	Moderate/Moderate	Moderate	Shallow to Moderately deep	Unfrozen to Sporadic	Low to Moderate	Low to Moderate	Moderate to High	Moderate	Fine - Poor Coarse - Fair
Gtb-f	Basal till (frozen)	Bottoms of larger U-shaped valleys and adjacent gentle slopes.	Gravelly silty sand and gravelly sandy silt; no layering or sorting; cobbles and boulders poorly rounded and striated.	Gentle to Steep	GM, SM, ML	Frozen	Moderate	Shallow (perched)	Continuous	High	High	Low if Thawed. High when Frozen	Low	Fine - Poor Coarse - Poor
O	Organic deposits	In swales between small rises on lowlands and in high elevation bedrock areas. Flat surface to steplike terraces.	Decomposed and undecomposed organic material with some silt.	Flat	Pt, OL	Poor/Moderate to High	Low	At Surface	Discontinuous Overlies Continuous	High	High	Very low	Low	Nil
L-f	Lacustrines (frozen)	Lowlands (below 3000') flat surface in the Tyone - Oshetna River area.	Sandy silt and silty sand with occasional pebbles, sorted and layered.	Gentle	SP, SW, ML	Frozen	High	Shallow (perched)	Continuous	High	High	Low if Thawed. High when Frozen	Low	Poor
<u>L</u> Gta-f	Lacustrine sediments over ablation till	Gently rolling to hummocky surface surrounding Butte Lake	Stratified sandy silt and silty sand over unsorted silty sandy gravel.	Gentle to Moderate	SP, SW, ML GW, GM, SW, SM	Frozen	Moderate	Shallow (perched)	Continuous	Moderate to High	Moderate to High	Low if Thawed. High when Frozen	Low	Fine - Poor Coarse - Fair
<u>L</u> Gtb-f	Lacustrine deposits over basal till	Lowlands, (below 3000') between Stephan Lake and Watana Creek, and extending upstream past the Tyone River.	Well sorted silty sand and sandy silt overlying basal till.	Gentle to Moderate	SP, SW, ML, GM, SM, ML	Lacustrine-Good/Good Basal Till-Frozen	Lacustrine-High Basal Till-Moderate	Moderately deep	L - Discontinuous Gtb-f - Continuous	High	High	Low when Thawed. High when Frozen	Low	Poor
Cs-f Gtb-f	Solifluction deposits (frozen) over basal till (frozen)	Smooth to lobate steplike topography on gentle slopes above the proglacial lake level, west of Tsusena Creek.	Unsorted gravels, sands, & silts with thin ice layers, contorted soil layering.	Moderate to Steep	GM, SM, ML	Frozen	Moderate	Shallow (perched)	Continuous	High	High	Low when Thawed. High when Frozen	Low	Poor
Cs-f Gta	Solifluction deposits (frozen) over ablation till	Smooth to lobate and hummocky topography along Deadman Creek.	Silty, sandy, gravel and silty gravelly sand showing contorted layering.	Moderate to Steep	GW, GM, SW, SM	Frozen	Moderate	Shallow (perched)	Continuous	High	High	Low if Thawed. High when Frozen	Low	Poor
Cs-f Fpt	Solifluction deposits (frozen) over terrace sediments	Smooth to lobate flows of frozen fine grained materials, found on terrace of the Susitna, frequent between the Tyone and Oshetna Rivers.	Silty, sand and sandy silt showing contorted layering over gentle sorted and layered rounded cobbles, gravel and sand.	Gentle	SW, SM, ML GW, GP, SW, SP, SM, ML	Frozen	Moderate	Shallow (perched)	Continuous	High	High	High when Frozen. Low when Thawed.	Low	Fine - Poor Coarse - Fair
Cs-f Bxu	Solifluction deposits (frozen) over bedrock	Smooth to lobate steplike topography on the flanks of some mountains, north and south of the Devil Canyon area.	Mixed gravels sands and silts with thin ice layers and faint contorted soil layering over bedrock	Moderate to Steep	GW, GM, SW, SM, ML Bedrock	Frozen	High	Shallow (perched)	Continuous	High	High	High	Low	Poor
Gtb-f Bxu	Frozen basal till over bedrock	Rolling lowland areas and moderate to steeply sloping river canyon walls. Transitional to high mountains areas.	Gravels, silty sand and sandy silt with no layering or sorting, overlying bedrock.	Moderate to Steep	SP, SM, ML Bedrock	Frozen	Moderate	Shallow (perched)	Continuous	High	High	Low if Thawed. High when Frozen	Low	Poor
Gta Bxu	Ablation till over un-weathered bedrock	Hummocky rolling surface transitional to higher mountains adjacent to Deadman Creek.	Rounded and striated cobbles, gravel and sand, no sorting or layering, over bedrock.	Gentle to Steep	GW, GM, SW, SM Bedrock	Good/High	Moderate	Shallow to Moderately deep	Discontinuous	Low to Moderate	Low to Moderate	Low if Thawed. High when Frozen	Moderate	Fine - Poor Coarse - Fair
C Bxu+Bxu	Colluvium over bedrock and bedrock exposures	Higher elevation mountain areas and steep slopes along the Susitna River and its major tributaries.	Angular blocks of rock with some sand and silt overlying bedrock.	Steep to Near-Vertical	GP, GW, GM, SW, SM Bedrock	Good/Low to High	Moderate to High	Deep	Sporadic	Low to High	Low to Moderate	Low to Very High	Moderate to High	Fine - Poor Coarse - Fair
C Bxw	Colluvium over weathered, poorly consolidated bedrock	Small cliffs cut into tertiary non-marine sediments along Watana Creek, and tertiary volcanics in Fog Creek.	Angular rubble with silt and sand over poorly consolidated or highly weathered bedrock.	Steep to Near-Vertical	GW, GM, SW SM, ML	Good/Low to Moderate	Moderate	Deep	Continuous	Low to High	Low to Moderate	Low to Moderate	Moderate	Fine - Poor Coarse - Poor

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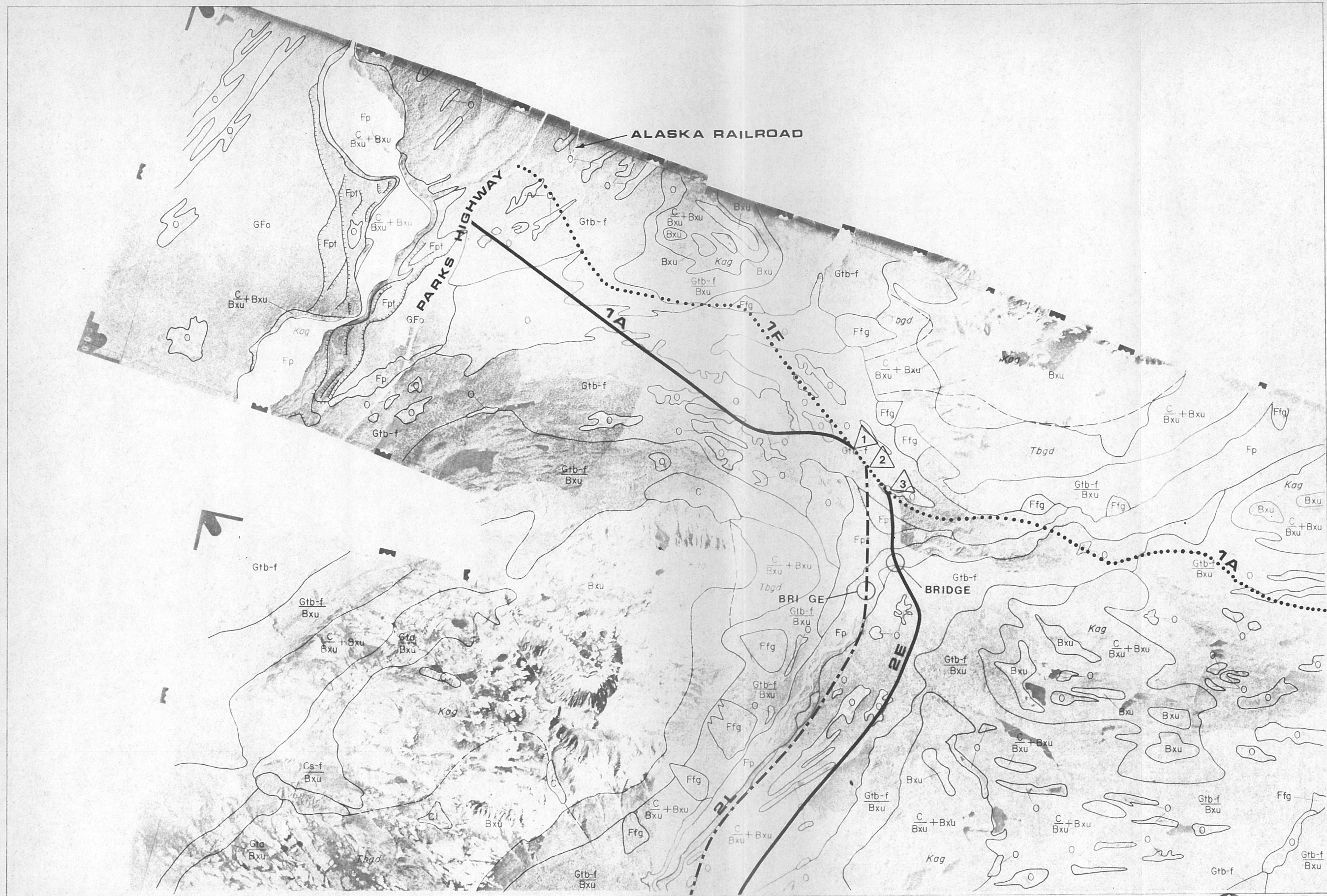
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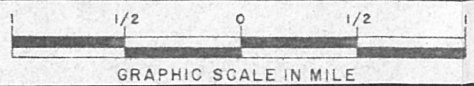




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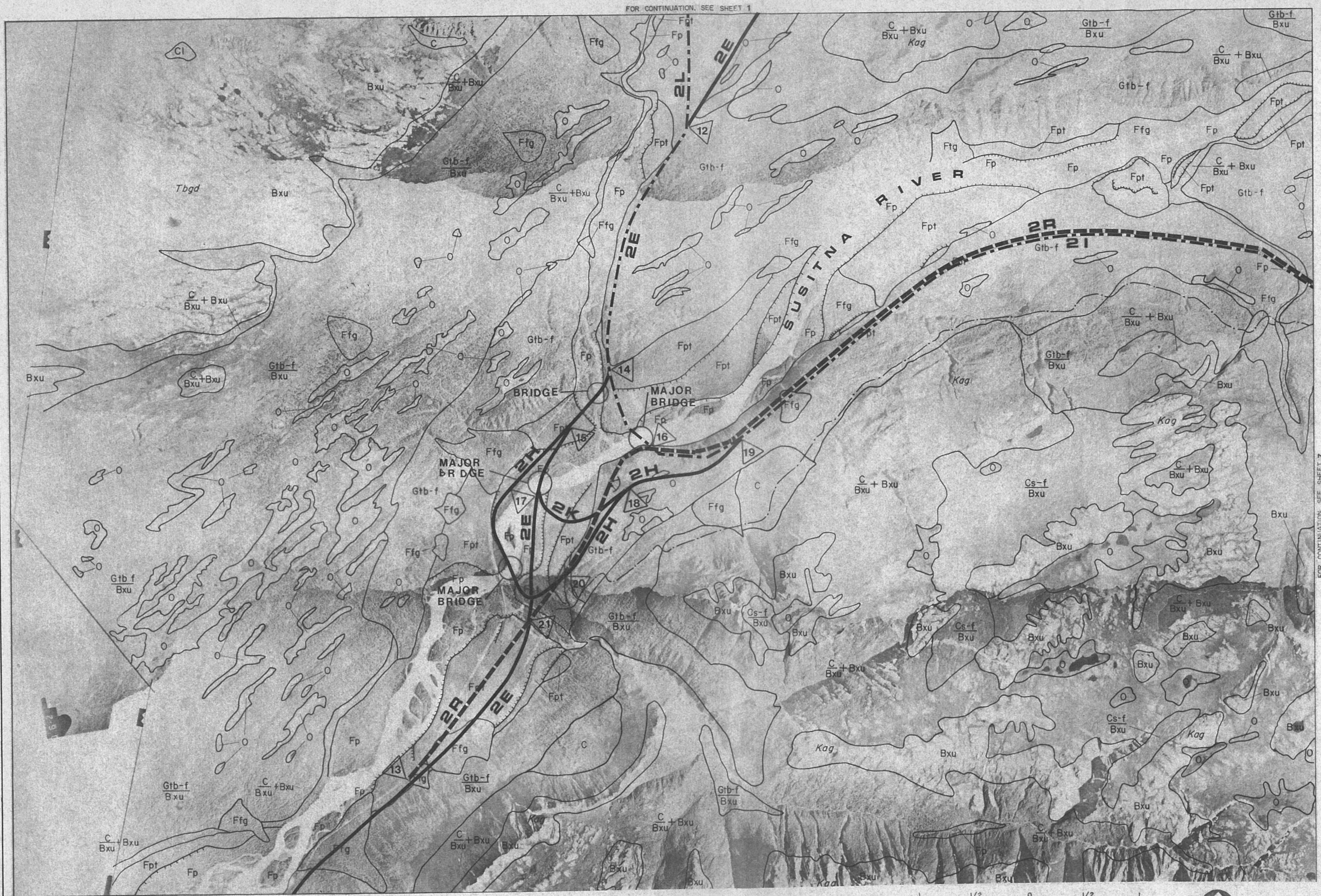
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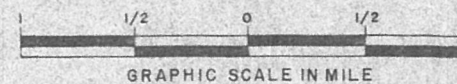
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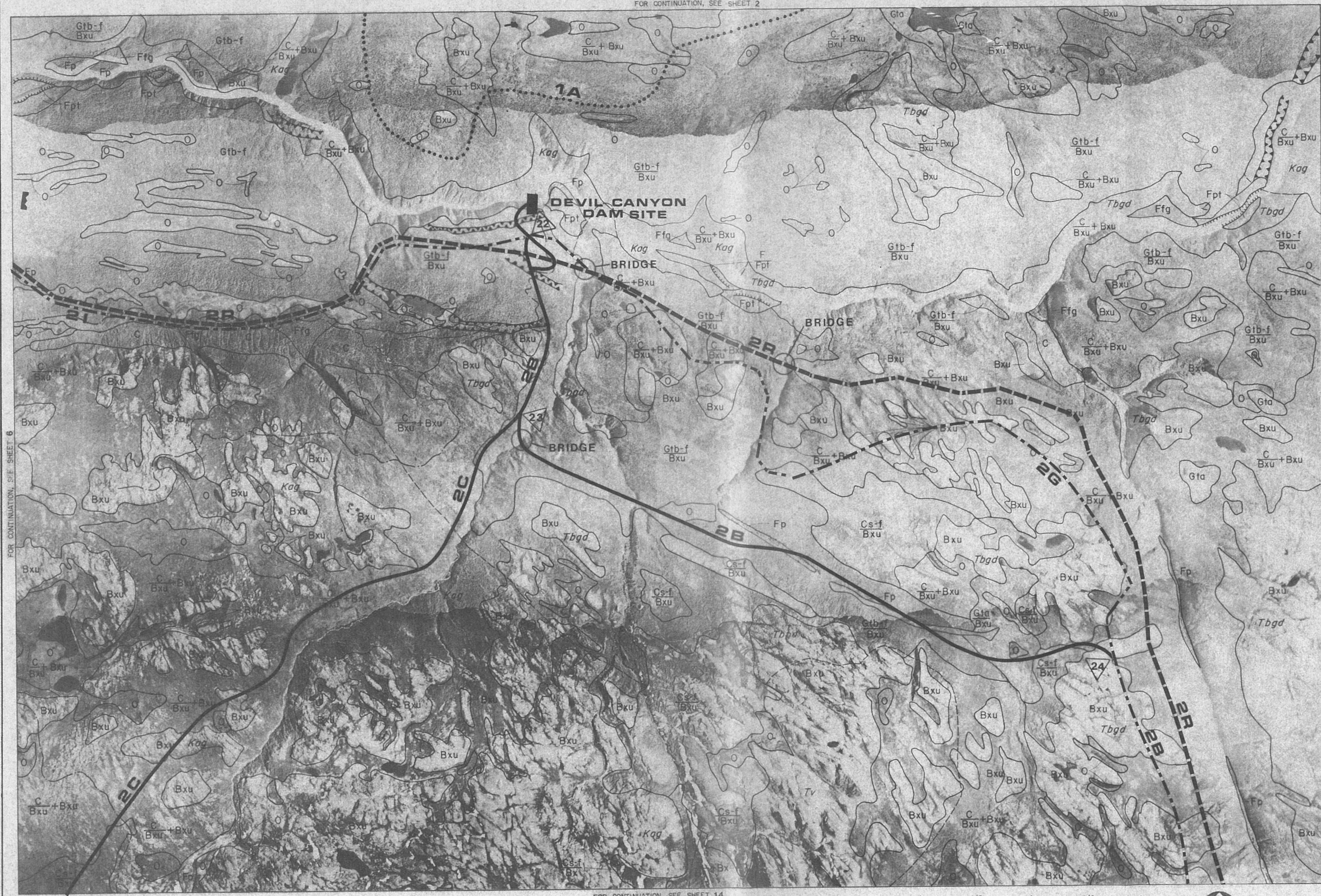
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FOR CONTINUATION, SEE SHEET 2



FOR CONTINUATION, SEE SHEET 14

GRAPHIC SCALE IN MILE



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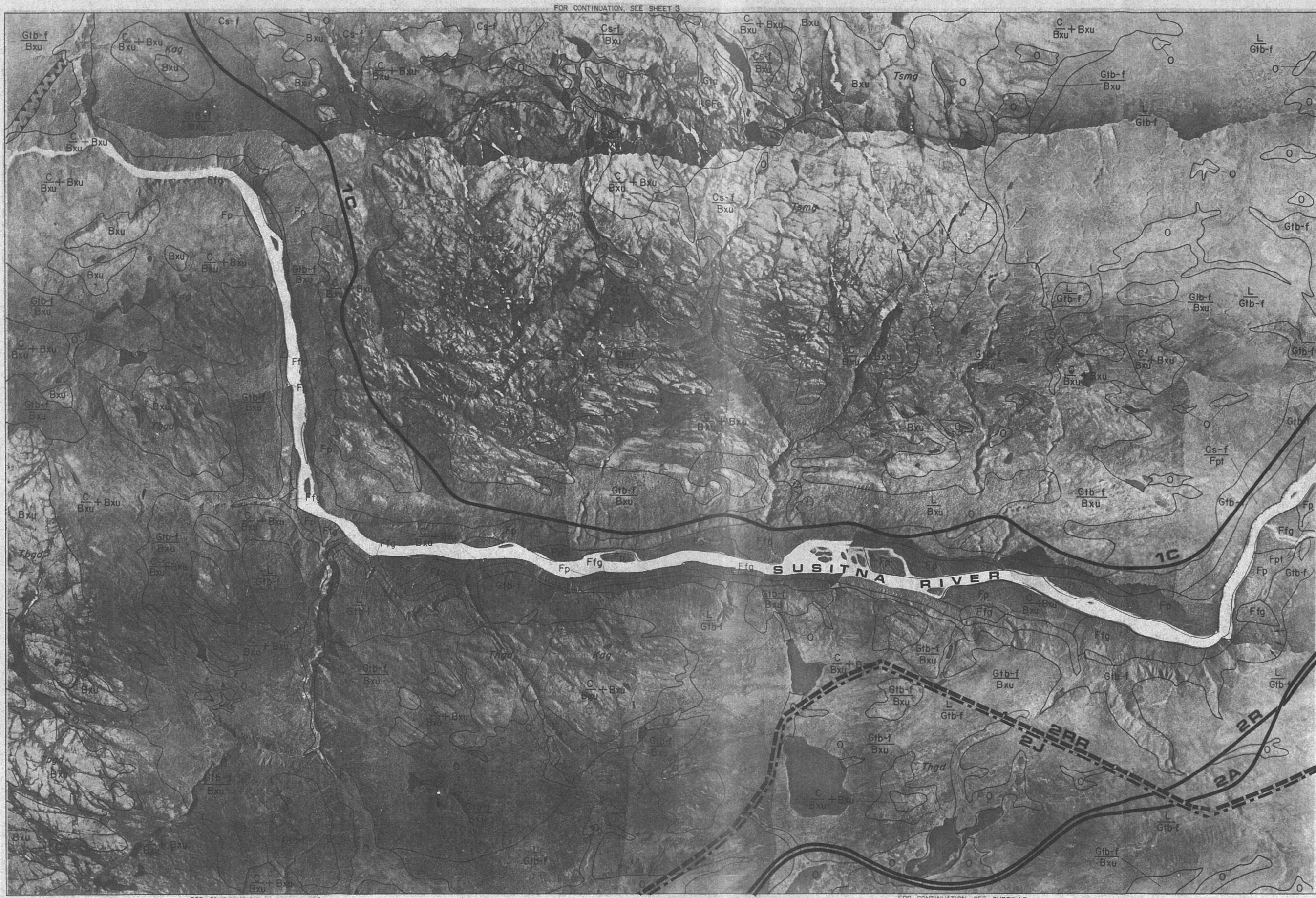
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FOR CONTINUATION, SEE SHEET 14

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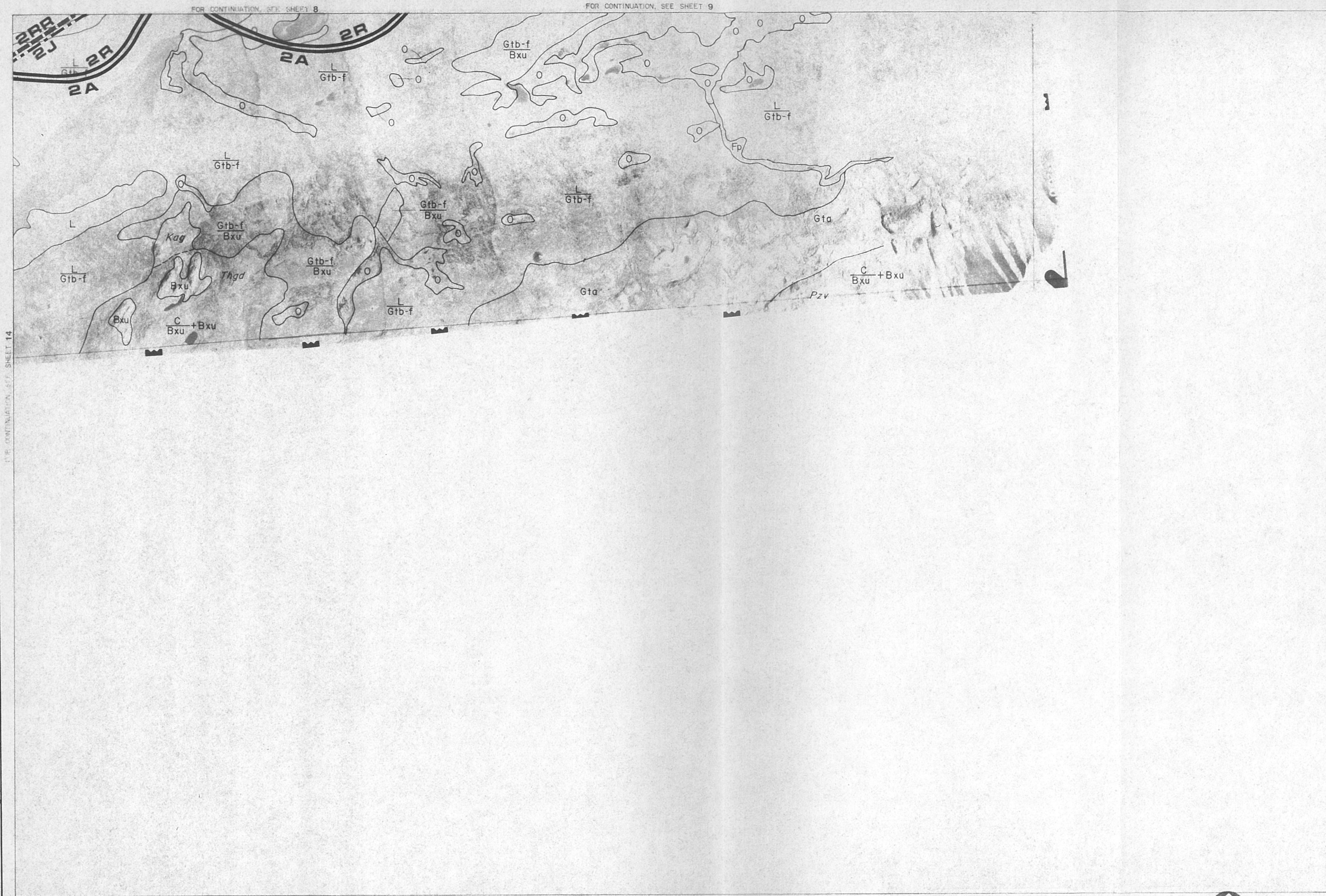
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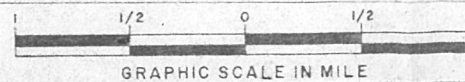




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FOR CONTINUATION, SEE SHEET 8

FOR CONTINUATION, SEE SHEET 9



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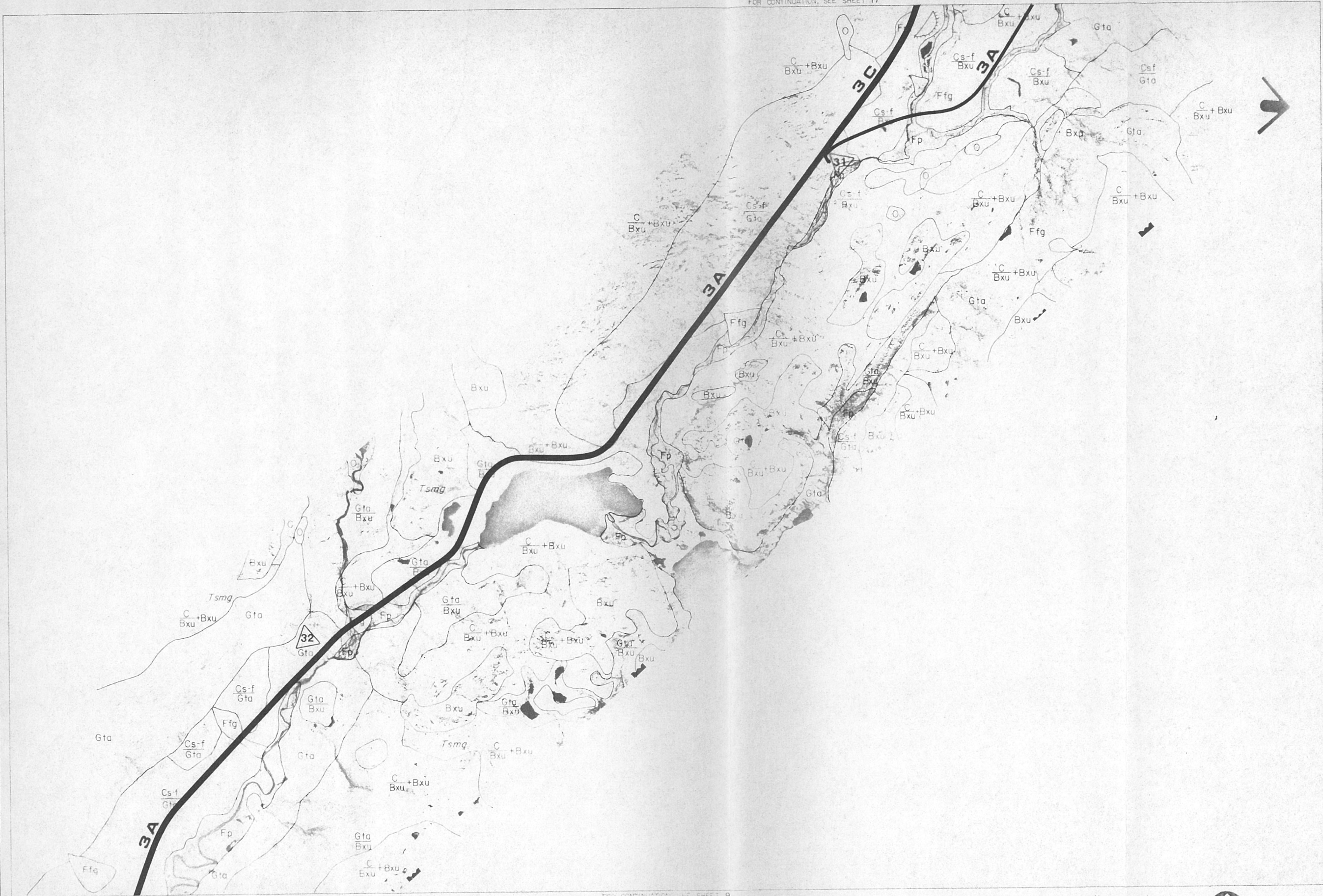
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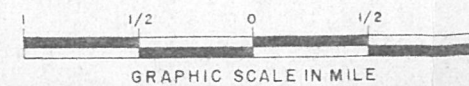
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FOR CONTINUATION, SEE SHEET 9



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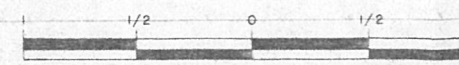
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GRAPHIC SCALE IN MILE



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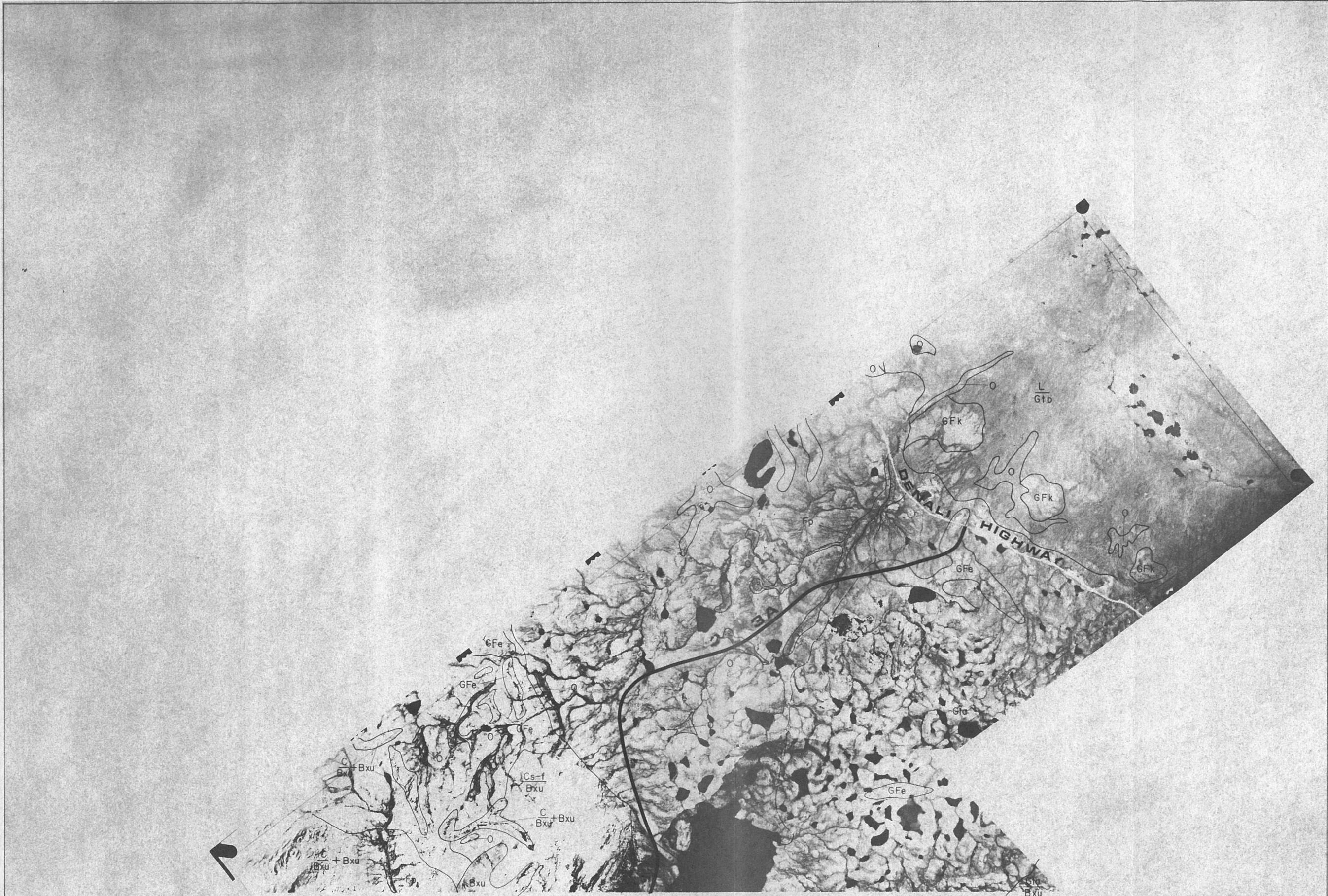
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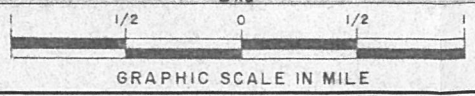
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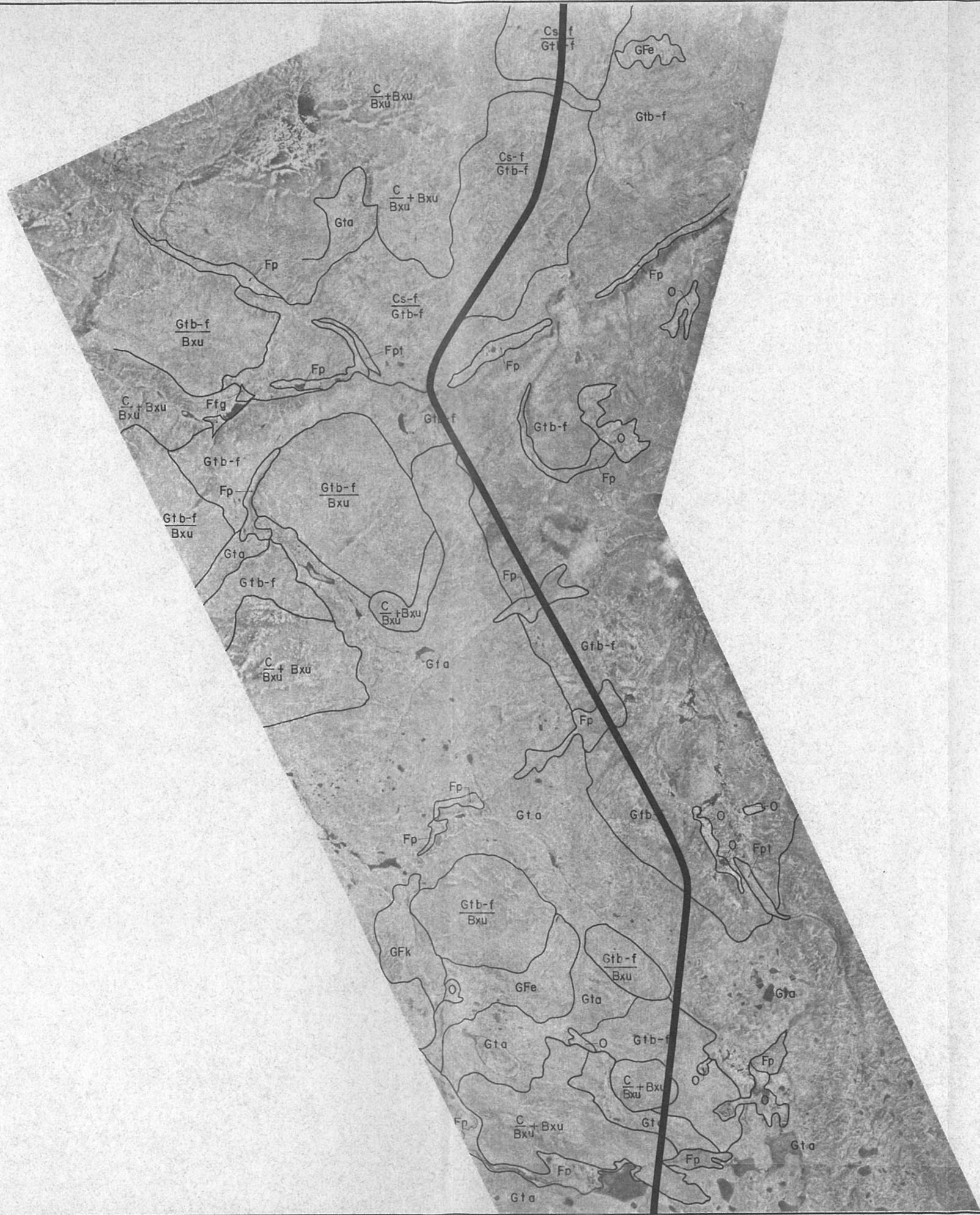
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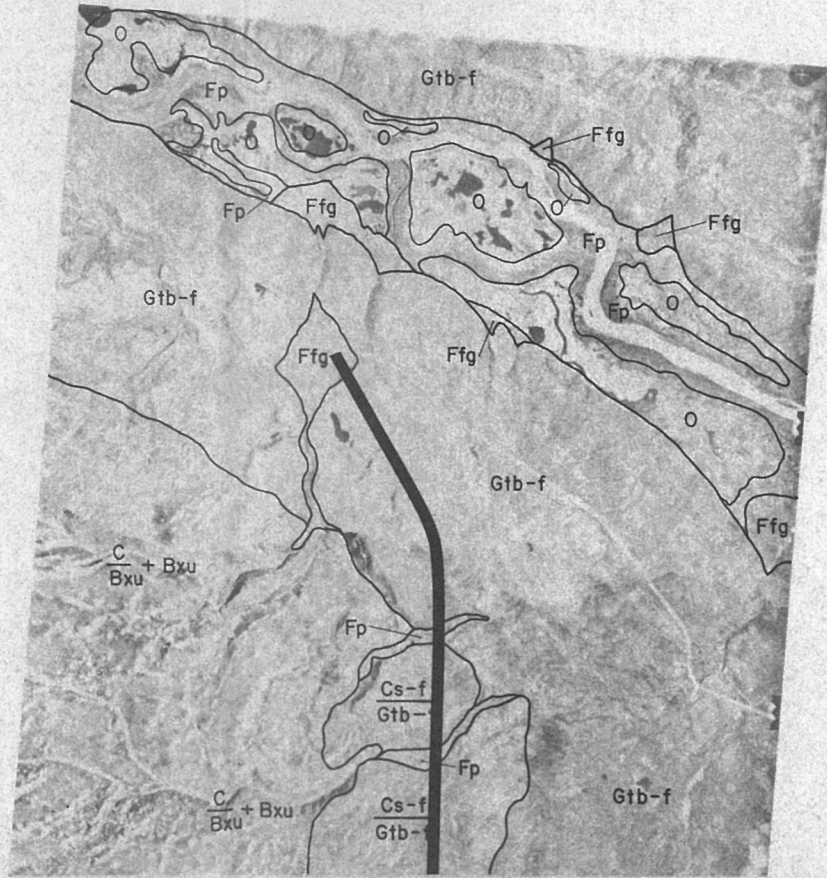
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APPENDIX E

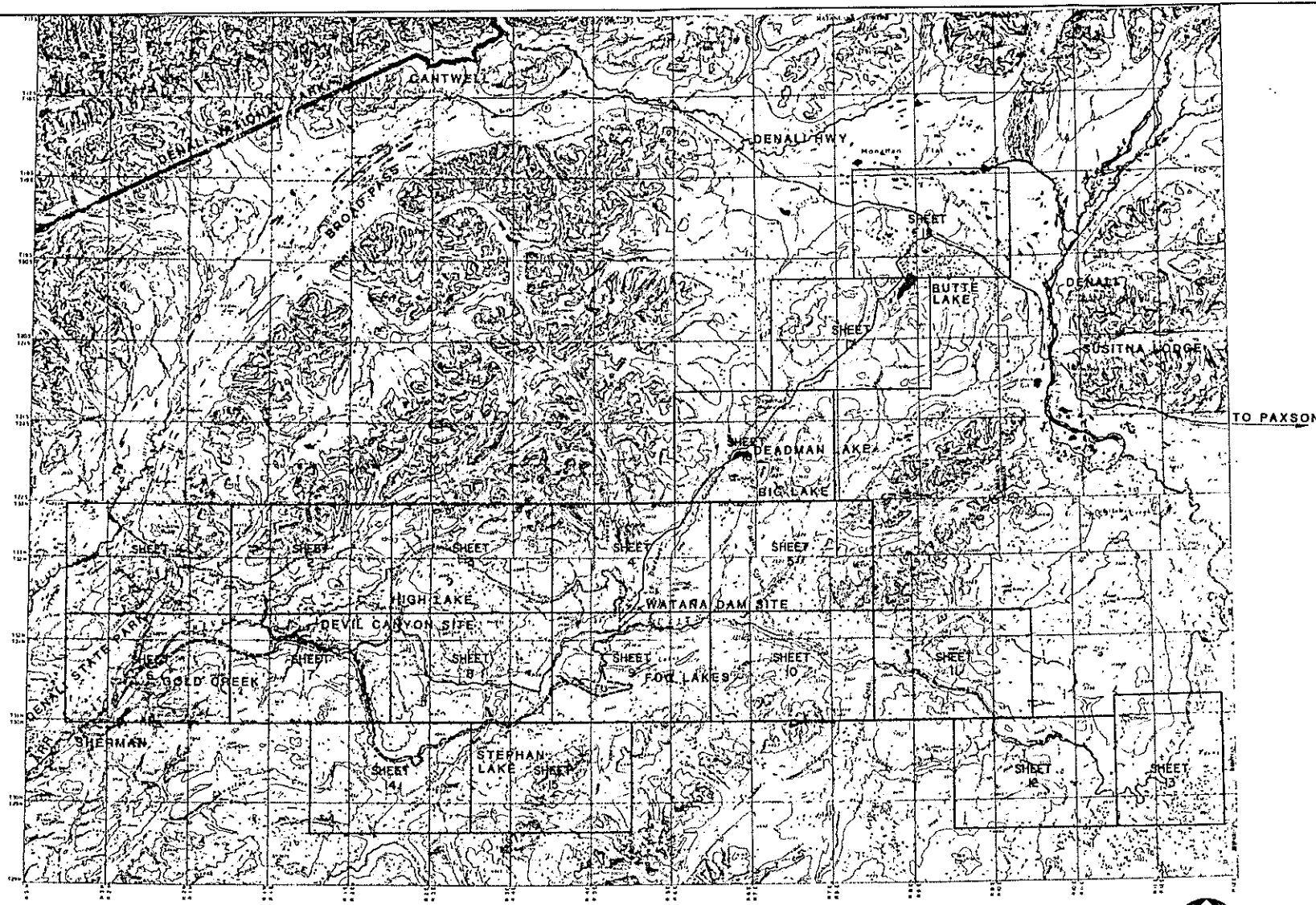
ENVIRONMENTAL CONCERNS

## Appendix E - Environmental Conflicts

Appendix E is a series of maps on which the more obvious and/or critical potential environmental conflicts are indicated. This data has been provided by the Environmental team and is fully considered in analyzing the access plans.

The following exhibits do not cover the currently preferred alignment from Deadman Lake to the Denali Highway. This segment was selected to avoid the caribou calving area around Butte Lake. The new line does infringe on summer Caribou range.



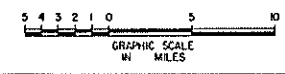


### LEGEND

- CORRIDOR 1
- CORRIDOR 2
- CORRIDOR 3
- RAILROAD

### NOTE

SHEETS NO. 5, 10, 12, & 13  
ARE OMITTED. NO ACCESS  
CORRIDORS ARE CONTAINED  
THEREIN.



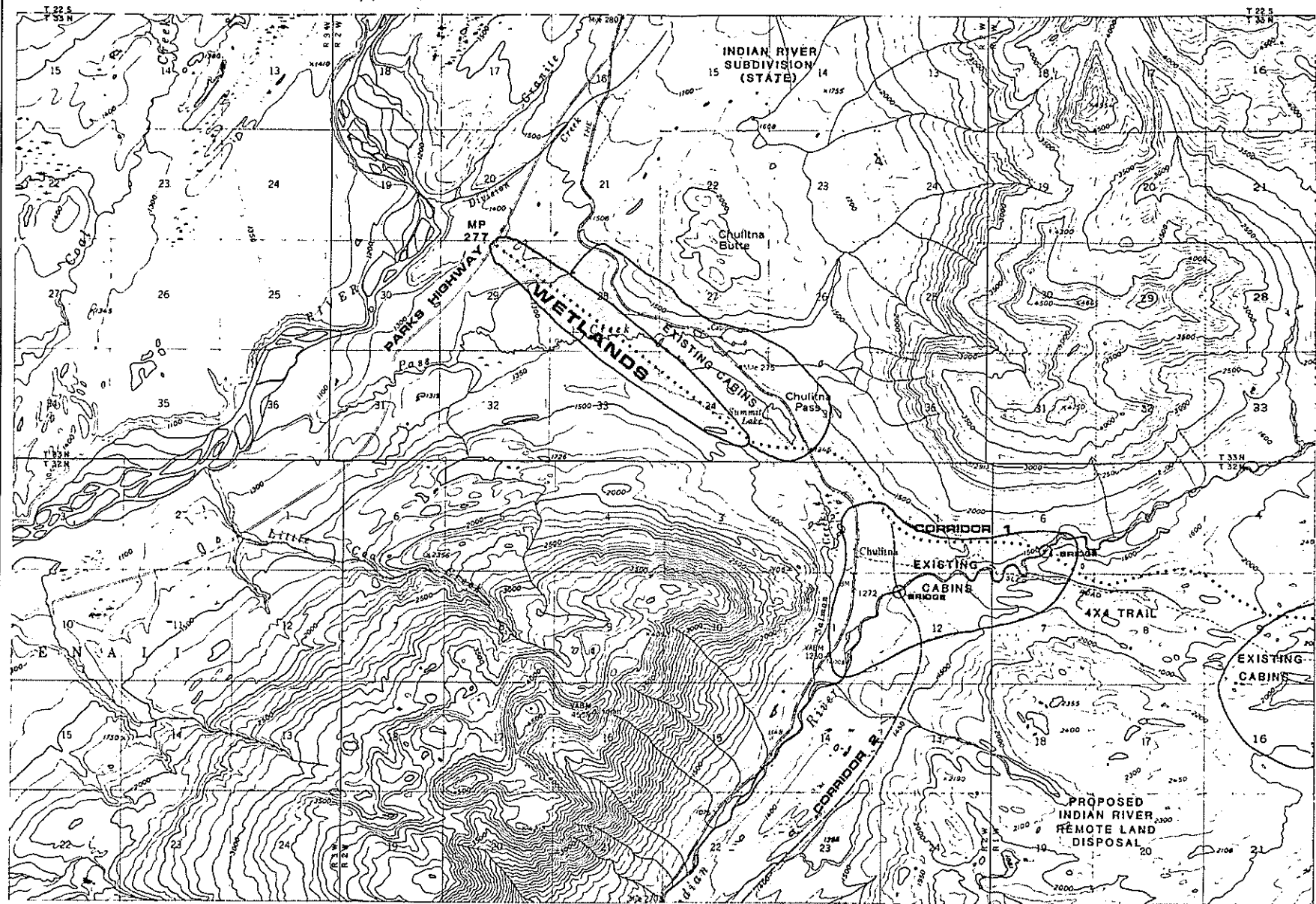
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## INDEX MAP

ALASKA POWER AUTHORITY  
SUSITNA HYDROELECTRIC PROJECT

20 10 5 1 0	20 10 5 1 0
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FOR CONTINUATION, SEE SHEET 6



SCALE 1" = 2000'

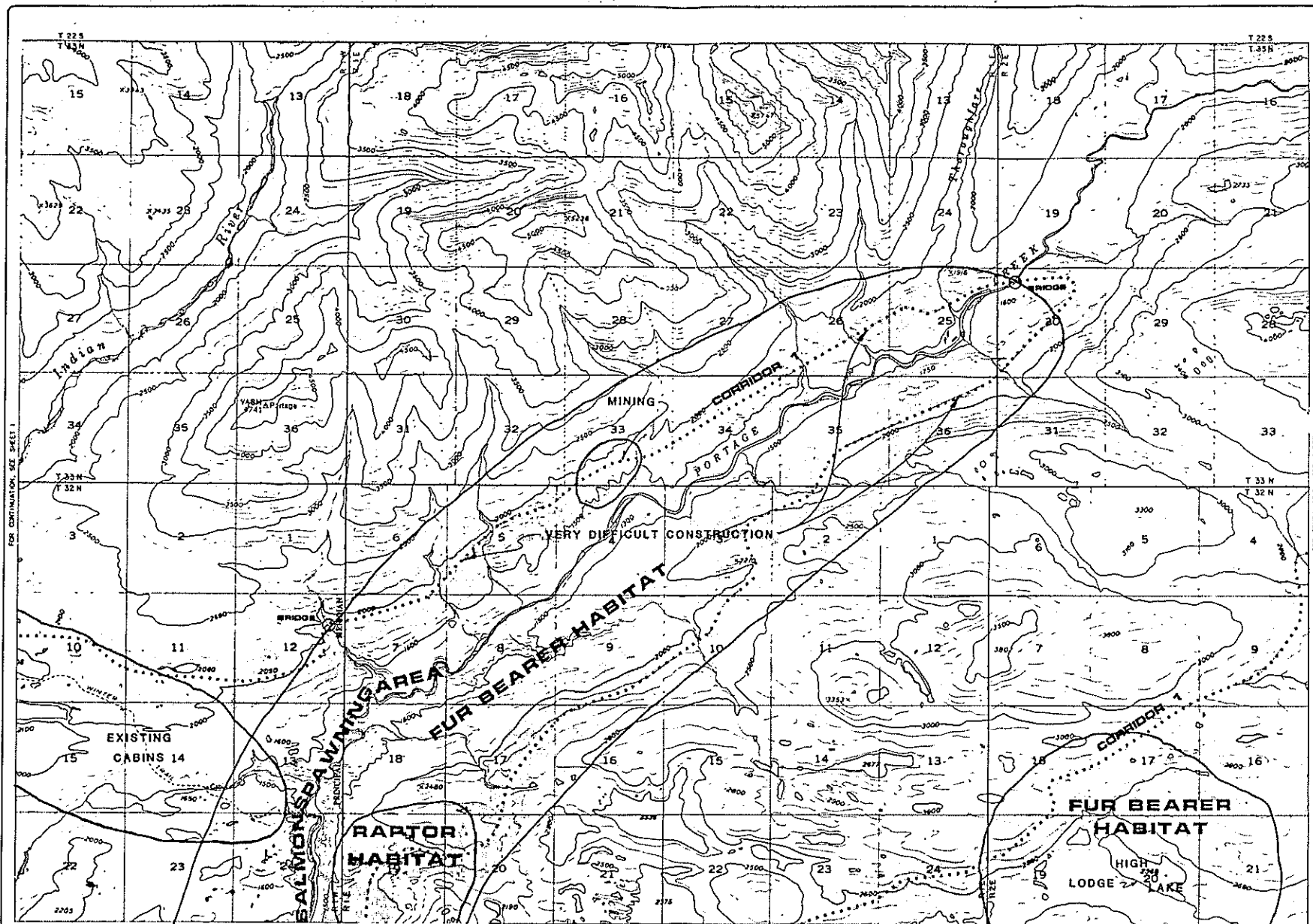
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SUSTITNA HYDROELECTRIC PROJECT

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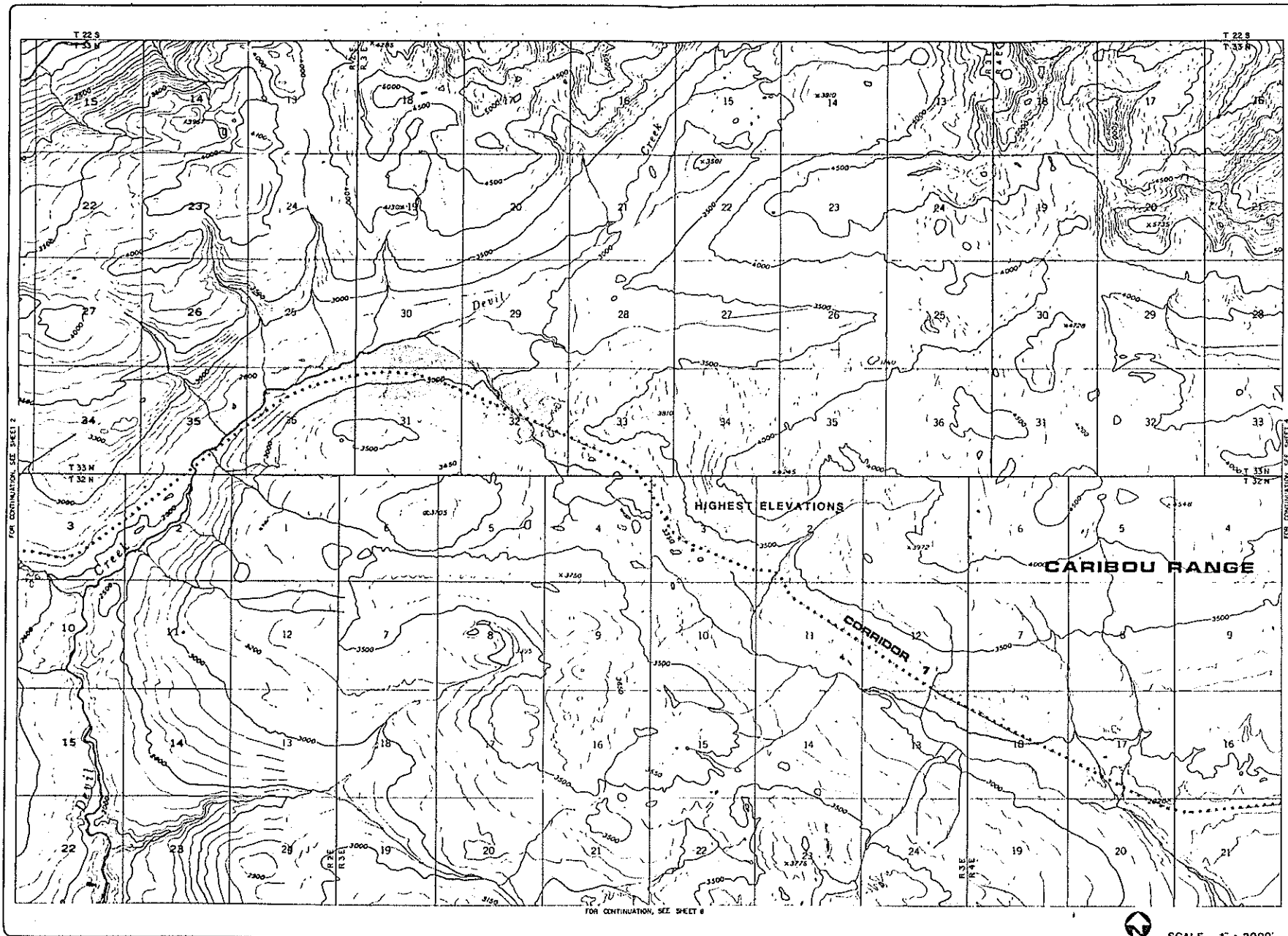
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SUSTITNA HYDROELECTRIC PROJECT

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FOR CONTINUATION, SEE SHEET 4

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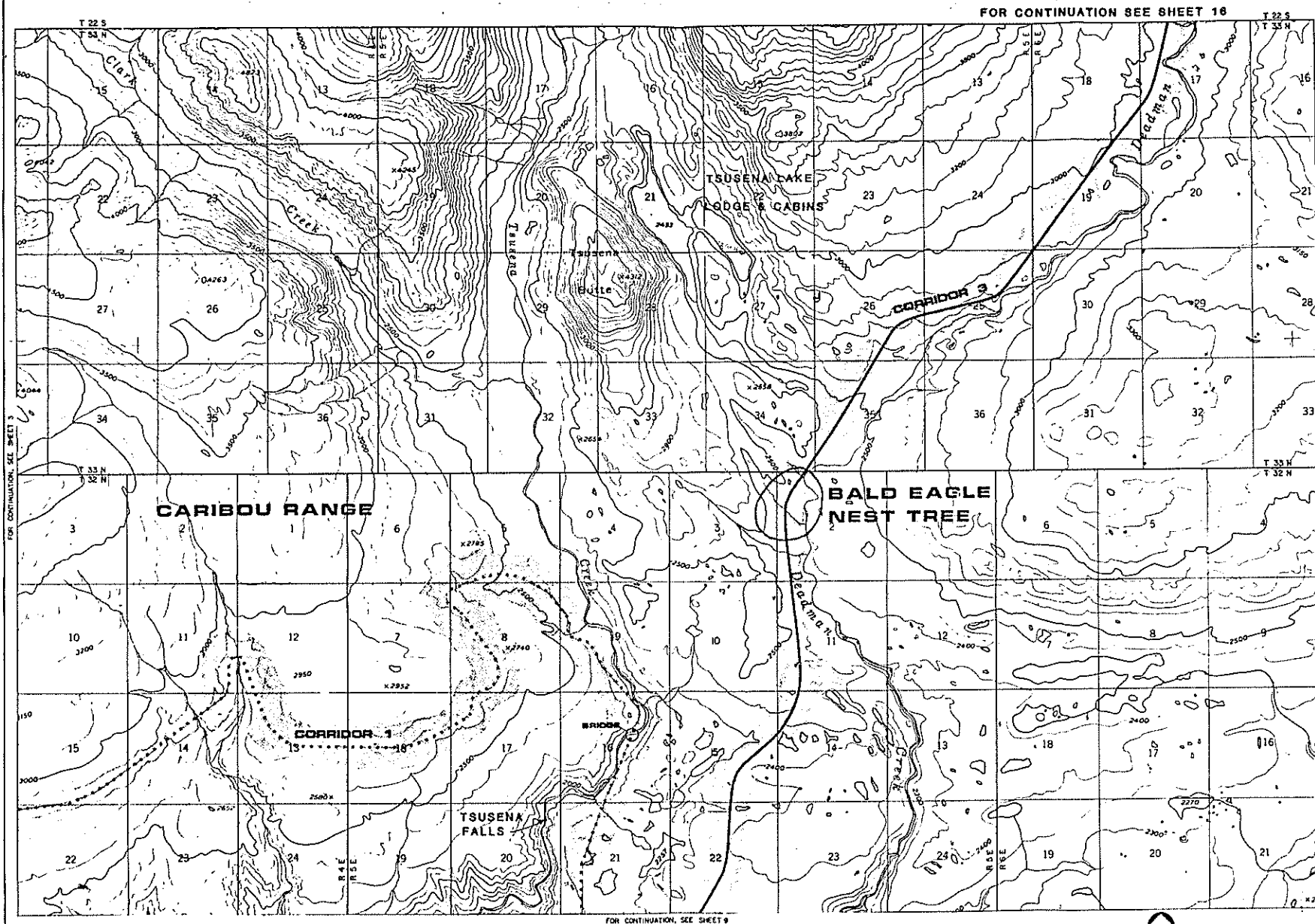
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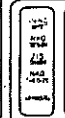


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# ACCESS CORRIDORS

ALASKA POWER AUTHORITY  
SUSITNA HYDROELECTRIC PROJECT



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SCALE 1" = 2000'

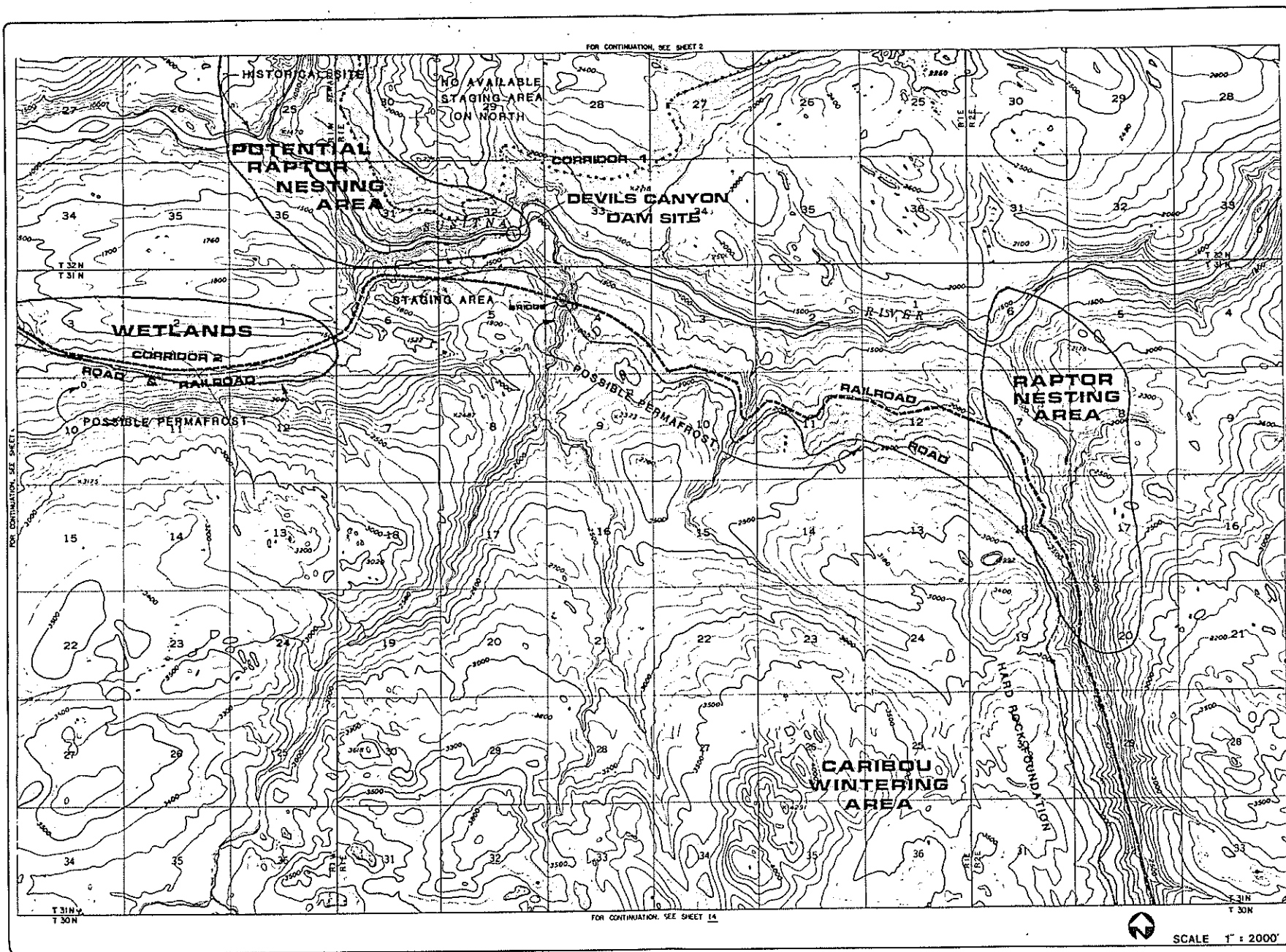
This topographic map depicts a section of the Yukon River and its surrounding terrain. Key features include:
 

- Proposed Infrastructure:** Two proposed railroads are shown: 'CORRIDOR 1 RAILROAD' running diagonally from the upper left towards the center, and 'CORRIDOR 2 ROAD & RAILROAD' running horizontally across the middle-right section.
- Wetlands:** A large area in the center is labeled 'WETLANDS' and is enclosed by a thick black boundary line.
- Permafrost:** An area on the right side of the map is labeled 'POSSIBLE PERMAFROST'.
- Geographical Features:** The 'YUKON RIVER' is prominent in the upper right. 'ISUSITNA BRIDGE' is marked on the river. 'ARRAS CREEK' flows into the river from the left. 'EXISTING CABIN' is labeled near the bottom left, and 'EXISTING CABIN' is also labeled near the top center.
- Topography:** The map uses contour lines to show elevation, with labels such as 1000, 1500, 2000, 2500, 3000, and 3500 feet.
- Grid System:** A coordinate grid is overlaid on the map, with letters A through K along the top and numbers 1 through 36 along the right side.
- Annotations:** 'Mile 265' is noted near the center. 'T 31 N' and 'T 30 N' are marked at the bottom edge. 'R 2 K' and 'R 3 K' are marked along the right edge.



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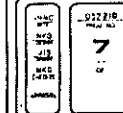


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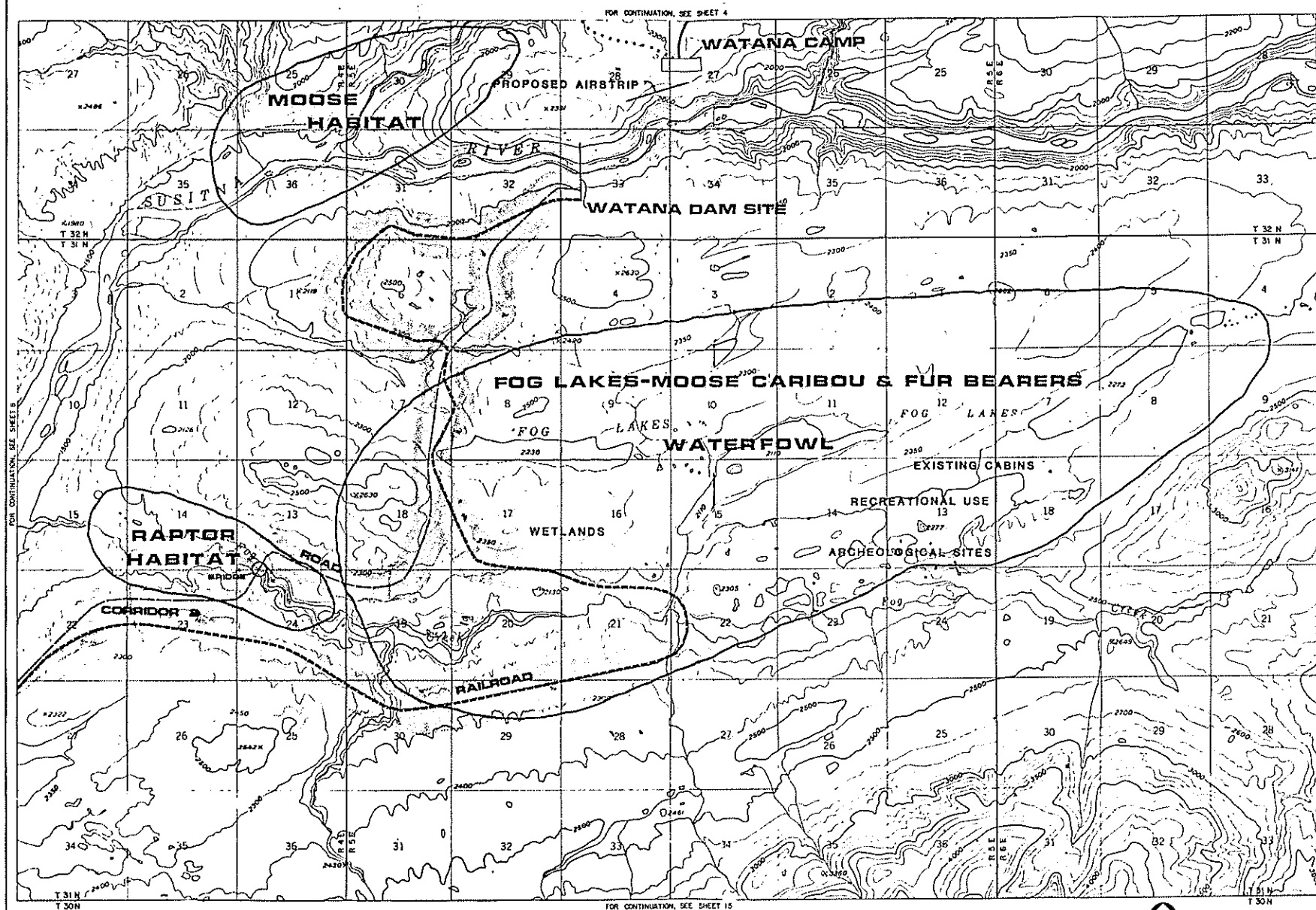
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SUSITNA HYDROELECTRIC PROJECT

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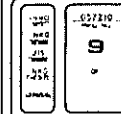


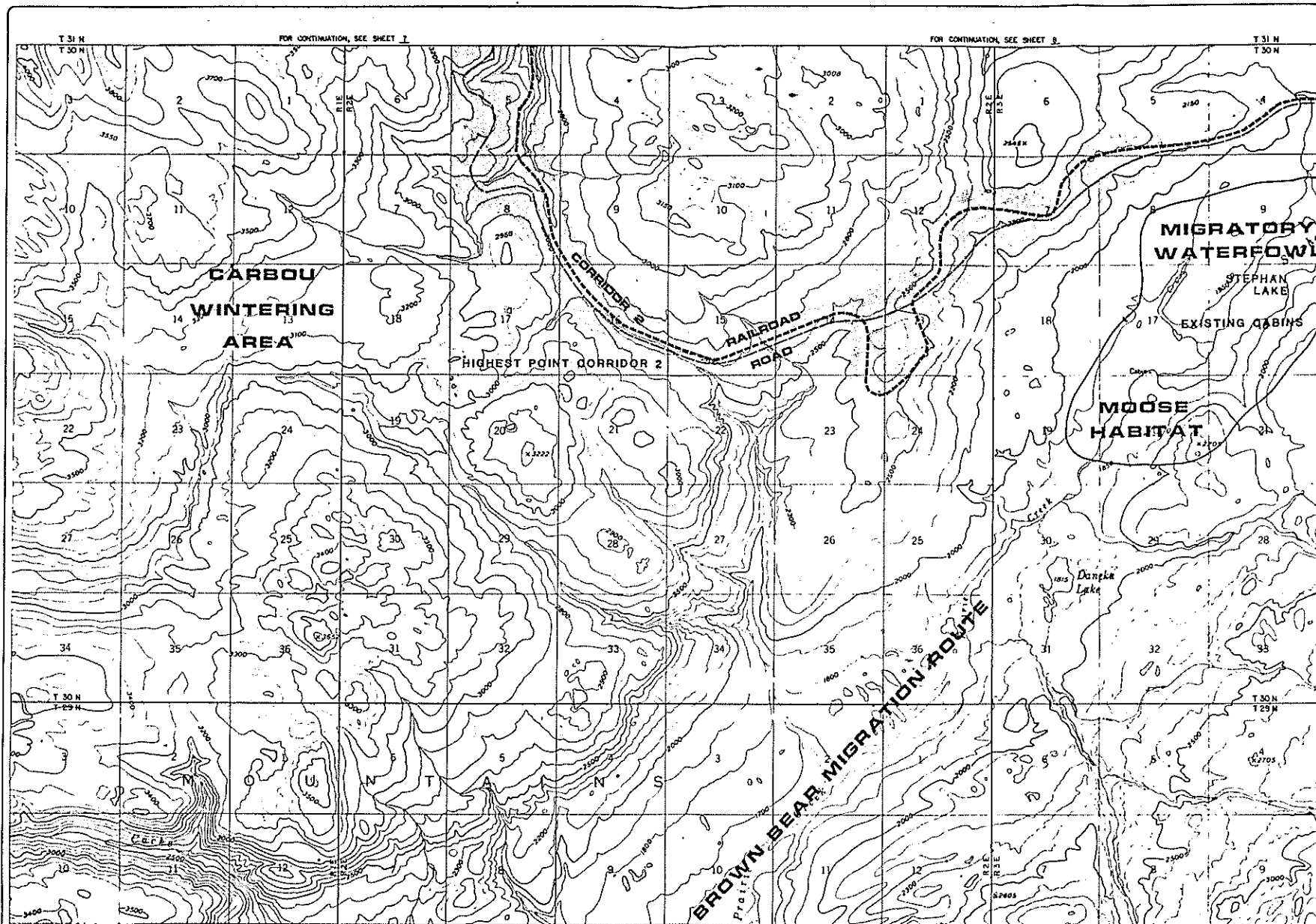
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SUSTINA HYDROELECTRIC PROJECT

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SCALE 1" = 2000'





SEE SHEET 4

SEE SHEET 17

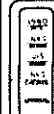
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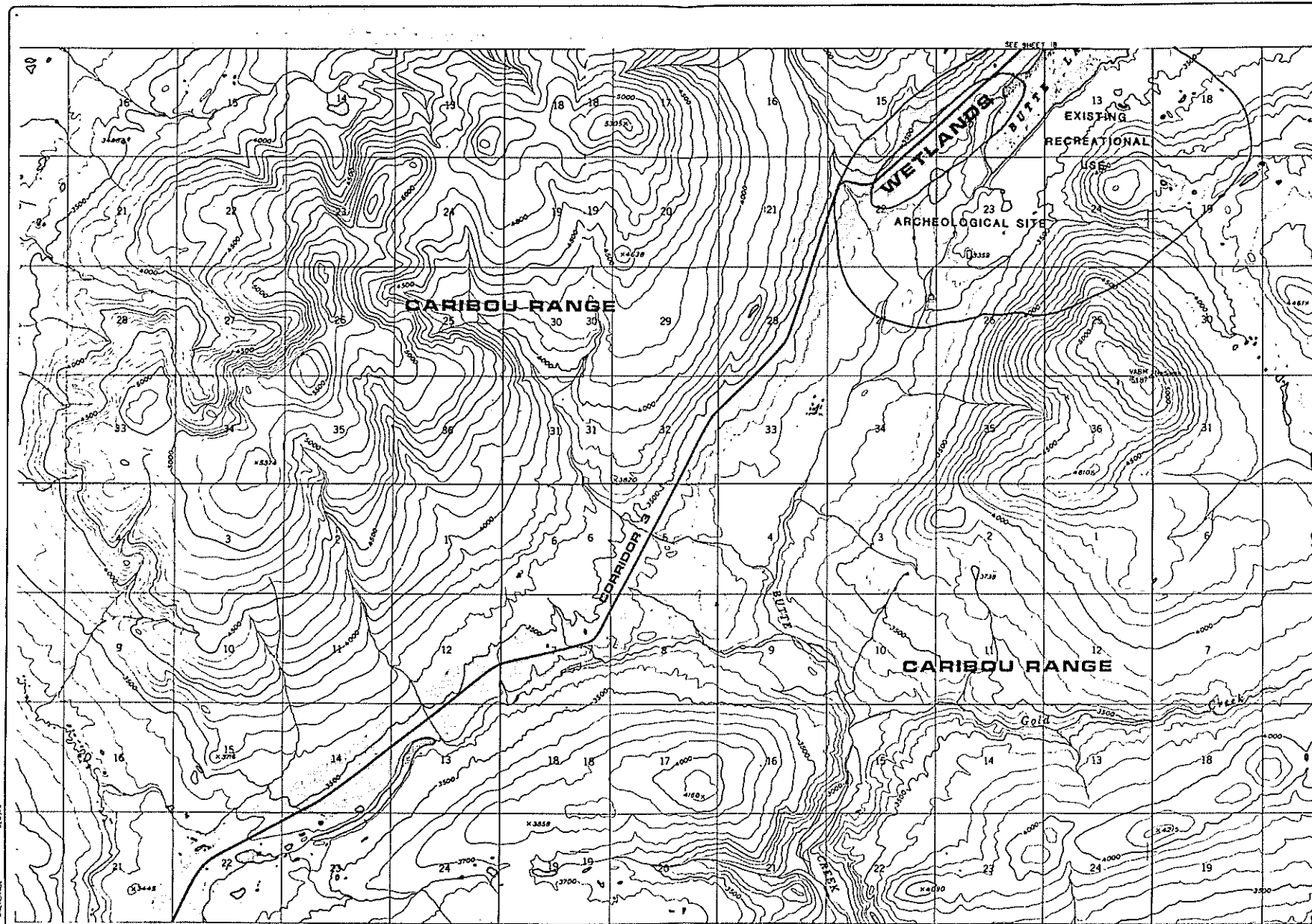
ACCESS CORRIDORS

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SUSTITNA HYDROELECTRIC PROJECT



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SCALE 1" = 2000'

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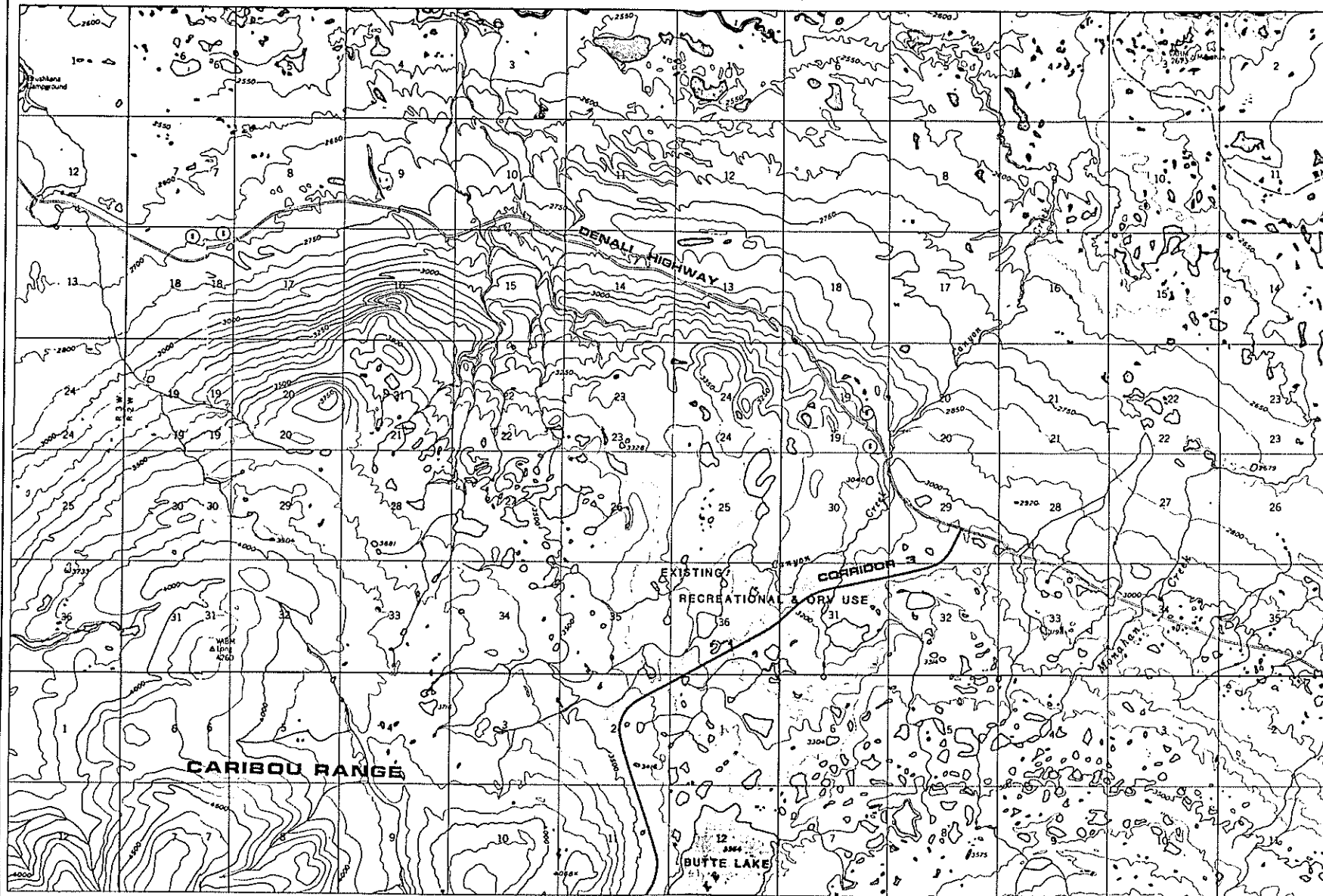
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SEE SHEET 17

SCALE 1" = 2000'

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ACCESS CORRIDORS

ALASKA POWER AUTHORITY  
SUSTINA HYDROELECTRIC PROJECT

18

APPENDIX F

COST ESTIMATES

## APPENDIX F - COST ESTIMATES

The overall costs of the various access plans must be a considered in the selection process. The access plans and their estimated costs are outlined herein. The process by which the estimates were generated is documentaed and the primary components of each plan are set forth.

### F.1 - Introduction

Common elements to all plans include quantities to be moved, the ports through which all commodities are assumed to flow and the ton-mile costs of haul for rail and truck. The costs differences developed here in will result from differences in length, difficulty of construction and maintinance, bridges, rail heads, and the length of haul on each mode.

### F.2 - Sea Ports

The Alaska sea ports identified for use in supplying the Susitna Hydroelectric Project are Anchorage and Whitter.

Anchorage is the perferred port for those items suitable for shipments in conventional containers and trucks. The port apparently has adequate capacity and the best facilities of any Alaska ports. The draw back in Anchorage is the lack of capabilities for roll-on roll-off rail shipments.

Whittier is unique in that there is roll-on roll-off rail capability. Because of freight rates and handling charges Whitter is the obvious choice for arrival of all materials that can be shipped by rail car.

Seward and Valdez were investigated and eliminated as primary parts for reasons of distance, port facilities and/or port costs.

TABLE F-2.1  
ACROSS THE DOCK HANDLING COSTS

Material From Seattle (6)	Cost in \$/Ton			
	(1) To Anchorage	(2) To Seward	(4) To Whittier	(1) To Valdez
Reinforcing Steel	72.00	72.00	55.00	86.00
Structural Steel	85.40	85.40	55.00	125.00
Cement	66.00	66.00	55.00(3)	80.00
General Cargo	80.00	80.00	55.00	110.00
Equipment	160.00	160.00	120.00	191.00
Explosives	89.00	Not Allowed	55.00	115.00

- 1 Quoted by Pacific Western.
- 2 Information not received - Estimated equal to Anchorage. Rates for fuel included in modal alternate section.
- 3 Rate for 140,000 lb Hopper Cars - Rates for Bags 100.00/ton as per ARR.
- 4 Rates derived from quotation by ARR.
- 5 Includes Stevedoring at all ports.
- 6 Explosives must flow through Prince Rupert, B.C.

Line Haul rates were collected from the Alaska Railroad and several trucking firms. Comparison of line haul rates is shown below.

TABLE F-2.2  
LINE HAUL RATES IN DOLLARS/TON-MILE

Item	Rail	Truck
Equipment	0.1878	0.2069
Steel	0.2577	0.2069
Cement	0.1565	0.2069
Fuel	0.1450	0.2069
General Cargo	0.1262	0.2069
Explosives	0.6267	0.2069

While certain items may move by truck with lower costs, the mix of items and quantities make it clear that the overall most cost effective line haul mode is rail. For this reason all plans contemplate rail haul to the maximum extent practicable.

#### F.4 - Railhead

Railhead facilities will be required at one or more locations depending on the final plan adopted. The logistics estimates indicate a need to be able to handle a flow of 40 to 60 rail car loads per week. The detailed requirements for the railhead will vary with location however for the purposes of the study a typical facility has been developed and will be considered as applicable at all locations.

The typical railhead layout is based on the following requirements. The proposed layout is shown in Figure F-4.1. The estimated construction cost of the typical rail head is \$5,160,000 as shown in Table F-4.1.

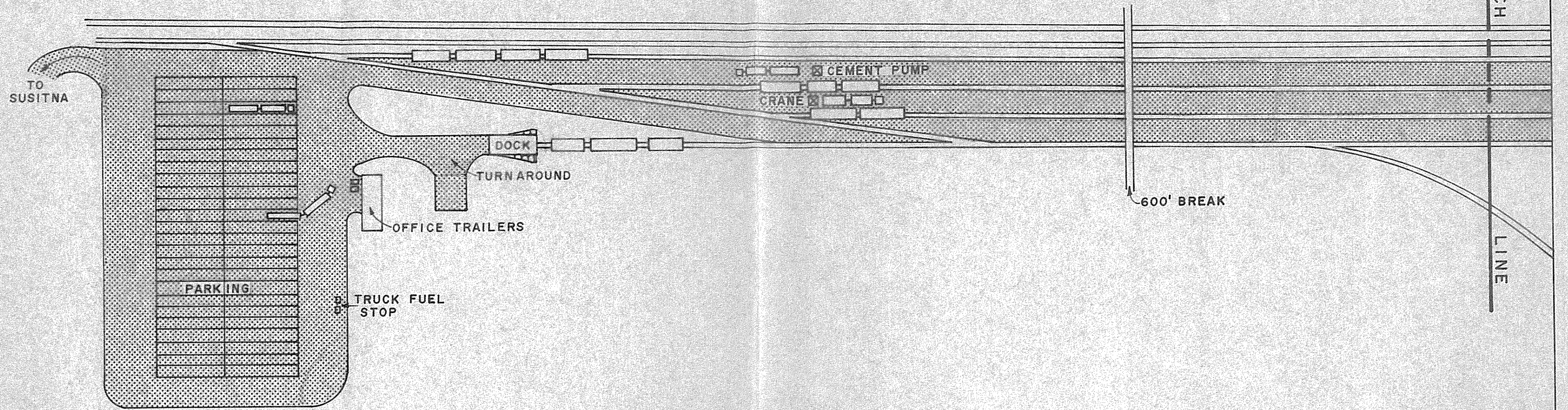
Scope: The rail head must be capable of handling about 50 cars at a time.

- 1) Piggybacks
- 2) Containerized (Sealand type)
- 3) Tank Cars
- 4) Hopper Cars

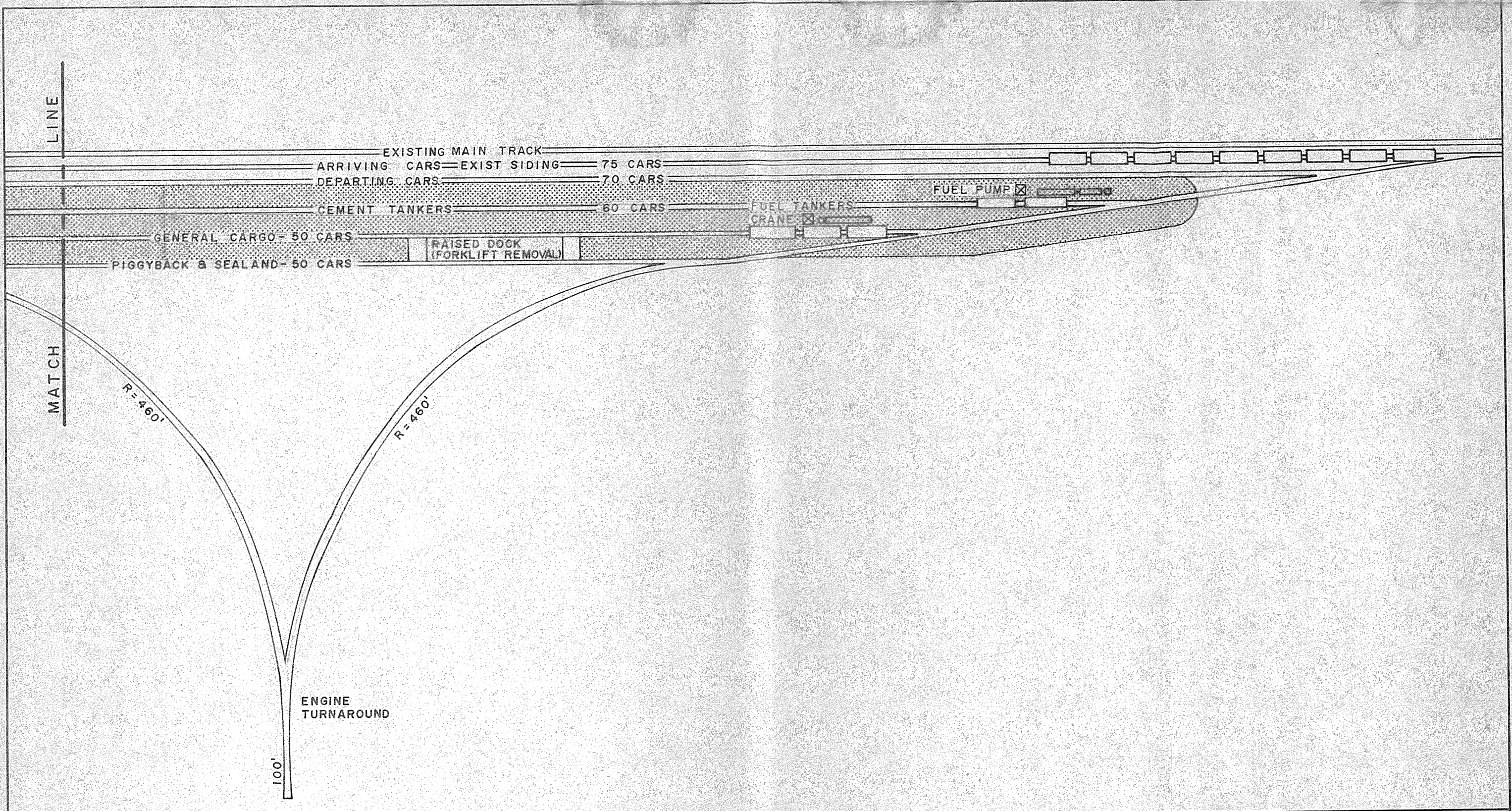
#### Elements:

- 1) Sidings to store rail cars arriving and departing
- 2) Siding (s) to store rail tankers for on-demand pumping into truck tankers
- 3) Cement pumping areas










REVISIONS


DATE	INT'L



**ALASKA POWER AUTHORITY**  
SUSITNA HYDROELECTRIC PROJECT

**TYPICAL PLAN**  
**RAIL TO TRUCK TRANSFER FACILITY**

PROJ. No. 052210

 <b>R&amp;M CONSULTANTS, INC.</b> <small>ENGINEERS • GEOLOGISTS • PLANNERS • SURVEYORS</small>	DWN.	P.T.
	CKD.	
	APPVD	

- 4) Piggyback off loading area (ramp)
- 5) Containerized off loading area (w/crane or forklift)  
(contractors to supply equipment)
- 6) Truck storage and maneuvering area
- 7) Office space and employee facilities (contractor supplies)
- 8) Truck fueling/servicing (contractor supplies)

#### Details

- ° Degree of curvature should not exceed  $12^{\circ} 30'$
- ° Require 45' length of track per car. Minimum main line or ladder to ladder spacing 18' center to center. Minimum body to body track spacing 14 feet.
- ° Maximum angle of ladder to sideing, for a slow moving freight yard, #8 frog, is  $7^{\circ} 9' 10''$ .
- ° Arrival and departure tracks should each be long enough to hold the longest train anticipated. Optimum yard capacity = 110% of arrival rate.

#### Parameters:

- ° Volume: 50 cars/wk. Use a maximum of 50 cars arriving in 1 day. These could all be of one type.

- ° Length: need 45' per car = 2,250'
- ° Between Sidings: Need 2 lane road (24' plus track width), minimum 14' from No. 1 to 2, 14' from No. 2 to 3, 29' from No. 3 to 4, and 29' from No. 4 to 5.
- ° Ladder Lengths: When spacing = 14', difference in length =  $111\frac{1}{2}'$ , when spacing = 29', difference in length = 231'
- ° Actual Lengths: No. 5 Minimum = 2,250', leg could be longer if terrain dictates.

No. 4 = 2,250' (min.)

No. 3 = 2,250' + 2 (231) = 2,712

No. 2 = 2,712 + 2 (231) = 3,174

No. 1 = 3,174 +  $111\frac{1}{2}'$  = 3,397

Note, No. 1 siding already exists at Gold Creek and is 4000' long.

- ° Turnaround:  
R = 460'  
A = 100' (2 cars) (Tangent length beyond switch)
- ° Trucks: WB-60, WB-50, maximum turning radius = 45', minimum turning radius = 19.8, maximum length = 65', max width = 8.5' or for wide load parking slots: use 12' x 70' aisle: 55' wide to allow for turn into stalls, # of slots = 50 ea.

#### Sources:

- ° Hennes, Robert G. and Ekse, Martin I., Fundamentals of Transportation Engineering. McGraw Hill Book Company, 1955 New York.

- ° Merritt, Frederick S., Standard Handbook for Civil Engineers  
2nd Ed. McGraw - Hill Book Company 1976 New York.

TABLE F-4.1  
RAIL HEAD COST ESTIMATE

		UNIT	1981 ANCHORAGE
	<u>AMOUNT</u>	<u>PRICE</u>	<u>PRICE</u>
1. Clearing	25 ac.	\$4,000/ac.	\$ 100,000
2. Waste Excavation	78,000 cy	\$3.50/cy	273,000
3. Common Excavation	505,000 cy	\$3.00/cy	1,515,000
4. Rock Excavation	-0-	-0-	-0-
5. Borrow	-0-	-0-	-0-
6. Grade A Base	4,900 cy	\$12.00/cy	58,800
7. D-1 Base	2,400 cy	\$15.00/ton	36,000
8. AC Surfacing	2,200 tons	\$55.00/ton	121,000
9. Fabric	-0-	-0-	-0-
10. Topsoil and Seed	15 ac.	\$2,500/ac	37,500
11. Traffic Control Devices	L.S.		500
12. Subballast	25,800 cy	\$6.00/yd	154,800
13. Trackage	19,700 l.f.	\$100/l.f.	1,970,000
14. Dock Lumber (6"x6")	16 mbf	\$400/mbf	<u>6,400</u>
		1981 TOTAL	\$4,273,000
		Round to	\$4,300,000
		Converting to 1982 Dollars (20% index increase)	\$5,160,000

## F.5 - Bridges

Bridges are major cost items and for some plans, major schedule constraints. Layout plans for the major bridges are included. Bridge cost estimates are based on Alaska Department of Transportation and Public Facilities average bid information. This information was provided by a Department of Transportation and Public Facilities estimator. Bridge prices up-dated to 1982 dollars are approaching \$150.00/square foot of deck for complete installations.

The railroad bridges normally include heavier members and foundation elements however they are narrower. Information received from the Alaska Railroad Engineering department indicates that square foot costs for railroad bridges are approximately double that for highway bridge. Therefore a cost of \$300.00/square foot will be used for estimating railroad bridge costs.

Figure F 5.1 shows a 440-foot continuous welded plate girder structure over Indian River. This structure, with slight variations in height and/or length is typical of all possible crossings of Indian River.

Figure F 5.2 shows the Susitna River structure proposed for segment 2-L. Other segments crossing the Susitna near Gold Creek would have a bridge that would have different alignment characteristics, however over-all demensions would be similar in most cases. Cost estimates are based on the structure shown.

Figure F5.3 shows the road and railroad bridges over Cheechako Creek immediately above Devil Canyon. This structure is in a location that makes it a major time constraint.



Figure F5.4 shows the roadway structure over Fog Creek.

Figure F5.5 a roadway structure over an unnamed creek about two miles east of Cheechako Creek in Corridor 2.

Figure F5.6 shows the type and approximate size of structure that would be required to serve as a high bridge at Devil Canyon. This bridge will take approximately three years to construct. The \$150/square foot cost is probably low for this type of structure however there is no equivalent Alaska bridge, so that estimate is used.

#### F.6 Quantity Estimating Cross Sections

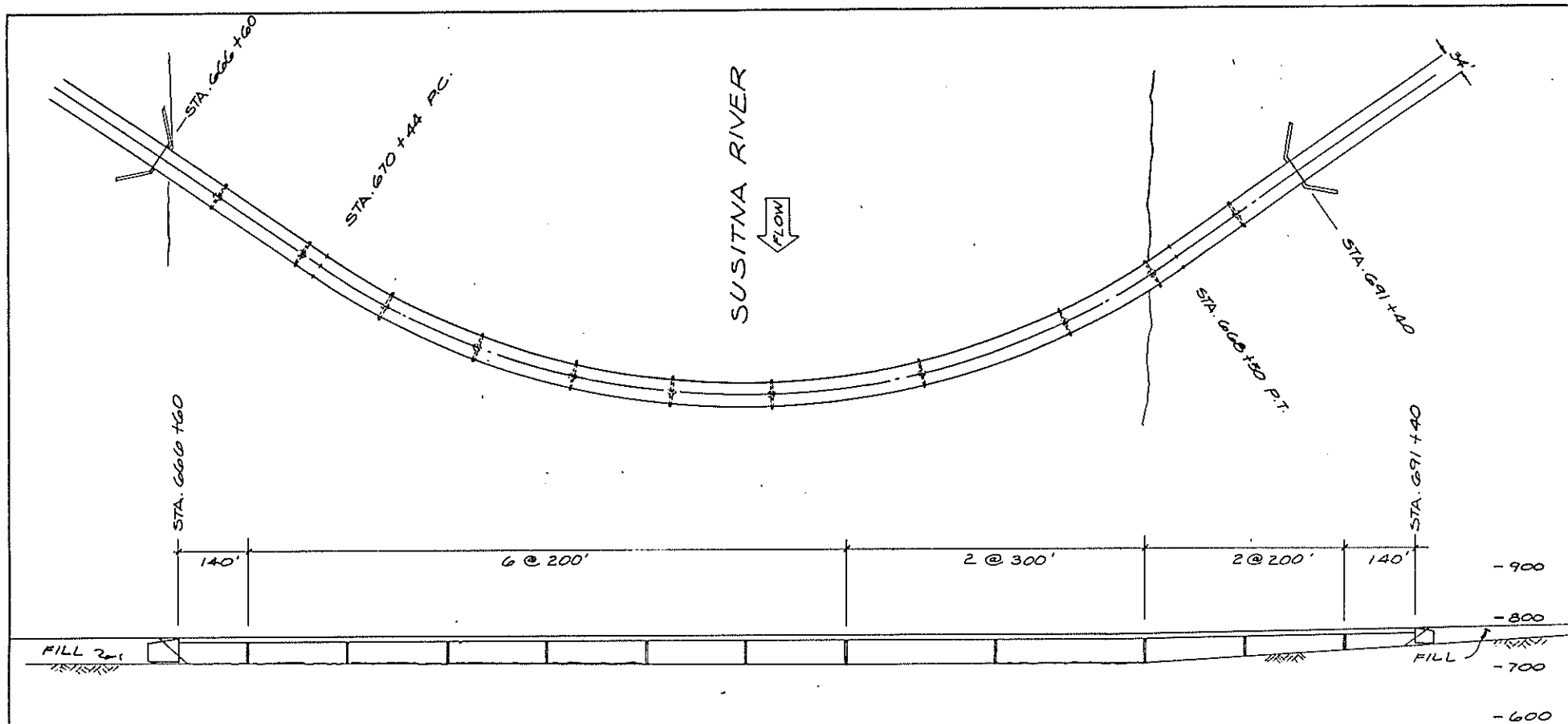
For purposes of estimating excavation quantities along the preferred routes within each of the 3 corridors and the railroad corridor, cross slopes were taken from available contour maps along with lengths of alignments.

Cross sections were prepared for cross slopes of 0-10%, 15%, 25%, 30%, 35%, 40%, 45%, and 50%. The upper 2 feet of material was considered as waste excavation on all alignments.

It was considered that average variations of subgrade from the ideal cut equal fill section would be 10 feet.

Frozen materials were considered to have a maximum cut of 10 feet to protect the 15 feet depth of frozen indicated in the soils information. This maximum cut depth requires a higher grade line than would be most economical for a balanced cut = fill section. Local borrow would be necessary to make up the difference.

On cross slopes up to 10%, particularly along corridor #3 a borrow pit type of cross section is proposed to provide material for



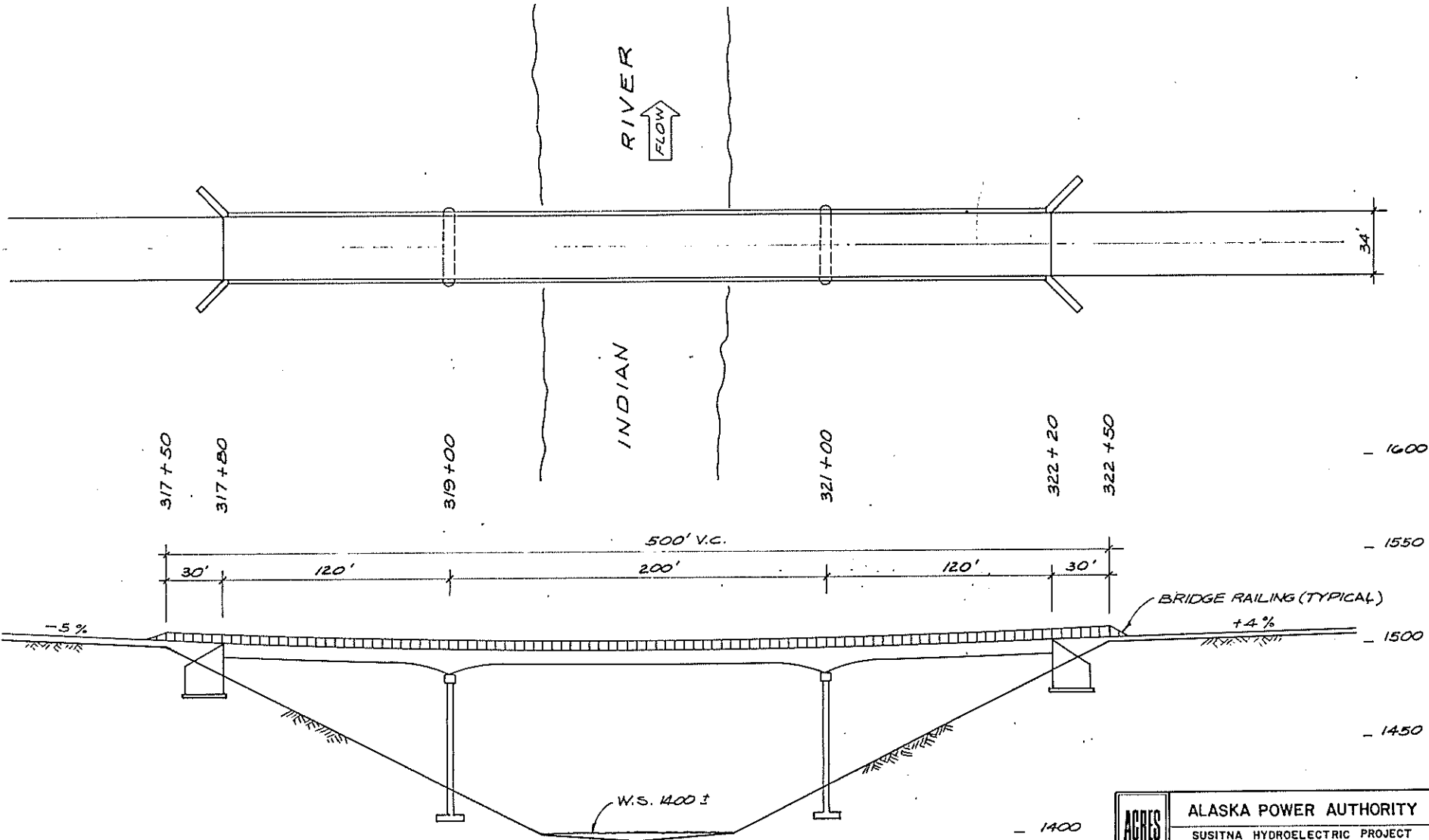
# **ORTHOTROPIC STEEL STRUCTURE 2480 FT. BRIDGE**



REVISION:	
DATE	INT'L

PROJ.# 052210

ACRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
SUSITNA ACCESS CORRIDOR		
<b>SUSITNA RIVER</b>		
<b>BRIDGE</b>		
<b>CORRIDOR # 2</b>		
DESIGN	DWN	OE P
REM CONSULTANTS, INC.	CKD	VG.
	APPVD	NKG



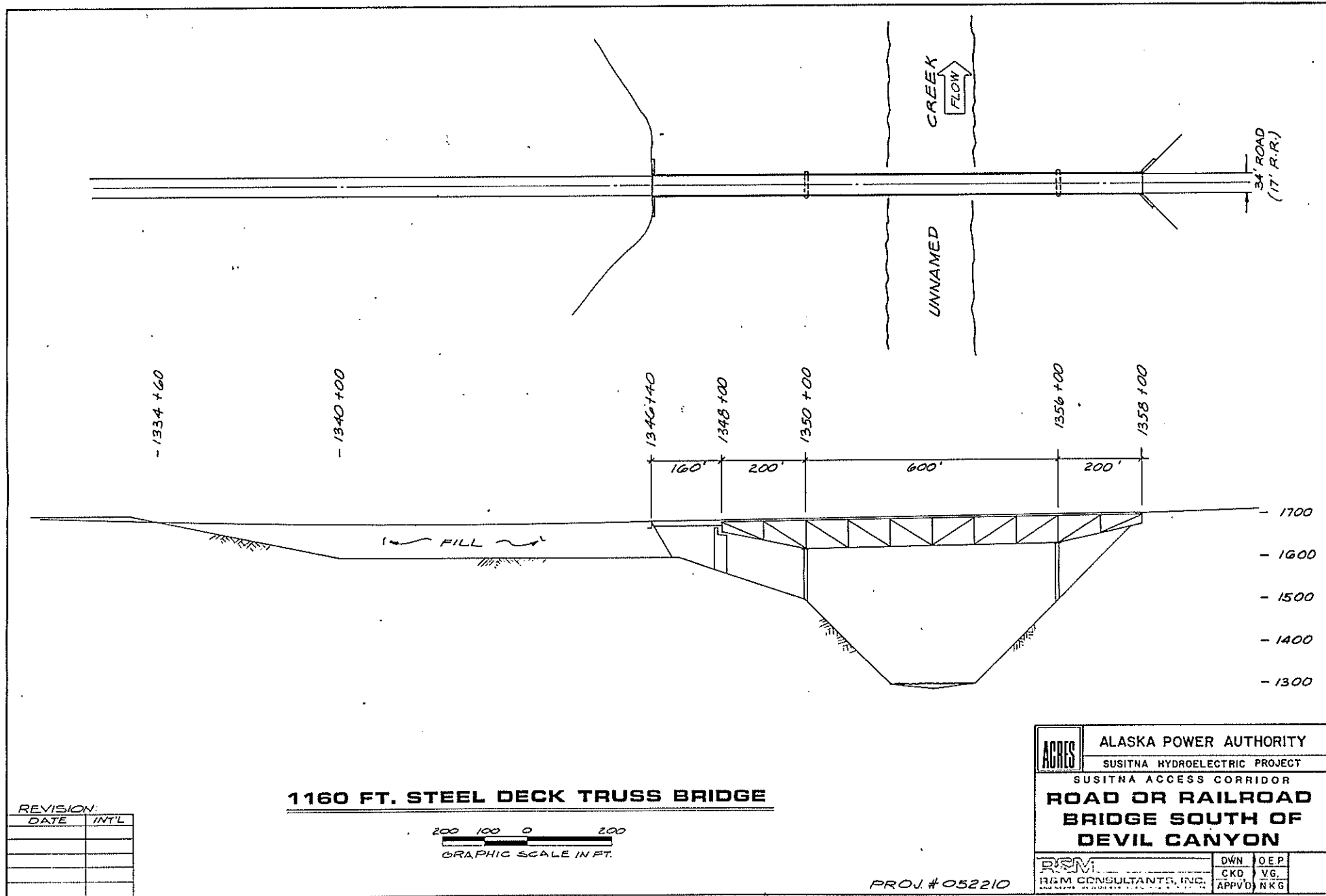
REVISION:	
DATE	INT'L

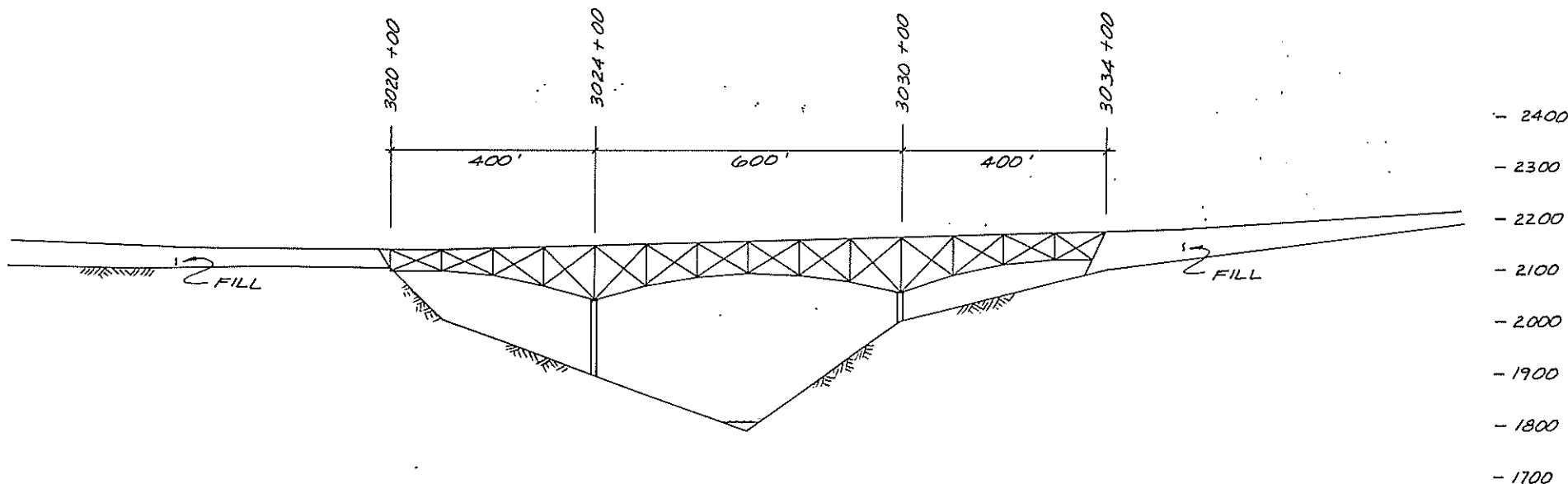
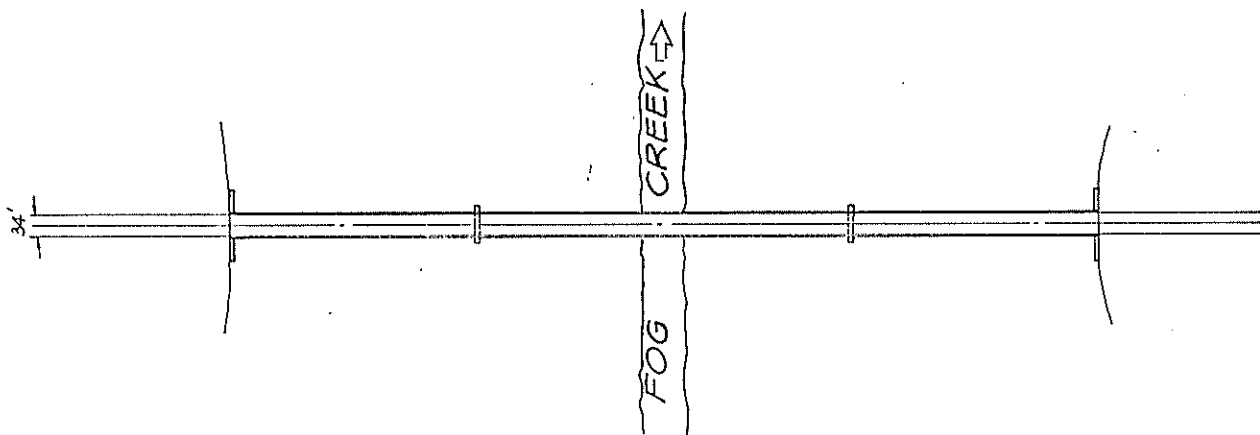
# **440 FT. CONTINUOUS WELDED PLATE GIRDER 3 SPAN BRIDGE**

50 25 0 50  
GRAPHIC SCALE IN FT.

PROJ. # 052210

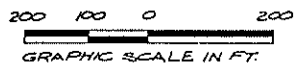
ACRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
	SUSITNA ACCESS CORRIDOR	
<b>INDIAN RIVER</b>		
<b>BRIDGE</b>		
<b>CORRIDOR # 1</b>		
R&M R&M CONSULTANTS, INC. REGISTERED PROFESSIONAL ENGINEERS ALASKA LICENSE NO. 10000	DWN	O.E.P.
	CKD	V.G.
	APP'D	N.K.S.





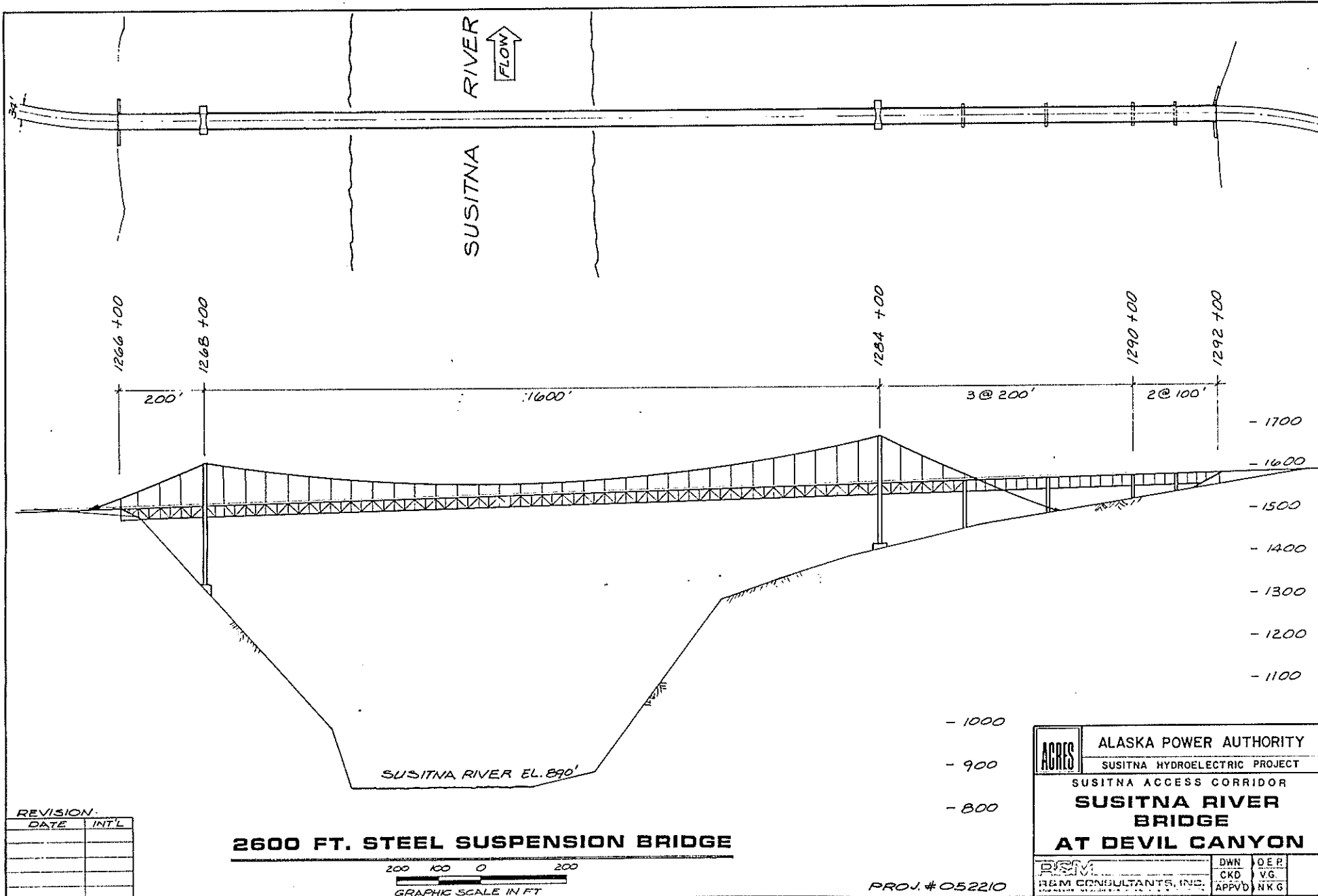
# **1400 FT. STEEL DECK TRUSS BRIDGE**

REVISION:	
DATE	INT'L



PROJ. # 052210

<b>ACRES</b>	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
SUSITNA ACCESS CORRIDOR		
<b>FOG CREEK BRIDGE</b>		
<b>REM</b> REM CONSULTANTS, INC.	DWN	O.E.P.
	CKD	V.G.
	APPVD	N.K.G.



REVISION:

DATE	INT'L

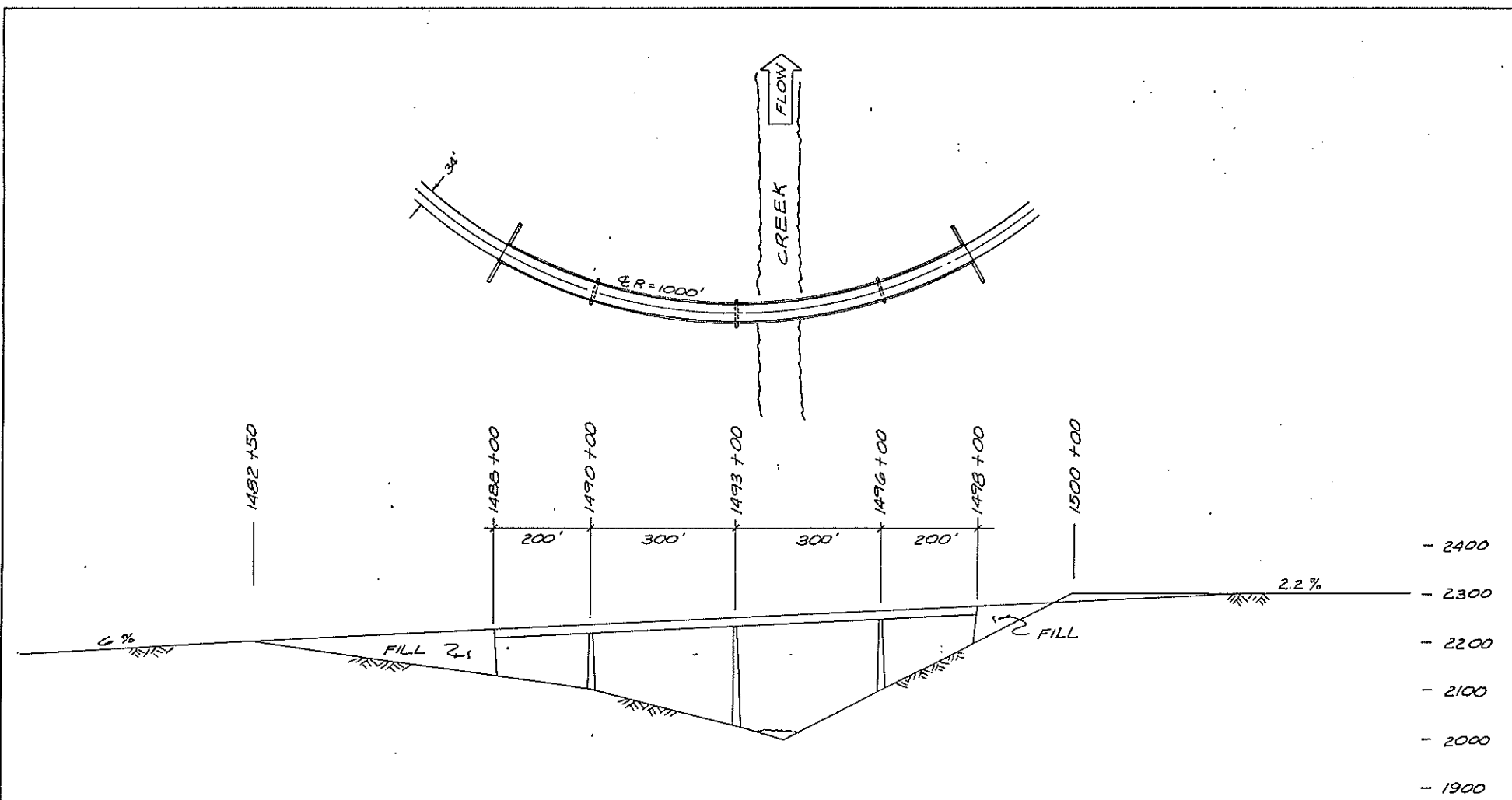
# 2600 FT. STEEL SUSPENSION BRIDGE



PROJ. # 052210

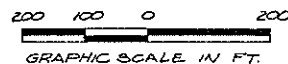
ACRES	ALASKA POWER AUTHORITY			
	SUSITNA HYDROELECTRIC PROJECT			
	SUSITNA ACCESS CORRIDOR			
<b>SUSITNA RIVER BRIDGE</b>				
<b>AT DEVIL CANYON</b>				
R&M CONSULTANTS, INC.	DWN	QEP		
	CKD	VG		
	APPVD	NKG		





# **1000 FT. STEEL BOX GIRDER BRIDGE**

REVISION:	
DATE	INTL



APRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
	SUSITNA ACCESS CORRIDOR	
<b>CORRIDOR # 2 BRIDGE</b>		
<b>SE OF DEVIL CANYON</b>		
REM	DWN CKD	DEP VG

raising the subgrade elevation above the existing ground. Stripped or waste material can go back into the borrow pits.

Up to 15% cross slope, cuts will probably not exceed 10 feet. so no quantity variations would be anticipated between frozen and unfrozen materials.

The 25%, 30%, and 35% cross slope sections indicate for unfrozen ground a + unfrozen and - unfrozen section 10 feet apart vertically with the excavation quantity balancing the fill quantities. The Frozen subgrade upper and lower limits with a maximum of 10 feet cut require borrow to balance.

On cross slopes of 40% and over, it was considered that after the 2 feet of waste excavation on the surface there would be another 3 feet of usable excavation before encountering rock excavation. In rock excavation, the frozen condition does not require the maximum 10 feet cut requirement.

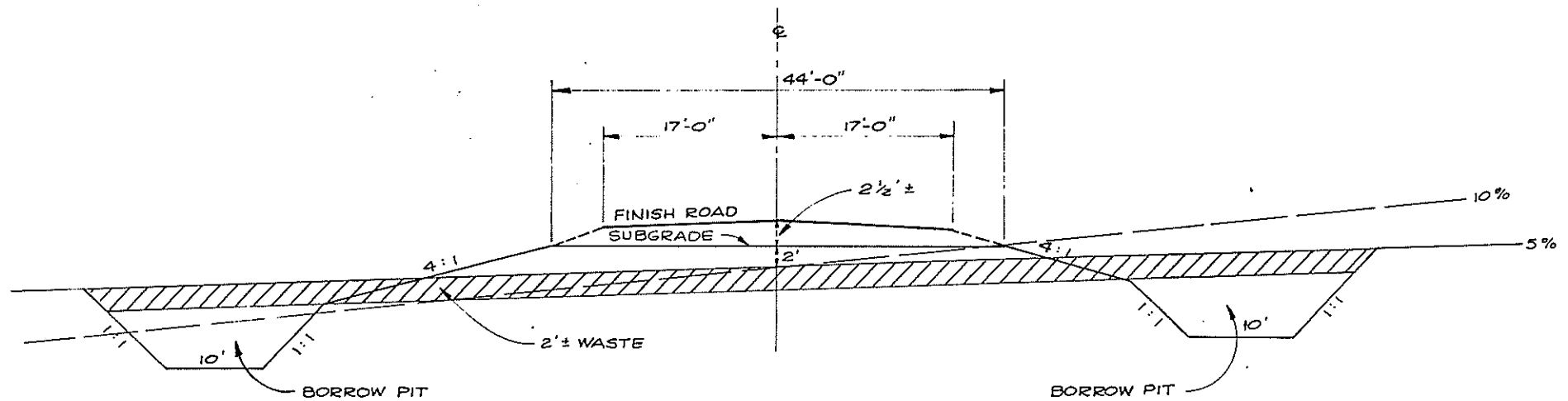
Fill slopes on the roadway sections vary depending on fill height. Cut slopes are used as  $\frac{1}{2}$ :1 in rock and  $1\frac{1}{2}$ :1 or flatter in normal materials.

Examination of the terrain unit maps provided additional information as to where rock and organics were to be encountered. Adjustments were made in rock and waste excavation from this information.

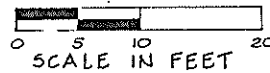
The sections used for estimating are shown in Figures F6.1-F6.16

#### F.7 - Drainage

The cross drainage requirements for the preferred alignment within each corridor were estimated. The design flows were determined



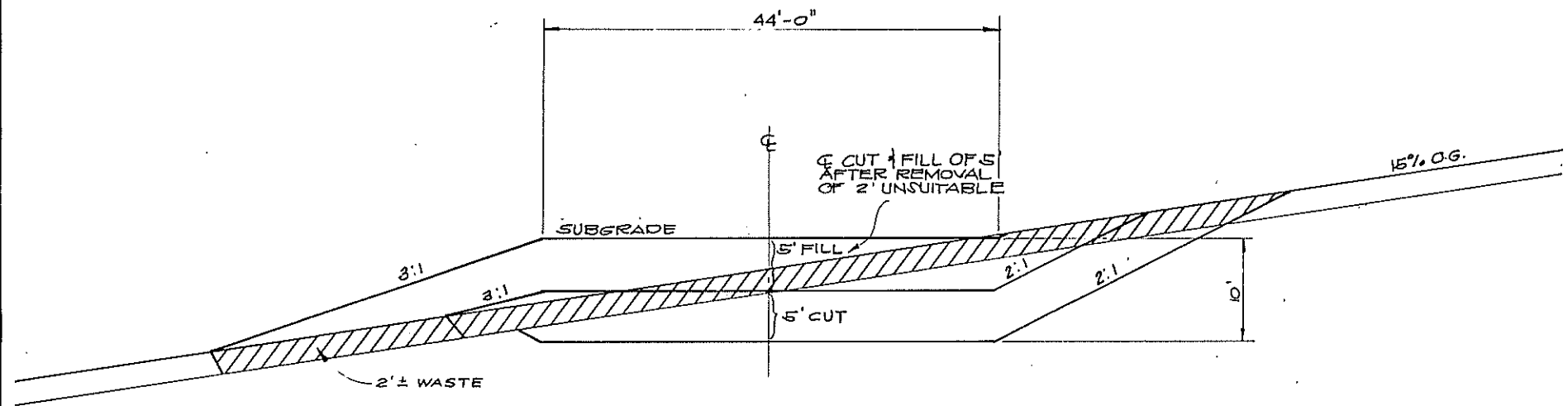
BORROW PIT SECTION  
0-10% CROSS SLOPE  
QUANTITY ESTIMATING  
CROSS SECTION



REV.	
DATE	INT.

APRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
<b>SUSITNA ACCESS ROAD</b>		
<b>TYPICAL BORROW PIT</b>		
<b>CROSS SECTION</b>		
<b>0-10% CROSS SLOPE</b>		
REM	DWN	PA
REM CONSULTANTS INC.	CKD	VG

PROJECT # 052210



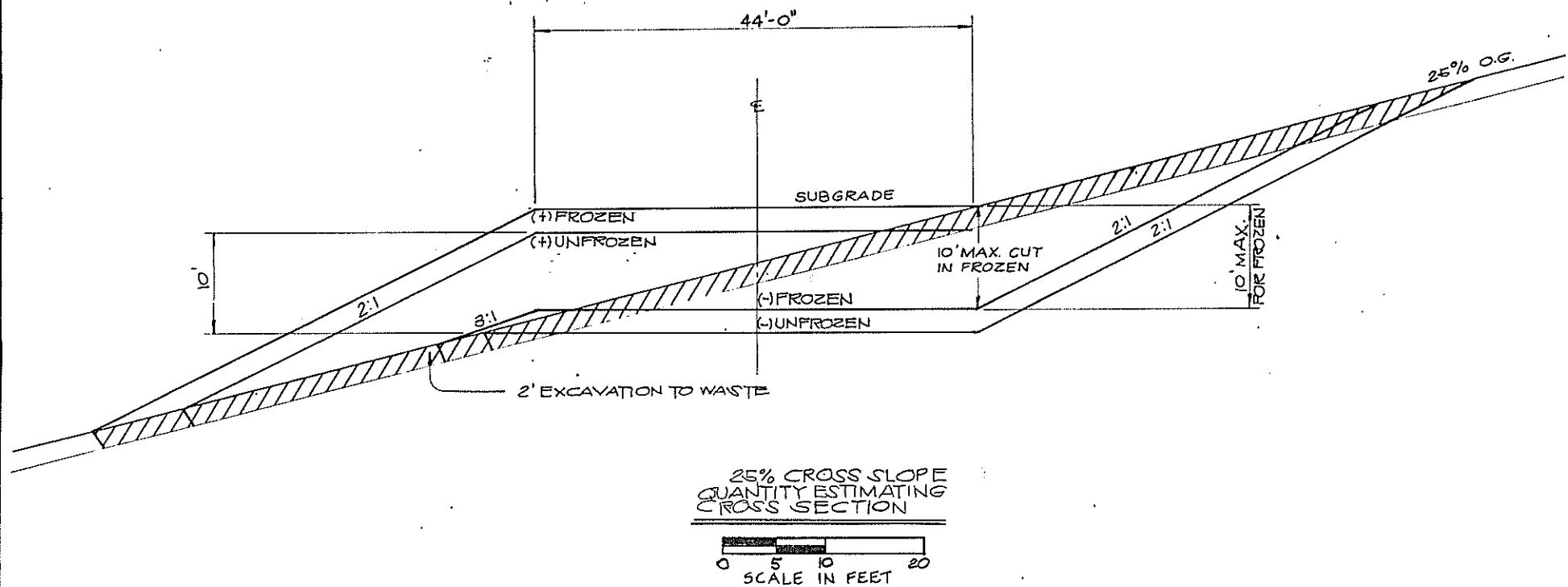
- 15% CROSS SLOPE  
QUANTITY ESTIMATING  
CROSS SECTION



REV	
DATE	INTL.

<b>ACRES</b>	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
<b>SUSITNA ACCESS ROAD</b>		
<b>ESTIMATING CROSS SECTION</b>		
<b>R&amp;M</b> R&M CONSULTANTS, INC.	DWN CKD APPV	REL VG

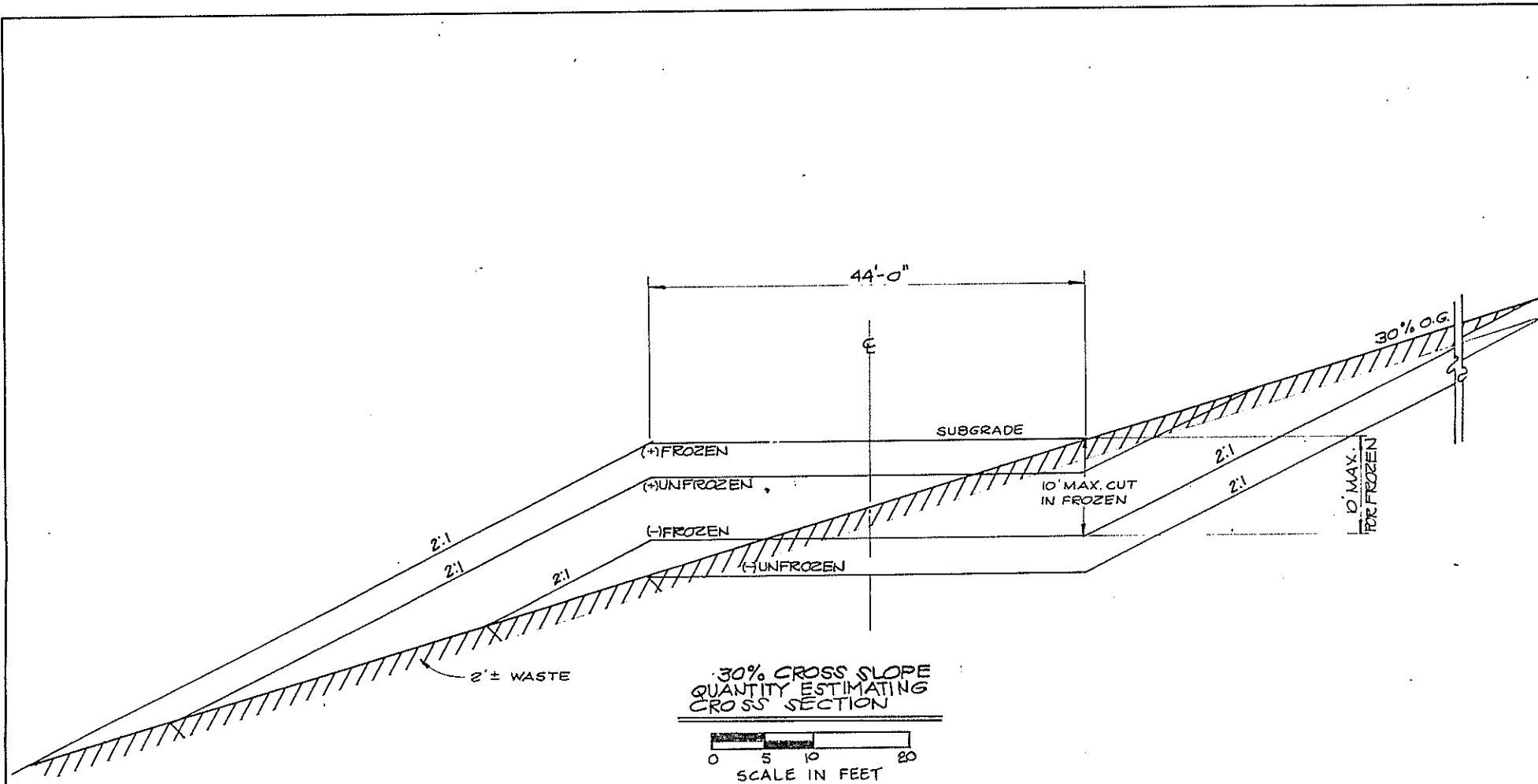
PROJ # 052210



REV.	DATE	BY

ACRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
SUSITNA ACCESS ROAD		
ESTIMATING CROSS SECTION		
R&M R&M CONSULTANTS, INC. ENGINEERS, SURVEYORS, PLANNERS, DESIGNERS	OWN	REL
	CKD	VG
APPROVED		

PROJ. # 052210

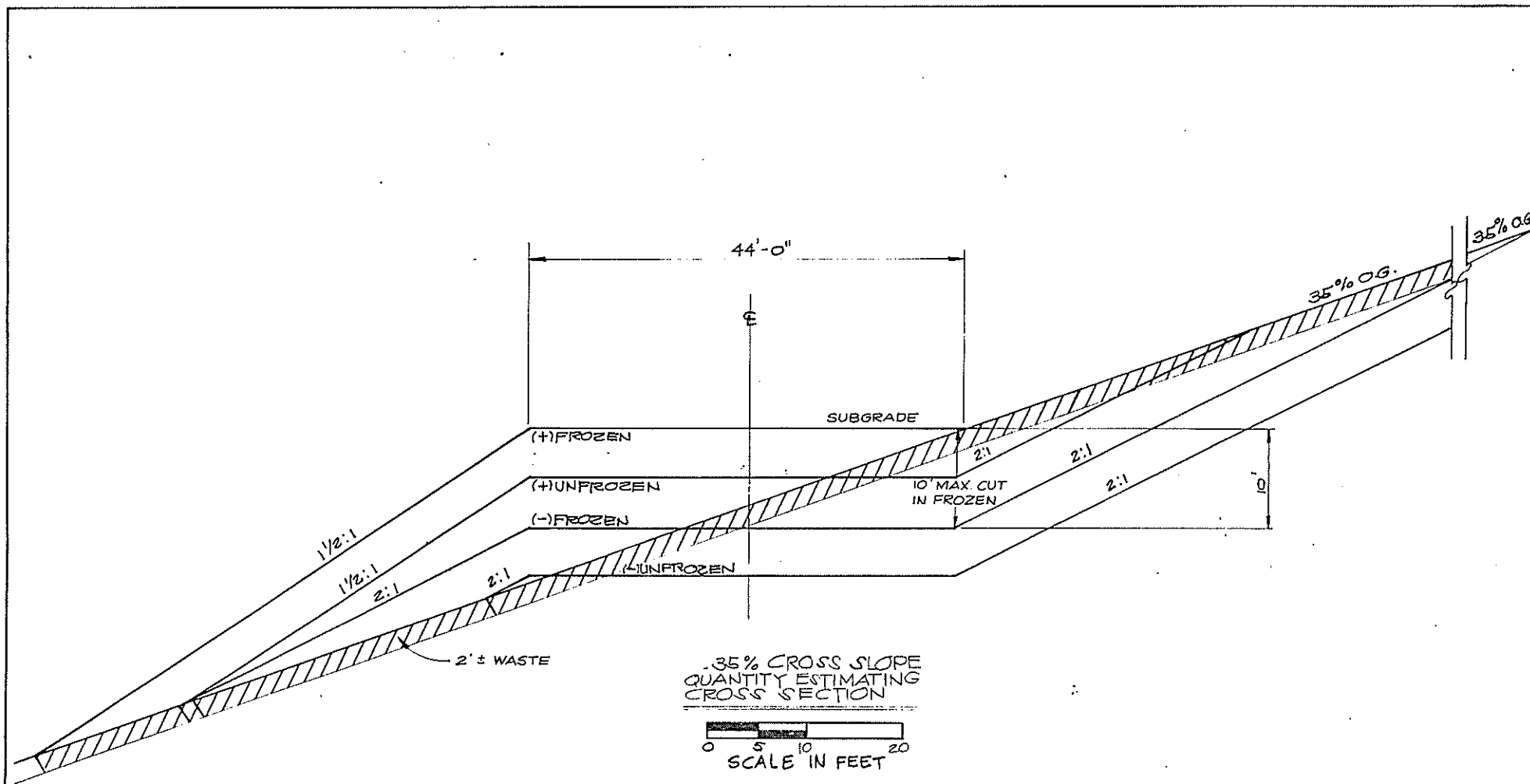


REV	DATE	INTL.

PROJ. # 052210

ACRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
SUSITNA ACCESS ROAD		
ESTIMATING CROSS SECTION		
DESIGNED BY	CKD	REL
APPROVED BY	VG	

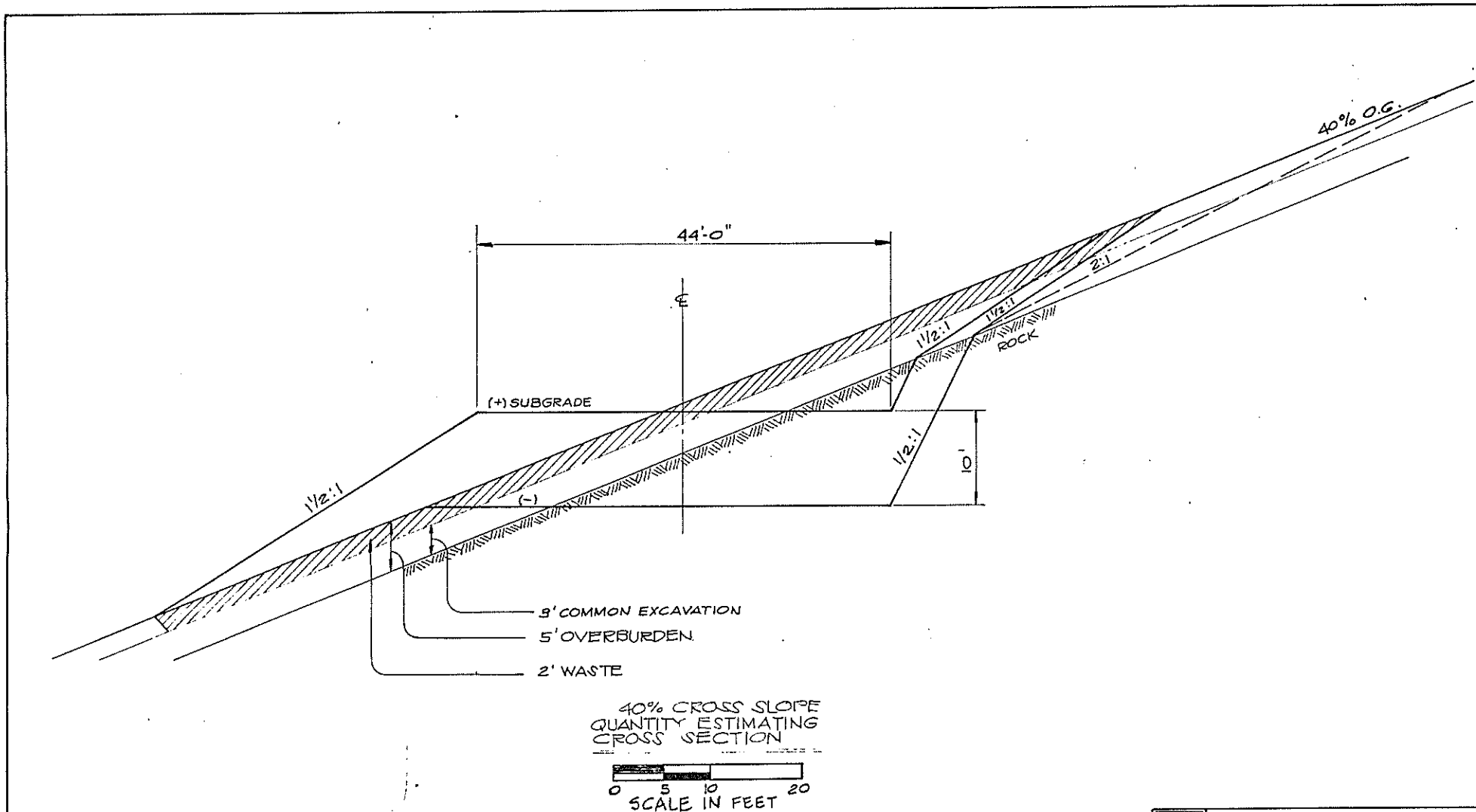




REV.	
DATE	INTL

ACRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
SUSITNA ACCESS ROAD		
ESTIMATING CROSS SECTION		
R&M R&M CONSULTANTS, INC.	DWN	REL
	CKD	VG

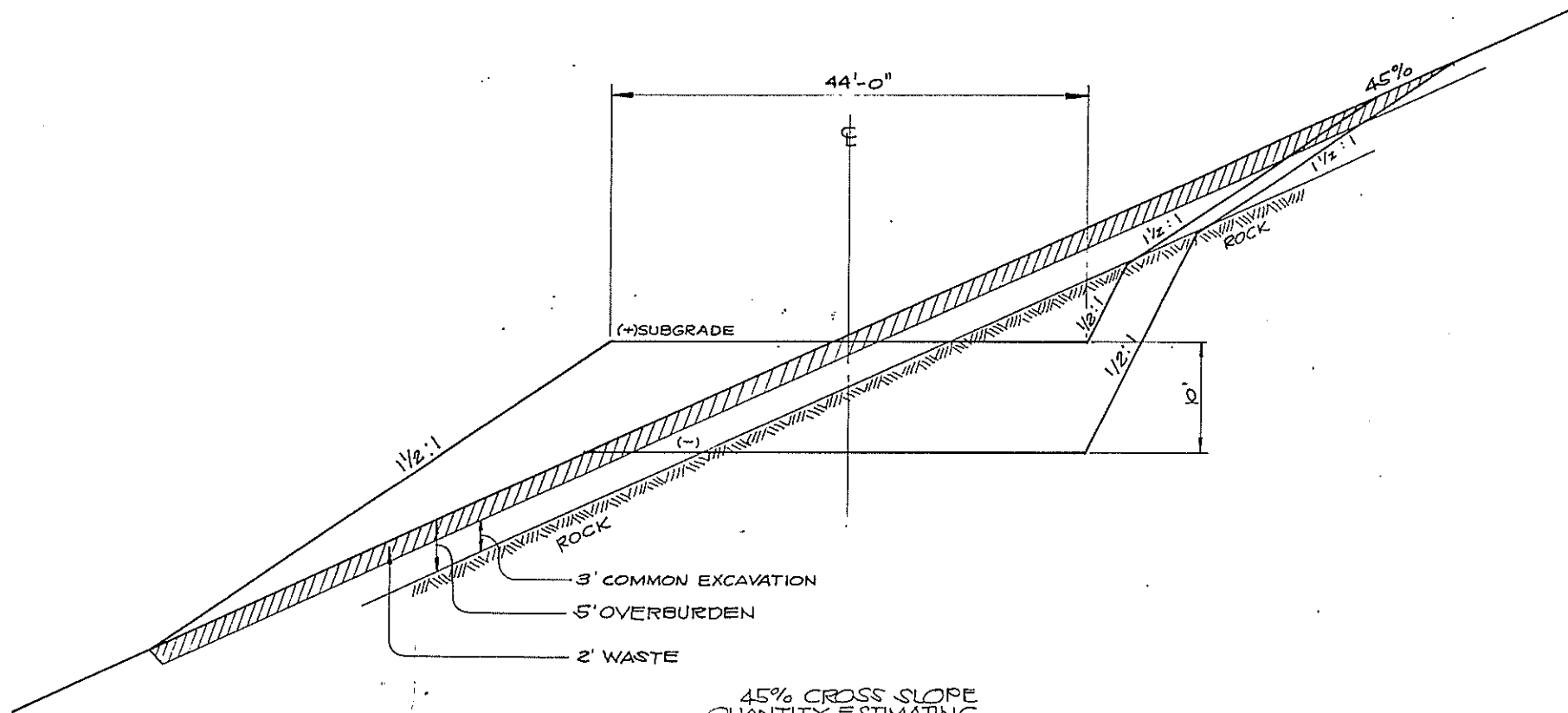
PROJ. # 052210



REV.	DATE	INTL

ACRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
SUSITNA ACCESS ROAD		
ESTIMATING CROSS SECTION		
RSM	DWN	REL
R&M CONSULTANTS, INC.	CKD	VG

PROJ. # 052210



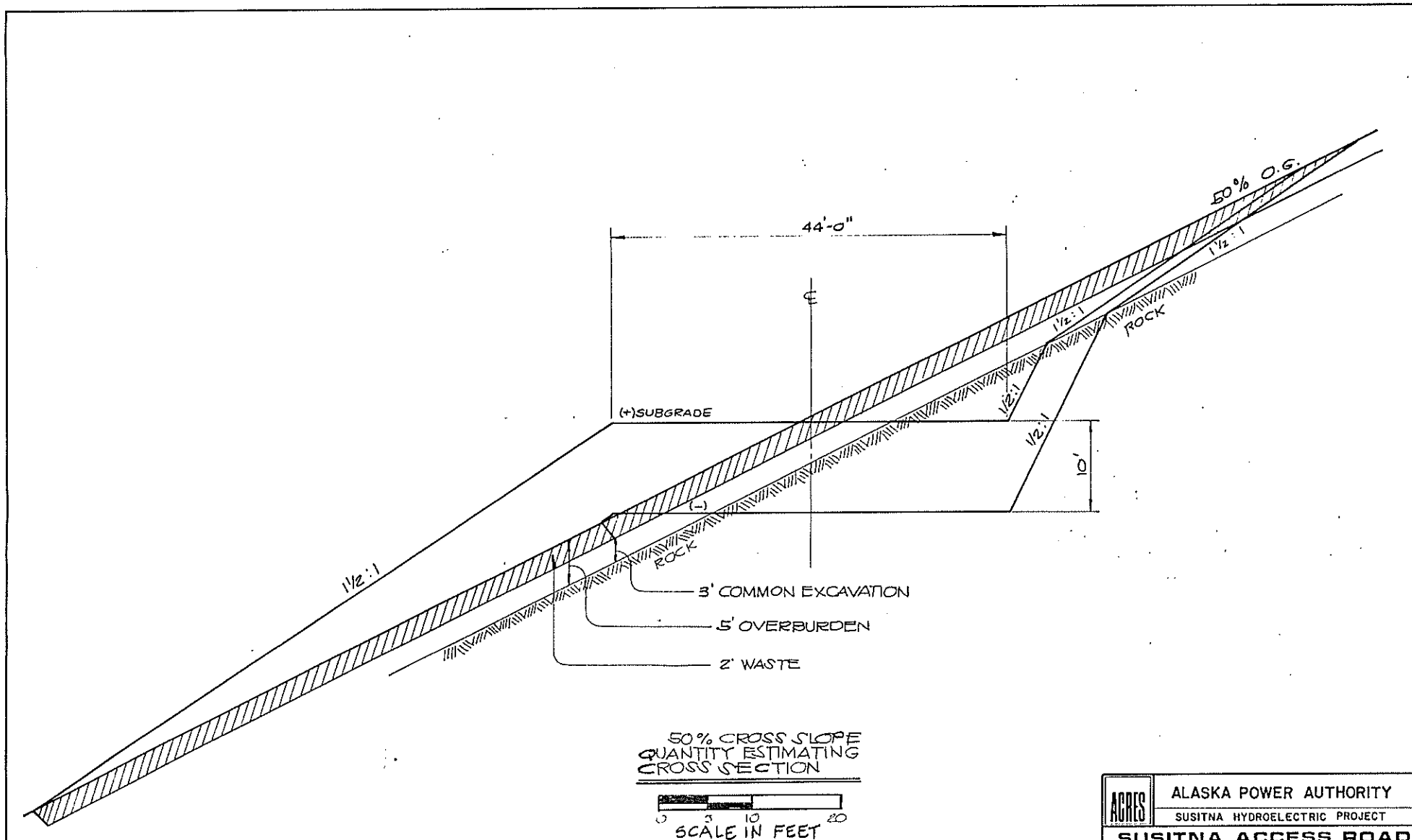
45% CROSS SLOPE  
QUANTITY ESTIMATING  
CROSS SECTION

0 5 10 20  
SCALE IN FEET

REV.	DATE	INTL.

PROJ # 052210

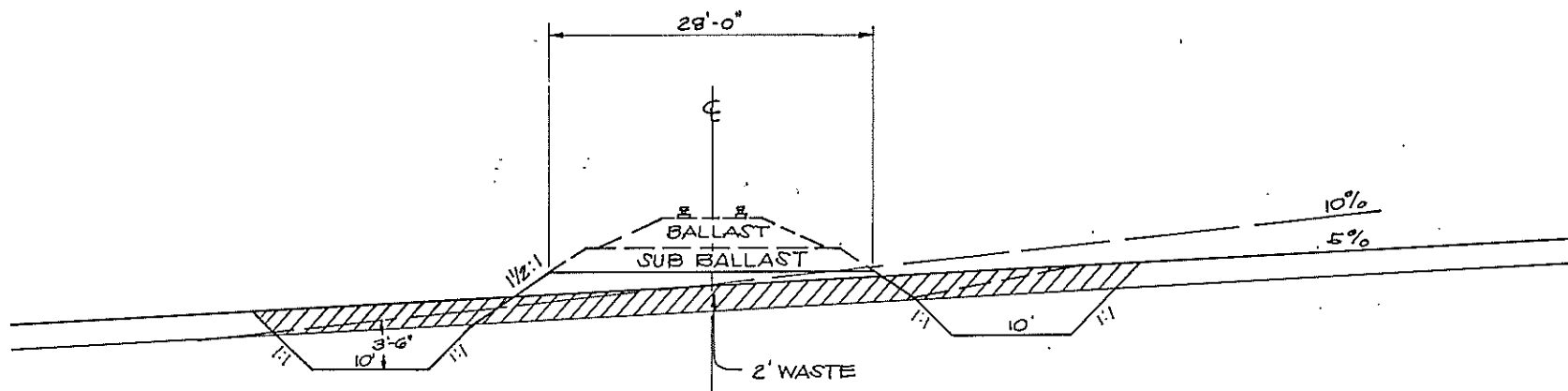
ACRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
SUSITNA ACCESS ROAD		
ESTIMATING CROSS SECTION		
R&M	DWN	REL
R&M CONSULTANTS, INC.	CKD	V G



REV.	DATE	INTL.

PROJ. # 052210

ACRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
SUSITNA ACCESS ROAD		
ESTIMATING CROSS SECTION		
REM REM CONSULTANTS, INC.	OWN CKD JEF/AL	REL V G



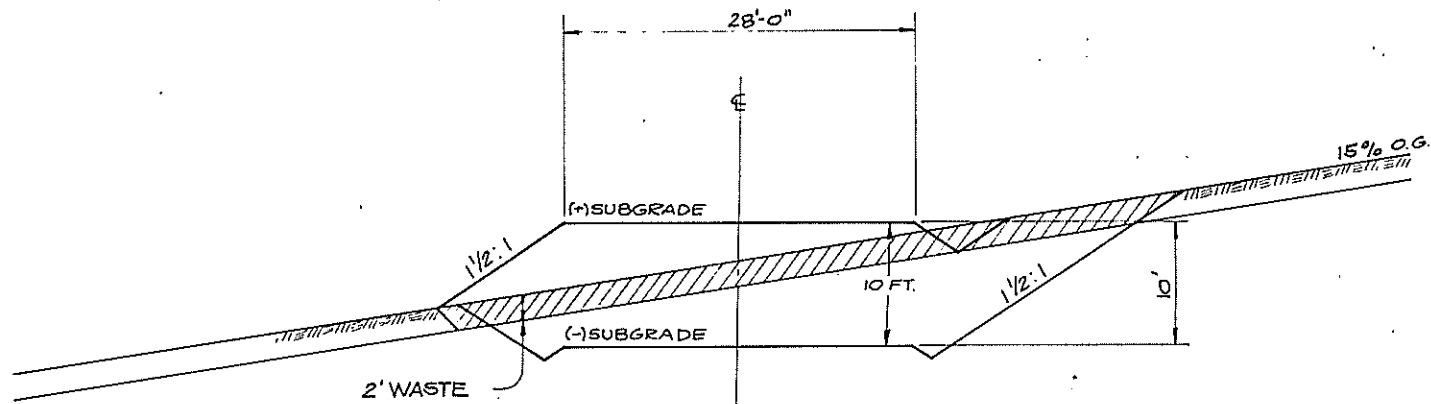
BORROW PIT SECTION  
0-10% CROSS SLOPE  
QUANTITY ESTIMATING  
CROSS SECTION



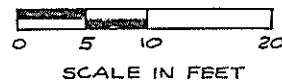
REV.	DATE	INT'L

PROJ.# 052210

ACRES	ALASKA POWER AUTHORITY			
	SUSITNA HYDROELECTRIC PROJECT			
SUSITNA ACCESS				
RAILROAD				
TYPICAL BORROW PIT				
CROSS SECTION				
0-10% CROSS SLOPE				
R&M R&M CONSULTANTS, INC.	DWN.	REL		
	CKD	VG		
	APPV	D		



15% CROSS SLOPE  
QUANTITY ESTIMATING  
CROSS SECTION

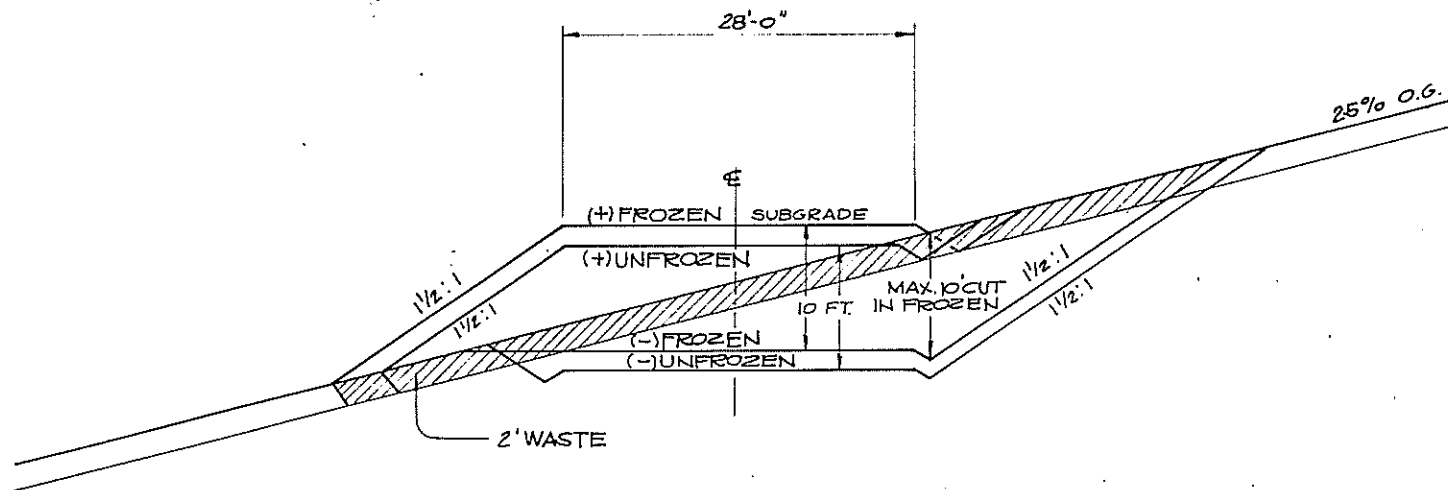


REV.	DATE	INTL

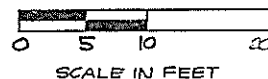
PROJ # 052210

ACRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
SUSITNA ACCESS RAILROAD ESTIMATING CROSS SECTION		
REM	DWN CKL REV	REL JG
REM CONSULTANTS, INC.		





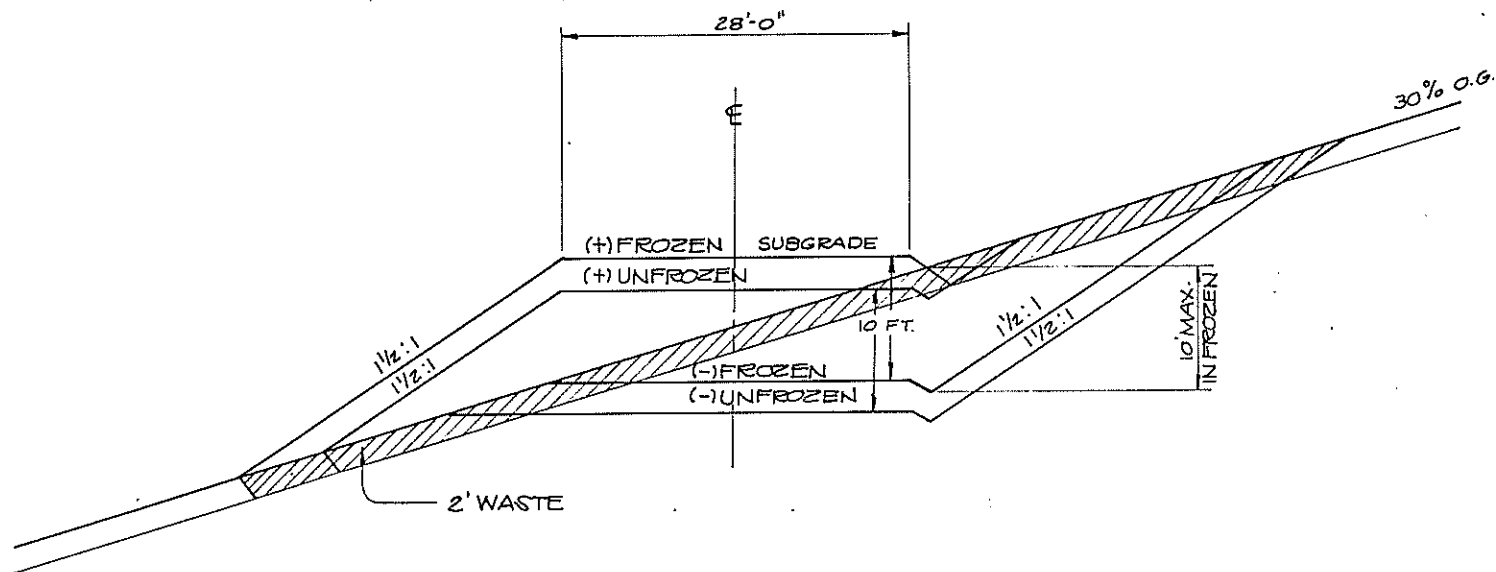
25% CROSS SLOPE  
QUANTITY ESTIMATING  
CROSS SECTION



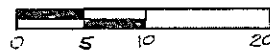
REV.	DATE	NTL

PROJ #052210

ACRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
SUSITNA ACCESS RAILROAD ESTIMATING CROSS SECTION		
REM	DWN	REL
REM CONSULTANTS, INC.	CKD	VG
	APPVD	



30% CROSS SLOPE  
QUANTITY ESTIMATING  
CROSS SECTION

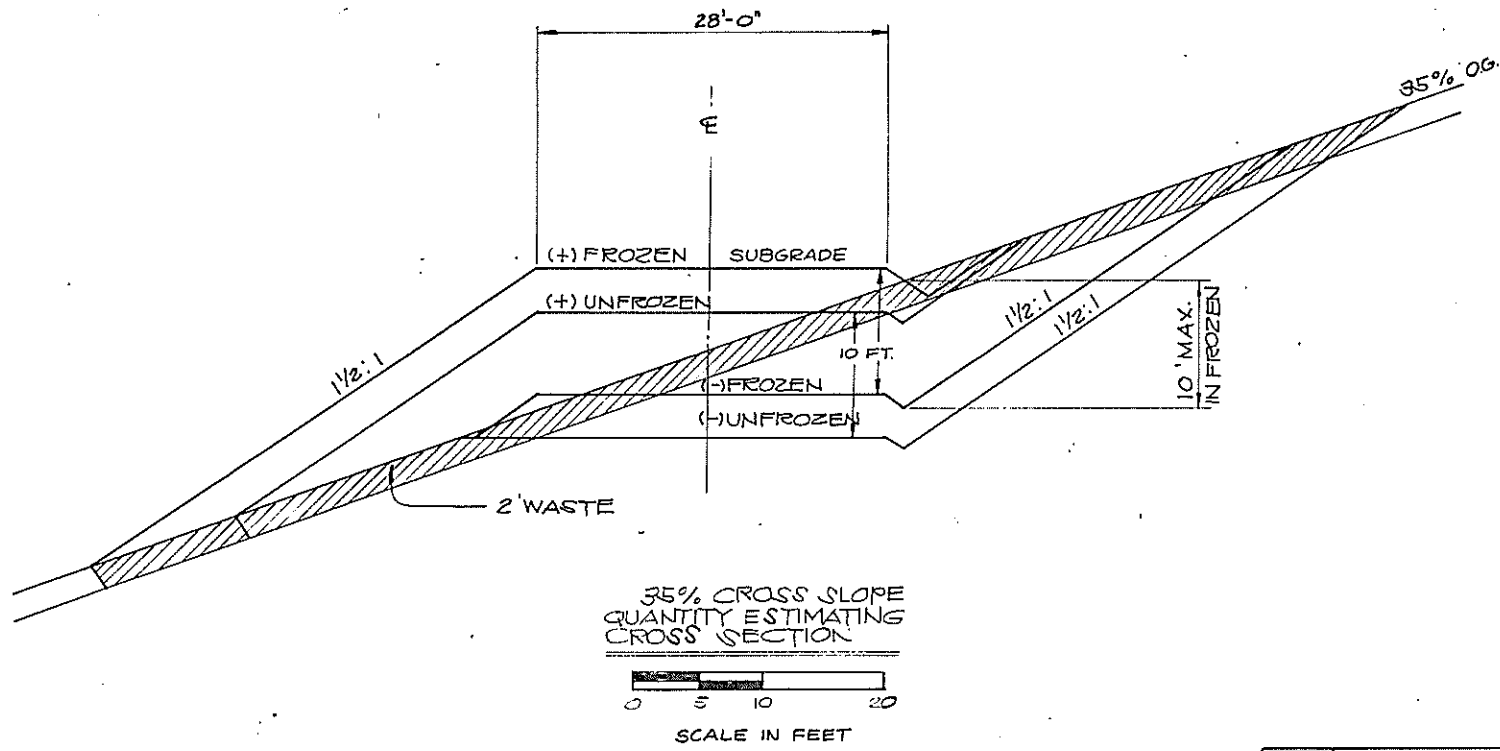


SCALE IN FEET

REV	
DATE	INTL.

<b>ACRES</b>	<b>ALASKA POWER AUTHORITY</b>	
	<b>SUSITNA HYDROELECTRIC PROJECT</b>	
<b>SUSITNA ACCESS RAILROAD ESTIMATING CROSS SECTION</b>		
<b>RSM RSM CONSULTANTS, INC.</b>	<b>OWN</b>	<b>REL</b>
	<b>CKD</b>	<b>V G</b>
	<b>APPROV</b>	

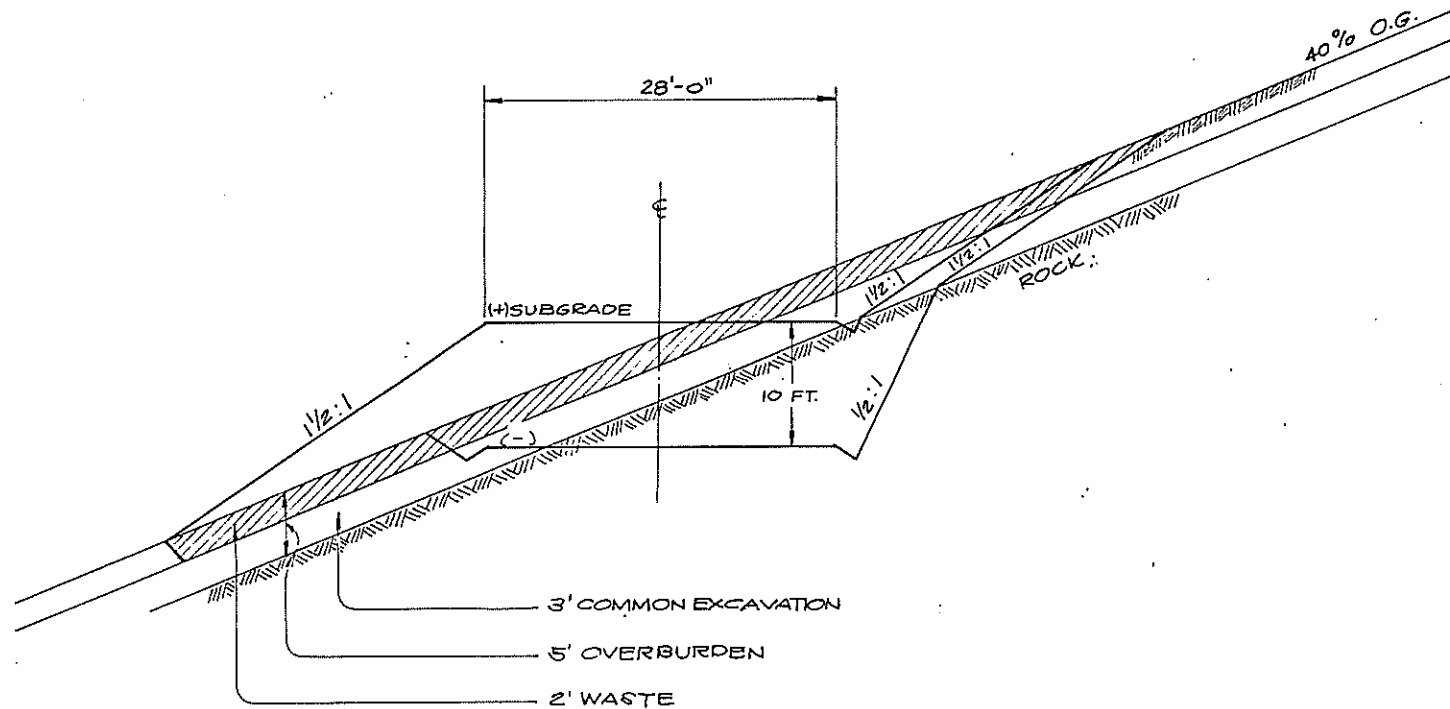
PROJ # 052213



REV.	
DATE	INT'L

PROJ # 052210

APRES	ALASKA POWER AUTHORITY	
	SUSITNA HYDROELECTRIC PROJECT	
SUSITNA ACCESS RAILROAD ESTIMATING CROSS SECTION		
R&M R&M CONSULTANTS, INC.	DWN CKD	REL VG
	APPROV.	





40% CROSS SLOPE  
QUANTITY ESTIMATING  
CROSS SECTION

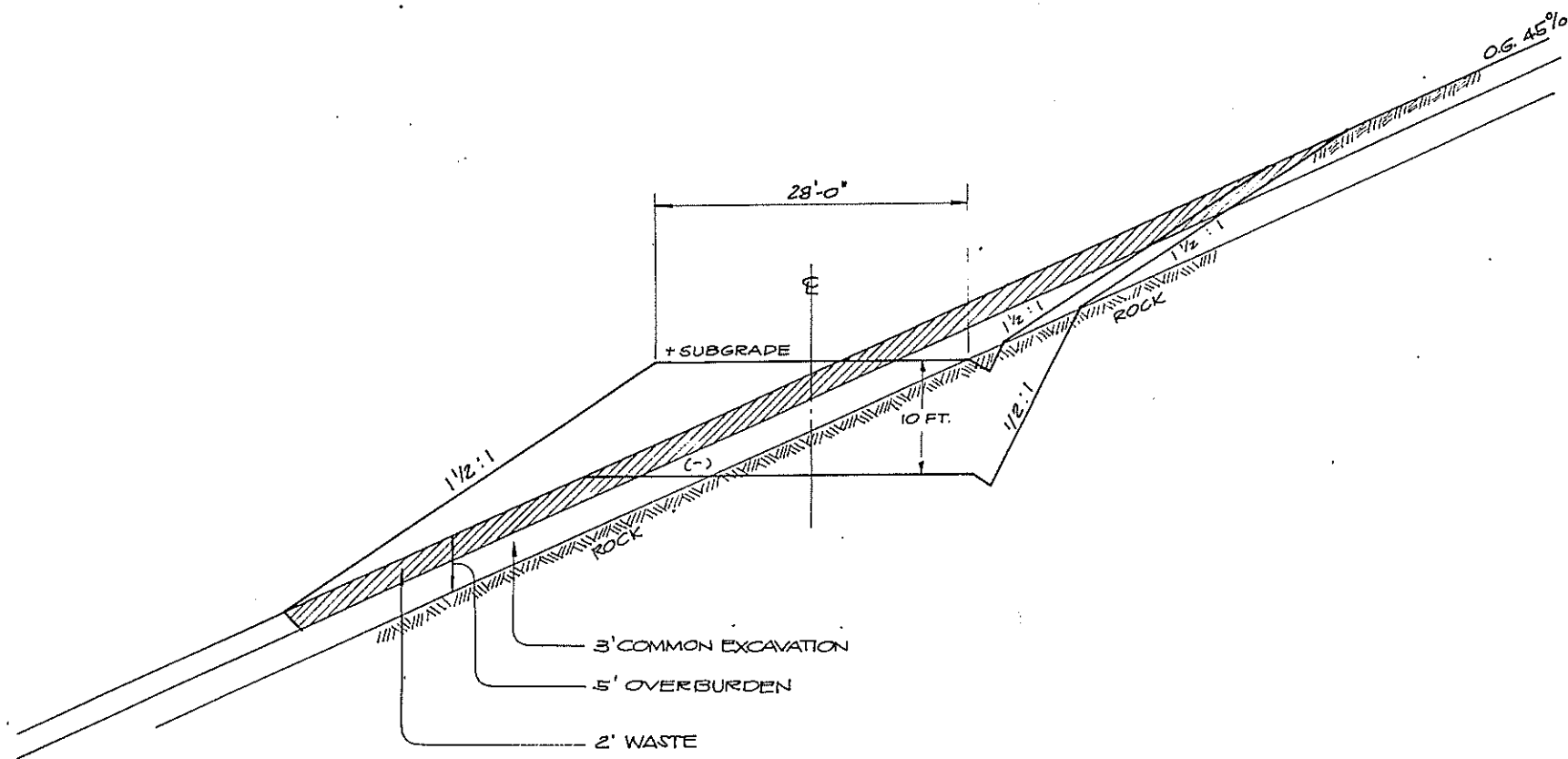


SCALE IN FEET

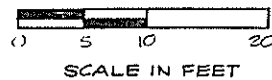
REV.	DATE	INTL.

PROJ. # 052210

	ALASKA POWER AUTHORITY		
	SUSITNA HYDROELECTRIC PROJECT		
SUSITNA ACCESS RAILROAD ESTIMATING CROSS SECTION			
 R&M CONSULTANTS, INC.	DWN	REL	
	CKD	VG	
	APPROV		



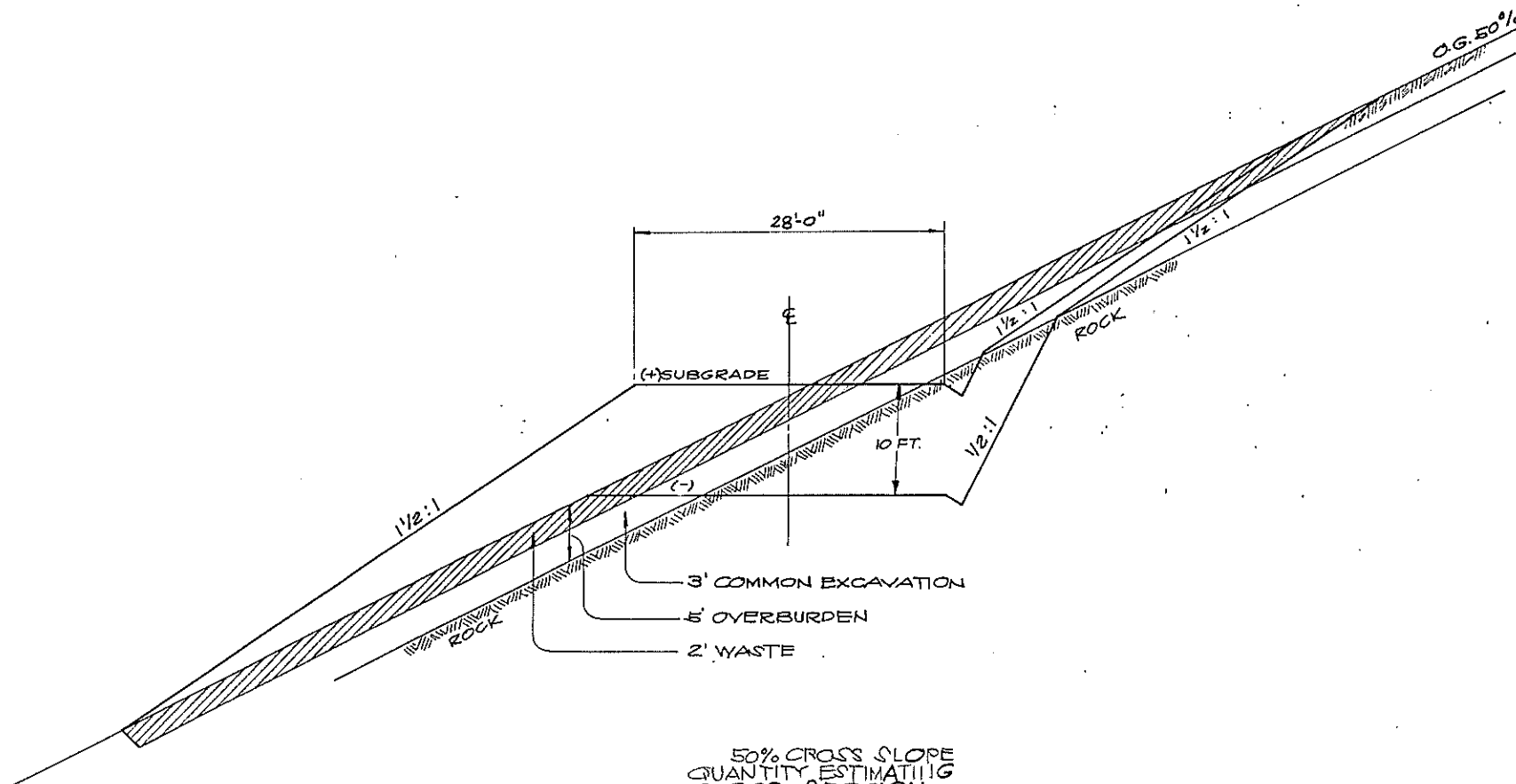
45% CROSS SLOPE  
QUANTITY ESTIMATING  
CROSS SECTION



REV.	DATE	INTL.

ACRES	ALASKA POWER AUTHORITY		
	SUSITNA HYDROELECTRIC PROJECT		
SUSITNA ACCESS RAILROAD ESTIMATING CROSS SECTION			
RSM	DWN	REL	
R&M CONSULTANTS, INC.	CKD	VG	

PM 14 05/10



50% CROSS SLOPE  
QUANTITY ESTIMATING  
CROSS SECTION



SCALE IN FEET

REV.	DATE	NTL.

PROJ # 052210

<b>ACRES</b>	<b>ALASKA POWER AUTHORITY</b>		
	<b>SUSITNA HYDROELECTRIC PROJECT</b>		
	<b>SUSITNA ACCESS</b>		
	<b>RAILROAD</b>		
	<b>ESTIMATING</b>		
<b>CROSS SECTION</b>			
<b>R&amp;M</b> R&M CONSULTANTS, INC.	OWN	REL	
	CKD	VG	
	APPV'D		



by defining the respective drainage areas on USGS quadrangle maps and applying regression equations developed by the U.S. Geologic Survey. "Flood characteristic of Alaskan Streams". Water Resources Investigation 78-129 R.D. Lamke 1979.

Culvert sizes and lengths developed by this process are shown in Table F 7.1.

TABLE F-7.1  
CULVERTS (in lineal feet)

Size DIA.	A-1 L.F.	A-2 L.F.	B-1 L.F.	B-2 L.F.	B-3 L.F.	C L.F.	R-1 L.F.	R-2 L.F.
18"	18,530	23,035	7,055	8,245	27,115	26,350	9,000	15,950
36"	300	0	100	200	200	100	200	200
42"	300	200	200	100	0	400	100	0
48"	100	0	0	0	100	600	0	100
54"	100	200	0	100	200	200	100	200
60"	400	400	100	100	100	300	100	100
72"	100	100	100	100	100	0	100	100
84"	0	100	0	0	100	200	0	100
96"	100	0	0	0	0	100	0	0
108"	0	200	0	0	0	200	0	0
120"	0	0	0	0	0	100	0	0
(1) 144"	0	100	0	0	0	0	0	0
(1) 168"	100	0	0	0	0	0	0	0

- (1) Pipes larger than 120" will be either multiplate culvert or pipe arch similar to "Armco Super Span".
- (2) 18" diameter pipes average 85' long under highway, 50' under railroad, larger pipes average 100 feet long.

#### F.8 - Consturction Cost Estimates

The construction costs estimates outlined below include mobilization, construction camps, construction survey and engineering service.

## Discussion of Bid Items

Clearing. Included is clearing and grubbing of vegetation to ten feet outside of excavation limits, and disposal of the material.

Waste Excavation. Removal and disposal of existing topsoil, muck, organics and other deliterious material.

Rock Excavation. Removal of material too hard to economically rip. Price includes placing in the fill or stock piling for later use in the structural section.

Common Excavation. All other excavation including removal and disposal or placement in fill.

Borrow. Where insufficient material is acquired for fill from common and rock excavation separate payment will be made to develop, excavate, and place material from borrow pits.

NFS Subbase. Non-frost susceptible granular material meeting standard specifications.

Grade "A" Base and D-1 Base. Granular, crushed material meeting standard specifications.

A.C. Surfacing. Bituminous concrete, including aggregate, asphalt binder, prime coat and tack coat.

Guardrail. Standard single rail guardrail.

Culverts. 18" cross culverts are figured per linear foot. Larger culverts (36" & over), for individual stream crossings are each multiplied by appropriate costs per foot, depending on diameter, and lumped into one sum. Costs includes placement, any special bedding requirements on materials, and head walls.

Fabric. Standard Mirafi or Typar filter fabric, to be placed over organics too deep to economically remove and replace.

Thaw Pipe. One thaw pipe per culvert. Price includes hangers, caps, standpipes, etc.

Topsoil and Seed. Topsoil will be manufactured from appropriate materials removed under waste excavation. Seed includes a hydroseed mixture of seed, fertilizer and lime.

Traffic Control Devices. Includes all standard signs and pavement markings, plus reflective paddle boards as delineators along the entire length of road.

Bridges. All highway bridges, regardless of type, are at present figured on the same per square foot basis. Rail bridges are also figured on a single price per square foot bases.

Rail Head. The lump sum price includes all clearing, excavation, subballast, ballast, track, switches, Grade "A" base, D-1 base, A.C. surfacing, topsoil and seeding, traffic control devices and timber crib docks as needed to complete a rail head facility on an existing track or at either damsite. The rail head includes five sidings for train make up and off loading of various types of equipment and material, two docks, a parking area for trucks, and an engine turn around. Contractor will provide his own warehouse, office, cranes, fuel facilities, cement pumps, fuel pumps and any other equipment deemed necessary.

Subballast. Granular material meeting standard specifications.

Trackage. Includes rail, ties, and ballast. Switches are considered as equivalent to 200 feet of track for the purpose of this estimate.

TABLE F-8.1

SUSITNA ACCESS CONSTRUCTION ESTIMATESSEGMENT A-1

## PARKS HIGHWAY TO DEVIL CANYON

STA 0+00 to 1,650+00 165,000 ft. = 31.25 Mi.

	<u>Quantity</u>	<u>Unit Price</u>	<u>Total</u>
Clearing	477 AC.	4,800.00	2,289,600
Waste Excavtion	1,294,200 C.Y.	4.00	5,176,800
Common Excavation	1,189,072 C.Y.	3.50	4,161,752
Rock Excavation	49,728 C.Y.	12.00	596,736
Borrow	515,600 C.Y.	5.00	2,578,000
NFS Subbase Material	321,750 C.Y.	7.00	2,252,250
Grade "A" Base Material	175,560 C.Y.	14.00	2,457,840
D-1 Base Material	73,260 Tons	18.00	1,318,680
A.C. Surfacing	67,089 Tons	66.00	4,427,874
Guardrail	17,650 L.F.	36.00	635,400
18" Culverts	18,530 L.F.	24.00	444,720
36" + Culverts	L.S.	-	254,400
Fabric	69,180 S.Y.	2.50	172,950
Thaw Pipes	20,030 L.F.	36.00	721,080
Top Soil & Seed	288 A.C.	3,000.00	864,000
Traffic Control Devices	31.25 mi.	15,000.00	468,750
Bridges	33,660 S.F.	150.00	5,049,000
Rail Head	1 ea.	5,160,000.00	<u>5,160,000</u>
TOTAL			\$39,029,832

TABLE F-8.2

SUSITNA ACCESS CONSTRUCTION ESTIMATESSEGMENT A-2

DEVIL CAYON TO WATANA (Incl. along corr. 3)  
 STA 1,650+00 to 3,828+00 217,800 ft. = 41.25 mi.

	<u>Quantity</u>	<u>Unit Price</u>	<u>Total</u>
Clearing	576 AC.	4,800.00	2,764,800
Waste Excavtion	1,536,500 C.Y.	4.00	6,146,000
Common Excavation	1,603,973 C.Y.	3.50	5,613,906
Rock Excavation	146,527 C.Y.	12.00	1,758,324
Borrow	156,700 C.Y.	5.00	783,500
NFS Subbase Material	424,710 C.Y.	7.00	2,972,970
Grade "A" Base Material	231,739 C.Y.	14.00	3,244,346
D-1 Base Material	96,704 Tons	18.00	1,740,672
A.C. Surfacing	88,557 Tons	66.00	5,844,762
Guardrail	6,050 L.F.	36.00	217,800
18" Culverts	23,035 L.F.	24.00	552,840
36" + Culverts	L.S.	-	245,000
Fabric	49,820 S.Y.	2.50	124,550
Thaw Pipes	24,335 L.F.	36.00	876,060
Top Soil & Seed	326 A.C.	3,000.00	978,000
Traffic Control Devices	41.25 mi.	15,000.00	618,750
Bridges	6,800 S.F.	150.00	<u>1,020,000</u>
TOTAL			\$35,502,280

TABLE F-8.3

SUSITNA ACCESS CONSTRUCTION ESTIMATESSEGMENT CORRIDOR #1 Alone - (295 STA of Cor #3 Included)

## PARKS HIGHWAY TO WATANA DAMSITE

STA 0+00 to 3,828+00 382,800 ft. = 72.50 mi.

	<u>Quantity</u>	<u>Unit Price</u>	<u>Total</u>
Clearing	1053 AC.	4,800.00	5,054,400
Waste Excavtion	2,830,700 C.Y.	4.00	11,322,800
Common Excavation	2,793,045 C.Y.	3.50	9,775,658
Rock Excavation	196,255 C.Y.	12.00	2,355,060
Borrow	672,300 C.Y.	5.00	3,361,500
NFS Subbase Material	746,460 C.Y.	7.00	5,225,220
Grade "A" Base Material	407,299 C.Y.	14.00	5,702,186
D-1 Base Material	169,964 Tons	18.00	3,059,352
A.C. Surfacing	155,646 Tons	66.00	10,272,636
Guardrail	23,700 L.F.	36.00	853,200
18" Culverts	41,565 L.F.	24.00	997,560
36" + Culverts	L.S.	-	499,400
Fabric	119,000 S.Y.	2.50	297,500
Thaw Pipes	44,365 L.F.	36.00	1,597,140
Top Soil & Seed	614 A.C.	3,000.00	1,842,000
Traffic Control Devices	72.50 mi.	15,000.00	1,087,500
Bridges	40,460 S.F.	150.00	6,069,000
Rail Head	1 ea.	5,160,000.00	<u>5,160,000</u>
TOTAL			\$74,532,112



TABLE F-8.4

SUSITNA ACCESS CONSTRUCTION ESTIMATESSEGMENT B-1

## PARKS HIGHWAY TO GOLD CREEK

STA 0+00 to 700+00      70,000 ft. = 13.26 Mi.

	<u>Quantity</u>	<u>Unit Price</u>	<u>Total</u>
Clearing	210 AC.	4,800.00	1,008,000
Waste Excavtion	575,480 C.Y.	4.00	2,301,920
Common Excavation	570,180 C.Y.	3.50	1,995,630
Rock Excavation	35,850 C.Y.	12.00	430,200
Borrow	126,600 C.Y.	5.00	633,000
NFS Subbase Material	136,500 C.Y.	7.00	955,500
Grade "A" Base Material	74,480 C.Y.	14.00	1,042,720
D-1 Base Material	31,080 Tons	18.00	559,440
A.C. Surfacing	28,462 Tons	66.00	1,878,492
Guardrail	9,800 L.F.	36.00	352,800
18" Culverts	7,055 L.F.	24.00	169,320
36" + Culverts	L.S.	-	42,700
Fabric	18,844 S.Y.	2.50	47,110
Thaw Pipes	7,555 L.F.	36.00	271,980
Top Soil & Seed	130 A.C.	3,000.00	390,000
Traffic Control Devices	13.26 mi.	15,000.00	198,900
Bridges	84,320 S.F.	150.00	12,648,000
Rail Head (Gold Creek)	1 ea.	5,160,000.00	<u>5,160,000</u>
TOTAL			\$30,085,712

TABLE F-8.5

SUSITNA ACCESS CONSTRUCTION ESTIMATESSEGMENT B-2

## GOLD CREEK TO DEVIL CANYON

STA 700+00 to 1,350+00 65,000 ft. = 12.31 Mi.

	<u>Quantity</u>	<u>Unit Price</u>	<u>Total</u>
Clearing	161 AC.	4,800.00	772,800
Waste Excavtion	422,890 C.Y.	4.00	1,691,560
Common Excavation	335,935 C.Y.	3.50	1,175,773
Rock Excavation	23,625 C.Y.	12.00	283,500
Borrow	445,200 C.Y.	5.00	2,226,000
NFS Subbase Material	126,750 C.Y.	7.00	887,250
Grade "A" Base Material	69,160 C.Y.	14.00	968,240
D-1 Base Material	28,860 Tons	18.00	519,480
A.C. Surfacing	26,429 Tons	66.00	1,744,314
Guardrail	6,700 L.F.	36.00	241,200
18" Culverts	8,245 L.F.	24.00	197,880
36" + Culverts	L.S.	-	50,400
Fabric	8,777 S.Y.	2.50	21,942
Thaw Pipes	8,845 L.F.	36.00	318,420
Top Soil & Seed	86 A.C.	3,000.00	258,000
Traffic Control Devices	12.31 mi.	15,000.00	184,650
Bridges	0	150.00	<u>0</u>
TOTAL			\$11,541,409

TABLE F-8.6

SUSITNA ACCESS CONSTRUCTION ESTIMATESSEGMENT B-3

## DEVIL CANYON TO WATANA

STA 1,350+00 to 3,275+00 192,500 ft. = 36.46 Mi.

	<u>Quantity</u>	<u>Unit Price</u>	<u>Total</u>
Clearing	631 AC.	4,800.00	3,028,800
Waste Excavtion	1,750,160 C.Y.	4.00	7,000,640
Common Excavation	1,564,430 C.Y.	3.50	5,475,505
Rock Excavation	246,750 C.Y.	12.00	2,961,000
Borrow	101,100 C.Y.	5.00	505,500
NFS Subbase Material	375,375 C.Y.	7.00	2,627,625
Grade "A" Base Material	204,820 C.Y.	14.00	2,867,480
D-1 Base Material	85,470 Tons	18.00	1,538,460
A.C. Surfacing	78,271 Tons	66.00	5,165,886
Guardrail	8,300 L.F.	36.00	298,800
18" Culverts	27,115 L.F.	24.00	650,760
36" + Culverts	L.S.	-	63,100
Fabric	96,541 S.Y.	2.50	241,353
Thaw Pipes	27,615 L.F.	36.00	994,140
Top Soil & Seed	410 A.C.	3,000.00	1,230,000
Traffic Control Devices	36.46 mi.	15,000.00	546,900
Bridges	121,040 S.F.	150.00	<u>18,156,000</u>
TOTAL			\$53,351,949

TABLE F-8.7

SUSITNA ACCESS CONSTRUCTION ESTIMATESSEGMENT CORRIDOR #2 - entire length

PARKS HIGHWAY TO WATANA DAMSITE

STA 0+00 to 3,275+00 3,275,00 lf. = 62.03 Mi.

	<u>Quantity</u>	<u>Unit Price</u>	<u>Total</u>
Clearing	1002 AC.	4,800.00	4,809,600
Waste Excavtion	2,748,530 C.Y.	4.00	10,994,120
Common Excavation	2,470,545 C.Y.	3.50	8,646,908
Rock Excavation	306,225 C.Y.	12.00	3,674,700
Borrow	672,900 C.Y.	5.00	3,364,500
NFS Subbase Material	638,625 C.Y.	7.00	4,470,375
Grade "A" Base Material	348,460 C.Y.	14.00	4,878,440
D-1 Base Material	145,410 Tons	18.00	2,617,380
A.C. Surfacing	133,162 Tons	66.00	8,788,692
Guardrail	24,800 L.F.	36.00	892,800
18" Culverts	42,415 L.F.	24.00	1,017,960
36 + Culverts	L.S.	-	156,200
Fabric	124,162 S.Y.	2.50	310,405
Thaw Pipes	44,015 L.F.	36.00	1,584,540
Top Soil & Seed	626 A.C.	3,000.00	1,878,000
Traffic Control Devices	62.03 mi.	15,000.00	930,450
Bridges	205,360 S.F.	150.00	30,804,000
Rail Head (Gold Creek)	1 ea.	5,160,000.00	<u>5,160,000</u>
TOTAL			\$94,979,070

TABLE F-8.8

SUSITNA ACCESS CONSTRUCTION ESTIMATESSEGMENT C = CORRIDOR 3DENALI HIGHWAY TO WATANA

STA 0+00 to 2,340+00      234,000 Lf. = 44.32 Mi.

This estimate includes upgrading and paving of  $\pm$  25 miles of Denali Highway.

	<u>Quantity</u>	<u>Unit Price</u>	<u>Total</u>
Clearing	800 AC.	4,800.00	3,840,000
Waste Excavtion	2,245,400 C.Y.	4.00	8,981,600
Common Excavation	2,450,800 C.Y.	3.50	8,577,800
Rock Excavation	41,800 C.Y.	12.00	501,600
Borrow	20,000 C.Y.	5.00	100,000
NFS Subbase Material	470,000 C.Y.	7.00	3,290,000
Grade "A" Base Material	300,000 C.Y.	14.00	4,200,000
D-1 Base Material	162,500 Tons	18.00	2,925,000
A.C. Surfacing	148,813 Tons	66.00	9,821,658
Guardrail	4,200 L.F.	36.00	151,200
18" Culverts	30,350 L.F.	24.00	728,400
36" + Culverts	L.S.	-	450,000
Fabric	12,907 S.Y.	2.50	32,268
Thaw Pipes	28,650 L.F.	36.00	1,031,400
Top Soil & Seed	514 A.C.	3,000.00	1,542,000
Traffic Control Devices	69.32 mi.	15,000.00	1,039,800
Bridges	0	150.00	0
Rail Head (Cantwell)	1 ea.	5,160,000.00	<u>5,160,000</u>
TOTAL			\$52,372,726

Note: This estimate includes quantities for upgrading and paving Denali Highway from Cantwell to STA. 0+00 on Segment C. The subtotal for just the Denali Highway is \$7,307,762.

TABLE F-8.9

SUSITNA ACCESS CONSTRUCTION ESTIMATESSEGMENT R-1

RAILROAD - GOLD CREEK TO DEVIL CANYON

STA 490+00 to 1,350+00      86,000 Lf = 16.29 Mi.

	<u>Quantity</u>	<u>Unit Price</u>	<u>Total</u>
Clearing	156 AC.	4,800.00	748,800
Waste Excavtion	376,480 C.Y.	4.00	1,505,920
Common Excavation	335,320 C.Y.	3.50	1,173,620
Rock Excavation	2,200 C.Y.	12.00	26,400
Borrow	108,500 C.Y.	5.00	542,500
18" Culverts	9,000 L.F.	24.00	216,000
36" + Culverts	L.S.	-	93,100
Fabric	3,121 S.Y.	2.50	7,803
Thaw Pipes	10,100 L.F.	36.00	363,600
Top Soil & Seed	101 A.C.	3,000.00	303,000
Bridges	0 S.F.	300.00	0
Subballast	166,667 yds.	7.00	1,166,669
Trackage (Inchl. siding and 3 switches	90,600 L.F.	120.00	10,872,000
Railhead (Devil Canyon)	1 ea.	5,160,000.00	<u>5,160,000</u>
TOTAL			\$22,179,412



TABLE F-8.10

SUSITNA ACCESS CONSTRUCTION ESTIMATESSEGMENT R-2

## DEVIL CANYON TO WATANA

STA 1,350 to 3,545+00      219,500 L.F. = 41.57 Mi.

	<u>Quantity</u>	<u>Unit Price</u>	<u>Total</u>
Clearing	461 AC.	4,800.00	2,212,800
Waste Excavtion	1,162,740 C.Y.	4.00	4,650,960
Common Excavation	722,200 C.Y.	3.50	2,527,700
Rock Excavation	168,960 C.Y.	12.00	2,027,520
Borrow	29,000 C.Y.	5.00	145,000
18" Culverts	15,950 L.F.	24.00	382,800
36" + Culverts	L.S.	-	63,100
Fabric	65,378 S.Y.	2.50	163,445
Thaw Pipes	16,450 L.F.	36.00	592,200
Top Soil & Seed	320 A.C.	3,000.00	960,000
Bridges	41,820 S.F.	300.00	12,546,000
Subballast	421,296 C.Y.	7.00	2,949,072
Trackage (Inchl. 2 sid-			
ings and 4 switches	228,300 L.F.	120.00	27,396,000
Railhead (Watana)	1 ea.	5,160,000.00	<u>5,160,000</u>
TOTAL			\$61,776,597

TABLE F-8.11

SUSITNA ACCESS CONSTRUCTION ESTIMATESSEGMENT Railroad (entire corridor)

## GOLD CREEK TO DEVIL CANYON

STA 490+00 to 3,545+00      305,500 L.F. = 57.86 Mi.

	<u>Quantity</u>	<u>Unit Price</u>	<u>Total</u>
Clearing	618 AC.	4,800.00	2,961,600
Waste Excavtion	1,539,220 C.Y.	4.00	6,156,880
Common Excavation	1,057,520 C.Y.	3.50	3,701,320
Rock Excavation	171,160 C.Y.	12.00	2,053,920
Borrow	137,500 C.Y.	5.00	687,500
18" Culverts	24,950 L.F.	24.00	598,800
36" + Culverts	L.S.	-	156,200
Fabric	68,499 S.Y.	2.50	171,248
Thaw Pipes	26,550 L.F.	36.00	955,800
Top Soil & Seed	421 A.C.	3,000.00	1,263,000
Bridges	41,820 S.F.	300.00	12,546,000
Subballast	587,963 C.Y.	7.00	4,115,741
Trackage (Inchl. 2 sid- ings and 4 switches	318,900 L.F.	120.00	38,268,000
Railhead (at each dam)	2 ea.	5,160,000.00	<u>10,320,000</u>
TOTAL			\$83,956,009

TABLE F-8.12  
SUSITNA D&C COSTS

	<u>A-1</u>	<u>A-2</u>	<u>A(#1)</u>
SUBTOTAL - ITEMIZED CONSTR. COST = X	\$39,029,832	\$35,502,280	\$74,532,112
Mobilization = .1X	3,902,983	3,550,228	7,453,211
Surveys = .1X	3,902,983	3,550,228	7,453,211
Camp = .1X	3,902,983	3,550,228	7,453,211
Contingency = .2X	<u>7,805,966</u>	<u>7,100,456</u>	<u>14,906,422</u>
 TOTAL CONSTRUCTION COST = 1.5X	 48,544,747	 53,253,420	 111,798,167
 Design Fee = F = 5% Constr. Cost = .075X	 2,927,237	 2,662,671	 5,558,908
Design Survey = .10F = .0075X	292,723	266,267	558,991
Design Soils = .15F = .01125X	439,086	399,400	838,486
Construction Inspection = .80F = .06X	2,341,790	2,130,137	4,471,927
Quality Control = .15F = .01125X	<u>439,086</u>	<u>399,400</u>	<u>838,486</u>
 TOTAL DESIGN COSTS = .165X	 \$ 6,439,922	 \$ 5,856,876	 \$ 12,297,798
 TOTAL D&C COSTS = 1.665X	 \$64,984,669	 \$59,111,296	 \$124,095,965

TABLE F-8.13  
SUSITNA D&C COSTS

	<u>B-1</u>	<u>B-2</u>	<u>B-3</u>	<u>B(#2)</u>
SUBTOTAL - ITEMIZED CONSTR. COST = X	\$30,085,712	\$11,541,409	\$53,351,949	\$ 94,979,070
Mobilization = .1X	3,008,571	1,154,141	5,335,195	9,497,907
Surveys = .1X	3,008,571	1,154,141	5,335,195	9,497,907
Camp = .1X	3,008,571	1,154,141	5,335,195	9,497,907
Contingency = .2X	<u>6,017,142</u>	<u>2,308,282</u>	<u>10,670,390</u>	<u>18,995,814</u>
TOTAL CONSTRUCTION COST = 1.5x	45,128,568	17,312,114	80,027,924	142,468,605
Design Fee = F = 5% Total Constr. Cost = .075x	2,256,428	865,606	4,001,396	7,123,430
Design Survey = .10F = .0075x	225,643	86,561	400,140	712,343
Design Soils = .15F = .01125x	338,464	129,841	600,209	1068,515
Construction Inspection = .80F = .06x	1,805,143	692,484	3,201,117	5,698,744
Quality Control = .15F = .01125x	<u>338,464</u>	<u>129,841</u>	<u>600,209</u>	<u>1,068,514</u>
TOTAL DESIGN COSTS = .165x	\$ 4,964,142	\$ 1,904,332	\$ 8,803,071	\$ 15,671,547
TOTAL D&C COSTS = 1.665x	\$50,092,710	\$19,216,446	\$88,830,995	\$158,140,152

TABLE F-8.14  
SUSITNA D&C COSTS

	<u>C</u>
SUBTOTAL - ITEMIZED CONSTR. COST = X	\$52,372,726
Mobilization = .1X	5,237,273
Surveys = .1X	5,237,273
Camp = .1X	5,237,273
Contingency = .2X	<u>10,474,545</u>
 TOTAL CONSTRUCTION COST = 1.5X	 78,559,090
 Design Fee = F = 5% Constr. Cost = .075X	 3,927,955
Design Survey = .10F = .0075X	392,795
Design Soils = .15F = .01125X	589,193
Construction Inspection = .80F = .06X	3,142,364
Qual. Control = .15F = .01125X	<u>589,193</u>
 TOTAL DESIGN COSTS = .165X	 \$ 8,641,500
 TOTAL D&C COSTS = 1.665X	 \$87,200,590

TABLE F-8.15

## SUSITNA D&amp;C COSTS

	<u>R-1</u>	<u>R-2</u>	<u>R(RR)</u>
SUBTOTAL - ITEMIZED CONSTR. COST = X	\$22,179,412	\$ 61,776,597	\$ 83,956,009
Mobilization = .1X	2,217,941	6,177,660	8,395,601
Surveys = .1X	2,217,941	6,177,660	8,395,601
Camp = .1X	2,217,941	6,177,660	8,395,601
Contingency = .2X	<u>4,435,882</u>	<u>12,355,319</u>	<u>16,791,202</u>
 TOTAL CONSTRUCTION COST = 1.5x	 33,269,117	 92,664,896	 125,934,014
 Design Fee = F = 5% Constr. Cost = .075x	 1,663,456	 4,633,245	 6,296,701
Design Survey = .10F = .0075x	166,346	463,324	629,670
Design Soils = .15F = .01125x	249,518	694,987	944,505
Construction Inspection = .80F = .06x	1,330,765	3,706,596	5,037,361
Quality Control = .15F = .01125x	<u>249,518</u>	<u>694,987</u>	<u>944,505</u>
 TOTAL DESIGN COSTS	 \$ 3,659,603	 \$10,193,139	 \$ 13,852,742
 TOTAL D&C COSTS	 \$36,928,720	 \$102,858,034	 \$139,786,755



## F.9 - Maintenance Costs

The cost of maintaining the transportation facilities can be significant over a period of years. These costs are tabulated below based on Department of Transportation and Public Facilities average annual costs of \$10,000 per month.

TABLE F-9.1  
MAINTENANCE COSTS

<u>Plan</u>	<u>Section</u>	<u>Factor</u>	<u>Length</u>	<u>Annual Cost</u>	<u>Years Used</u>	<u>Total Cost</u>
1	B-1	1.0	13.26	\$132,600	15	\$1,989,000
	B-2	1.2	12.31	147,720	15	2,215,800
	B-3	1.3	36.46	473,980	8	<u>3,791,840</u>
						\$7,996,640
2	R-1	0.5	16.29	81,450	15	\$1,221,750
	R-2	0.7	41.57	290,990	8	<u>2,327,920</u>
						\$3,549,670
3	B-1	1.0	13.26	132,600	7	\$ 928,200
	B-2	1.2	12.31	147,720	7	1,034,040
	C	0.8	44.32	354,560	8	2,836,480
	Denali Hwy.	0.8	21.00	168,000	8	<u>1,344,000</u>
						\$6,142,720
4	C	0.8	44.32	354,560	8	\$2,836,480
	Denali Hwy.	0.8	21.00	168,000	8	1,344,000
	R-1	0.5	16.29	81,450	7	<u>570,150</u>
						\$4,750,630
5	B-1	1.0	13.26	132,600	15	\$1,989,000
	B-2	1.2	12.31	147,720	15	2,215,800
	A-2	1.0	41.25	412,500	8	<u>3,300,000</u>
						\$7,504,800
6	C	0.8	44.32	354,560	8	\$2,836,480
	Denali Hwy.	0.8	21.00	168,000	8	1,344,000
	R-1	0.5	16.29	81,450	7	570,150
	A-2	1.0	41.25	412,500	7	<u>2,887,500</u>
						\$7,638,130

7	C	0.8	44.32	354,560	8	\$2,836,480
	Denali Hwy.	0.8	21.00	168,000	8	1,334,000
	B-1	1.0	13.26	132,600	7	928,200
	B-2	1.2	12.31	147,720	7	1,034,040
	A-2	1.0	41.25	412,500	7	<u>2,887,500</u>
						\$9,030,220
8	B-2	1.2	12.31	147,720	15	\$2,215,800
	A-2	1.0	41.25	412,500	7	<u>2,887,500</u>
						\$5,103,300

#### F.10 - Logistics Costs

The logistic costs are the costs directly associated with movement of freight. Table F.10-1 tabulates the railroad costs associated with Watana. Table F.10-2 tabulates the railroad costs associates with Devil Canyon. Table F.10-3 tabulates the truck haul costs for both dams. Table F.10-4 shows the combined logistic costs for all plans.

# WATANA LOGISTIC BREAKDOWN

Table F-10.1

	Rail Barge Whittier			Container Barge (Anchorage)		Rail Road					
	Tons	Cost \$/ton	Cost	Cost \$/ton	Cost	Cost \$/ton Mi.	62 Mi. Whittier to Anchorage	149 Mi. Anchorage to Gold Creek	16 Mi. Gold Creek to Devil Canyon	42 Mi. Devil Canyon to Watana	56 Mi. Gold Creek to Cantwell
Const. Equipment	16,000	120.00	\$ 1,920,000	-	-	0.1878	186,298	447,715	48,077	126,202	168,269
Explosives	20,000	55.00	1,100,000	-	-	0.6267	777,108	1,867,566	200,544	526,428	701,904
Cement	350,000	55.00	19,250,000	-	-	0.1565	3,396,050	8,161,475	876,400	2,300,550	3,067,400
Rein. Steel	33,000	55.00	1,815,000	-	-	0.2577	527,254	1,267,111	136,066	357,172	476,230
Rock Bolts	12,500	55.00	687,500	-	-	0.2577	199,718	479,966	51,540	135,293	180,390
Steel Support	3,600	55.00	198,000	-	-	0.2577	57,519	138,230	14,843	38,964	51,952
Mics., str., etc. equip.	15,000	55.00	825,000	-	-	0.1262	117,366	282,057	30,288	79,506	106,008
Constr. Fuel	300,000	55.00	16,500,000	-	-	0.1450	2,697,000	6,481,500	696,000	1,827,000	2,436,000
Camp Fuel	51,000	55.00	2,805,000	-	-	0.1450	458,490	1,101,855	118,320	310,590	414,120
Tires & Parts	21,800	-	-	80.00	1,744,000	0.1878		610,002	65,505	171,950	229,266
Camp Supplies	74,600	-	-	80.00	5,968,000	0.1262		1,402,763	150,632	395,410	527,213
Village	1,400	-	-	80.00	112,000	0.1262		26,325	2,827	7,421	9,894
Contingency & Misc.	196,600	-	-	80.00	15,728,000	0.1262		3,696,827	396,975	1,042,059	1,389,412
	1,095,500		45,100,500		23,552,000		8,416,803	25,963,392	2,788,017	7,318,545	9,758,058
			1		2		3	4	5	6	7

# DEVIL CANYON LOGISTIC BREAKDOWN

Table F10.2

		Rail Barge Whittier		Container Barge (Anchorage)		Rail Road			
	Tons	Cost \$/ton	Cost	Cost \$/ton	Cost	Cost \$/ton Mi.	62 Mi. Whittier to Anchorage	149 Mi. Anchorage to Gold Creek	16 Mi. Gold Creek to Devil Canyon
Const. Equipmment	5,000	120.00	\$600,000	-	-	.1878	58,218	139,911	15,024
Explosive	3,000	55.00	165,000	-	-	.6267	116,566	280,135	30,082
Cement	650,000	55.00	35,750,000	-	-	.1565	6,306,950	15,157,025	1,627,600
Rein. Steel	22,000	55.00	1,210,000	-	-	.2577	351,503	844,741	90,710
Rock Bolts	3,000	55.00	165,000	-	-	.2577	47,932	115,192	12,370
Steel Support	2,200	55.00	121,000	-	-	.2577	35,150	84,474	9,071
Misc., str., elc. equip.	13,500	55.00	742,500	-	-	.1262	105,629	253,851	27,259
Constr. Fuel	68,000	55.00	3,740,000	-	-	.1450	611,320	1,469,140	157,760
Camp Fuel	30,000	55.00	1,650,000	-	-	.1450	269,700	648,150	69,600
Tires & Parts	18,700	-	-	80.00	1,496,000	.1878	0	523,267	59,190
Camp Supplies	44,000	-	-	80.00	3,520,000	.1262	0	827,367	88,845
Village	1,300	-	-	80.00	104,000	.1262	0	24,445	2,625
Contingency & Misc.	205,900	-	-	80.00	16,472,000	.1262	0	3,871,702	415,753
	1,066,600		\$44,143,500		\$21,592,000		7,902,968	24,239,400	2,602,889
			8		9		10	11	12

# ROAD HAUL SEGMENT COSTS

F.10-3

<u>Item</u>	<u>Tons</u>	<u>\$/ton Mi. Rate</u>	<u>Gold Creek to Devil Canyon 12 Mi. (B-2)</u>	<u>Devil Canyon to Watana 36 Mi. (B-3)</u>	<u>Cantwell to Watana 65 Mi.</u>	<u>Devil Canyon to Watana 41 Mi. North</u>
All Watana	1,095,500	.2069	2,719,907 15	8,159,722 16	14,732,832 17	9,293,017 18
All Devil	1,066,600	.2069	2,648,154 19			

## LOGISTICS TOTALS

Table F.10-4

Plan 1:	Use: Water: 1, 2, 8, 9	\$134,388,000
	Rail to Gold Creek : 3, 4, 10, 11	66,522,563
	Truck to Dams: 15, 16, 19	<u>13,527,783</u>
	TOTAL	\$214,438,346
Plan 2:	Use: Water: 1, 2, 8, 9	\$134,388,000
	Rail to Gold Creek: 3, 4, 10, 11	66,522,563
	Rail to Dams: 12, 5, 6	<u>12,709,451</u>
	TOTAL	\$213,620,014
Plan 3 & 7:	Use: Water: 1, 2, 8, 9	\$134,388,000
	Rail to Gold Creek: 3, 4, 10, 11	66,523,563
	Rail to Cantwell: 7	9,758,058
	Truck to Watana from Cantwell: 17	14,732,832
	Truck to Devil Canyon via Gold Creek:	<u>2,648,154</u>
	TOTAL	\$228,050,607
Plan 4 & 6:	Use: Water: 1, 2, 8, 9	\$134,388,000
	Rail to Gold Creek: 3, 4, 10, 11	66,522,563
	Rail to Cantwell: 7	9,758,058
	Rail to Devil 12	2,602,889
	Truck to Watana from Cantwell 17	<u>14,732,832</u>
	TOTAL	\$228,004,342
Plan 5 & 8:	Use: Water: 1, 2, 8, 9	\$134,388,000
	Rail to Gold Creek: 3, 4, 10, 11	66,522,563
	Truck to Devil Canyon: 15, 19	5,368,061
	Northside Truck to Watana 18	<u>9,293,017</u>
	TOTAL	\$215,571,641