HARZA-EBASGO
Susitna Joint Venture
Document Number

## SUSITNA HYDROELECTRIC PROJECT

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## INSTREAM ICE SIMULATIONS: SUPPLEMENTARY STUDIES FOR MIDDLE SUSITNA RIVER

FINAL REPORT

MARZA-EBASCO SUSITNA JOINT VENTURE

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## INSTREAM ICE SIMULATIONS: SUPPLEMENTARY STUDIES FOR MIDDLE SUSITNA RIVER

Report by Harza-Ebasco Susitna Joint Venture

> Prepared for Alaska Power Authority

> > Final Report November 1985

## NOTICE

ANY QUESTIONS OR COMMENTS CONCERNING
THIS REPORT SHOULD BE DIRECTED TO
THE ALASKA POWER AUTHORITY
SUSITNA PROJECT OFFICE

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G	Watana Only	2001	1981-82	Case C	Inflow- Matching	Original	Present
H	Watana Only	2001	1981-82	Case C	Warmest Water	Original	Present
I	Watana Only	2001	1981-82	Case C	Lowest Port	Original	Present

.

<sup>1)</sup> See note on page ix

## LIST OF EXHIBITS (continued)

## ICECAL SIMULATION RESULTS

Exhibit	Project Status	Energy <sup>1</sup> Demand	Weather Period	Flow Requirement	Intake Operating Policy	Watana Intake Design	Devil Canyon Cone Valve Intake
J	Watana Only	2001	1981-82	Case E-VI	Inflow- Matching	Original	Present
K	Watana Only	2001	1981-82	Case E-VI	Warmest Water	Original	Present
L	Watana Only	2001	1971-72	Case C	Warmest Water	Original	Present
М	Watana & Devil Canyon	2002	1981-82	Case C	Warmest Water	Original	Present
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<sup>1)</sup> See note on page ix

#### LIST OF EXHIBITS (continued)

#### ICECAL SIMULATION RESULTS

Exhibit	Project Status	Energy <sup>1</sup>	Weather Period	Flow Requirement	Intake Operating Policy	Watana Intake Design	Devil Canyon Cone Valve Intake
V	Watana & Devil Canyon	2002	1981-82	Case C	Warmest Water	1800/1770	Present
W	Watana & Devil Canyon	2002	1981-82	Case C	Warmest Water	Original	High
х	Watana & Devil Canyon	2002	1981-82	Case C	Warmest Water	1800/1770	High

1) The projected energy demands in the Amendment to the License Application (Alaska Power Authority 1985) have been revised from the original License Application (Alaska Power Authority 1983). The exhibits in this report show the energy demand years based on the original License Application. The following table is provided to facilitate conversion of energy demand years shown on the exhibits in this report to energy demand years for the amended License Application.

	ENERGY DEMAND YEAR			
	Shown on Exhibit	Amended License Application		
Three Stage Project				
Watana (Elev. 2000)	2001	mid-Stage I		
Watana (Elev. 2000) and Devil Canyon	2002	mid-Stage II		
Watana (Elev. 2185) and Devil Canyon	2020	late-Stage III		
Two Stage Project				
Watana (Elev. 2185)	2001	mid-Stage I		
Watana (Elev. 2185) and Devil Canyon	2002	early—Stage III		

#### SUMMARY

River ice simulation results are presented herein as a supplement to those included in the "Instream Ice Simulation Study" (Harza-Ebasco 1984b). The supplementary simulations are intended to include recent refinements in the proposed Susitna Hydroelectric Project and to evaluate the sensitivity of Susitna River ice processes to various parameters. The following were considered:

- a) Revised "three-stage" construction of the project
- b) Alternative instream flow requirements
- c) Alternative operating policies for multi-level power intakes
- d) Alternative low levels for Watana power intake
- e) Alternative levels for Devil Canyon outlet works.

Results of the river ice simulations support the following conclusions:

- Expected river ice conditions with the proposed Case E-VI flow requirements are not significantly different from those with Case C or Case E-I requirements.
- 2. It is expected that the "warmest water" and the "lowest port" alternative operating policies may tend to reduce somewhat the ice cover development relative to the proposed "inflow-matching" policy. However, this trend did not hold for all of the sensitivity simulations and should not be counted on as a general rule. In particular, with Devil Canyon Dam in operation the alternative operating policies have no significant effect on river ice.

- 3. It is expected that provision of lower ports at the Watana power intake would generally tend to reduce somewhat the extent of the ice front progression and the maximum river stages near the upstream extent of the cover. However, substantial reductions in the ice conditions are not expected to occur consistently unless a very low intake port at Elevation 1636 is provided.
- 4. An alternative high intake (elevation 1425) for the Devil Canyon outlet works has no significant effect on expected river ice conditions relative to the present design, although it increases release temperatures during brief periods of summer operation.

#### 1.0 INTRODUCTION

This report presents the results of river ice simulations for the middle reach of the Susitna River (i.e., downstream of the proposed Susitna Hydroelectric Project and upstream of the Chulitna River confluence - see Figure 1). These river ice simulations are provided as a supplement to the previously published "Instream Ice Simulation Study' (Harza-Ebasco 1934b). One purpose of the present study is to provide updated river ice results based on recent refinements to the proposed Susitna Hydroelectric Project. In particular, these updated results are based on the revised "Case E-VI" instream flow requirements and the "Three-Stage" construction sequence (Alaska Power Authority 1985), which has replaced the "Two-Stage" project proposed in the original License Application (Alaska Power Authority 1983). This report is also intended to evaluate the sensitivity of Susitna River ice processes to several parameters beyond the scope of the earlier report. These include alternative power intake operating policies, alternative designs for the Watana multi-level power intakes, alternative instream flow requirements and alternative intake elevations for the Devil Canyon outlet works. The scope of these alternatives is discussed in Chapter 2.

Many of the sensitivity simulations described in this report were carried out with the Case C flow requirements and the "two-stage" project prior to the adoption of the "Case E-VI" flow requirements and the "three-stage" project by the Alaska Power Authority. The general trends of the sensitivity results are not expected to be affected by these changes in flow requirements and construction staging. Conclusions regarding sensitivity of river ice processes are therefore considered valid.

The methodology for the supplementary river ice simulations herein is identical to that employed for the Instream Ice Simulation Study (Harza-Ebasco 1984b). The calibrated river ice model ICECAL (Harza-Ebasco 1984a) is used to generate the simulations. Each ICECAL simulation is based on the results of a corresponding reservoir temperature simulation (via the DYRESM model, Alaska Power Authority 1984, Harza-Ebasco 1984d) and a stream temperature

simulation (via the SNTEMP model, Arctic Environmental Information and Data Center 1984, Alaska Power Authority 1984). Results of the ICECAL model are presented in terms of representative ice thicknesses and water surface elevations as a function of time and location along the river. Results continue to be focused at the river mile locations of those slough and side channels believed to be most important in terms of salmon production.

A more complete description of the background, methodology, capabilities and limitations of the river ice modeling process is included in the previously published reports (Harza-Ebasco 1984a, Harza-Ebasco 1984b).

#### 2.0 SCOPE OF RIVER ICE SIMULATIONS

#### 2.1 General

Initial ICECAL simulations included in the "Instream Ice Simulation Study" (Harza-Ebasco 1984b) were based on conditions presented in the original License Application (Alaska Power Authority 1983). These conditions included a "two-stage" construction sequence (i.e., Watana completed in 1996, Devil Canyon completed in 2002), the Case C flow requirements (Figure 2), multi-level Watana power intake geometry shown in Figure 3, and the "inflow-matching" operating policy for the power intakes (i.e., an attempt to match the reservoir release water temperatures with the natural flow temperatures). These initial simulations were performed for a variety of weather conditions and project energy demands.

Several refinements to the proposed Susitna Hydroelectric Project have recently been adopted by the Alaska Power Authority, and are fully discussed in the License Application Amendment currently under preparation (Alaska Power Authority 1985). In particular, these refinements include the "Case E-VI" flow-requirements (Figure 2) and the "three-stage" construction sequence for the project as outlined below:

- Stage I A lower Watana Dam (normal maximum pool elevation 2000 ft. MSL) would be constructed.
- Stage II The full Devil Canyon Dam (normal maximum pool elevation 1455 ft. MSL) would be added.
- Stage III Watana Dam would be raised to its ultimate height (normal maximum pool elevation 2185 ft. MSL).

This report includes ICECAL simulations which are based upon these project refinements as currently adopted. These ICECAL simulations were performed for operation of Stage I, Stage II and Stage III based on the 1981-82 weather

conditions (an average winter in terms of mean air temperatures). The "inflow-matching" power intake operating policy and the Case E-VI flow requirements, adopted by the Alaska Power Authority, were assumed for these simulations. The effects of the alternative Case E-I flow requirements (Figure 4), relative to the adopted Case E-VI requirement, were also simulated. Case E-I was selected for these sensitivity studies since it has the highest minimum summer flow requirements of the suggested alternative flow constraints (Harza-Ebasco 1984c). The summer minimum flow requirement for Case E-I is 14,000 cfs as compared to 9,000 cfs for Case E-VI. Ice conditions for summer minimum flow requirements between these two extremes are expected to be within the simulated range of conditions for E-VI and E-I.

As detailed in the following sections, this report also includes a number of sensitivity simulations. These simulations were performed to investigate the effects on river ice due to alternative flow requirements, additional low power intakes at Watana Dam, alternative intake operating policies which attempt the release of warmer water, and alternative intake elevations for the Devil Canyon outlet works. The scope of these sensitivity simulations is shown in Table I. Although these sensitivity simulations, as well as those presented in the "Instream Ice Simulation Study" (Harza-Ebasco 1984b), were based upon the original "two-stage" project, the general trends of the results are believed applicable to the "three-stage" project also. Conclusions regarding the sensitivity of river ice to weather conditions, flow requirements, power intake designs, operating policies and outlet works designs, based on the simulations of the "two-stage" project, are therefore also believed valid for the "three-stage" project.

## 2.2 Alternative Operating Policies for Watana and Devil Canyon Multi-Level Power Intakes

Water temperatures within the proposed Watana and Devil Canyon reservoirs will vary with time and depth. The multi-level power intake structures proposed for the Watana and Devil Canyon reservoirs are therefore intended to provide some degree of control over the reservoir release temperatures discharged to the river through the powerhouse. Alternative policies considered

herein for operating the multi-level power intakes include "inflowmatching", "warmest water" and "lowest port". The "inflow-matching" policy, which was assumed for the "Instream Ice Simulation Study" (Harza-Ebasco 1984b) and has been adopted by the Alaska Power Authority for the License Application studies (Alaska Power Authority 1983, 1985), represents a yearround attempt to match the reservoir release temperatures with the natural temperature of the flow entering the reservoir. In effect, "inflow-matching" results in winter release of the coldest water available to the power intakes. The "inflow-matching" policy also is expected to result in the lowest possible suspended sediment concentration in the reservoir outflow during the winter, thereby minimizing the project effects in this regard (Alaska Power Authority 1985). The "warmest water" policy represents a yearround policy of releasing the warmest water available to the power intakes. For both "inflow-matching" and "warmest water" policies, the particular intake port selected for operation will vary with the changing reservoir levels and temperature profiles. The "lowest port" operating policy means that the lowest port of the multi-level power intake will be operated yearround regardless of water temperatures.

Comparisons of river ice simulations for these three alternative operating policies are based on the "two-stage" project, Case C and Case E-VI alternative flow requirements (see Section 2.3) and the weather conditions of 1981-82 and 1971-72 (average and cold winters, respectively, in terms of mean air temperature).

## 2.3 Alternative Instream Flow Requirements

River ice simulations based on the "Case C" and "Case E-VI" alternative instream flow requirements are compared in this report. The "Case C" instream flow requirement (Figure 2) was proposed in the original Susitna Hydroelectric Project License Application (Alaska Power Authority 1983) and was assumed for the "Instream Ice Simulation Study" (Harza-Ebasco 1984b). The "Case E-VI" flow requirement (Figure 2) represents a recommended refinement of "Case C" as described in the report "Evaluation of Alternative Flow Requirements" (Harza-Ebasco 1984c) and the License Application Amendment

(Alaska Power Authority 1985). Comparisons of river ice simulations for "Case C" and "Case E-VI" are based on both "inflow-matching" and "warmest water" operating policies (Section 2.2), Watana and Watana + Devil Canyon operating ("two-stage" project), and the 1981-82 weather conditions (an average winter in terms of mean air temperatures). Figure 5 shows a comparison of the simulated Case C and Case E-VI flow rates released from Watana reservoir for Watana operating alone with 2001 energy demand and the 1981-82 weather conditions. Figure 6 shows corresponding flows released from Devil Canyon reservoir with the 2002 energy demand.

## 2.4 Alternative Designs for Watana Multi-Level Power Intake

River ice simulations are provided for several alternative designs of the Watana multi-level power intake structure as detailed in Table 2. The "original design" shown in Figure 3 corresponds to that proposed in the original License Application (Alaska Power Authority 1983) and is also applicable to Stage III of the "three-stage" project. This design includes intake ports at elevations 2151, 2114, 2077 and 2040 ft. MSL with an approach channel at elevation 2025 ft. MSL. This "original design" was assumed for the "Instream Ice Simulation Study" (Harza-Ebasco 1984b). The alternative Watana power intake designs considered herein are similar to the "original design" but with one additional low level port at elevation 1880, 1800 or 1636 ft. MSL (Table 2). These alternative power intake designs are considered in order to determine if an additional low level port can effectively provide warmer winter reservoir releases and subsequently reduced river ice cover development downstream relative to that with the "original design". Comparisons of river ice simulations for the alternative power intake designs are based on the "warmest water" operating policy (Section 2.2), "Case C" flow requirements (Section 2.3), Watana and Watana + Devil Canyon operating ("two-stage" project) and the 1971-72 and 1981-82 weather conditions.

## 2.5 Alternative Designs for Devil Canyon Outlet Works

River ice simulations are included for two alternative designs for the intake to the Devil Canyon outlet works. The "present design" provides the outlet works intakes at elevation 930 and 1050 ft. MSL and was used for the "Instream Ice Simulation Study" (Harza-Ebasco 1984b). As discussed in the License Application Amendment (Alaska Power Authority 1985), an alternative "high level" intake at elevation 1425 ft. MSL was considered for the purpose of warming the reservoir release temperatures by 1°C to 2°C during summer operation of the outlet works. River ice simulations were performed to determine if such a change in summer release temperatures would have any effect on winter conditions. River ice results for the "present design" and "high level" outlet works are compared on the basis of the "warmest water" power intake operating policy (Section 2.2), "Case C" flow requirements (Section 2.3), the "original" and Elev. 1800 Watana power intake designs (Section 2.4) and the average 1981-82 winter weather conditions.

#### 3.0 RESULTS

## 3.1 General

The supplementary river ice simulation results are presented in Exhibits A through X. These exhibits are presented in the same format as those of the "Instream Ice Simulation Study" (Harza-Ebasco 1984b) and include the following information:

- Profile of maximum river stages which occurred during the simulation period and the corresponding ice cover thickness which existed on the date of maximum stage.
- Location of the ice front and 0°C water isotherm throughout the simulation.
- Time history of water surface elevation, ice thickness and water temperature at selected slough and side channel locations.

Tables 3, 6 and 9 present a summary of the maximum simulated river stages and simulated ice front progression for the various alternatives considered in this study (see Chapter 2). With a similar format, Tables 4, 7 and 10 summarize the maximum simulated total ice cover thicknesses (i.e., solid + slush ice components - Harza-Ebasco 1984b) and Tables 5, 8 and 11 show the maximum solid ice component thicknesses for the various alternatives.

For comparative purposes, Tables 3 through 11 include summary results of certain river ice simulations already presented in the Instream Ice Simulation Study (Harza-Ebasco 1984b) with simulations prepared for this supplementary study.

## 3.2 Three-Stage Project

River ice simulations for the current "three-stage" Susitna Hydroelectric Project are presented in Exhibits A, B and C. These results are summarized in Tables 3, 4 and 5 and Figures 7 through 10. These results are based on the "inflow-matching" operating policy and Case E-VI flow requirements. (Additional simulations based on the Case E-I flow requirements are shown in Exhibits D, E and F and are also summarized in Tables 3, 4 and 5.) The results are shown for operation of Stage I, Stage II and Stage III and are based on the average winter weather conditions of 1981-82. Results of the corresponding reservoir temperature simulations are shown in Figures 14, 15 and 16. Simulated flow rates released from the reservoirs are shown in Figures 11, 12 and 13. Simulations of Stage I and Stage II are believed to be representative of typical ice conditions throughout the duration of those particular stages. The Stage III simulation represents conditions when the project's annual energy output is nearing its ultimate capacity.

The river ice simulation results for Stage I, Stage II and Stage III indicate the following:

## 3.2.1. Stage I Operation

- a) Ice cover progression upstream of Talkeetna in an average winter is expected to begin in mid-December, approximately 3 weeks later than for natural conditions. The ice cover would reach a maximum extent near RM 139 in late January and would melt-out by late April, about 2 weeks earlier than the spring breakup of natural conditions.
- b) Maximum total ice cover thicknesses in an average winter would range from 3 feet to 9 feet along the river, and are generally similar to those of natural conditions. Maximum solid ice thicknesses of 3 feet are expected.

- c) Maximum river stages within the ice-covered reach (downstream of RM 139) in an average winter would generally be 2 to 6 feet higher than those of natural conditions and additional sloughs, including Slough 11, would be overtopped. Those sloughs overtopped under natural conditions would be overtopped by greater amounts with Stage I operating.
- d) Upstream of the ice cover, the river would remain open with some border ice and anchor ice expected within approximately 10 to 25 miles upstream of the cover.
- e) River ice results with Case E-I flow-requirements are similar to those with Case E-VI.

## 3.2.2. Stage II Operation

- a) Ice cover progression upstream of Talkeetna in an average winter is expected to be further delayed from Stage I operation, beginning in late December (approximately 6 weeks later than under natural conditions). Ice front progression is expected to reach a maximum extent near RM 133 in late January and would melt-out by late March, about 6 weeks earlier than the natural spring breakup.
- b) Maximum total ice cover thicknesses in an average winter would range from 2 to 6 feet and would be less than or equal to those of natural conditions. Solid ice thicknesses of up to 3 feet are expected.
- c) Maximum river stages within the ice-covered reach (downstream of RM 133) in an average winter would typically be 1 to 4 feet higher than those of natural conditions and would cause an additional overtopping event at Slough 8.
- d) Upstream of the ice cover, maximum river stages would be less than or equal to those of natural conditions, and Slough 9A would no longer be overtopped. Water temperatures in this reach (i.e., upstream of RM 133)

would remain above 0°C for Stage II operation in an average winter and no border or anchor ice is expected.

 e) River ice results with Case E-I flow requirements are similar to those with Case E-VI.

## 3.2.3. Stage III Operation

- a) Ice cover progression upstream of Talkeetna in an average winter is expected to start at the beginning of January, similar to that of Stage II operation and about 6 weeks later than under natural conditions. The ice cover is expected to reach a maximum extent near RM 114 in late January and would melt out by early March, about 9 weeks earlier than the natural spring breakup.
- b) Maximum total ice cover thicknesses in an average winter would range from 1 to 3 feet and would be several feet less than under natural conditions. Solid ice thicknesses are not expected to exceed 1.5 feet.
- c) Maximum river stages within the ice-covered reach (downstream of RM 114) in an average winter would be about 2 feet higher than those of natural conditions.
- d) Upstream of the ice cover, maximum river stages would be typically less than those of natural conditions. Slough overtoppings in this reach would be less frequent and less severe than under natural conditions.
- e) River ice results with Case E-I show somewhat greater ice development than with Case E-VI. Slough overtoppings and the timing of the ice front progression, however, remain similar for Case E-I and Case E-VI.
- f) The Stage III simulation described above is based on the projected energy demand when the project is operating near its ultimate capacity. Earlier in the Stage III operation, it is expected that river ice conditions would be generally similar to those described above, except that the ice

cover may progress to a point between RM 120 and RM 126. This conclusion is based on simulation of the final stage of the two-stage project (equivalent to Stage III) for an energy demand which is slightly less than the demand during the early years of Stage III operation (Exhibit N).

# 3.3 Alternative Operating Policies for Watana and Devil Canyon Multi-Level Power Intakes - "Two-Stage" Project

### 3.3.1 Watana Operating Alone with 2001 Energy Demand

River ice simulation results for the alternative power intake operating policies for Watana operating alone ("two-stage" Project) are presented in Exhibits G through L. A summary of these results is shown in Tables 6, 7 and 8. (Note that these exhibits and tables also consider the effects of the alternative instream flow requirements - see Section 3.4.)

Review of Tables 6, 7 and 8 suggests that the relative effects on river ice of the alternative Watana power intake operating policies (i.e. "inflow-matching", "warmest water" and "lowest port" - see Section 2.2) do not follow a simple general trend. These river ice results, however, are consistent with the corresponding results of the reservoir temperature simulations (DYRESM model) and can best be discussed in conjunction with the DYRESM results. Figures 17, 18 and 19 show these corresponding reservoir temperature simulation results for the alternative power intake operating policies based on Watana operating alone with 2001 energy demand.

Figure 17 shows that, based on Case C flows and 1981-82 weather conditions, the "lowest port" operating policy provides significantly warmer releases (often by 1°C or more) during the winter months than either the "inflow-matching" or "warmest water" policies. This is reflected in the river ice results (Tables 6, 7 and 8) which show a significantly reduced ice front extent, reduced ice thickness and river stages and fewer slough overtoppings for the "lowest port" policy relative to "inflow-matching" or "warmest water." Figure 17 also shows that the "lowest port" policy provides summer

releases in the range of 6 to 8°C. These temperatures are often 4°C colder than those obtained using the "inflow-matching" or "warmest water" policies. Further downstream, however, this temperature difference is only about 2°C (Alaska Power Authority 1985). To some extent, these cold summer releases of the "lowest port" policy may allow the reservoir to store a relatively large amount of thermal energy (compared to the alternative policies) which can subsequently be released in the form of warmer water the following winter. Based on Case C flows and the 1981-82 weather conditions, it therefore appears that the "lowest port" policy is more effective than the other policies in reducing the extent of river ice development.

Based on the Case C flows and 1981-82 weather conditions, Tables 6, 7 and 8 show that the "warmest water" operating policy is not effective in reducing river ice development relative to "inflow-matching". In fact, simulated results of the "warmest water" policy at some locations show greater ice thicknesses and river stages than the "inflow-matching" policy. These river ice results are consistent with the corresponding reservoir temperature simulation results (see Figure 17) which show that, for Case C flows and 1981-82 weather, the "warmest water" policy provides winter releases which are often cooler than those of the "inflow-matching" policy. Although this result may appear unusual, it should be emphasized that these alternative power intake operating policies are year-round policies. As shown in Figure 17, the summer releases of the "warmest water" policy are often warmer than those with "inflow-matching". The "warmest water" policy may therefore cause faster depletion of thermal energy storage in the reservoir and subsequently colder water available for release the following winter.

A comparison of the "warmest water" and "inflow-matching" policies is also made for the Case E-VI flows with 2001 energy demand and 1981-82 weather conditions. The simulated river ice results for Case E-VI are again consistent with the corresponding reservoir temperature simulation results shown in Figure 18. With Case E-VI (see Figure 18), the "warmest water" policy again shows summer releases which are often warmer than those of "inflow-matching", but also shows warmer winter releases. In this case, the reservoir ice cover

formed earlier with the "warmest water" policy than with the "inflow-matching" policy and subsequently tended to insulate the reservoir from the further cooling effects of wind and air temperature. The earlier ice cover formation with "warmest water" policy appears to be caused by removal of greater amounts of warm water from near the reservoir surface, resulting in cooler surface temperatures. As shown in Tables 6, 7 and 8, simulated river ice results for Case E-VI with the "warmest water" policy show reduced ice thicknesses, river stages and ice front extent and fewer slough overtoppings relative to "inflow-matching".

Alternative operating policies for Watana operating alone with 2001 energy demand and Case C flows are also simulated for 1971-72 weather conditions (cold winter). For these conditions, Figure 19 shows that reservoir releases with the "warmest water" policy are warmer during the winter months than those with the "inflow-matching" policy. These release temperatures are again reflected in the simulated river ice results. As shown in Tables 6, 7 and 8, the "warmest water" policy (with Case C flows, 2001 energy demand, 1971-72 weather) results in reduced ice thicknesses and river stages and fewer slough overtoppings in the reach upstream of River Mile 126 relative to the "inflow-matching" policy.

## 3.3.2 Watana and Devil Canyon Operating with 2002 Energy Demand

River ice simulation results for the "inflow-matching" and "warmest water" power intake operating policies for Watana and Devil Canyon operating ("Two-Stage" Project) with 2002 energy demand are presented in Exhibits M, N and O. These results are based on Case C and Case E-VI flows and the 1981-82 (average) weather conditions. As shown in Tables 6, 7 and 8, the river ice results for the "warmest water" policy are nearly identical to those with with "inflow-matching" policy. The corresponding reservoir temperature simulation results (Figures 20 and 21) show that the "warmest water" policy provides slightly warmer winter releases than "inflow-matching", but this difference is not great enough to significantly affect the river ice development.

## 3.4 Alternative Instream Flow Requirements - "Two-Stage" Project

## 3.4.1 Watana Operating Alone with 2001 Energy Demand

River ice simulation results for Watana operating alone with the Case C and Case E-VI alternative flow requirements are presented in Exhibits G, H, J and K. These comparisons are based on the "Two-Stage" Project, the 1981-82 weather conditions and 2001 energy demand and consider both "inflow-matching" and "warmest water" intake operating policies. Results are summarized in Tables 6, 7 and 8. As discussed in Section 3.3.1, trends in river ice simulation results reflect the corresponding trends in the reservoir temperature simulation results. Simulated Watana reservoir release temperatures for the alternative instream flow requirements are compared in Figures 22 and 23.

Based on the "inflow-matching" policy, simulated reservoir release temperatures during the winter for Case C and Case E-VI show significant time-variation (Figure 22) but the average winter release temperatures for the two flow cases appear quite similar. The corresponding river ice simulations for "inflow-matching" show that Case E-VI causes slightly greater ice thicknesses and river stages upstream of River Mile 126 and slightly reduced ice thicknesses and river stages downstream of River Mile 126 relative to Case C. The extent of the ice cover progression and the occurrences of slough overtoppings, however, remains nearly the same for Case C and Case E-VI.

Based on the "warmest water" policy, Figure 23 shows that Case E-VI results in warmer winter reservoir releases (often by 1°C) than those of Case C. This is reflected in reduced river ice extent, reduced river stages and fewer slough overtoppings for the Case E-VI river ice simulations relative to Case C (Tables 6, 7 and 8) based on the "warmest water" policy.

## 3.4.2 Watana and Devil Canyon Operating with 2002 Energy Demand

River ice simulation results for the alternative flow requirements with both dams operating are presented in Exhibits M, N and O. Comparisons of Case C and Case E-VI are based on the "Two-Stage" Project, the 1981-82 weather conditions and 2002 energy demand and include "inflow-matching" and "warmest water" operating policies. Corresponding results of the Devil Canyon reservoir release temperature simulations are shown in Figures 24 and 25.

Figures 24 and 25 show that the simulated winter releases from Devil Canyon reservoir for Case E-VI are generally quite similar or only slightly colder than those of Case C. This trend is reflected in the river ice simulations which show generally similar river stages, ice thicknesses and slough overtoppings for Case C and Case E-VI flow requirements.

# 3.5 <u>Alternative Designs for Watana Multi-Level Power Intake - "Two-Stage"</u> <u>Project</u>

## 3.5.1 Watana Operating Alone with 2001 Energy Demand

River ice simulation resules for alternative Watana power intake designs (see Section 2.4) are presented in Exhibits H, L and P through U based on Watana operating alone ("Two-Stage" Project), 2001 energy demand, Case C flows and the "warmest water" operating policy. These results are summarized for comparison in Tables 9, 10 and 11. Figures 26 and 27 show simulated reservoir release temperatures for several of these alternatives and are consistent with the trends in river ice simulation results.

Tables 9, 10 and 11 show that the addition of a lower level intake port may tend to reduce somewhat the extent of the simulated river ice cover and corresponding river stages near the upstream extent of the cover. Based on the 1971-72 weather conditions, the largest reduction in ice extent, relative to the original intake design, is simulated for the addition of an intake port at elevation 1636 ft. For this alternative, the ice cover extent is

reduced by 9 miles and simulated overtopping at sloughs 9A, 11, 20 and 21 is prevented, relative to the original intake design.

Provision of a lower level intake port at elevation 1880 or 1800 ft., however, does not necessarily result in significantly reduced river ice development. Based on the 1971-72 weather conditions, for example, an additional intake at elevation 1880 ft. provides no reduction in river ice extent or slough overtoppings relative to the original intake design. A lower level intake at elevation 1800 ft. shows only a very slight reduction in river ice extent and prevents at most only one additional slough (Slough 21-A6) from overtopping relative to the original design.

It therefore appears that the addition of lower level Watana power intake ports at elevation 1636 would substantially reduce the extent of river ice development relative to the "original design". Intake ports at elevations 1880 or 1800 ft, however, may not be very effective.

## 3.5.2 Watana and Devil Canyon Operating with 2002 Energy Demand

River ice simulation results for alternative Watana intake designs are presented in Exhibits M, V, W and X based on Watana and Devil Canyon operating ("Two-Stage" Project), 2002 energy demand, 1981-82 weather conditions, Case C flows and the "warmest water" intake operating policy. These results are summarized for comparison in Tables 9, 10 and 11. Note that comparisons are based on both "present" and "high" alternative designs for the Devil Canyon outlet works (see Section 2.5). Figures 28 and 29 show the corresponding reservoir release temperature simulation results.

Tables 9, 10 and 11 show that an additional Watana intake port at elevation 1800 results in a very slight reduction in river ice development relative to the original Watana intake designs. For the most part, river stages and slough overtoppings with the lower (Elevation 1800) intake are the same as those with the original design. This trend occurs based on both the "present design" and the "high level" Devil Canyon outlet works. It therefore again

appears that lower level Watana power intakes at elevations 1880 or 1800 ft may not be very effective in reducing river ice development.

### 3.6 Alternative Pesigns for Devil Canyon Outlet Works - "Two-Stage" Project

River ice simulation results for the "present" and "high level" designs for the Devil Canyon outlet works (see Section 2.5) are presented in Exhibits M, V, W and X. These alternatives are based on 1981-82 weather conditions, the "Two-Stage" Project, 2002 energy demand, Case C flows and "warmest water" operating policy. The results are summarized for comparison in Tables 9, 10 and 11. Corresponding results of the reservoir release temperature simulations are shown in Figures 30 and 31.

As shown in Tables 9, 10 and 11, there is no significant difference in river ice results between the alternative Devil Canyon outlet works designs. This is true based on both the "original design" and the alternative "El. 1800" design for the Watana power intakes. The similarity of winter reservoir release temperatures for the alternative Devil Canyon outlet works is apparent from Figures 30 and 31.

#### 4.0 CONCLUSIONS

The following conclusions are based on the river ice simulations presented in this study and the "Instream Ice Simulation Study" (Harza-Ebasco 1984b).

#### 4.1 "Three-Stage" Project as Currently Adopted - Average Winter Weather

Expected river ice conditions during an average winter with operation of Stage I, Stage II and Stage III are as shown in Figure 10 and described in Section 3.2 of this report. Ice front progression at Talkeetna, with Stage I operating, would be delayed about 3 weeks (relative to natural conditions) until mid-December, and would be further delayed until late December or early January with the operation of Stages II and III respectively. Spring meltout in the Middle Susitna River with Stage I operating would be completed by late April about 2 weeks earlier than the natural breakup. With addition of Stages II and III, the meltout would be further advanced, occurring in late to early March, respectively.

The maximum upstream extent of the ice cover during an average winter would be in the vicinity of RM 139 with Stage I operating. This ice cover extent would be reduced to near RM 133 with Stage II operating and further reduced to the vicinity of RM 114 with Stage III operating. The total thickness of the river ice cover with Stage I operating would be generally similar to that of natural conditions. Ice cover thickness would be progressively reduced with the addition of Stages II and III.

Maximum river stages within the ice-covered reaches during operation of Stages I, II and III would generally be several feet higher than those of natural conditions. The frequency and magnitude of slough overtoppings within the ice-covered reaches during project operation would therefore be greater than under natural conditions (Table 3). Mitigation measures such as construction of berms will therefore be undertaken with the project to prevent these sloughs from overtopping. Upstream of the ice-cover, however, maximum river stages with the project operating would be generally less than or equal to those of natural conditions. Frequency and magnitude of slough

overtoppings upstream of the ice cover with the project in operation would therefore be less than or equal to natural conditions.

#### 4.2 Weather Conditions

The conclusions of Section 4.1 above are based on the average winter weather conditions of 1981-82. In a cold winter, such as that of 1971-72, the ice front progression upstream of Talkeetna would be expected to begin several weeks earlier and would extend a few miles further upstream than with the average winter conditions. The maximum with-project ice front progression would occur with Stage I operating during a cold winter and would be expected to reach the vicinity of RM 142 (versus RM 139 in an average winter). Maximum ice cover thicknesses and river stages in a cold winter are likely to be about 2 feet greater than those in an average winter. Further slough overtopping would therefore be expected in a cold winter.

In a very warm winter, such as that of 1976-77, the extent of the ice cover is expected to be a few miles downstream of that in an average winter. Maximum ice cover thicknesses and river stages in a very warm winter are expected to be about 2 feet less than those in an average winter. Fewer and less severe slough overtoppings are therefore expected in a very warm winter.

## 4.3 Alternative Power Intake Operating Policies

The conclusions of Section 4.1 above were based on the recommended "inflow-matching" operating policy for the multi-level power intakes. It is expected that the "warmest water" and the "lowest port" alternative operating policies may tend to reduce somewhat the ice cover extent and maximum ice thicknesses and may result in fewer slough overtoppings, relative to the "inflow-matching" policy. However, this trend did not hold for all of the sensitivity simulations and should not be counted on as a general rule. In particular, with Devil Canyon Dam in operation (Stages II or III) the alternative operating policies are expected to have no significant effect on river ice.

#### 4.4 Alternative Instream Flow Requirements

The expected river ice conditions with the Case E-I or Case C flow requirement are not significantly different from those with the recommended Case E-VI requirements.

#### 4.5 Alternative Designs for Watana Power Intake

The conclusions of Section 4.1 above are based on the Stage I and Stage III multi-level power intake elevations shown in Table II. It is expected that provision and use of alternative lower intake ports would generally tend to reduce somewhat the extent of the ice front progression and the maximum river stages near the upstream extent of the cover. However, substantial reductions in the ice conditions are not expected to occur consistently unless a very low intake port at Elevation 1636 is provided.

## 4.6 Alternative Elevations for Devil Canyon Outlet Works

It is expected that an alternative high level intake at elevation 1425 ft. MSL would have no significant effect on river ice relative to the present design for the Devil Canyon outlet works.

#### 5.0 REFERENCES

- Alaska Power Authority 1983, Before the Federal Energy Regulatory Commission, Project No. 7114, Application for Major License, The Susitna Hydroelectric Project prepared by Acres American, Inc.
- Alaska Power Authority 1984, Before the Federal Energy Regulatory Commission, Project No. 7114, Application for Major License, The Susitna Hydroelectric Project, Alaska Power Authority Comments on the Federal Energy Regulatory Commission Draft Environmental Impact Statement of May 1984, Appendices IV and V. Prepared by The Harza-Ebasco Susitna Joint Venture.
- Alaska Power Authority 1985, Before the Federal Energy Regulatory Commission, Project No. 7114, Amendment to the Application for Major License, The Susitna Hydroelectric Project (Draft) prepared by Harza-Ebasco Susitna Joint Venture.
- Arctic Environmental Information and Data Center 1984, Susitna Hydroelectric Project, Assessment of the Effects of the Proposed Susitna Hydroelectric Project on Instream Temperature and Fishery Resources in the Watana to Talkeetna Reach, Draft Report for Harza-Ebasco for Alaska Power Authority.
- Harza-Ebasco 1984a, Susitna Hydroelectric Project, Instream Ice, Calibration of Computer Model, for Alaska Power Authority.
- Harza-Ebasco 1984b, Susitna Hydroelectric Project, Instream Ice Simulation Study, Final Report, for Alaska Power Authority.
- Harza-Ebasco 1984c, Susitna Hydroelectric Project, Evaluation of Alternative Flow Requirements, for Alaska Power Authority.

Harza-Ebasco 1984d, Susitna Hydroelectric Project, Eklutna Lake Temperature and Ice Study, with Six Months Simulations for Watana Reservoir prepared for the Alaska Power Authority.

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**TABLES** 

# SUSITNA HYDROELECTRIC PROJECT SCOPE OF SUPPLEMENTARY RIVER ICE SIMULATIONS TWO-STAGE PROJECT

					TANA C					NA + DI 2002 D		ANYON
				1981-82	2		197	1-72		198	1-82	
			CASE (		CAS	E E-VI	CAS	EC	CAS	SE C	CASI	E E-VI
		1	W	L	1	W	1	W	1	W	1	W
DEVIL CANYON OUTLET WORKS	WATANA POWER INTAKE DESIGN											
	ORIGINAL	G	н	1	J	K	Δ	L	Δ	M	N	0
	1880/1850		P					R				
PRESENT DESIGN El. 930, 1050	1800/1770 1800/1500		Q					S		٧		
								T				
	1636/1470							U				
HIGH LEVEL	ORIGINAL									w		
El. 1425	1800/1770				6					x		

LEGEND: G,H,I ..etc ICECAL EXHIBIT PRESENTED HEREIN

Δ

ICECAL SIMULATION PRESENTED PREVIOUSLY (HARZA-EBASCO 1984b)

POWER INTAKE
OPERATING POLICIES:

I INFLOW-MATCHING

W WARMEST WATER

LOWEST PORT

TABLE 1

WEATHER CONDITIONS

PROJECT STATUS

REQUIREMENTS OPERATING

**FLOW** 

POLICIES

TABLE 2

# SUSITNA HYDROELECTRIC PROJECT ALTERNATIVE WATANA POWER INTAKE DESIGNS PORT ELEVATIONS IN FEET M.S.L.

	Original Design*	Alt. 1880/1850	Alt. 1800/1770	Alt. 1800/1500	Alt. 1636/1470	Stage I
Level 1	2151	2151	2151	2151	2151	1964.5
Level 2	2114	2114	2114	2114	2114	1926.5
Level 3	2077	2077	2077	2077	2077	1888.5
Level 4	2040	2040	2040	2040	2040	1850.5
Level 5	_	1880	1800	1800	1636	1812.5
Approach Channel	2025	1850	1770	1500	1470	1800

<sup>\*</sup> Stage III design is same as "original design", except approach channel is at El. 1800.

### TABLE 3

# SUSITNA HYDROELECTRIC PROJECT MAXIMUM SIMULATED WINTER RIVER STAGES 1981-82 WEATHER CONDITIONS (AVERAGE WINTER) THREE-STAGE PROJECT VS NATURAL CONDITIONS

SLOUGH OR	RIVER	THRESHOLD	NATURAL	WATAN	A ONLY	W	TANA AND	DEVIL CANY	ON
SIDE CHANNEL	MILE	ELEVATION	CONDITIONS	STA	GE I	STAC	DE II	STAC	3E III
				CASE E-VI	CASE E-I	CASE E-VI	CASE E-I	CASE E-VI	CASE E-
Whiskers	101.5	367	368	370	370	370	370	370	370
Gash Creek	1120	Unknown	455	457	458	459	458	457	457
6A	112.3	(Upland)	457	459	461	461	461	459	460
8	114.1	476	472	475	478	476	476	474	475
MSII	115.5	482	484	487	490	487	487	485	486
MS II	115.9	487	486	489	493	490	490	487	488
Curry	120.0	Unknown	523	526	526	521	520	518	522
Moose	123.5	Unknown	549	555	555	551	551	545	545
BA West	126.1	573	671	575	574	573	573	569	569
8A East	127.1	582	583	585	585	584	584	581	582
9	129.3	604	606	607	607	605	605	603	603
9 11/5	130.6	Unknown	620	620	621	619	619	617	617
4th July	131.8	Unknown	629	633	632	630	630	628	628
9A	133.7	651	651	656	656	649	649	650	650
10 u/s	134.3	657	657	664	663	655	655	656	656
11 d/s	135.3	Unknown	670	675	674	667	667	668	668
11	136.5	687	683	688	637	682	682	684	684
17	139.3	Unknown	LUPSTREAM	715	715	714	714	715	715
20	140.5	730	BOUNDARY OF	729	729	728	728	729	729
21 (A6)	141.8	747	NATURAL SIMULATIONS	747	747	746	746	747	747
21	142.2	755		753	753	752	752	753	753
22	144.8	788		787	786	785	785	787	787
LRX-3 Ice Front	Starting Dat		11-18	12:0	12:10	12 29	12 29	1-2	1-1
Max. Ice Front E			137 4/	139	139	133	133	114	120
Melt-Out/Breakup	Account to the same of		5 10	4-28	4-29	3.26	3 28	3.5	36

UPSTREAM EXTENT OF

- LOCATIONS WHERE MAXIMUM RIVER STAGE OVERTOPS A KNOWN SLOUGH THRESHOLD ELEVATION.
- 2. ALL RIVER STAGES IN FEET MSL.
- "INFLOW-MATCHING" POWER INTAKE OPERATING POLICY IS ASSUMED FOR PROJECT SIMULATIONS.
- 4. ICE COVER FOR NATURAL CONDITIONS EXTENDS UPSTREAM OF GOLD CREEK (RIVER MILE 137) BY MEANS OF BORDER ICE BRIDGING.

## SUSITNA HYDROELECTRIC PROJECT MAXIMUM SIMULATED TOTAL ICE THICKNESS 1981-82 WEATHER CONDITIONS (AVERAGE WINTER) THREE-STAGE PROJECT VS NATURAL CONDITIONS

SLOUGH OR	RIVER	THRESHOLD	NATURAL	WATAN	A ONLY	WA	TANA AND	DEVIL CANY	ON
SIDE CHANNEL	MILE	ELEVATION	CONDITIONS	STA	GE I	STAC	BE II	STAC	BE III
				CASE E-VI	CASE E-I	CASE E-VI	CASE E-I	CASE E-VI	CASE E-
Whiskers	101.5	367	4	3	3	3	3	2	2
Gash Creek	112.0	Unknown	4	3	4	5	5	1	3
6A	112.3	(Upland)	4	3	4	5	5	1	3
8	114.1	476	4	3	5	4	3	1	2
MSII	115.5	482	5	3	7	4	4	E 100 mg	1
MS II	115.9	487	7	3	8	6	7	100	1
Curry	120.0	Unknown	7	7	7	2	2		1
Moose	123.5	Unknown	7	9	9	5	4		
BA West	126.1	573	3	4	3	3	3	S 600 - 10	
8A East	127.1	582	3	3	3	2	2		
9	129.3	604	7	3	4	2	2		
9 u/s	130.6	Unknown	6	3	4	2	2		
4th July	131.8	Unknown	3	3	4	1	1		
9A	133.7	651	3	6	6				
10 u/s	134.3	657	3	9	7				
11 d/s	135.3	Unknown	3	7	6				
11	136.5	607	3	4	3				
17	139.3	Unknown	4-	0 21					
20	140.5	730							
21 (A6)	141.8	747		y 40 90					
21	142.2	755							
22	144.8	783							

NOTES:

UPSTREAM BOUNDARY OF NATURAL SIMULATIONS

<sup>1.</sup> ALL ICE THICKNESS IN FEET.

<sup>&</sup>quot;INFLOW-MATCHING" POWER INTAKE OPERATING POLICY IS ASSUMED FOR PROJECT SIMULATIONS.

# SUSITNA HYDROELECTRIC PROJECT MAXIMUM SIMULATED SOLID ICE THICKNESS 1981-82 WEATHER CONDITIONS (AVERAGE WINTER) THREE-STAGE PROJECT vs NATURAL CONDITIONS

SLOUGH OR	RIVER	THRESHOLD	NATURAL	WATAN	A ONLY	WA	TANA AND	DEVIL CANY	ON
SIDE CHANNEL	MILE	ELEVATION	CONDITIONS	STA	GE I	STAC	3E II	STAC	3E III
				CASE E-VI	CASE E-I	CASE E-VI	CASE E-I	CASE E-VI	CASE E-
Whiskers	101.5	367	4	3	3	3	3	2	2
Gash Creek	112.0	Unknown	4	3	3	3	3	0	1
6A	112.3	(Upland)	4	3	3	3	3	0	1
	114.1	476	4	3	3	3	3	0	1
MSII	115.5	482	1	3	3	2	2		0
MSII	115.9	487	1	3	3	2	2		0
Curry	120.0	Unknown	1	3	3	2	1		0
Moose	123 5	Unknown	•	3	3	,	1		
8A West	126.1	573	3	3	3	1	1		
8A East	127.1	502	3	2	2	1	1		
9	129.3	604	3	2	2	1	1		
9 u/s	130.6	Unknown	3	2	1	0	0		
ēth July	131.8	Unknown	3	2	1	0	0		
9A	133.7	651	3	1	1				
10 u/s	134.3	657	3	1	1				
11 d/s	135.3	Unknown	3	1	1				
11	136.5	607	3	1	1				
17	139.3	Unknown	11-						
20	140.5	730							
21 (A6)	141.8	747	A STAR STAR						
21	142.2	755							
22	144.8	783							

UPSTREAM BOUNDARY OF NATURAL SIMULATIONS

- 1. ALL ICE THICKNESS IN FEET.
- 2. "INFLOW MATCHING" POWER INTAKE OPERATING POLICY IS ASSUMED FOR PROJECT SIMULATIONS.
- 1 '0' REPRESENTS SOLID ICE FORMATION < 0.5' THICK

SUSITNA HYDROELECTRIC PROJECT

MAXIMUM SIMULATED WINTER RIVER STAGES, TWO-STAGE PROJECT: SENSITIVITY STUDIES
ALTERNATIVE POWER INTAKE OPERATING POLICIES AND INSTREAM FLOW REQUIREMENTS

				WAT	ANA ONLY	: 2001 EN	RGY DEM	AND		WATANA	DEVIL CA	NYON: 200	2 DEMA
SLOUGH OR	RIVER	THRESHOLD		WII	NTER 1981	82		WINTER	1971-72		WINTER	1981-82	
SIDE CHANNEL	MILE	ELEVATION	C	ASE C FLOV	vs	CASE	E-VI	CAS	E C	CAS	SE C	CASE	E-VI
		Access to the second	1	w	L	1	W	1	w	1	W	1	w
Whiskers	101.5	367	371	[371]	370	371	370	372	372	369	369	369	369
Gash Creek	112.0	Unknown	461	458	458	458	457	459	459	456	455	456	455
6A	112.3	(Upland)	464	461	460	460	460	461	461	458	458	459	458
8	114.1	476	477	476	475	475	475	476	477	475	475	476	476
MSII	115.5	482	489	[487]	487	488	487	489	489	485	485	485	485
MSII	115.9	487	491	490	490	490	489	491	492	488	488	488	487
Curry	120.0	Unknown	525	525	522	524	522	525	527	520	520	520	520
Moose	123.5	Unknown	553	556	552	552	546	555	556	548	548	548	548
8A West	126.1	573	574	574	573	575	569	575	575	568	568	571	571
8A East	127.1	582	584	585	582	585	582	586	585	580	581	581	581
9	129.3	604	606	606	602	607	603	610	607	601	601	601	601
9 u/s	130.6	Unknown	620	620	617	621	617	625	622	616	616	616	616
4th July	131.8	Unknown	632	633	628	633	628	636	633	627	627	627	627
9A	133.7	651	652	654	650	654	650	659	655	650	649	649	649
10 u/s	134.3	657	658	660	656	660	656	665	663	655	655	655	655
11 d/s	135.3	Unknown	667	670	668	668	668	676	674	667	667	667	667
11	136.5	687	683	684	684	684	684	690	687	682	682	682	682
17	139.3	Unknown	715	715	715	715	715	727	718	714	714	714	714
20	140.5	730	729	729	729	729	729	741	735	728	728	728	728
21 (A6)	141.8	747	747	747	747	747	747	751	749	745	746	746	746
21	142.2	755	753	753	753	754	754	755	754	752	752	752	752
22	144.8	788	787	787	787	787	787	787	787	785	785	785	785
			THE STATE OF					-	JPSTREAM	EXTENT O	F ICE COVE	R PROGRE	SSION
MULATED ICE F	RONT PRO	GRESSION:				A Comme							
e Front Start at R	ver Mile 98	6	12 30	12 28	12	12-28	13	11.28	12.1	12 30	11	12-30	12.3
laximum Ice Front			134	136	126	134	123	142	142	124	124	126	126
Melt Out Date			43	3 29	3 19	3 23	39	5 15	53	3.12	3 13	3 19	3 11

### TABLE 6

- LOCATIONS WHERE MAXIMUM RIVER STAGE OVERTOPS A KNOWN SLOUGH THRESHOLD ELEVATION.
- 2. OPERATING POLICIES FOR WATANA AND DEVIL CANYON POWER INTAKES:
  - I INFLOW-MATCHING
  - W WARMEST WATER
  - L LOWEST PORT
- 3. ALL RIVER STAGES IN FEET MSL.
- 4. "ORIGINAL DESIGN" FOR WATANA POWER INTAKE IS ASSUMED THROUGHOUT.
- 5. WINTER AIR TEMPERATURES: 1981-82 AVERAGE 1971-72 COLD
- 6. TWO-STAGE PROJECT.

TABLE 7

## SUSITNA HYDROELECTRIC PROJECT MAXIMUM SIMULATED TOTAL ICE THICKNESSES, TWO-STAGE PROJECT: SENSITIVITY STUDIES ALTERNATIVE POWER INTAKE OPERATING POLICIES AND INSTREAM FLOW REQUIREMENTS

				WAT	TANA ONL	7: 2001 EN	ERGY DEN	IAND		WATANA	+DEVIL CA	NYON:200	2 DEMAN
SLOUGH OR	RIVER	THRESHOLD		WII	NTER 1981	-82		WINTE	R 1971-72		WINTE	R 1981-82	
SIDE CHANNEL	MILE	ELEVATION	C	ASE C FLOW	NS	CASE	E-VI	CA	SE C	CA	SE C	CASE	- E-VI
100	13.17		1	W	L	1	w	1	w	1	w	1	W
Whiskers	101.5	367	3	3	2	3	2	5	5	2	2	3	2
Gash Creek	112.0	Unknown	7	3	3	2	2	5	5	2	2	3	2
6A	112.3	(Upland	7	. 4	3	2	2	5	5	3	2	4	3
8	114.1	476	4	3	3	2	1	5	5	3	3	4	3
MS II	115.5	482	5	4	4	3	1	5	5	3	2	3	1
MSII	115.9	487	6	6	6	3	1	5	6	4	3	4	3
Curry	120.0	Unknown	6	7	3	4	2	5	7	1	1	1	1
Moose	123.5	Unknown	5	9	5	4		6	8	1	1	3	3
8A West	126.1	573	2	3	2	2		5	4			1	1
8A East	127.1	582	2	2		2		4	3				
9	129.3	604	1	2		2		6	2				
9 u/s	130.6	Unknown	1	2		2		6	3				
4th July	131.8	Unknown	2	3		3		7	3				
9A	133 7	651	1	3		2		8	5				
10 u/s	134.3	657	1	3		2		9	7				
11 d/s	135.3	Unknown		2				8	5				
11	136 5	687						5	3				
17	139 3	Unknown						13	3				
20	140.5	730						12	5				
21 (A6)	141.8	747						3	1				
21	142.2	755				1		1				1	
22	144.8	788						The second					

- 1. OPERATING POLICIES FOR WATANA AND DEVIL CANYON POWER INTAKES:
- I INFLOW-MATCHING
  W WARMEST WATER
  L LOWEST PORT
- 2 ALL ICE THICKNESSES IN FEET
- 3. "ORIGINAL DESIGN" FOR WATANA POWER INTAKE IS ASSUMED THROUGHOUT
- 4. WINTER AIR TEMPERATURE: 1981-82 AVERAGE 1971-72 COLD
- 5. TWO STAGE PROJECT.

## SUSITNA HYDROELECTRIC PROJECT MAXIMUM SIMULATED SOLID ICE THICKNESSES, TWO-STAGE PROJECT: SENSITIVITY STUDIES ALTERNATIVE POWER INTAKE OPERATING POLICIES AND INSTREAM FLOW REQUIREMENTS

				WA	TANA ONL	7: 2001 EN	ERGY DEN	MAND		WATANA	DEVIL CA	NYON:2002	DEMAND	,
SLOUGH OR	RIVER	THRESHOLD		WI	NTER 1981	82		WINTER	1971 72		WINTER	1981-82		-
SIDE CHANNEL	MILE	ELEVATION	С	ASE C FLO	ws	CASE	E-VI	CA	SE C	CAS	SE C	CASE	E-VI	A
			1	W	L	1	W	1	w	1	w	1	w	
Whiskers	101.5	367	3	3	2	3	2	5	5	2	2	3	2	
Gash Creek	112.0	Unknown	3	3	2	2	1	5	5	2	2	2	2	
6A	112.3	(Upland)	3	3	2	2	1	5	5	2	2	2	2	
8	114.1	476	2	3	2	2	1	5	5	2	2	2	2	
MSII	115.5	482	2	2	1	2	1	5	4	1	1	1	1	
MS II	115.9	487	2	2	1	2	1	5	5	1	1	1	1	
Curry	120.0	Unknown	1	2	1	2	0	5	4	1	1	1	1	
Moose	123.5	Unknown	1	1	1	1		4	3	0	0	1	1	
8A West	126.1	573	1	1	0	1		4	3			1	0	
8A East	127.1	582	1	1		1		4	3					
9 '	129.3	604	1	1		1		4	2					
9 u/s	130.6	Unknown	1	1		0		4	2					
4th July	131.8	Unknown	0	1		0		4	2					1
9A	133.7	651	0	0		0		4	2					
10 u/s	134.3	657	0	0		0		3	2					
11 d/s	135.3	Unknown		0				3	2					
11	136.5	687						3	1					
17	139.3	Unknown						2	1					
20	140.5	730						2	1					SCHOOL
21 (A6)	141.8	747						1	0					
21	142.2	755						0						
22	144.8	788												

- 1. OPERATING POLICIES FOR WATANA AND DEVIL CANYON POWER INTAKES.
- I INFLOW MATCHING W WARMEST WATER
- L LOWEST PORT
- 2. ALL ICE THICKNESSES IN FEET.
- "ORIGINAL DESIGN" FOR WATANA POWER INTAKE IS ASSUMED THROUGHOUT.
- 4. WINTER AIR TEMPERATURE. 1981 82 AVERAGE 1971-72 COLD
- 5. TWO STAGE PROJECT.
- 6. '0' REPRESENTS SOLID ICE FORMATION
  < 0.5' THICK

101.5 112.0	THRESHOLD ELEVATION	ORIGINAL	INTER 1981 1880/1850			WI	NTER 1971	72			WINTER	1961-82		
101.5	The second	ORIGINAL	1890/1850	1800/1770									Annual Control of the	
	367			1000,1770	ORIGINAL	1880/1850	1800/1770	1800/1500	1636/1470	ORIGINAL	1800/1770	ORIGINAL	1800/1770	INTAKE DESIGN
	287								Anna de la	PRESEN	T (EL. 1050)	HIGH (	EL. 1425)	DEVIL CANYON
112.0	307	371	370	370	372	372	372	372	372	369	369	369	369	OUTIET WORKS
	Unknown	458	458	458	459	461	459	461	460	455	455	455	455	
112.3	(Upland)	461	461	460	461	464	461	464	462	458	458	458	458	
114.1	476	476	476	476	477	480	477	478	478	475	474	475	474	
115.5	482	487	487	488	489	490	491	490	489	485	485	485	485	
115.9	487	490	489	491	492	493	494	493	492	488	487	488	486	
120.0	Unknown	525	522	524	527	526	528	527	525	520	520	520	520	
123.5	Unknown	556	551	552	556	555	557	556	555	548	545	548	544	
126.1	573	574	572	574	575	574	574	575	574	568	568	568	568	LUPSTREAM EXTEN
127.1	582	585	582	584	585	585	585	585	584	581	581	581	581	OF ICE COVER
129.3	604	606	602	604	607	608	607	608	605	601	601	601	601	PROGRESSION
130.6	Unknown	620	617	617	622	624	621	621	620	616	616	616	616	
131.8	Unknown	633	628	628	633	635	633	633	631	627	627	627	627	
133.7	651	654	650	650	655	654	656	656	650	649	649	649	649	
134.3	657	660	656	656	663	660	663	662	657	655	655	655	655	
135.3	Unknown	670	668	667	674	672	673	673	668	667	667	667	667	
136.5	687	684	683	683	687	687	688	687	683	682	682	682	682	
139.3	Unknown	715	715	715	718	719	717_	716	715	714	714	714	714	
140.5	730	729	729	729	735	735	730	730	729	728	728	728	728	
141.8	747	747	747	747	749	749	747	747	747	746	746	746	746	
142.2	755	753	753	753	754	754	753	753	753	752	752	752	752	
144.8	788	787	787	787	787	787	787	787	787	785	785	785	785	
ONT PRO	CDESCION.		place									-20		
		12.29	1.2	1.1	12.1	12.2	12.2	12.3	12.6	1	1.1	1.1	1.1	
		and the second	District Lines		10000	4.500				1	No. of the last of the		7 7 10 10	
1,110		The second				14 12000						12		
	115.9 120.0 123.5 126.1 127.1 129.3 130.6 131.8 133.7 134.3 135.3 136.5 139.3 140.5 141.8 142.2 144.8	115.9 487 120.0 Unknown 123.5 Unknown 126.1 573 127.1 582 129.3 604 130.6 Unknown 131.8 Unknown 133.7 651 134.3 657 135.3 Unknown 136.5 687 139.3 Unknown 140.5 730 141.8 747	115.9 487 490 120.0 Unknown 525 123.5 Unknown 566 126.1 573 574 127.1 582 595 129.3 604 606 130.6 Unknown 620 131.8 Unknown 633 133.7 661 654 134.3 667 660 136.5 687 684 139.3 Unknown 715 140.5 730 729 141.8 747 747 142.2 755 753 144.8 788 787	115.9 487 490 489 120.0 Unknown 525 522 123.5 Unknown 556 551 126.1 573 574 572 127.1 582 585 582 129.3 604 606 602 130.6 Unknown 620 617 131.8 Unknown 633 628 133.7 651 654 650 134.3 657 660 656 135.3 Unknown 670 668 136.5 687 684 683 139.3 Unknown 715 715 140.5 730 729 729 141.8 747 747 747 142.2 755 753 753 144.8 788 787  DNT PROGRESSION: Mile 98.6 12 28 12 etent (River Mile) 136 126	115.9 487 490 489 491 120.0 Unknown 526 522 524 123.5 Unknown 566 551 552 126.1 573 574 572 574 127.1 582 585 582 584 129.3 604 606 602 604 130.6 Unknown 620 617 617 131.8 Unknown 633 628 628 133.7 651 654 650 650 134.3 657 660 656 656 135.3 Unknown 670 668 667 136.5 687 684 683 683 139.3 Unknown 715 715 715 140.5 730 729 729 729 141.8 747 747 747 747 142.2 755 753 753 753 144.8 788 787 787 787	115.9 487 490 489 491 492 120.0 Unknown 526 522 524 527 123.5 Unknown 566 561 562 566 126.1 573 574 572 574 575 127.1 582 585 582 584 585 129.3 604 606 602 604 607 130.6 Unknown 620 617 617 622 131.8 Unknown 633 628 628 633 133.7 651 654 650 650 655 134.3 657 660 656 656 656 663 135.3 Unknown 670 668 667 674 136.5 687 684 683 683 687 139.3 Unknown 715 715 715 715 718 140.5 730 729 729 729 729 729 141.8 747 747 747 747 747 747 142.2 755 753 753 753 754 144.8 788 787 787 787 787	115.9 487 490 489 491 492 493 120.0 Unknown 525 522 524 527 526 123.5 Unknown 566 551 552 556 555 126.1 573 574 572 574 575 574 127.1 682 585 582 584 585 685 129.3 604 606 602 604 607 608 130.6 Unknown 620 617 617 622 624 131.8 Unknown 633 628 628 633 635 133.7 651 654 650 650 655 654 134.3 657 660 668 667 674 672 135.3 Unknown 670 668 667 674 672 136.5 667 684 683 683 687 139.3 Unknown 715 715 715 718 719 140.5 730 729 729 729 735 735 141.8 747 747 747 747 747 747 749 749 142.2 755 753 753 753 754 754 144.8 788 787 787 787 787	115.9 487 489 491 492 493 494 120.0 Unknown 525 522 524 527 526 528 123.5 Unknown 556 551 552 556 555 557 126.1 573 574 572 574 575 574 574 127.1 582 585 582 584 585 585 585 129.3 604 606 602 604 607 608 607 130.6 Unknown 633 628 628 633 635 633 133.7 651 654 650 650 655 654 656 134.3 657 660 656 656 663 660 663 135.3 Unknown 670 668 667 674 672 673 136.5 687 684 683 683 687 687 139.3 Unknown 715 715 715 718 719 717 140.5 730 729 729 729 729 735 735 735 735 141.8 747 747 747 747 747 747 747 747 747 74	115.9 487 490 489 491 492 493 494 493 120.0 Unknown 526 522 524 527 526 528 527 123.5 Unknown 566 551 552 556 556 557 556 126.1 573 574 572 574 575 574 575 127.1 582 585 582 584 585 585 585 585 129.3 604 606 602 604 607 608 607 608 130.6 Unknown 620 617 617 622 624 621 621 131.8 Unknown 633 628 628 633 635 633 633 133.7 651 654 650 650 655 654 656 656 134.3 657 660 656 656 663 660 663 662 135.3 Unknown 670 668 667 674 672 673 673 136.5 687 684 683 683 687 687 688 687 139.3 Unknown 715 715 715 718 719 717 716 140.5 730 729 729 729 729 735 735 730 730 141.8 747 747 747 747 747 747 747 747 747 74	115.9 487 490 489 491 492 493 494 493 492 120.0 Unknown 525 522 524 527 526 528 527 525 123.5 Unknown 556 551 562 566 555 557 556 555 128.1 573 574 572 574 575 574 575 574 575 574 575 574 127.1 582 585 585 582 584 585 585 585 585 584 128.3 604 606 602 604 607 608 607 608 605 130.6 Unknown 620 617 617 622 624 621 621 620 131.8 Unknown 633 628 628 633 635 633 633 631 133.7 651 654 650 650 655 655 656 656 656 656 134.3 657 660 668 667 674 672 673 673 668 138.3 Unknown 670 668 667 674 672 673 673 668 139.3 Unknown 715 715 715 715 718 719 717 716 715 715 715 715 718 719 717 716 715 140.5 730 729 729 729 729 735 735 735 753 753 144.8 747 747 747 747 747 747 747 747 747 74	115.9 487 490 489 491 492 493 494 493 492 488 120.0 Unknown 525 522 524 527 526 528 527 525 520 123.5 Unknown 566 551 552 566 565 567 566 565 548 128.1 573 574 572 574 575 574 575 574 575 574 568 127.1 582 585 582 584 585 585 585 585 584 581 129.3 604 606 602 604 607 608 607 608 605 601 130.6 Unknown 620 617 617 62 624 621 621 620 616 131.8 Unknown 633 628 628 633 633 633 633 631 627 133.7 661 654 650 650 655 656 663 660 660 660 660 660 660 660 660 66	116.9 487 490 489 491 492 493 494 493 492 488 487 120.0 Unknown 525 522 524 527 526 528 527 525 520 520 123.5 Unknown 566 561 562 566 566 557 556 555 528 528 122.1 573 574 572 574 575 574 575 574 575 586 581 581 127.1 582 583 582 584 585 585 585 585 585 584 581 581 129.3 604 606 602 604 607 608 607 608 605 601 601 131.8 Unknown 620 617 617 622 624 621 621 620 616 616 131.8 Unknown 633 628 628 633 635 633 633 631 627 627 133.7 651 654 656 656 663 663 662 657 655 655 135.3 Unknown 670 668 667 674 672 673 673 668 667 667 667 138.5 G87 684 683 683 682 682 683 682 683 662 657 655 655 135.3 Unknown 715 715 715 715 718 719 717 716 715 714 714 140.5 730 729 729 729 729 735 735 735 730 729 728 728 141.8 747 747 747 747 747 749 749 749 747 747	116.9 487 489 491 492 493 494 493 492 488 487 488 120.0 Unknown 626 522 624 527 526 526 527 525 520 520 520 520 123.5 Unknown 556 551 552 566 556 556 557 556 555 548 545 548 128.1 573 524 572 574 575 574 575 574 575 574 575 574 575 588 588 588 588 127.1 582 585 585 582 584 585 585 585 585 586 565 601 601 601 801 130.6 Unknown 620 617 617 622 624 621 621 620 616 616 616 131.8 Unknown 633 628 628 633 635 633 633 631 627 627 627 133.7 651 654 650 656 656 656 656 656 656 656 656 656	116.9 487 490 489 491 492 493 494 493 492 488 487 488 486 120.0 Unknown 526 522 524 527 526 526 527 526 520 520 520 520 123.5 Unknown 566 551 552 556 556 556 557 556 555 548 545 548 545 128.1 581 581 128.1 581 581 581 581 128.3 604 606 602 604 607 608 607 608 607 608 607 608 601 601 601 601 601 130.6 Unknown 620 617 617 622 624 621 621 620 616 616 616 616 616 131.8 Unknown 633 628 628 633 635 633 633 631 627 627 627 627 627 627 627 627 627 627

<sup>1.</sup> LOCATIONS WHERE MAXIMUM RIVER STAGE OVERTOPS A KNOWN SLOUGH THRESHOLD ELEVATION.

5. TWO STAGE PROJECT.

<sup>2.</sup> ALL RIVER STAGES IN FEET MSL.

<sup>3.</sup> CASE C INSTREAM FLOW REQUIREMENTS AND "WARMEST WATER" POWER INTAKE OPERATING POLICY IS ASSUMED THROUGHOUT.

<sup>4</sup> WINTER AIR TEMPERATURE. 1981 82 AVERAGE: 1971 72 COLD

## SUSITNA HYDROELECTRIC PROJECT MAXIMUM SIMULATED TOTAL ICE THICKNESSES,TWO-STAGE PROJECT: SENSITIVITY STUDIES ALTERNATIVE DESIGNS FOR WATANA POWER INTAKE AND DEVIL CANYON OUTLET WORKS INTAKE

					WATANA	ONLY: 20	O1 ENERGY	DEMAND			WATANA	+DEVIL CA	NYON: 200	2 DEMAND	
SLOUGH OR	RIVER	THRESHOLD	w	INTER 1981	82		WI	NTER 1971	72			WINTER	1981-82		
SIDE CHANNEL	MILE	ELEVATION	ORIGINAL	1880/1850	1800/1770	ORIGINAL	1880/1850	1800/1770	1800/1500	1636/1470	ORIGINAL	1800/1770	ORIGINAL	1800/1770	WATANA PO
	- 100										PE.ESEN	T (tt. 1050)	HIGH	(EL. 1425)	OUTIET WO
Whiskers	101.5	367	3	2	2	5	5	5	4	3	2	2	2	2	oom w
Gash Creek	112.0	Unknown	3	4	4	5	7	4	7	5	2	1	2	1	
6A	112.3	(Upland)	4	5	3	5	7	4	7	5	2	2	3	1	
	114.1	476	3	3	3	5	6	4	5	4	3	2	3	2	
MSII	115.5	482	4	3	5	5	6	7	7	5	2	1	2	1	
MS II	115.9	487	6	5	6	6	7	11	8	6	3	2	3	1	
Curry	120.0	Unknown	7	2	5	7	7	9	7	5	1	1	1	1	
Moose	123.5	Unknown	9	4	5	8	8	9	8	8	1		1		
BA West	126.1	573	3	1	3	4	2	3	3	3					
BA East	127.1	582	2		2	3	2	2	2	2					
•	129.3	604	2		-2.1	2	3	3	3	1					
9 u/s	130.6	Unknown	2		200	3	5	2	3	1					
4th July	131.8	Unknown	3			3	4	3	3	1					
9A	133.7	651	3			5	3	5	5		l				
10 u/s	134.3	657	3			7	4	6	6		1				
11 d/s	135.3	Unknown	2			5	3	4	4						
11	136.5	687	10.00			3	3	3	3						
17	139.3	Unknown				3	4	2							
20	140.5	730	100			5	5								
21 (A6)	141.8	747				1	1								
21	142.2	755													
22	144.8	788				200									

<sup>1.</sup> ALL RIVER STAGES IN FEET MSL.

<sup>2.</sup> CAISE C INSTREAM FLOW REQUIREMENTS AND "WARMEST WATER" POWER INTAKE OPERATING POLICY IS ASSUMED THROUGH.

<sup>3.</sup> WIINTER AIR TEMPERATURE 1981 82 AVERAGE 1971 72 COLD

<sup>4.</sup> TWO STAGE PROJECT.

WATANA POWER
INTAKE DESIGN
DEVIL CANYON
OUTLET WORKS

### SUSITNA HYDROELECTRIC PROJECT

### MAXIMUM SIMULATED SOLID ICE THICKNESSES,TWO-STAGE PROJECT: SENSITIVITY STUDIES ALTERNATIVE DESIGNS FOR WATANA POWER INTAKE AND DEVIL CANYON OUTLET WORKS INTAKE

					WATANA	ONLY: 20	O1 ENERGY	DEMAND			WATANA	+DEVIL CA	NYON: 200	2 DEMAN
SLOUGH OR	RIVER	THRESHOLD	w	NTER 1981	82		w	INTER 1971	1-72			WINTER	1981-82	
SIDE CHANNEL	MILE	ELEVATION	ORIGINAL	1880/1850	1800/1770	ORIGINAL	1380/1850	1800/1770	1800/1500	1636/1470	ORIGINAL	1800/1770	ORIGINAL	1800/177
								-			PRESENT	(EL. 1050)	HIGH	(EL 1425)
Whiskers	101.5	367	3	2	2	5	5	5	4	3	2	2	2	2
Gash	112.0	Unknown	3	2	2	5	4	4	4	3	2	1	2	1
6A	112.3	(Upland)	3	2	1	5	4	4	4	3	2	1	2	1
	114.1	476	3	2	1	5	4	4	3	3	2	1	2	1
MSII	115.5	482	2	1	1	4	4	4	3	3	1	1	1	1
MS II	115.9	487	2	1	1	5	3	4	3	3	1	1	1	1
Curry	120.0	Unknown	2	1	1	4	3	3	3	3	1	0	١ ،	0
Mocse	123.5	Unknown	1	1	1	3	3	3	2	2	0		0	
BA West	126.1	573	1	0	1	3	2	2	2	1			1	
SA East	127.1	582	1		0	3	2	2	2	1			1	
9	129.3	604	- 1			2	2	2	2	0	1			
9 u/s	130.6	Unknown	1			2	2	2	2	0				
4th July	131.8	Unknown	1			2	2	2	2	0				
9A	133.7	651	0			2	2	1	1					
10 u/s	134.3	657	0			2	2	1	1		ll .			
11 d/s	135.3	Unknown	0			2	1	1	1					
11	136.5	687				1	1	1	1					
17	139.3	Unknown				1	1	0						
20	140.5	730				1	1							
21 (A6)	141.8	747				0	0							
21	142.2	755												
22	144.8	788												

<sup>1.</sup> ALL RIVER STAGES IN FEET MSL.

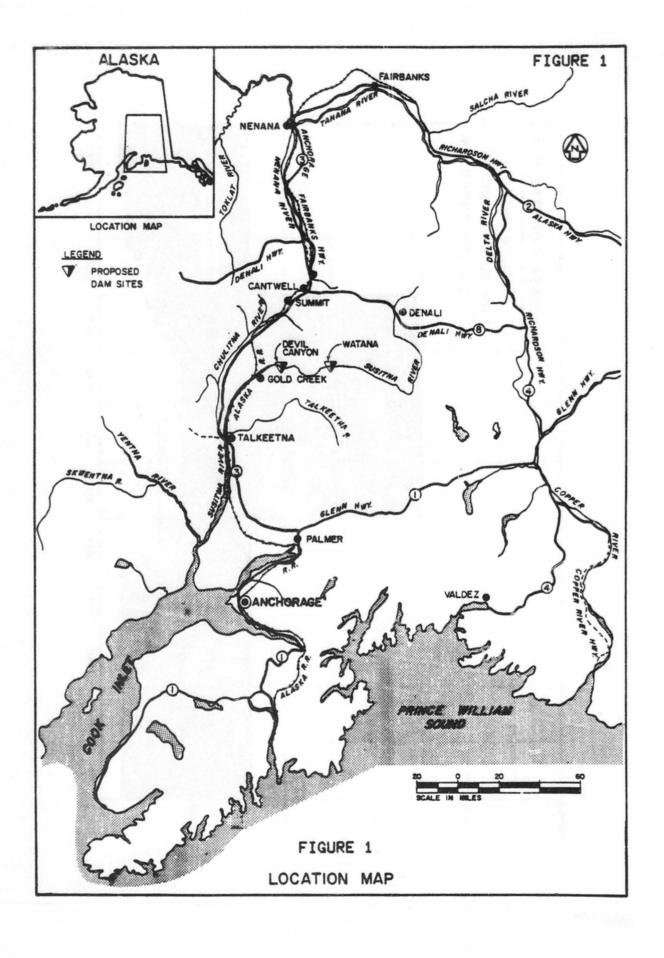
<sup>2.</sup> CASE C INSTREAM FLOW REQUIREMENTS AND "WARMEST WATER" POWER INTAKE OPERATING POLICY IS ASSUMED THROUGH

<sup>3.</sup> WINTER AIR TEMPERATURE 1981 82 AVERAGE 1971 72 COLD

<sup>4</sup> TWO STAGE PROJECT.

<sup>5. &</sup>quot;0" REPRESENTS SOLID ICL FORMATION > 0.5" THICK

### FIGURES

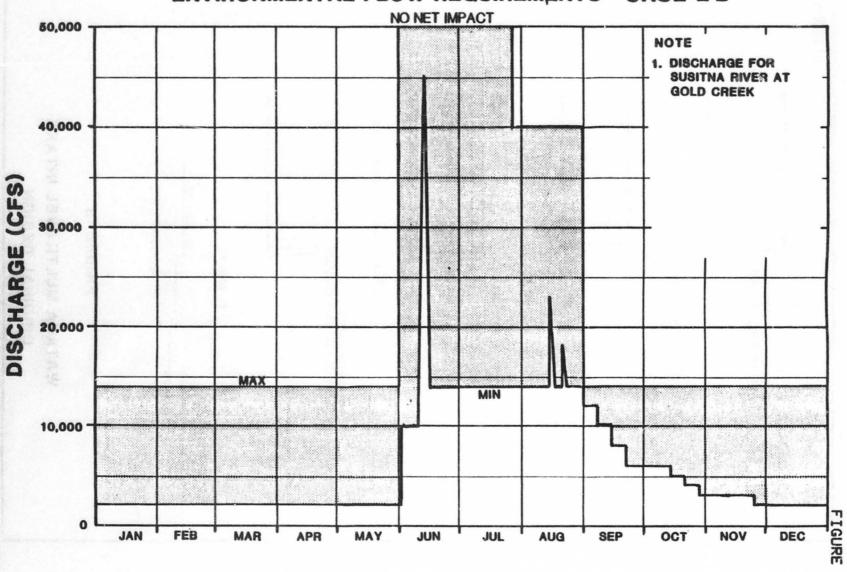


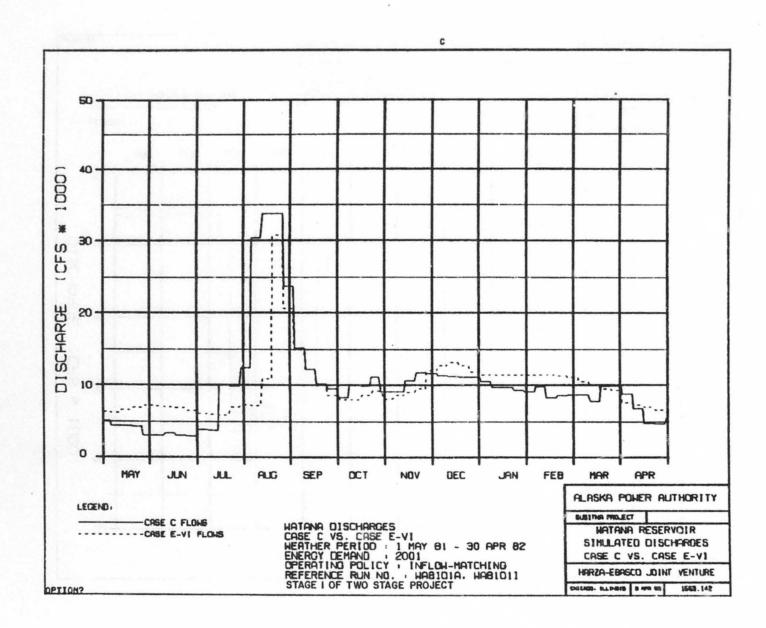
NORMAL MAXIMUM OPERATING RESERVOIR LEVEL (EL. 2185 FT.) EL 2151 FT. EL. 2114 FT. IT FT. (TYPICAL) EL. 2077 FT. 20 FT. (TYPICAL) MINIMUM OPERATING RESERVOIR LEVEL (EL. 2065 FT) EL 2040 FT. EL. 2030 FT.

FIGURE 3

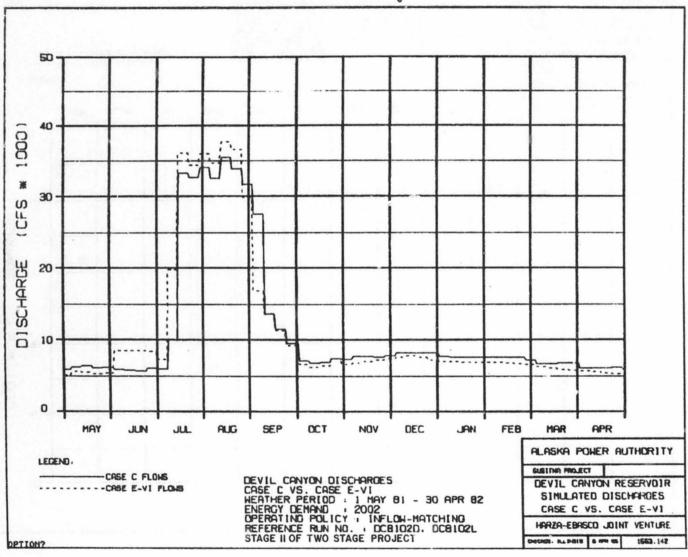
WATANA MULTILEVEL INTAKE ORIGINAL DESIGN

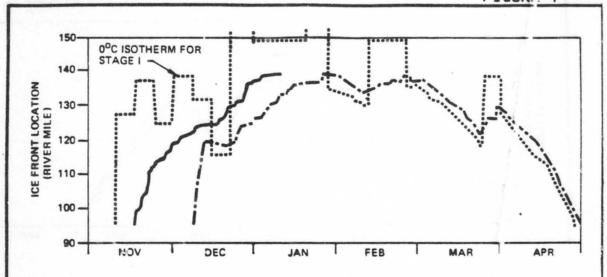
### ENVIRONMENTAL FLOW REQUIREMENTS CASE E I

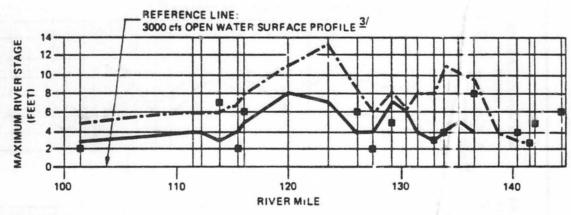


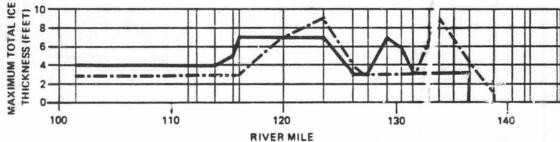












- STAGE I SIMULATION BASED ON CASE E-VI FLOWS. STAGE I ENERGY DEMAND, INFLOW MATCHING TEMPERATURE POLICY.
- NATURAL CONDITIONS NOT SIMULATED UPSTREAM OF RM 140.
- 3 3000 cfs REPRESENTS TYPICAL WINTER FLOW UNDER NATURAL CONDITIONS AT FREEZE UP.

### LEGEND:

NATURAL CO DITIONS

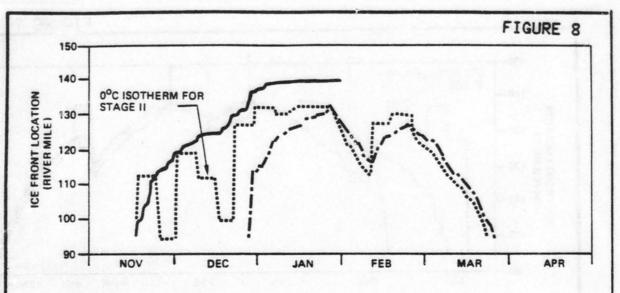
STAGE | OPER ATING

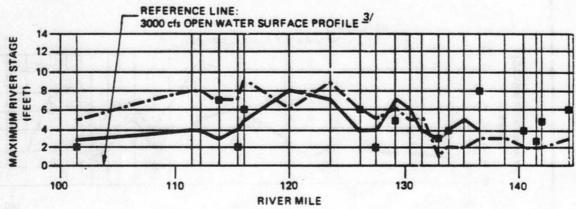
MATURAL SLI UGH BERM ELEVATION

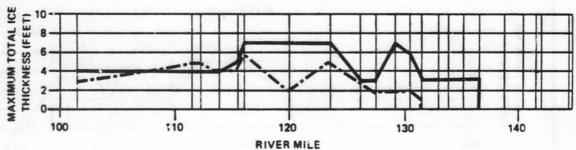
### FIGURE 7

SIMULATED RIVER ICE CONDITIONS STAGE I vs. NATURAL 1981-82 WEATHER CONDITIONS CASE E-VI FLOWS

MARZA - EBASCO SUSITNA JOINT VENTURE ALASKA POWER AUTHORITY







- 1. STAGE II SIMULATION BASED ON CASE E-VI FLOWS, MID STAGE II ENERGY DEMAND, INFLOW MATCHING TEMPERATURE POLICY
- 2. NATURAL CONDITIONS NOT SIMULATED UPSTREAM OF RM 140.
- 3. 3000 cfs REPRESENTS TYPICAL WINTER FLOW UNDER NATURAL CONDITIONS AT FREEZE UP'

### LEGEND:

NATURAL CONDITIONS

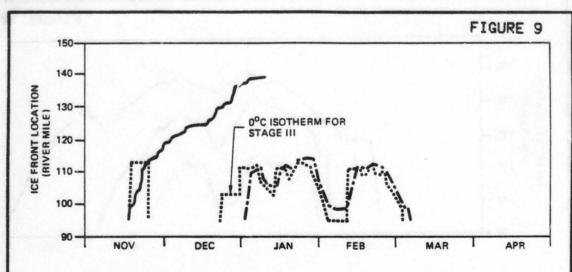
--- STAGE II OPERATING

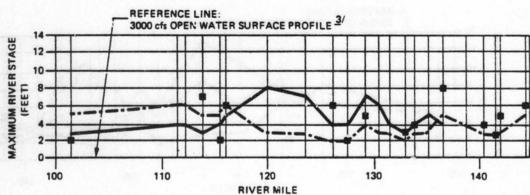
MATURAL SLOUGH BERM ELEVATION

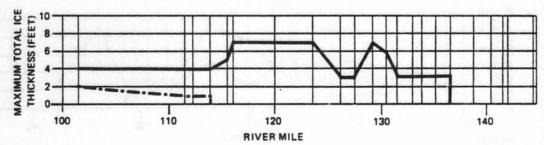
### FIGURE 8

SIMULATED RIVER ICE CONDITIONS STAGE II vs. NATURAL 1981-82 WEATHER CONDITIONS CASE E-VI FLOWS

HARZA = EBASCO SUSITIVE JOINT VENTURE
ALASKA POWER AUTHORITY







- 1. STAGE III SIMULATION BASED ON CASE E-VI FLOWS, LATE STAGE III ENERGY DEMAND, INFLOW MATCHING TEMPERATURE POLICY
- 2. NATURAL CONDITIONS NOT SIMULATED . UPSTREAM OF RM 140.
- 3. 3000 cfs REPRESENTS TYPICAL WINTER FLOW UNDER NATURAL CONDITIONS AT FREEZE UP.

### LEGEND:

NATURAL CONDITIONS
STAGE III OPERATING

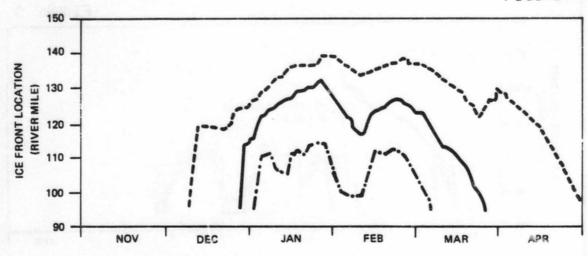
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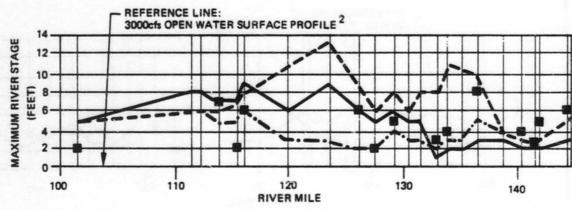
### FIGURE 9

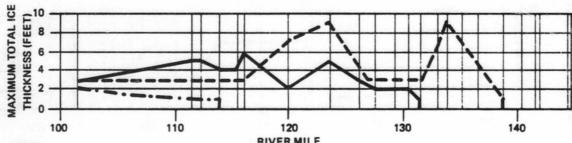
SIMULATED RIVER ICE CONDITIONS STAGE !!! vs. NATURAL 1981-82 WEATHER CONDITIONS CASE E-VI FLOWS

MARZA - EBASCO SUSITNA JOINT VENTUPE
ALASKA POWER AUTHORITY









- 1. SIMULATION BASED ON CASE E-VI FLOWS "INFLOW-MATCHING" POWER INTAKE OPERATION, THREE-STAGE PROJECT.
- 2. 3000cfs REPRESENTS TYPICAL WINTER FLOW UNDER NATURAL CONDITIONS AT FREEZE UP.

### RIVER MILE LEGEND:

STAGE I OPERATING
STAGE II OPERATING

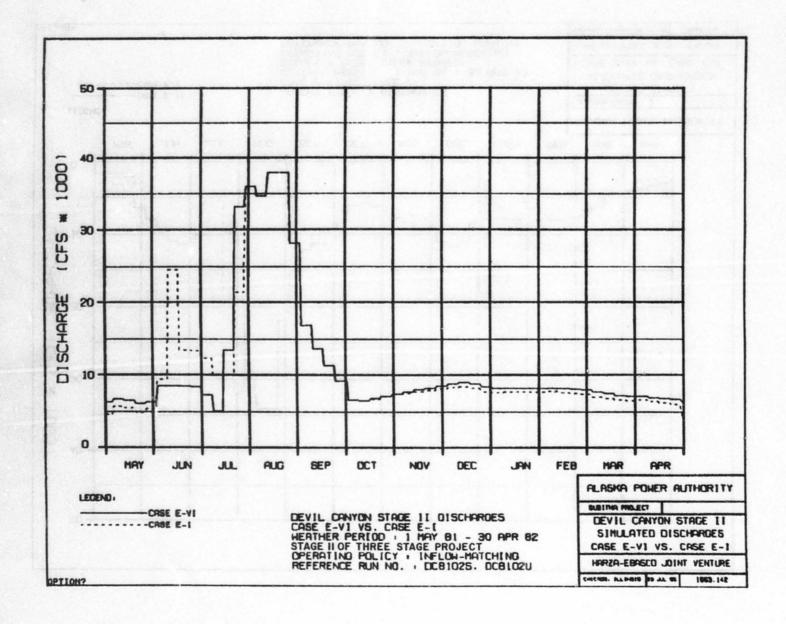
STAGE III OPERATING

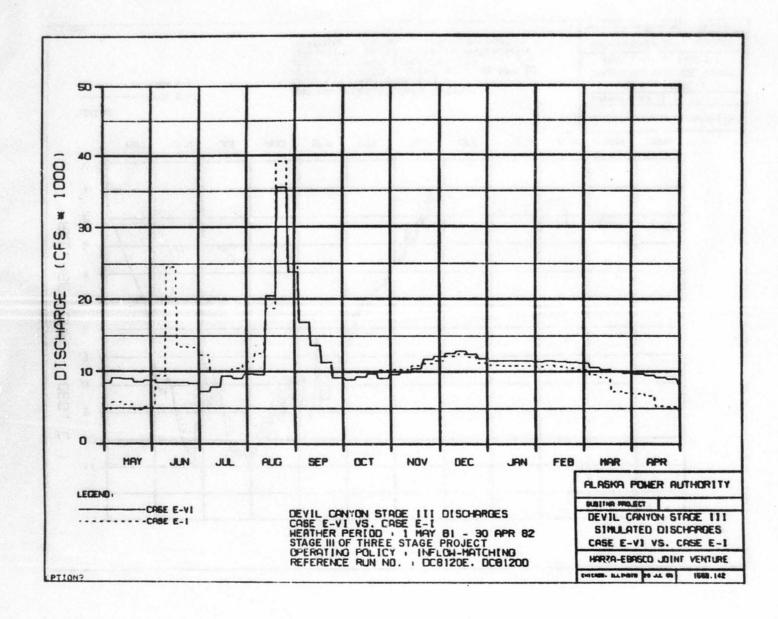
NATURAL SLOUGH BERM ELEVATION

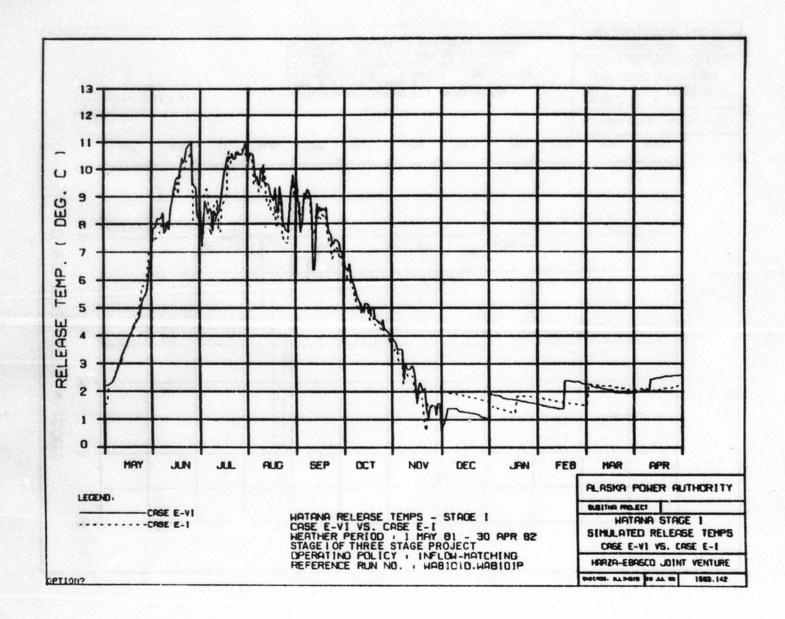
### FIGURE 10

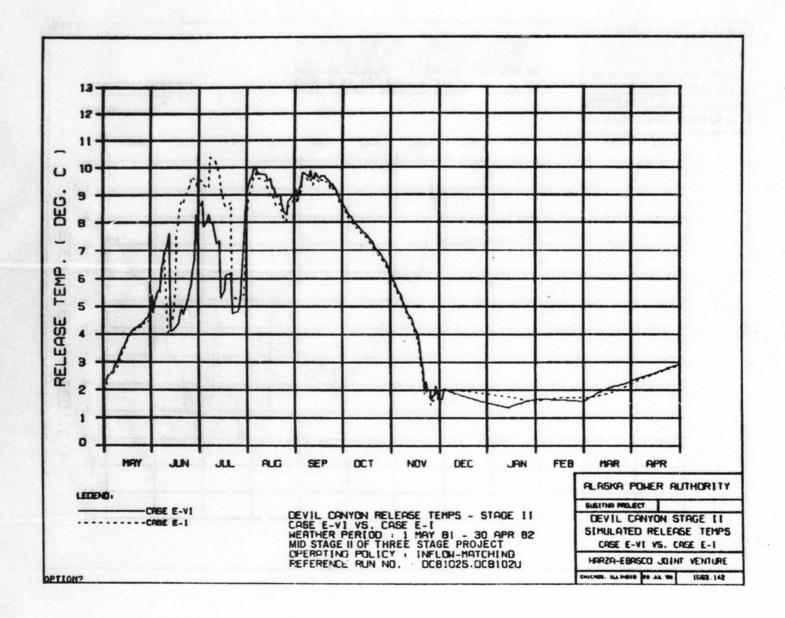
SIMULATED RIVER ICE CONDITIONS STAGES I, II AND III 1981-82 WEATHER CONDITIONS (AVERAGE WINTER)

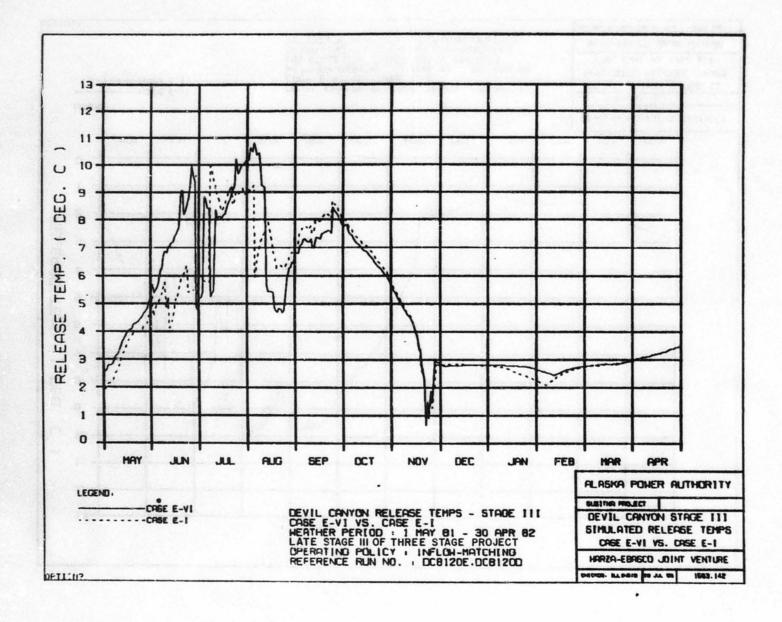
HARZA - EBASCO SUSITNA JOINT VENTURE
ALASKA POWER AUTHORITY

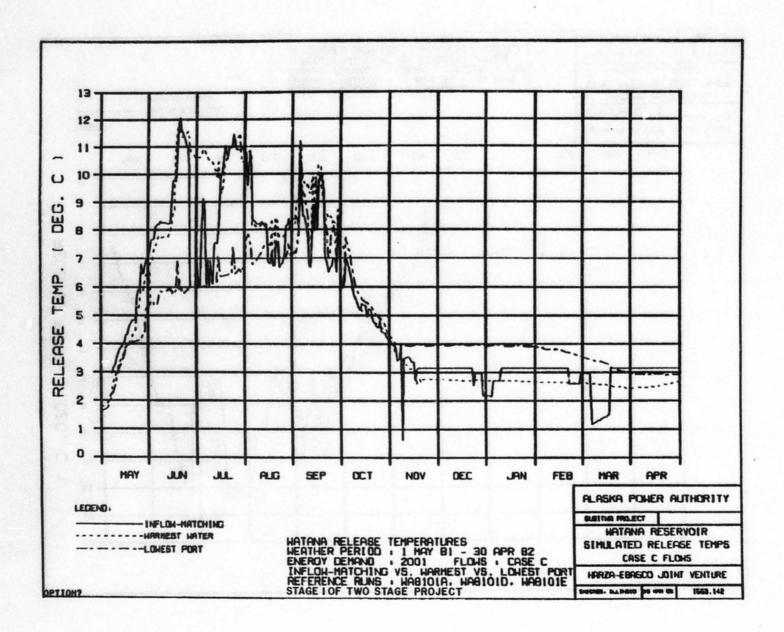


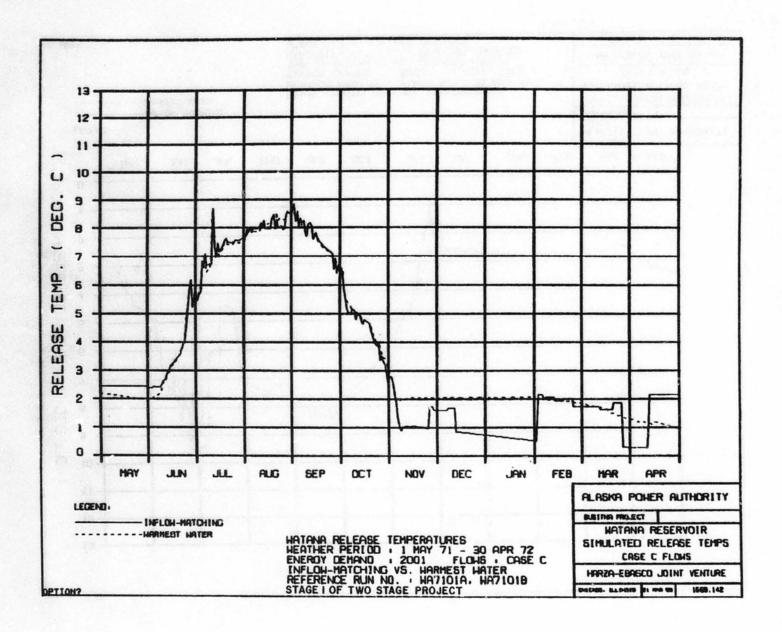


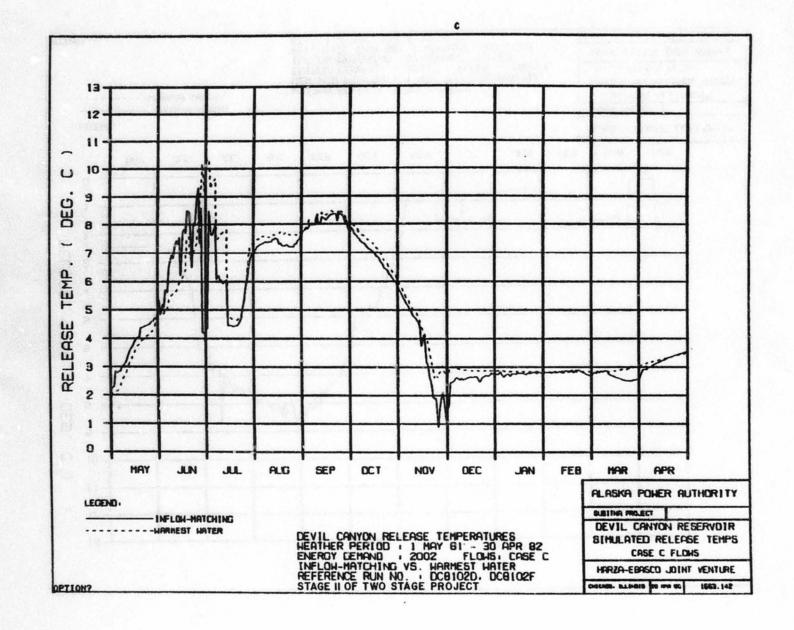


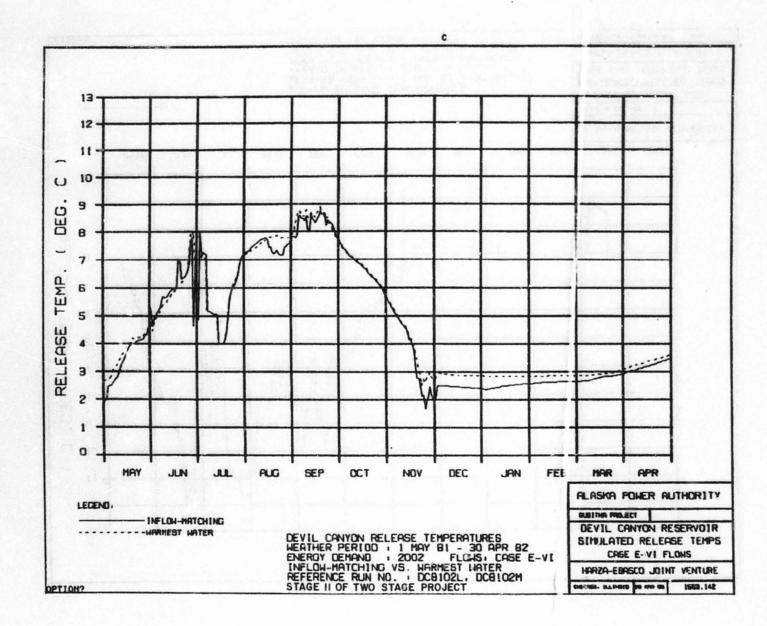


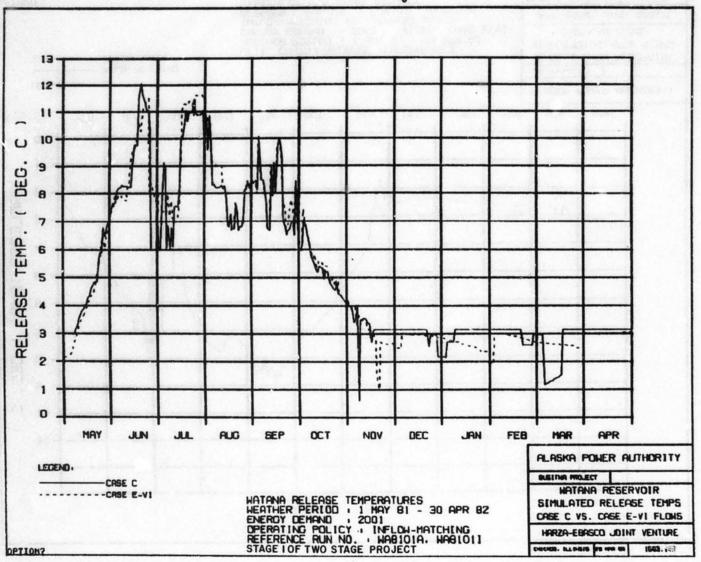


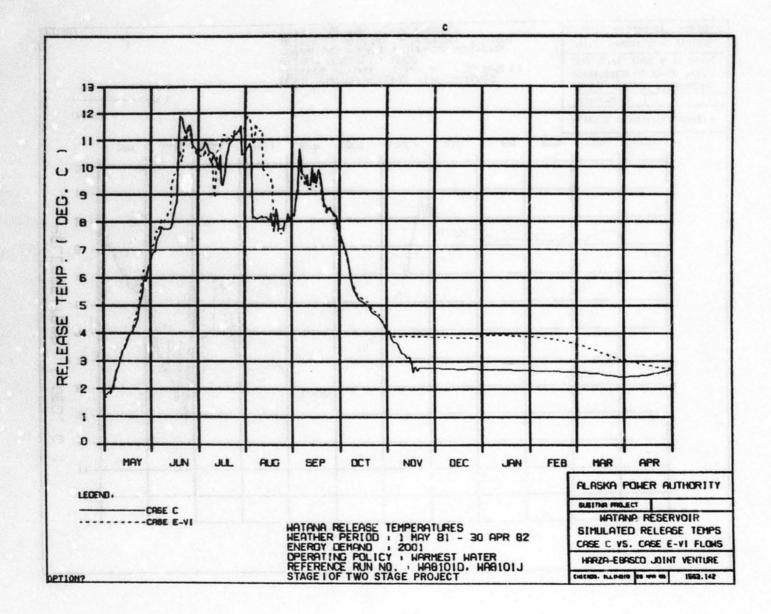


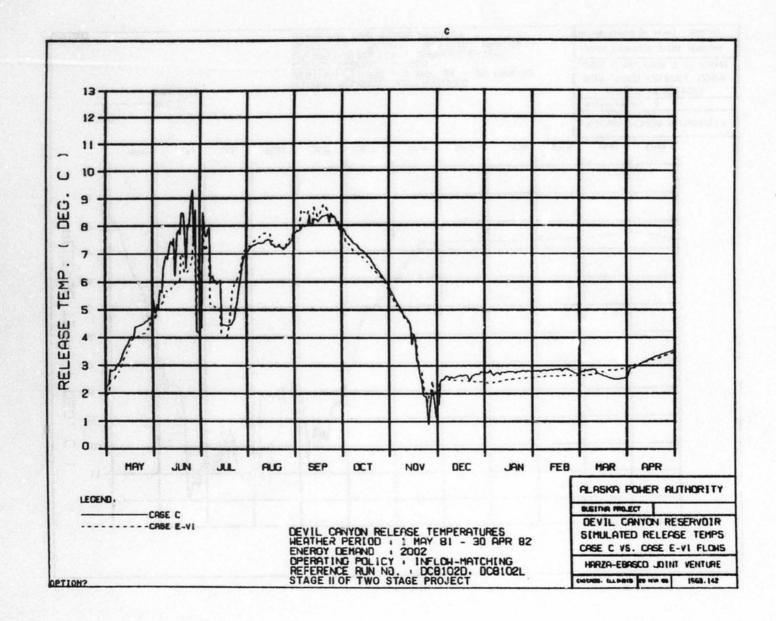


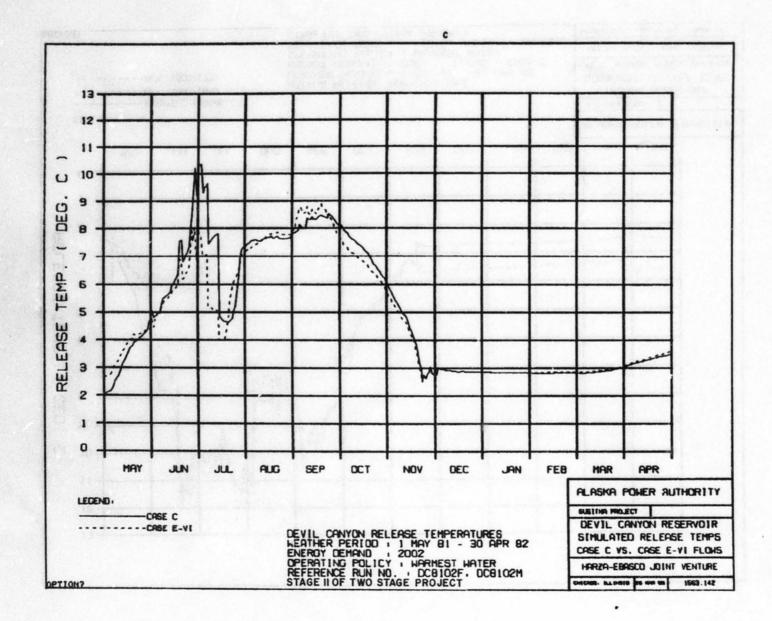


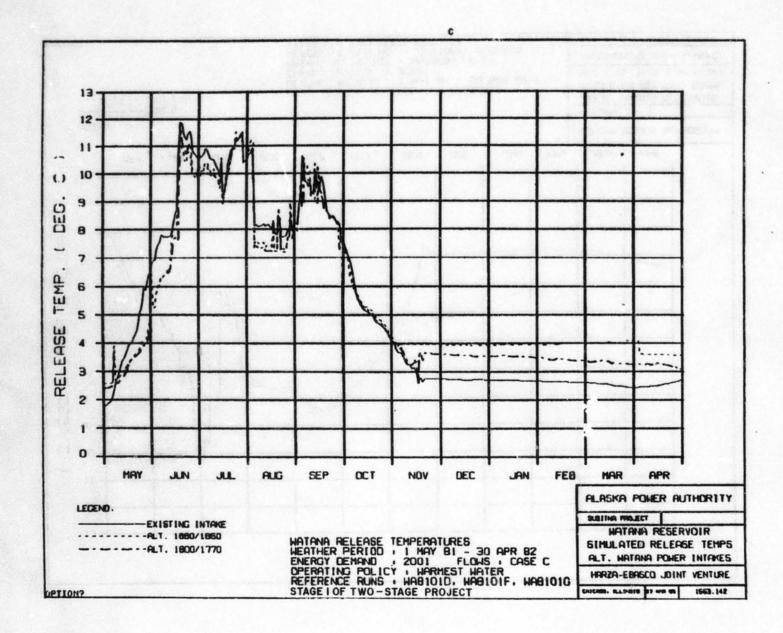


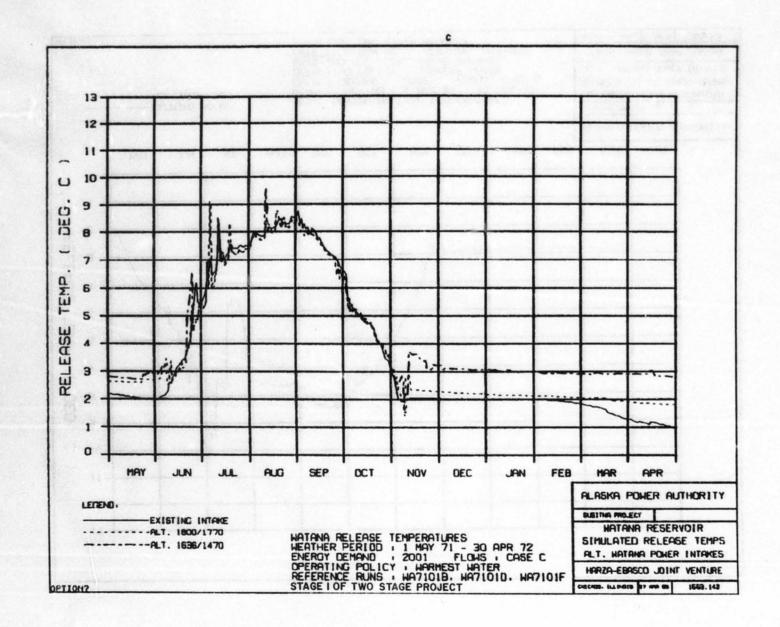


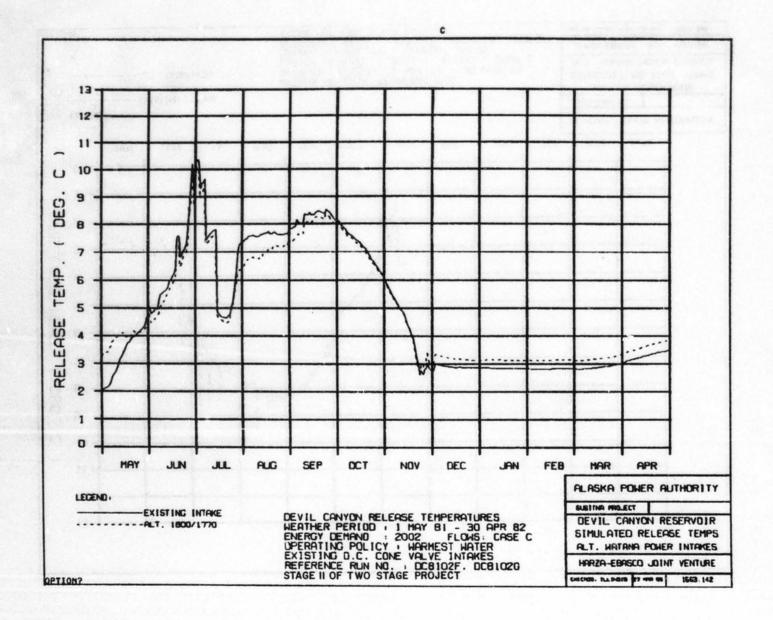


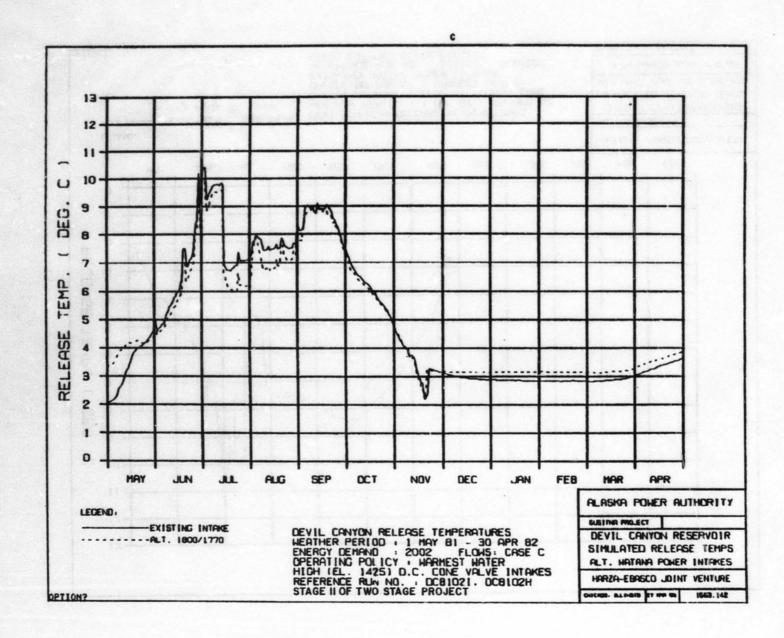


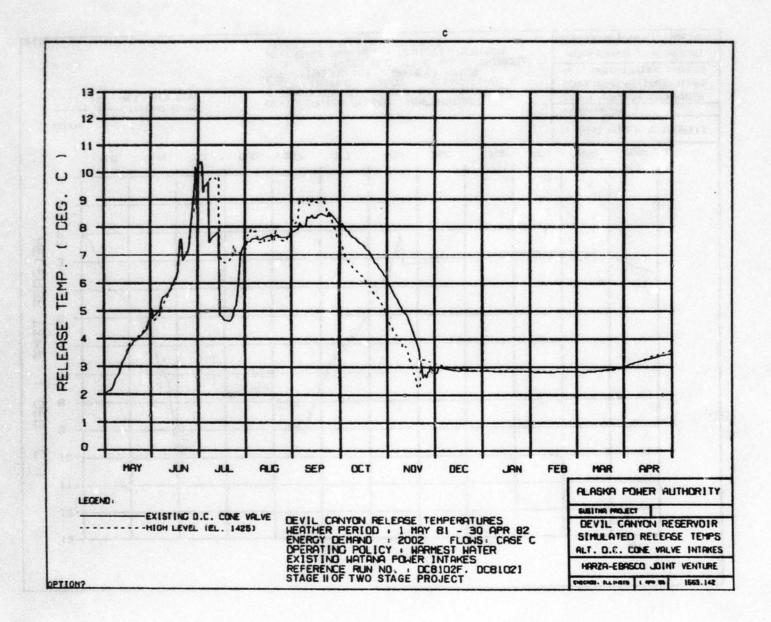


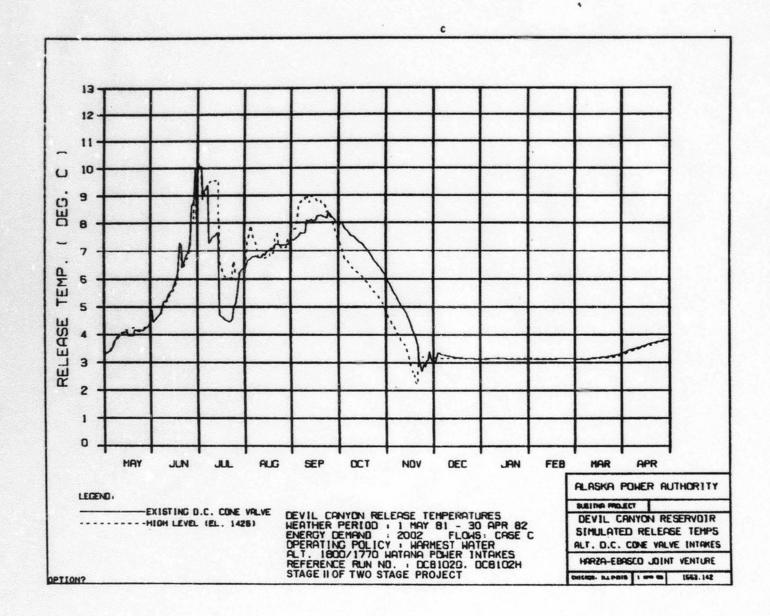






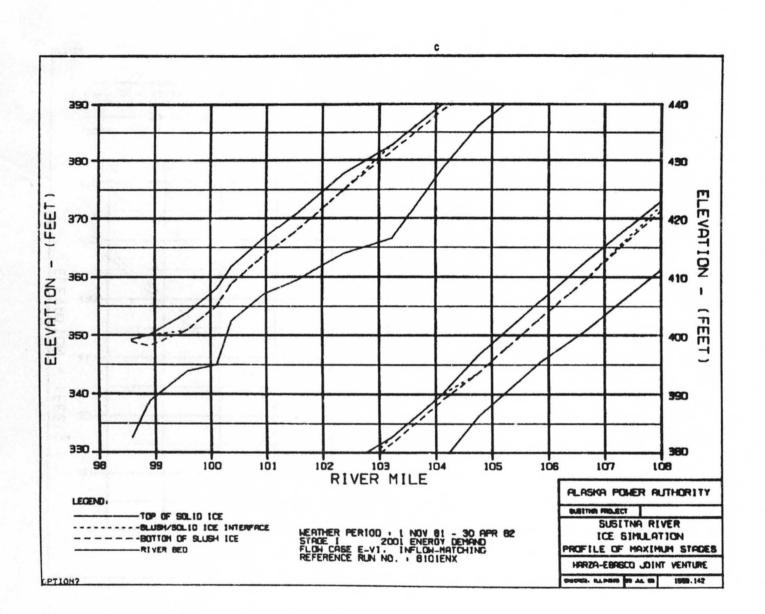




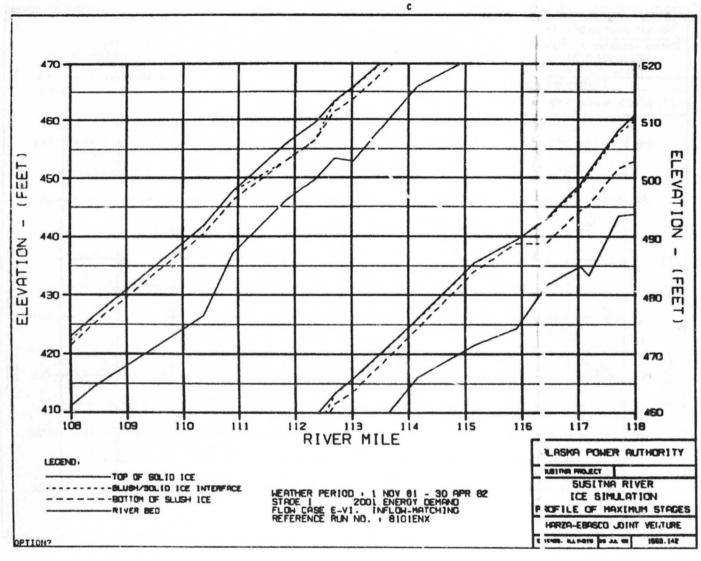


## EXHIBITS

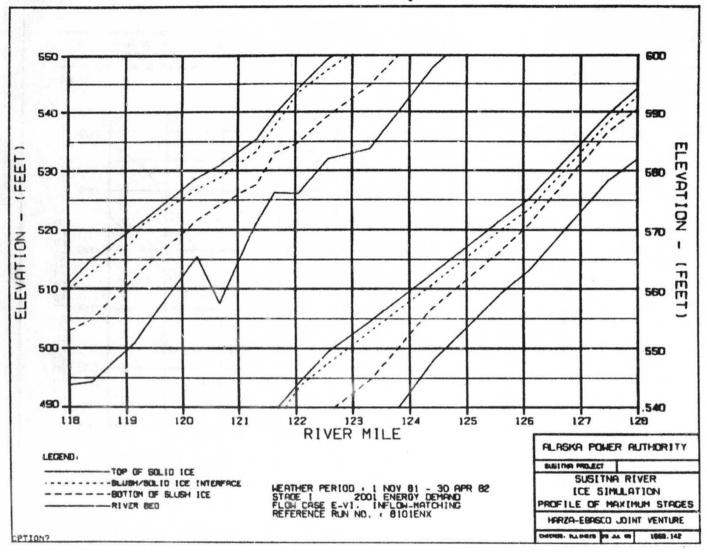
## EXHIBIT A



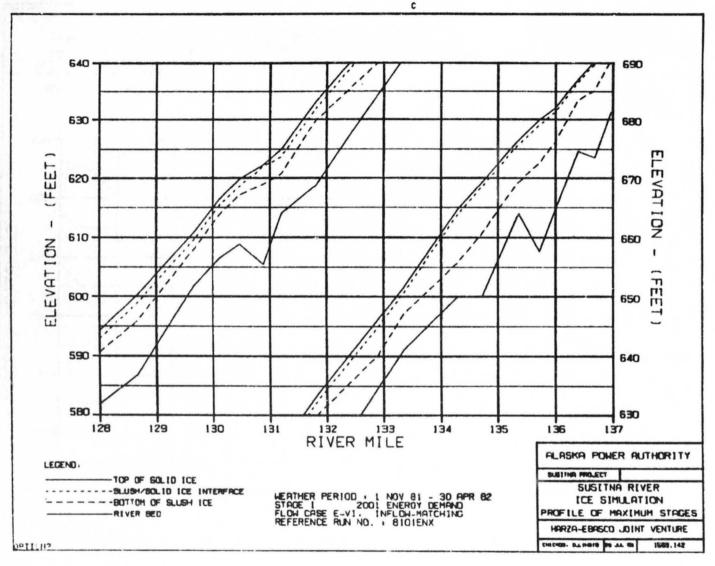




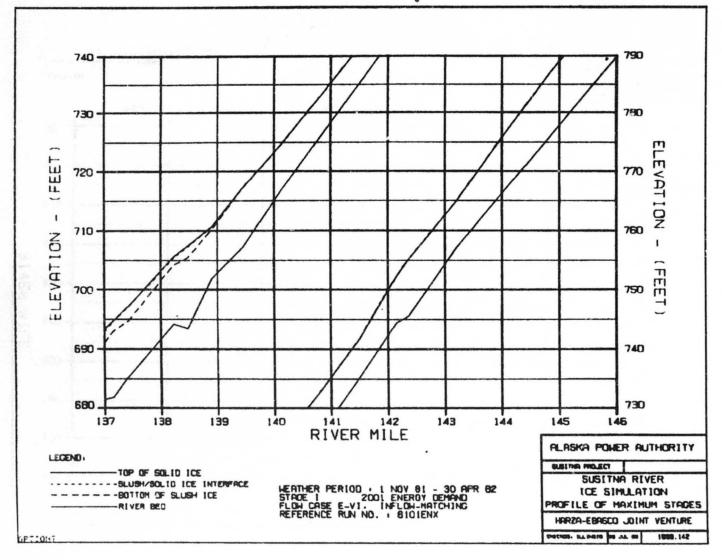


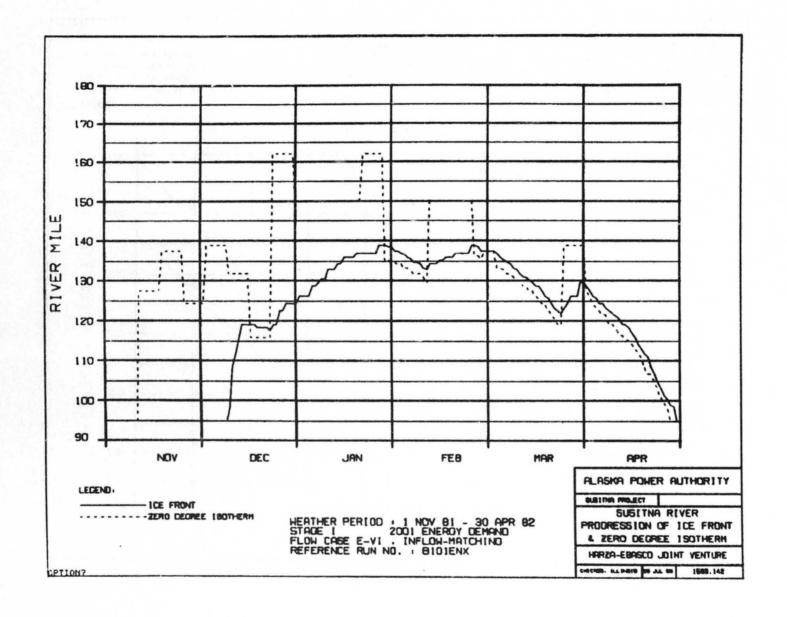


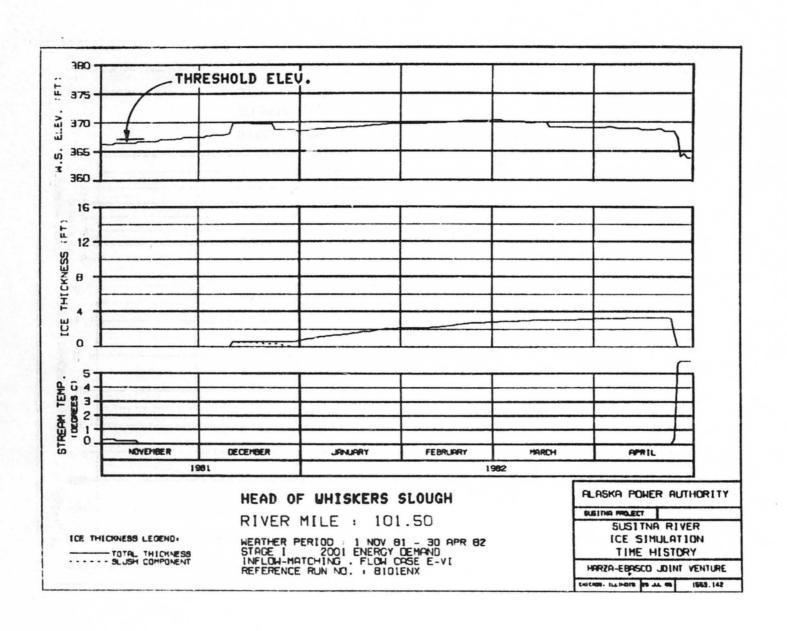


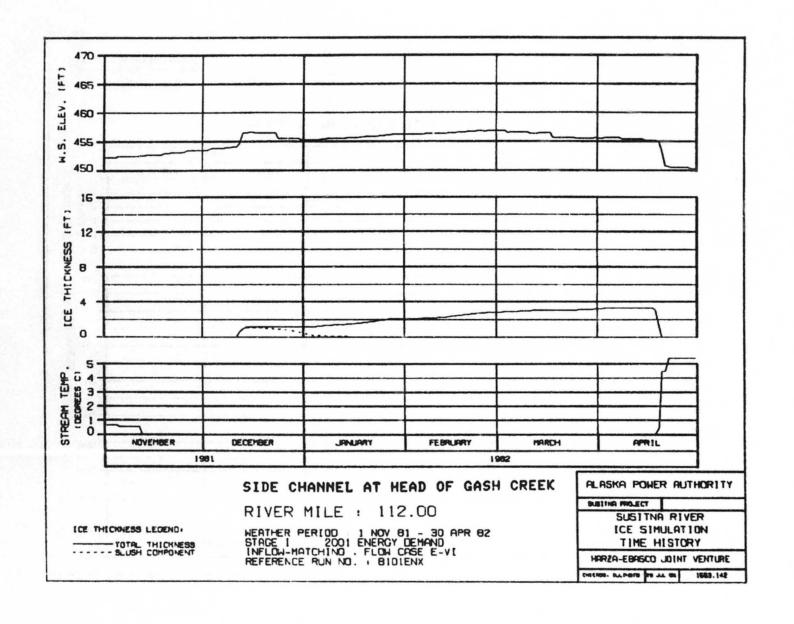


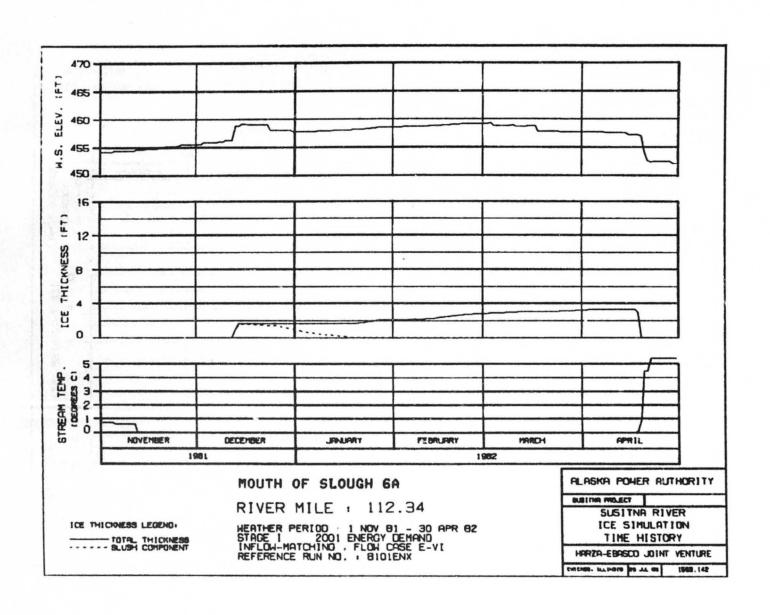


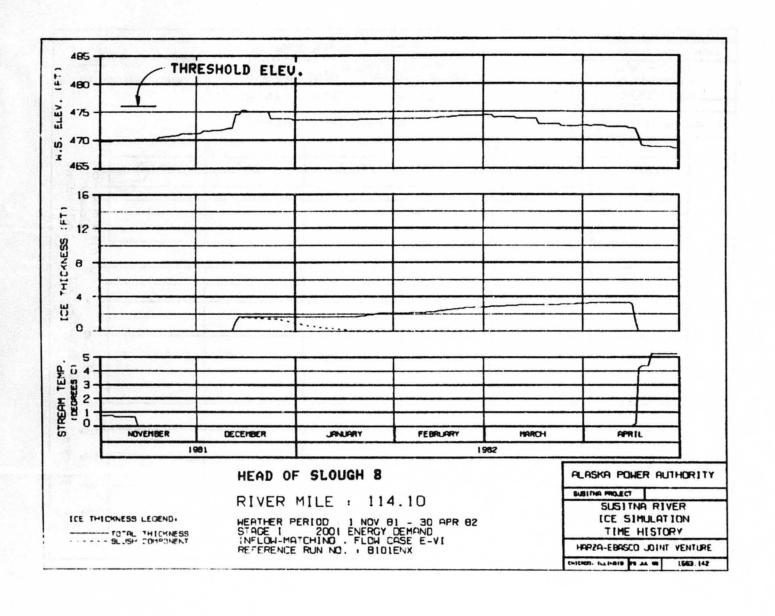


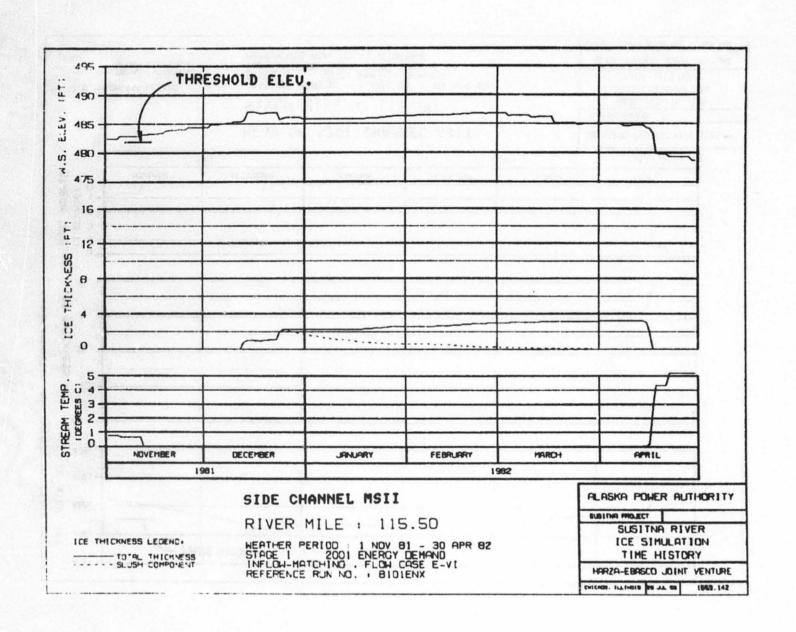


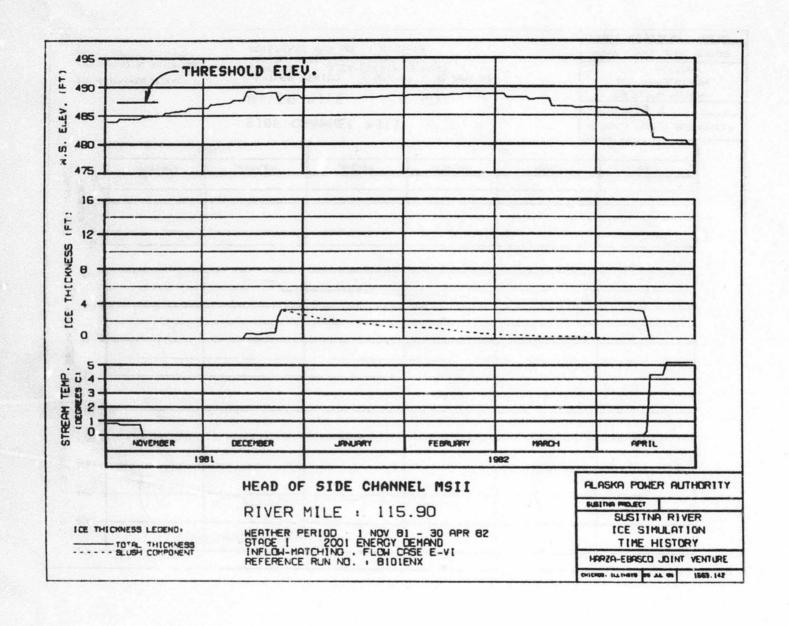


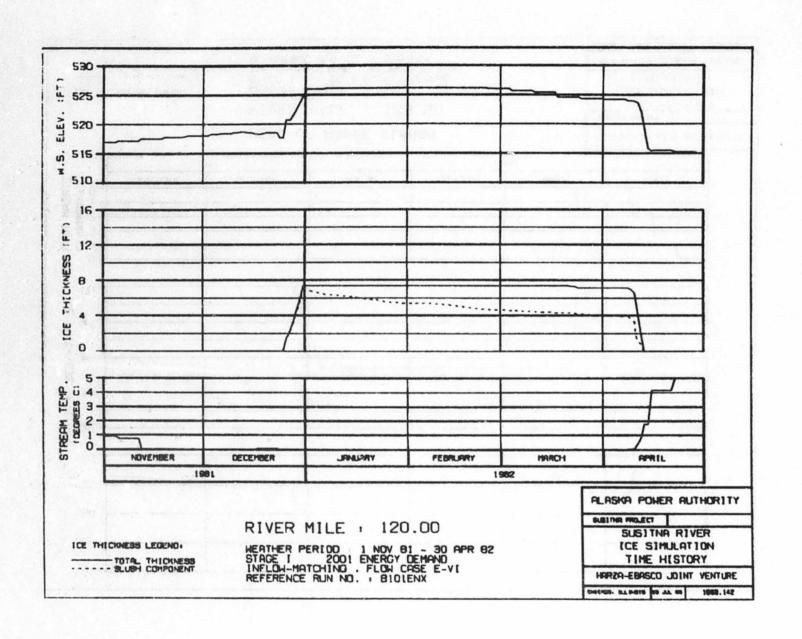


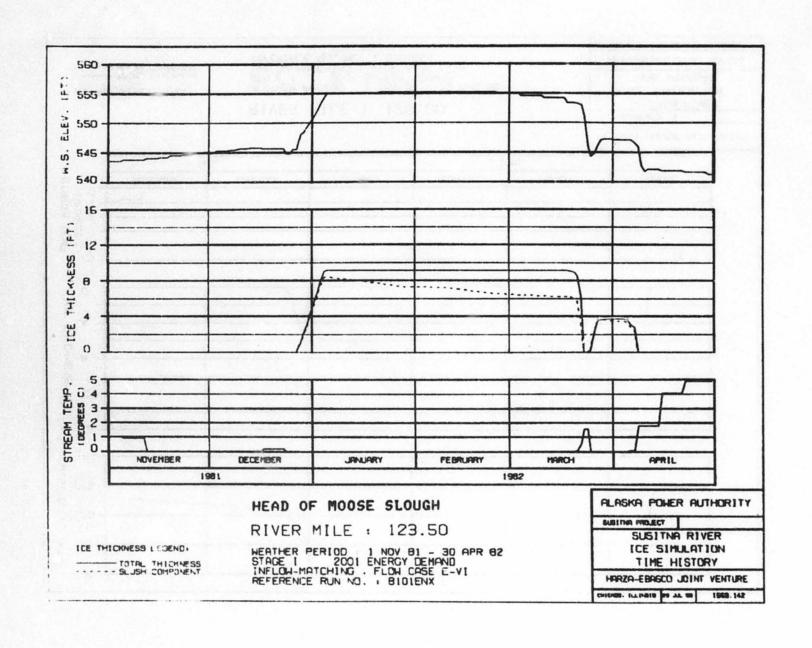


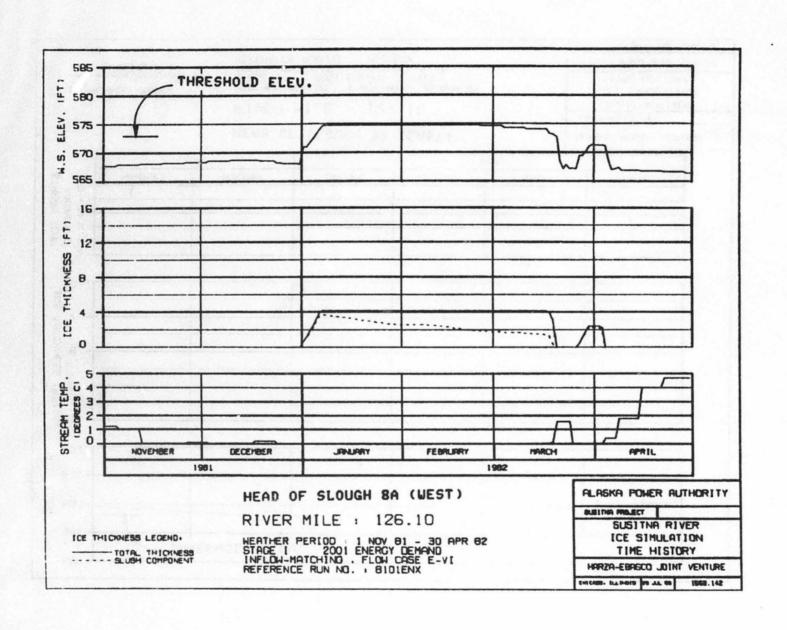


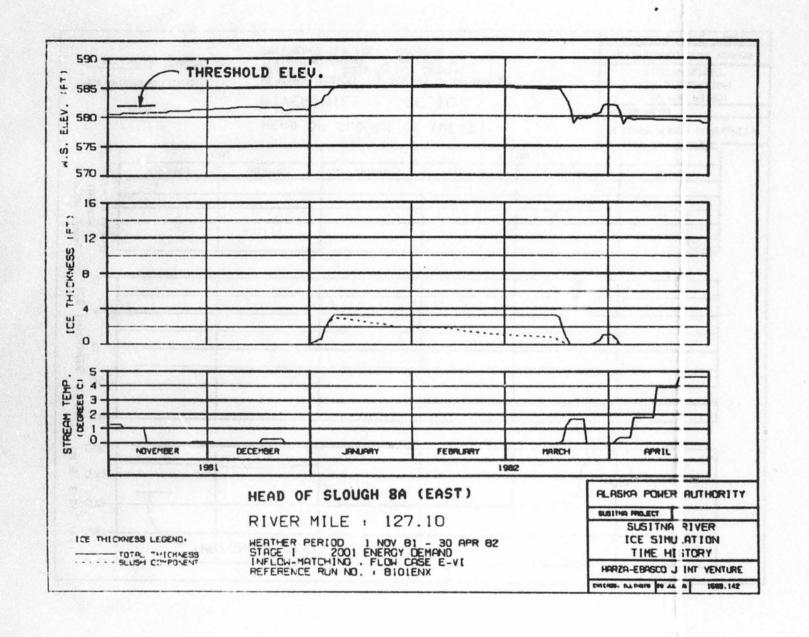


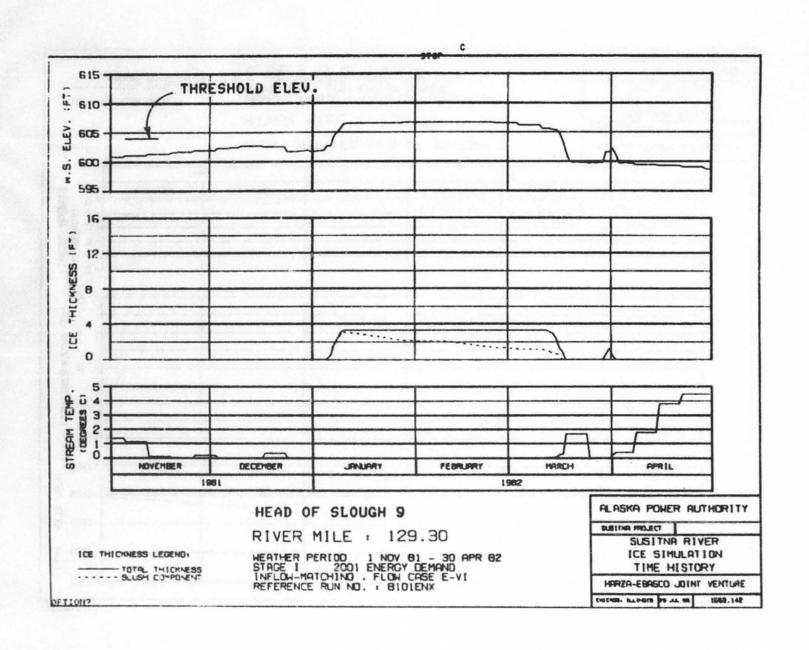


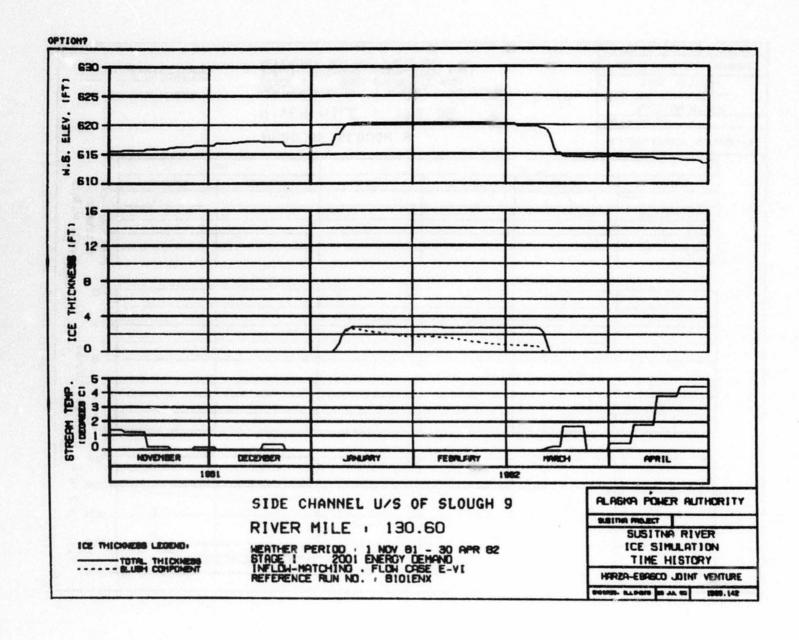


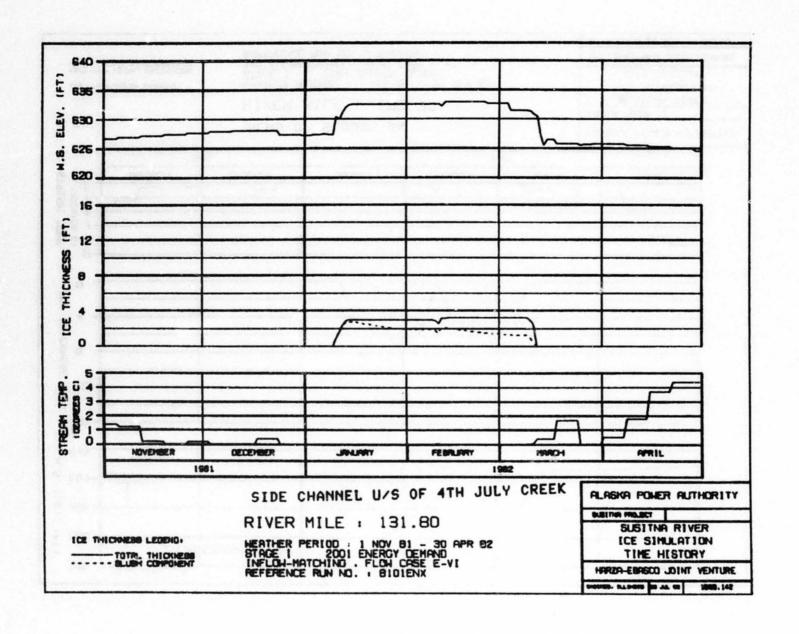


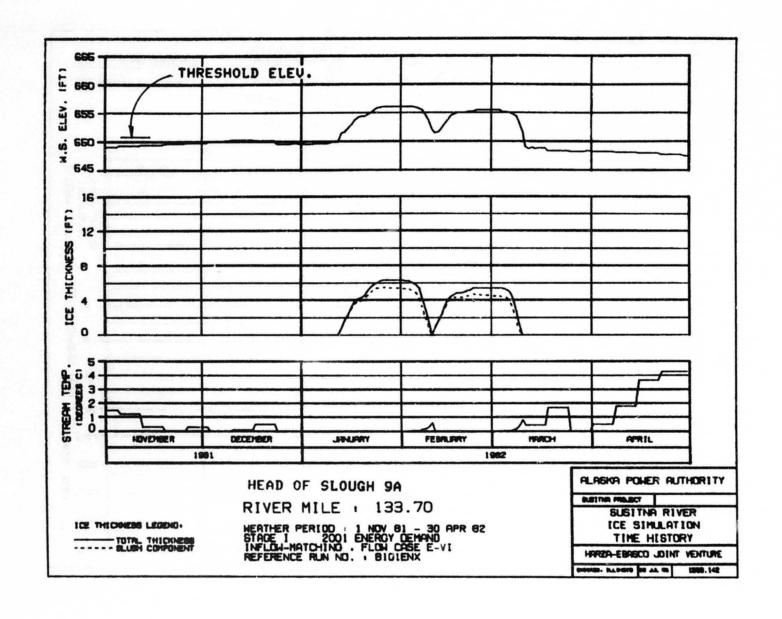




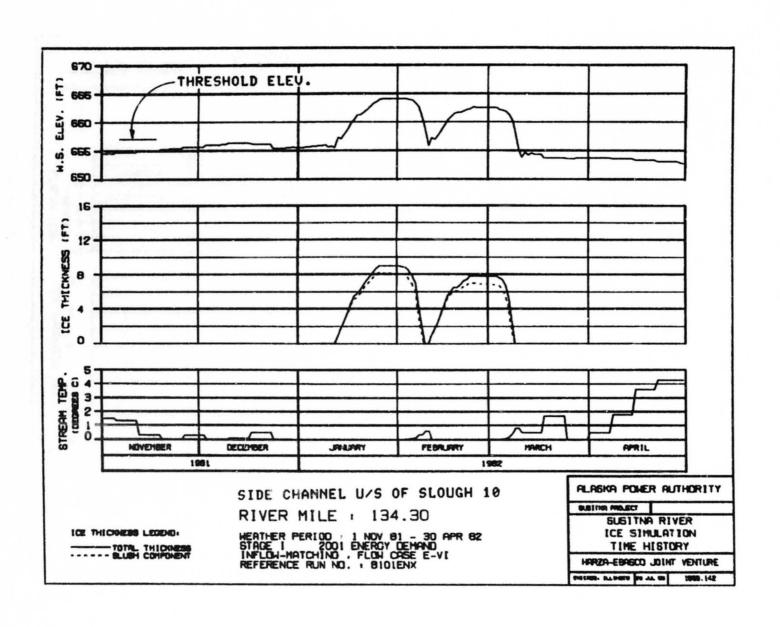


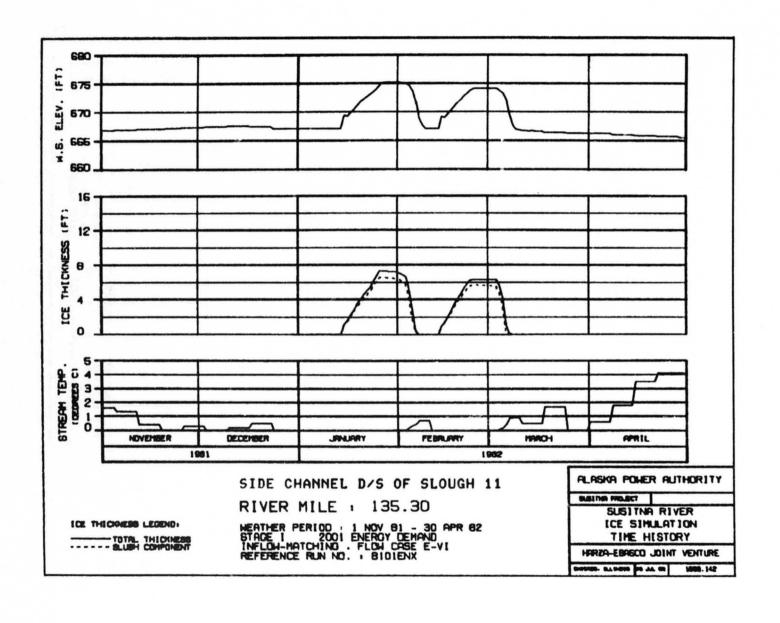


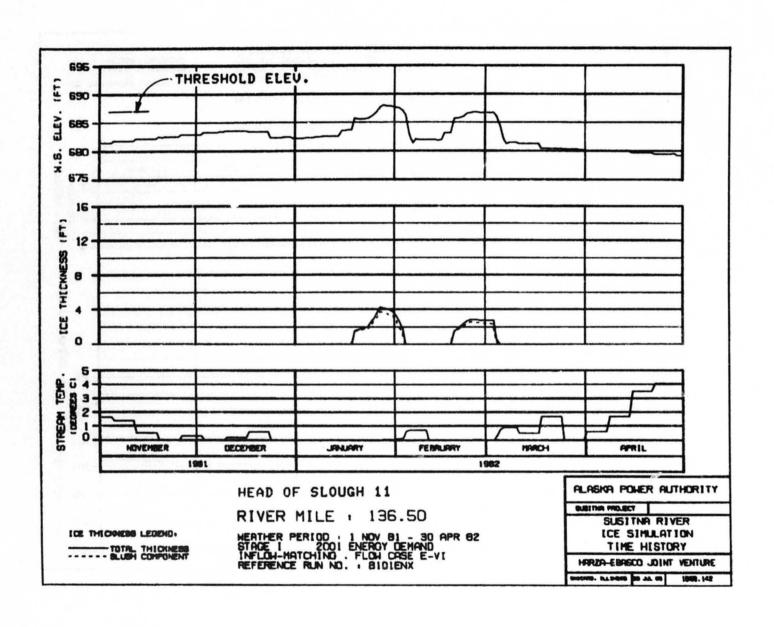


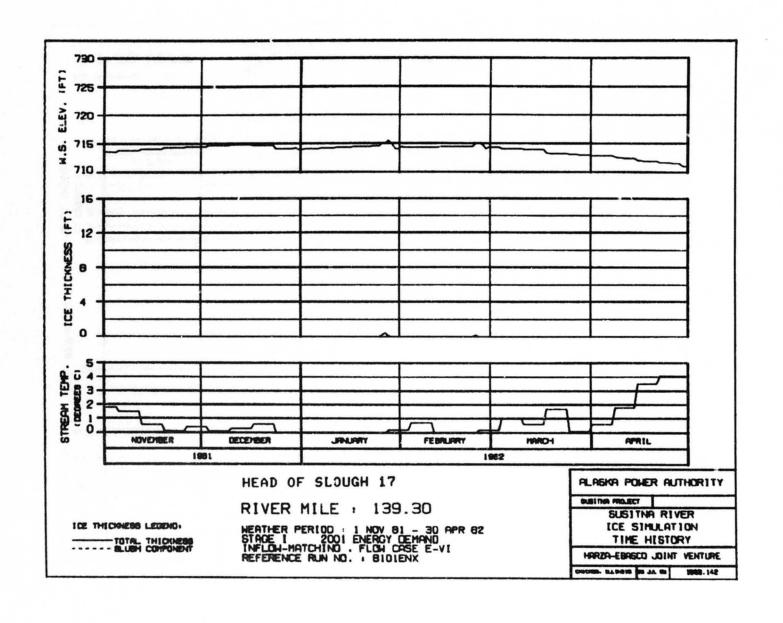


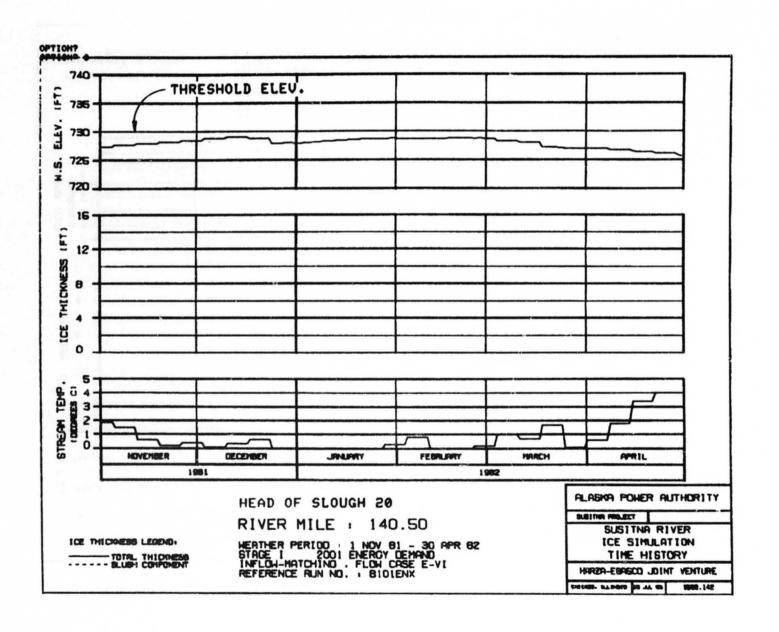
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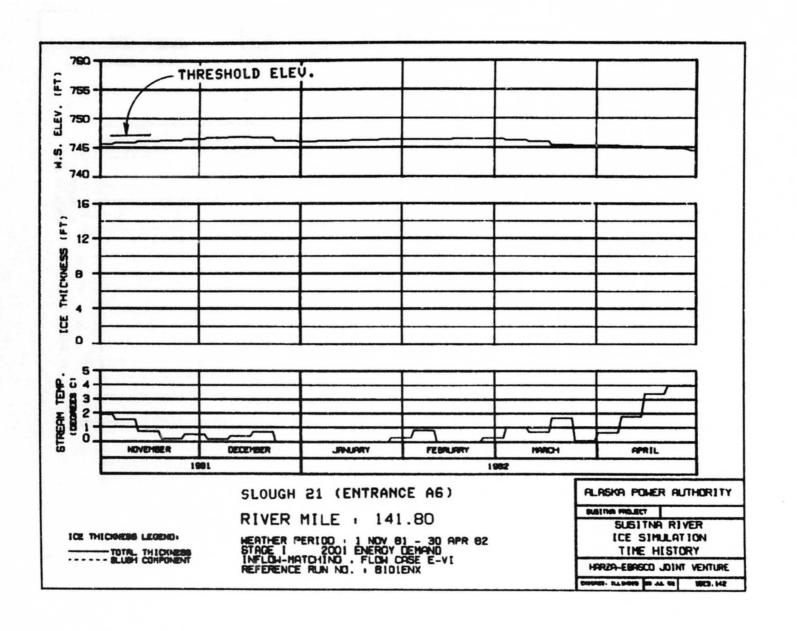


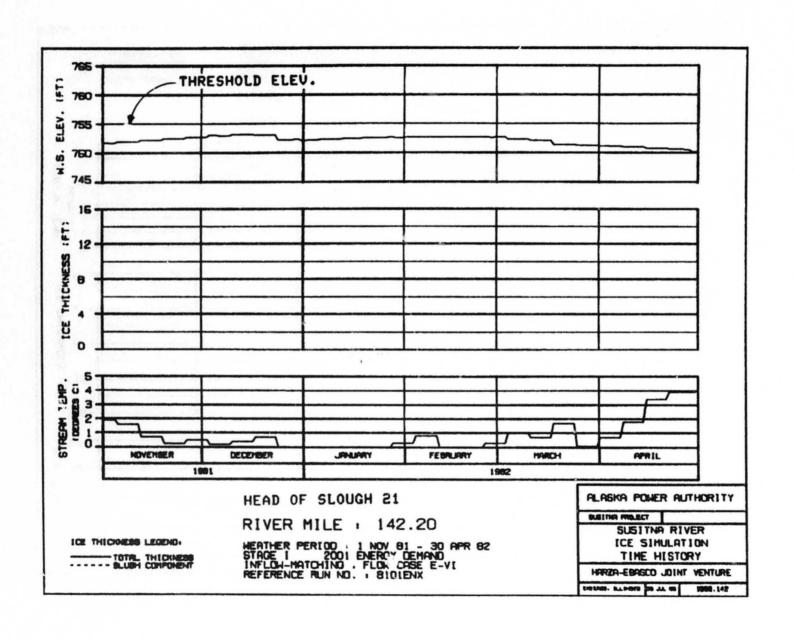


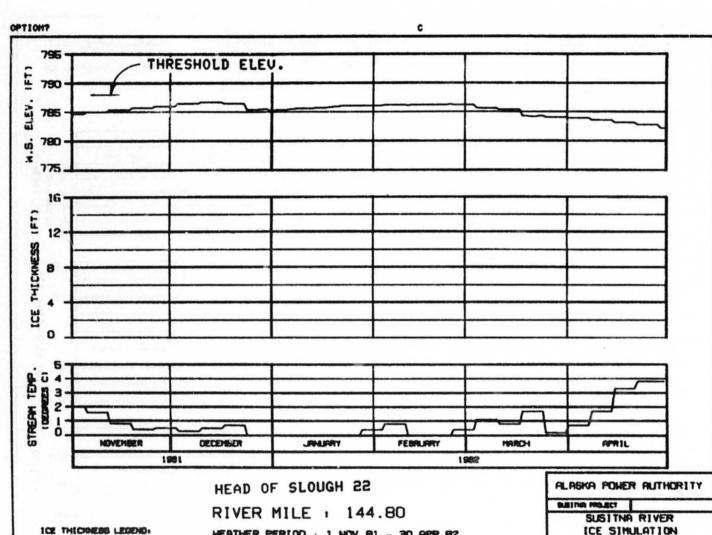










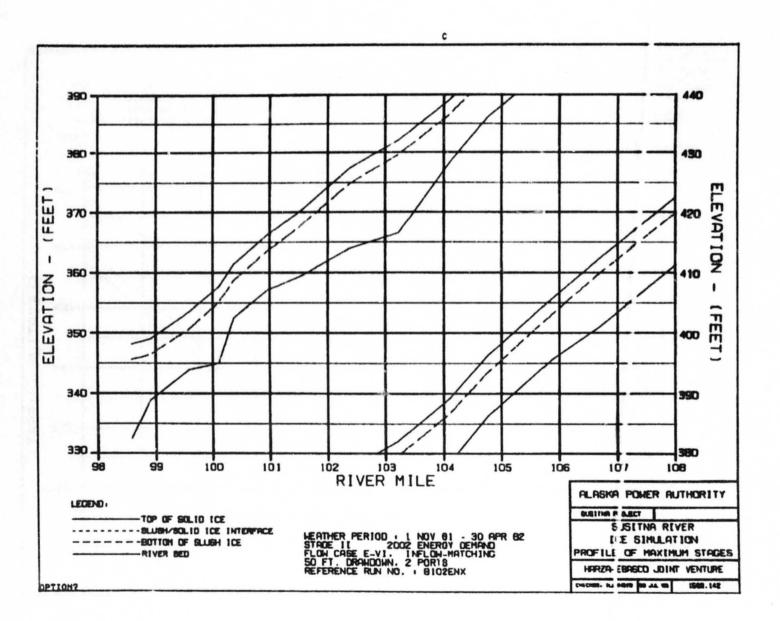


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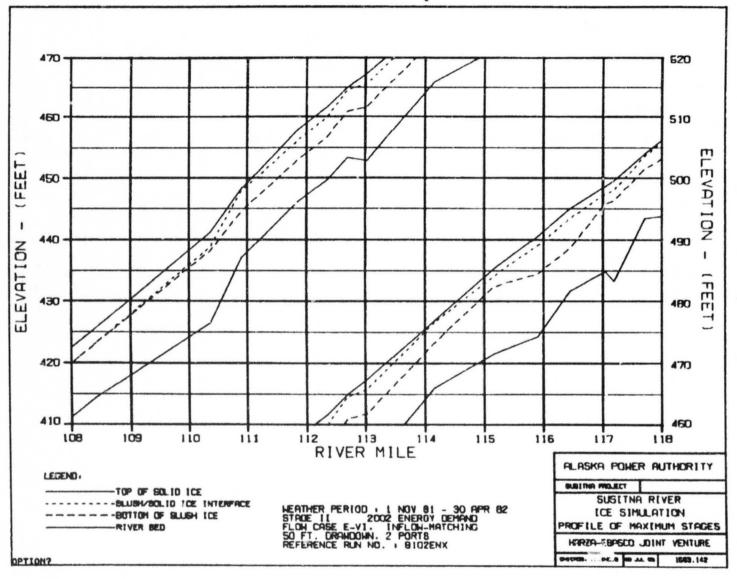
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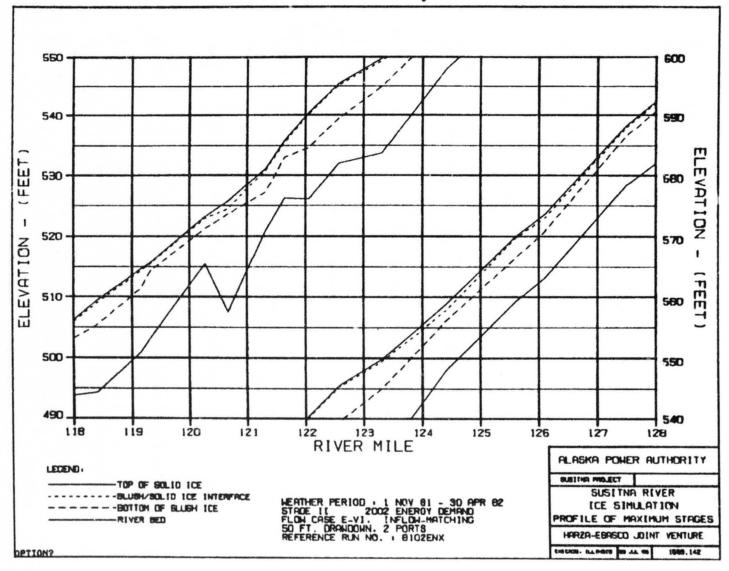
ICE THICHNESS LEGENO. HEATHER PERIOD : 1 NOV 81 - 30 APR 82 STAGE [ 2001 ENERGY DEMAND INFLOH-MATCHIND : FLOH CASE E-VI REFERENCE RUN NO. : 8101ENX TOTAL THICKNESS OPTION?

## EXHIBIT B

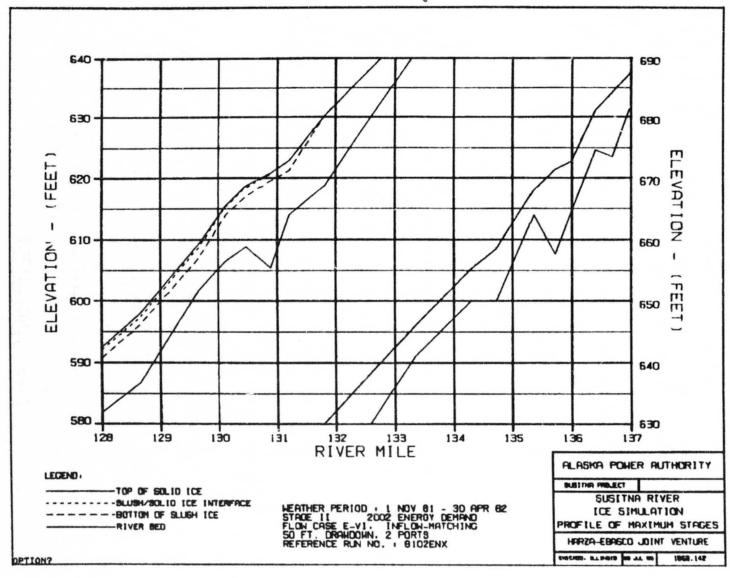


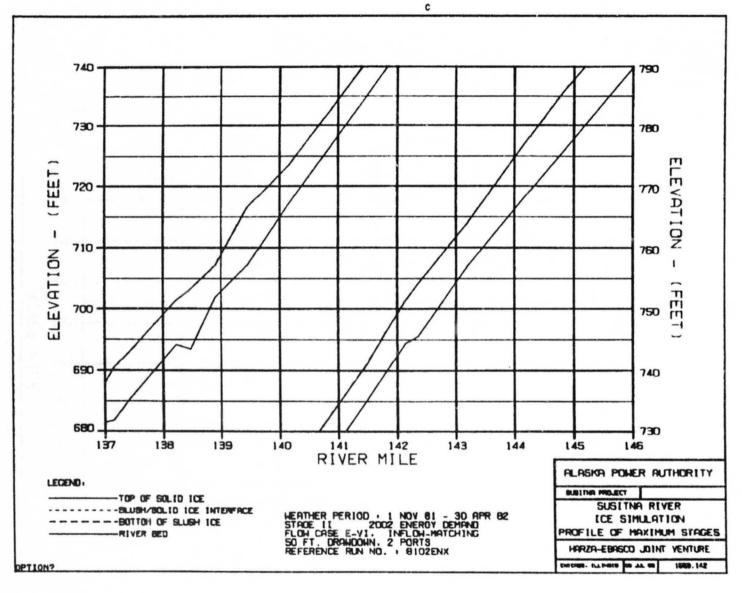
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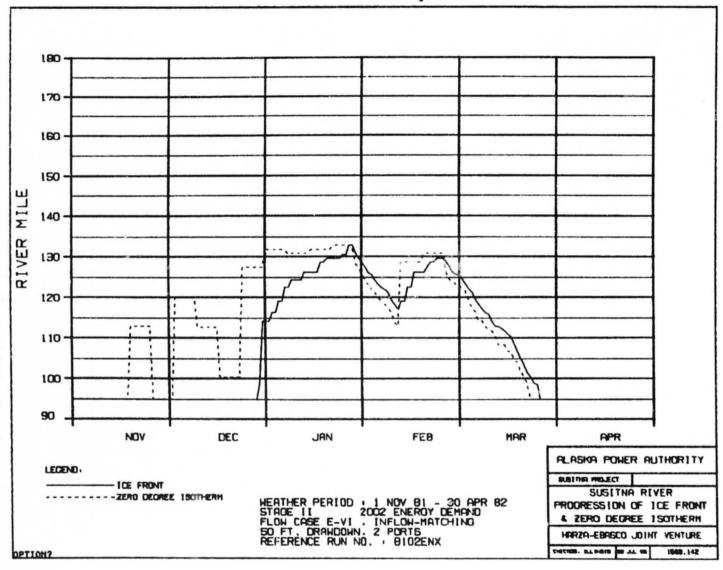




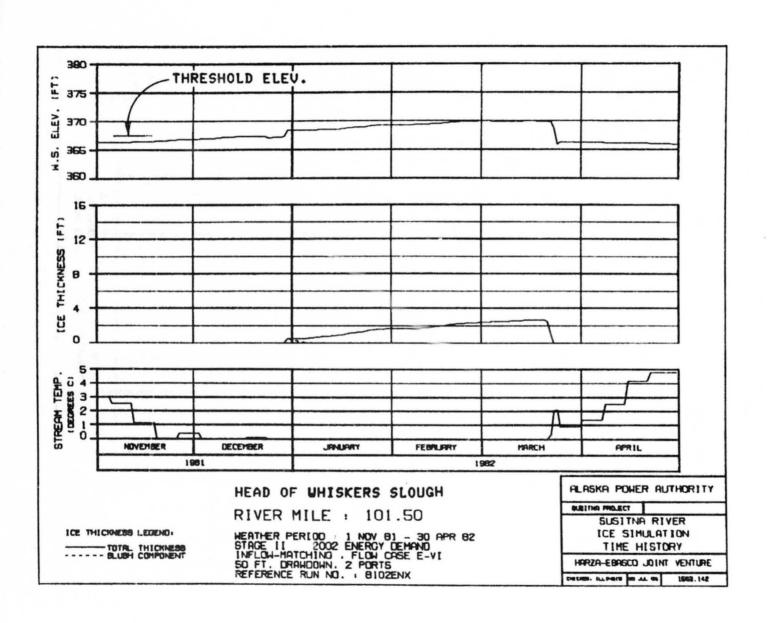




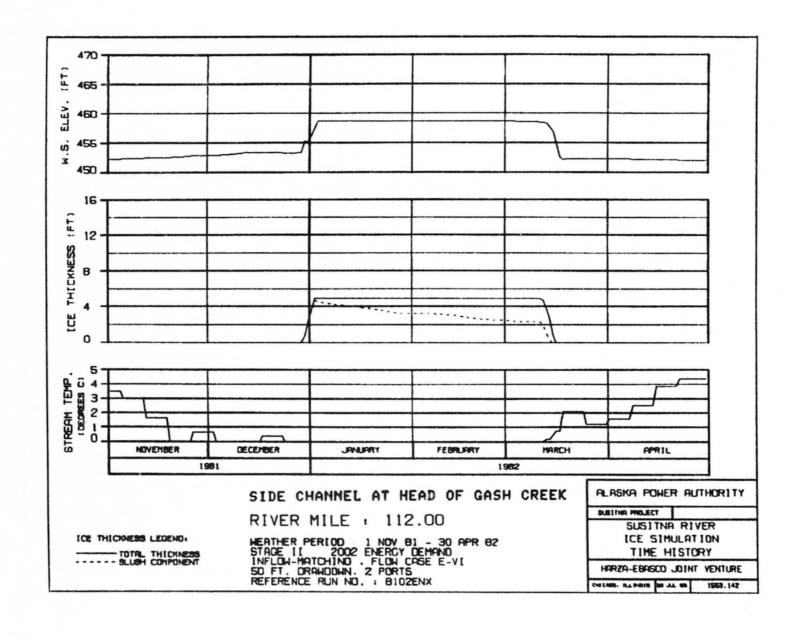


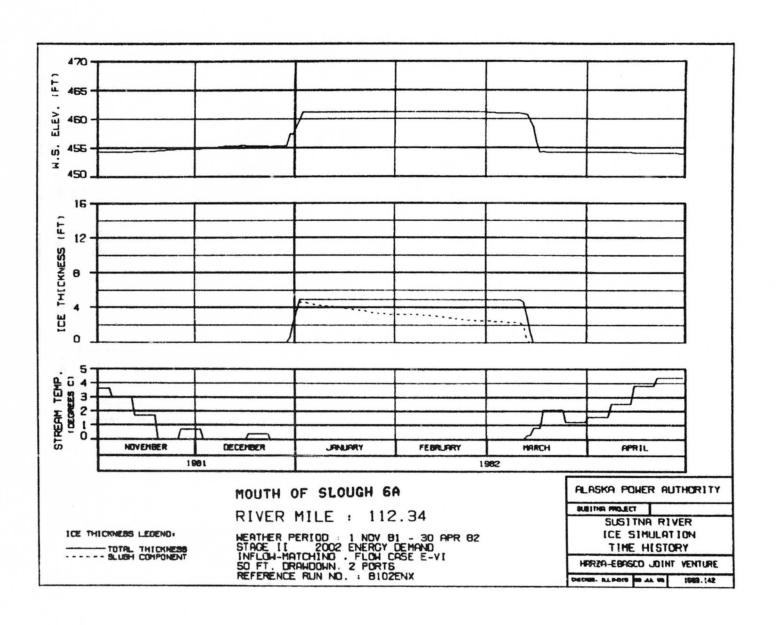


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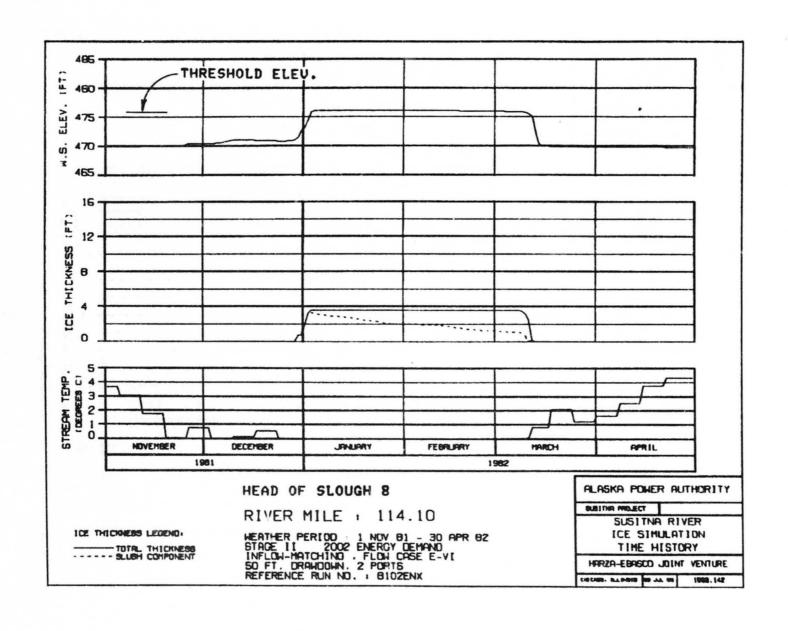
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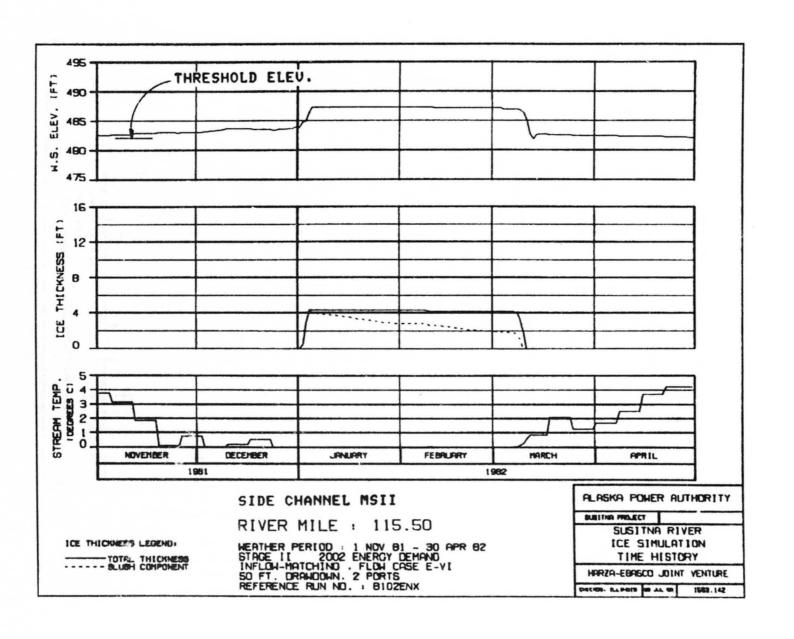


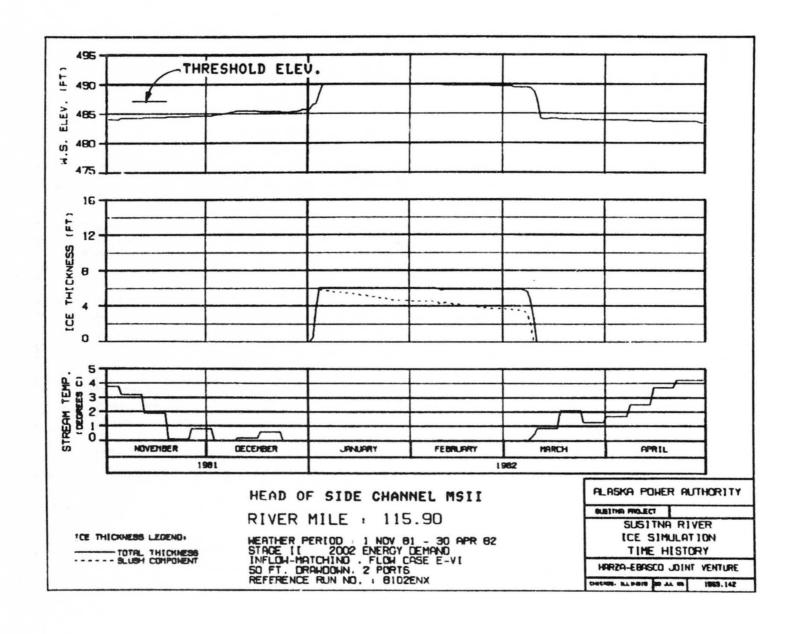


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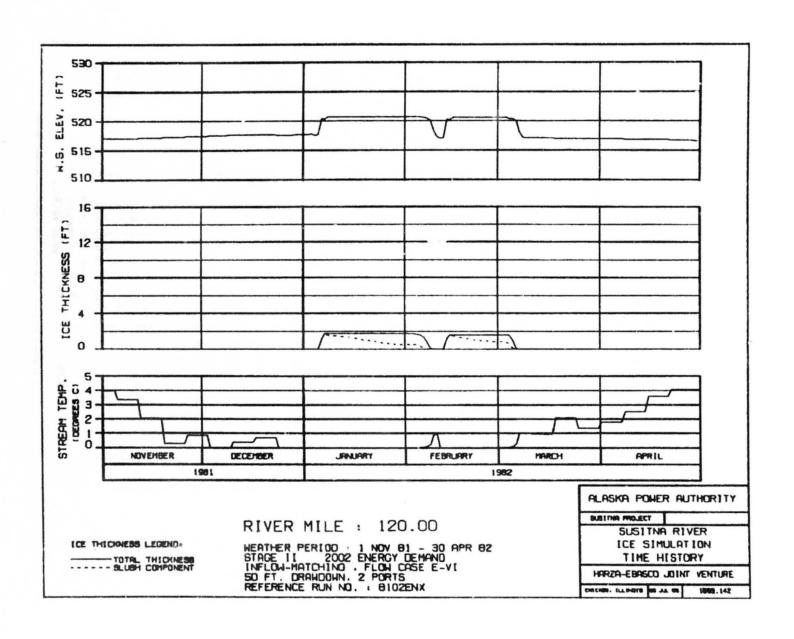


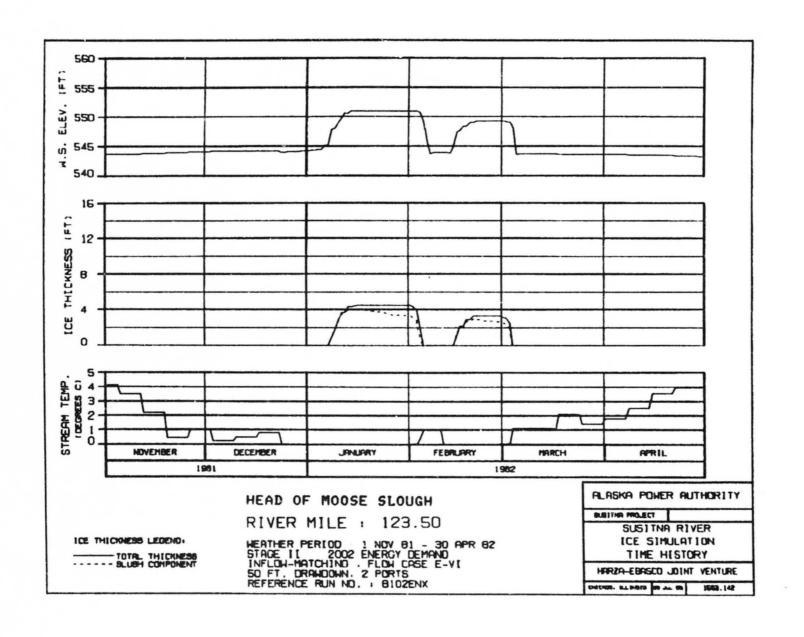


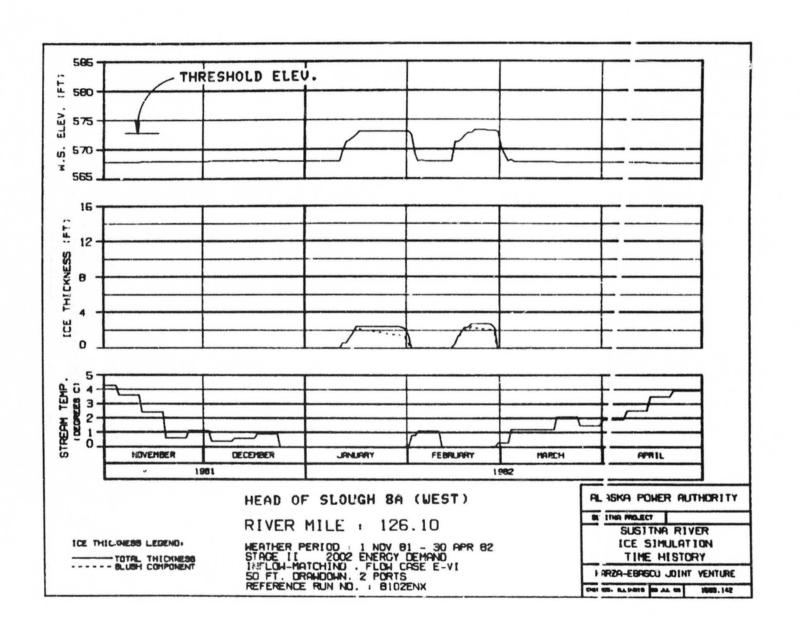


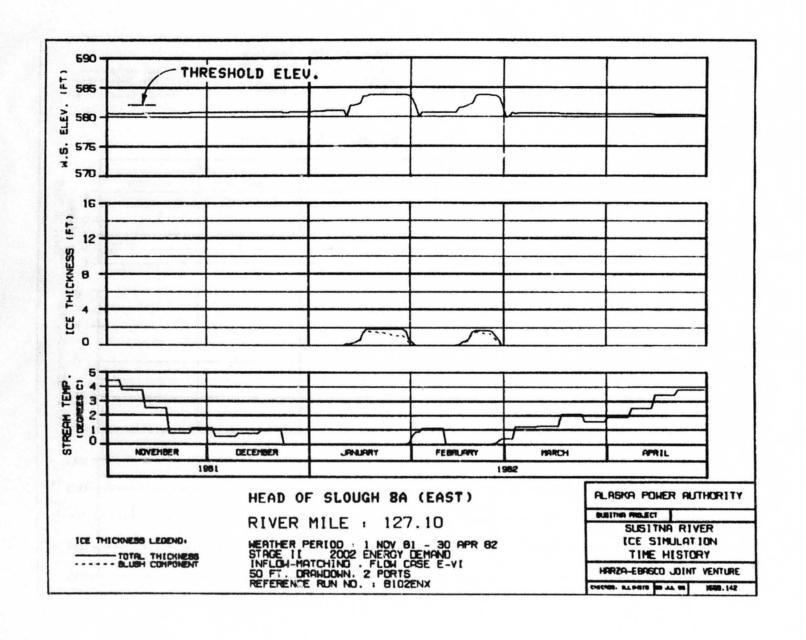


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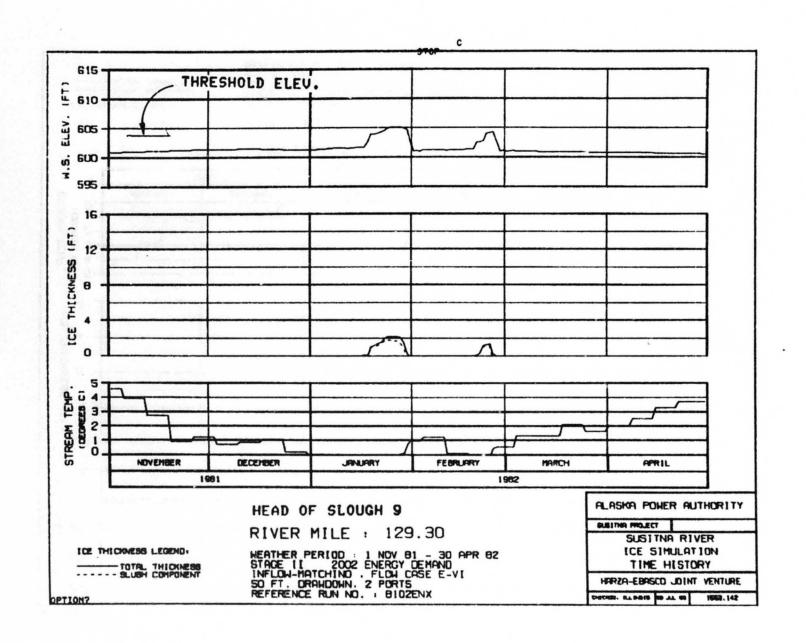


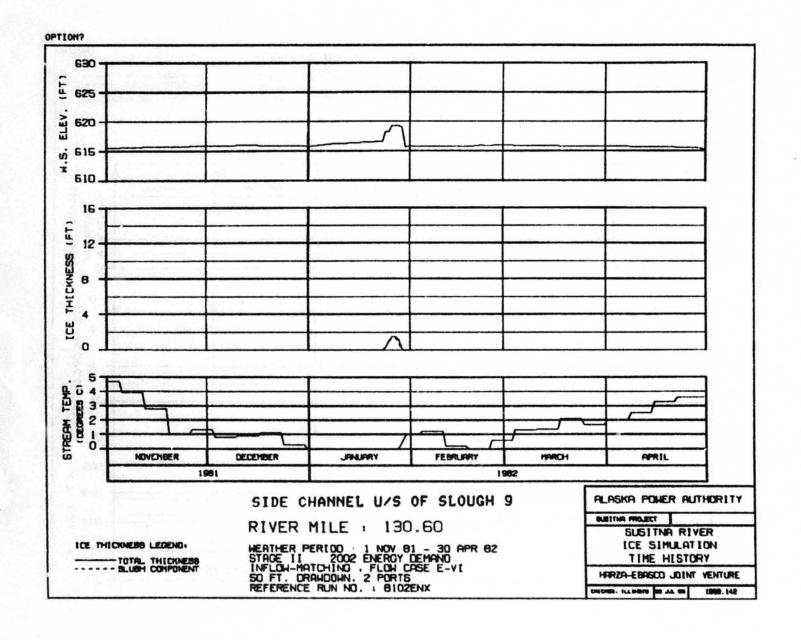


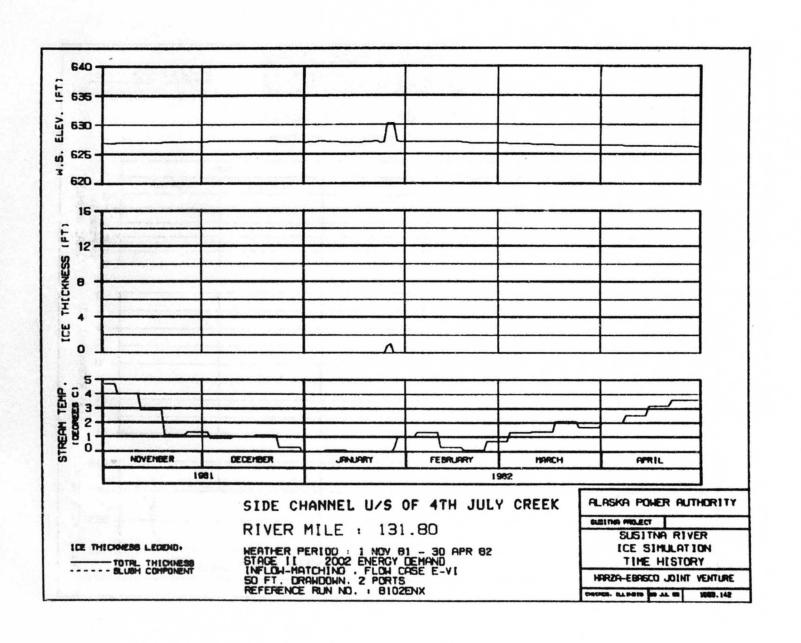


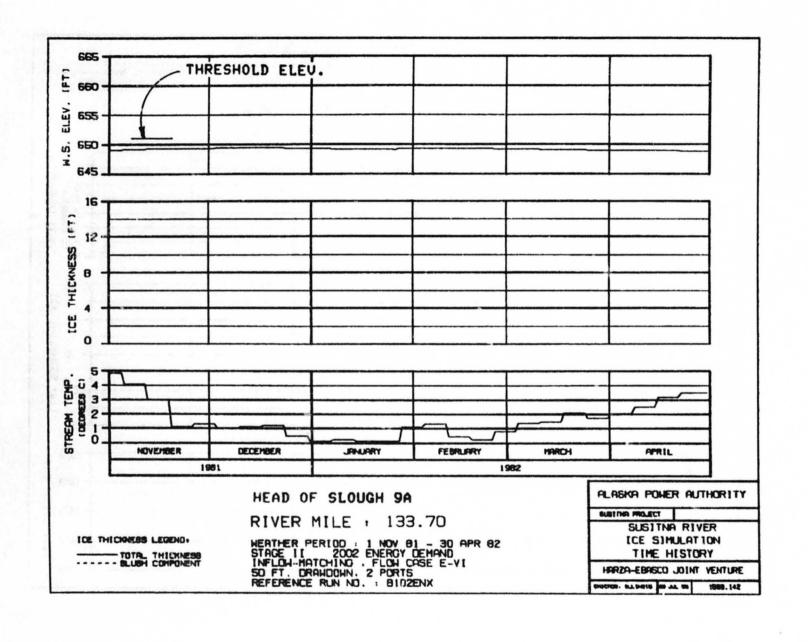


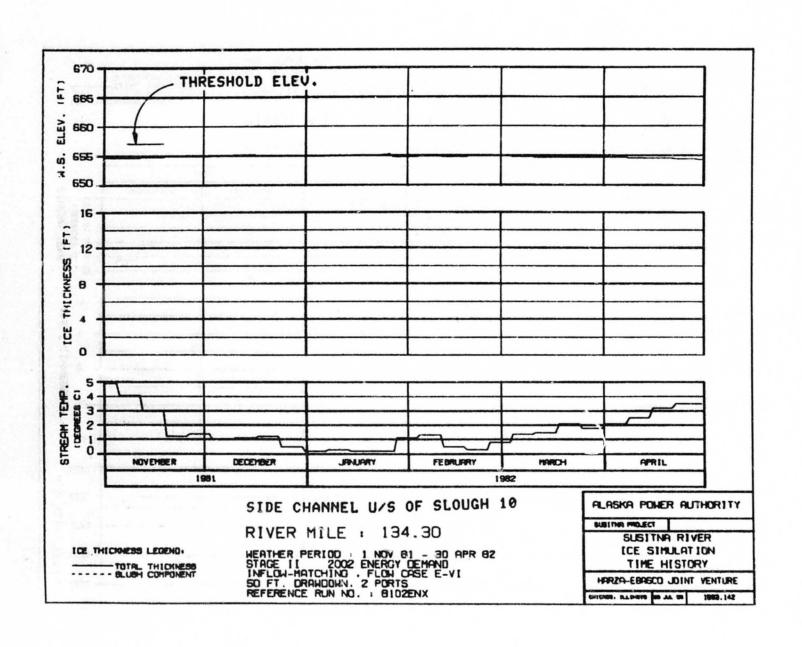
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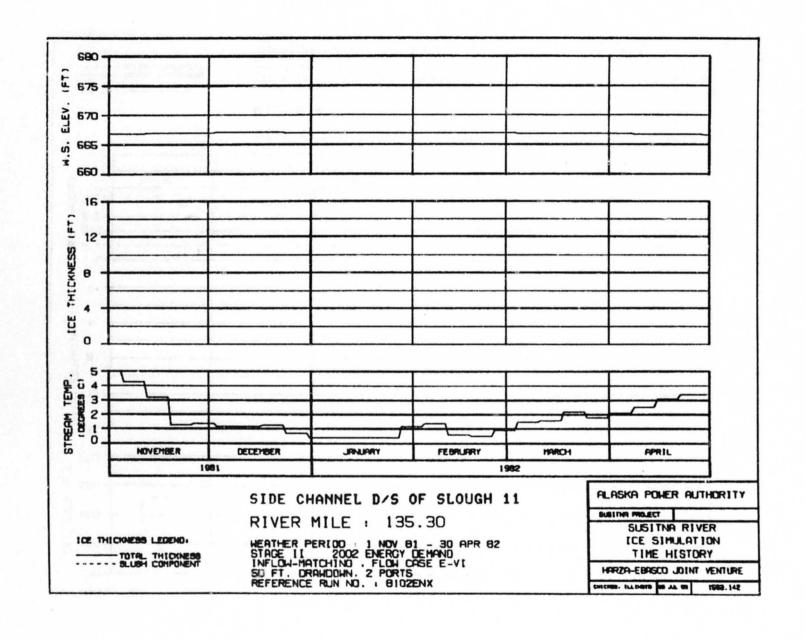




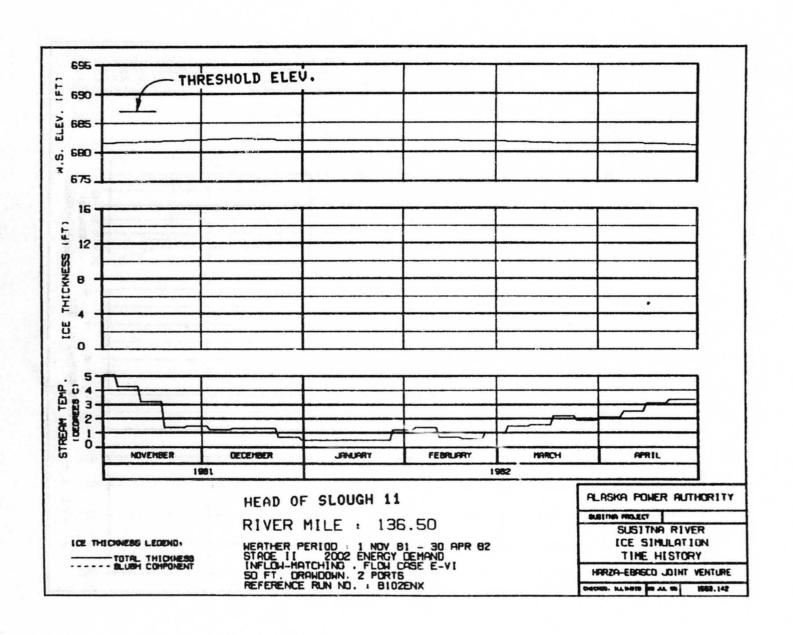


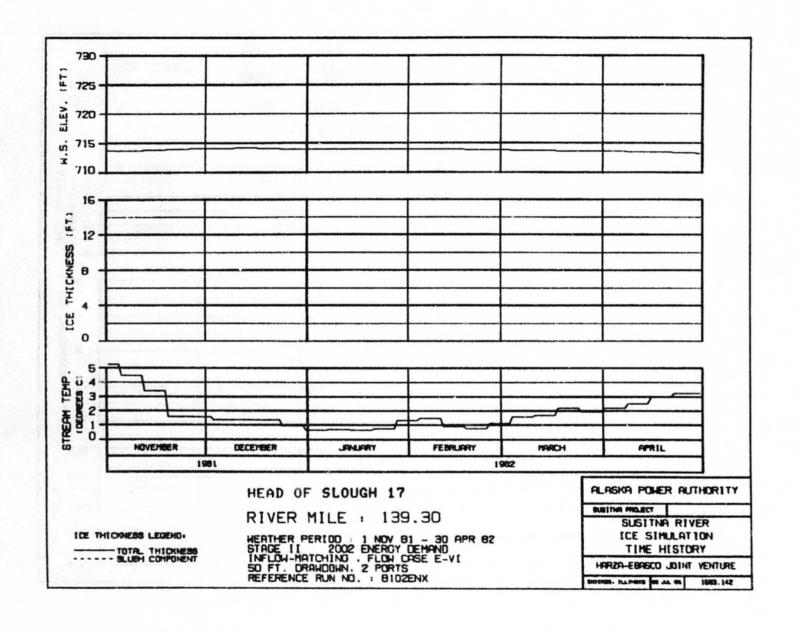




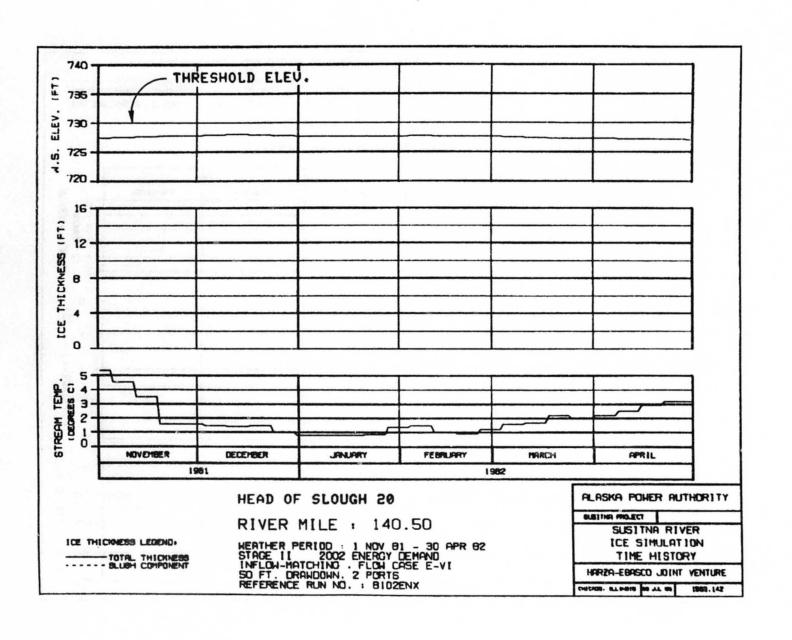


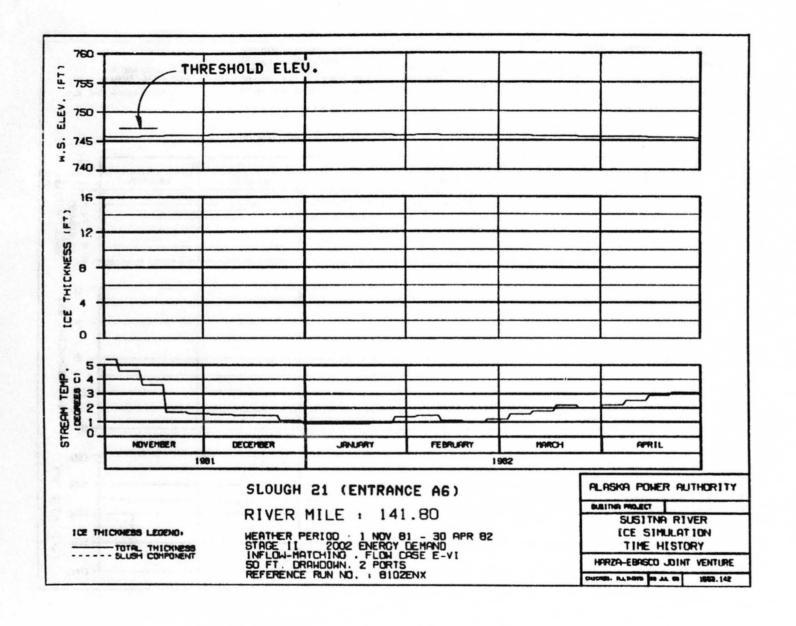
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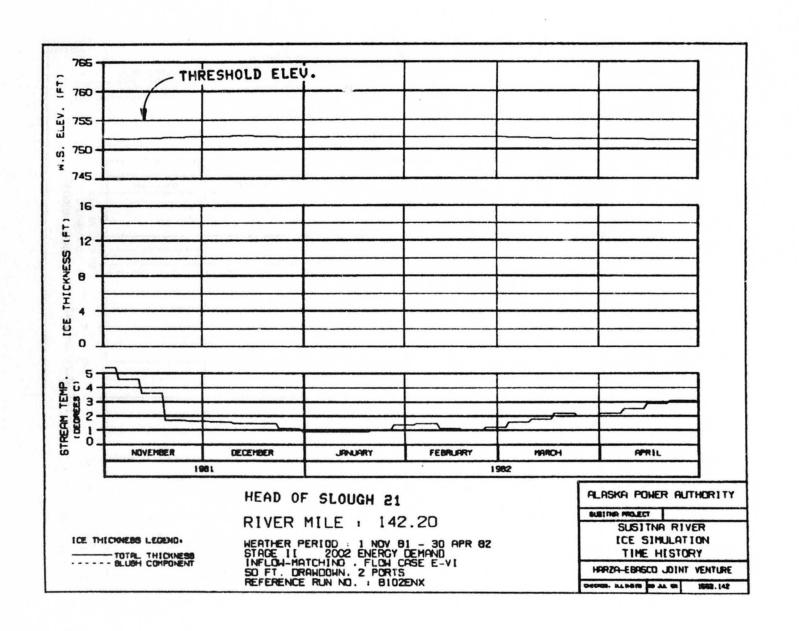


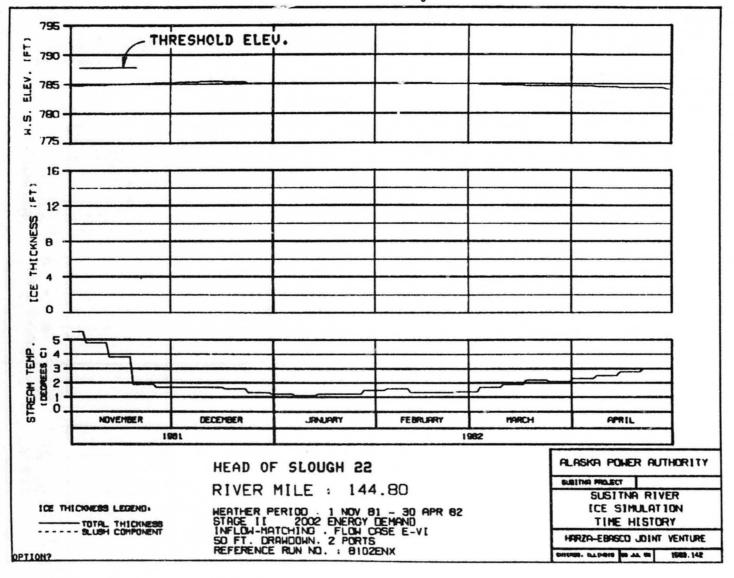
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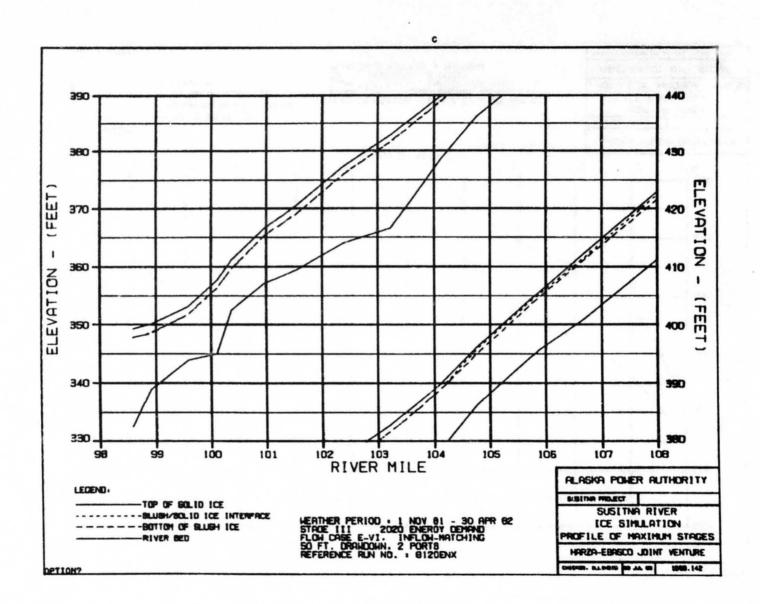


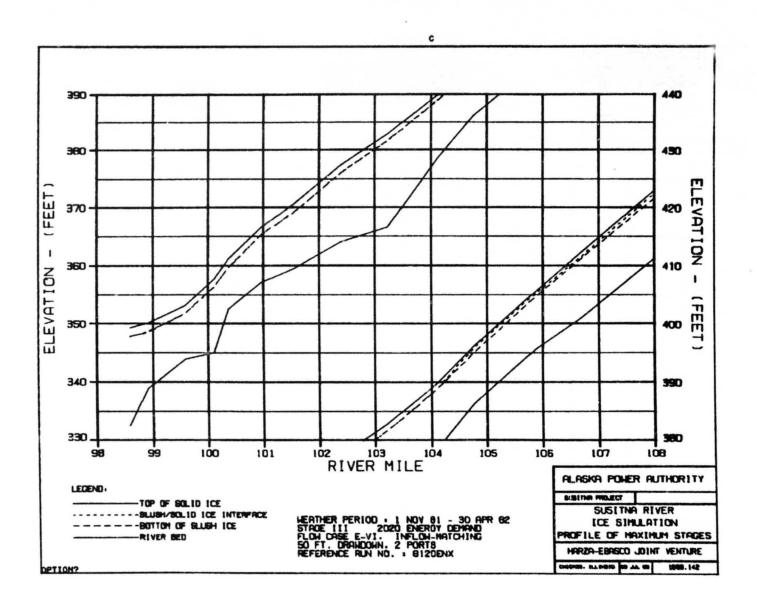
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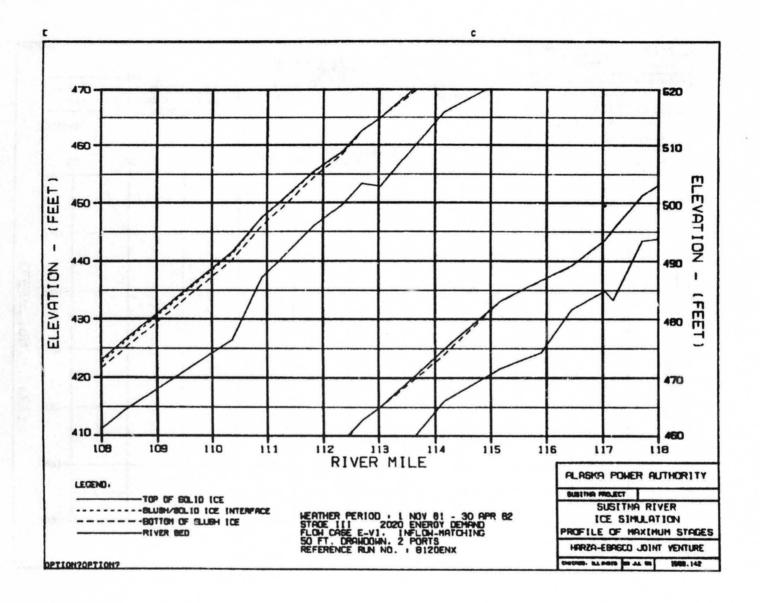


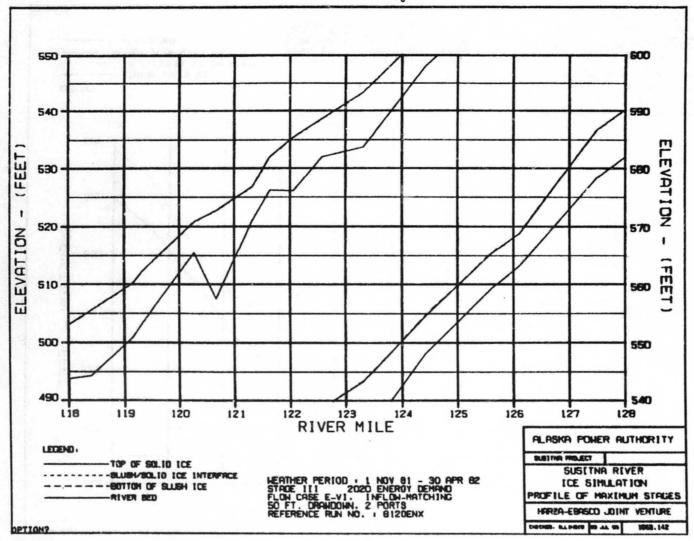


EXHIEIT C

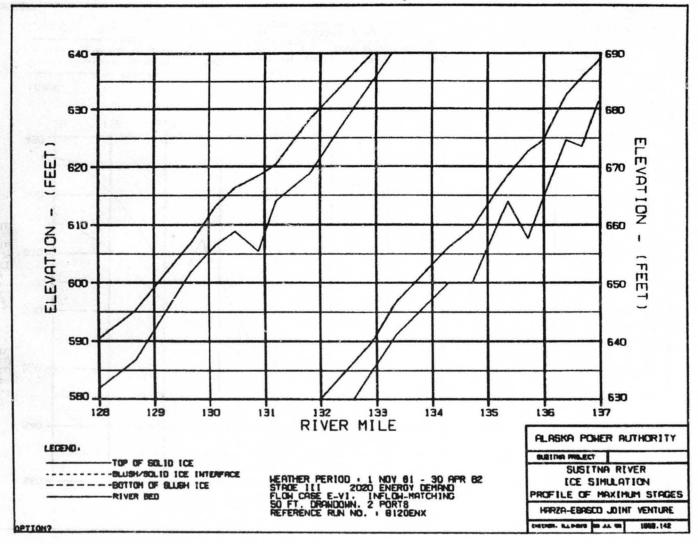


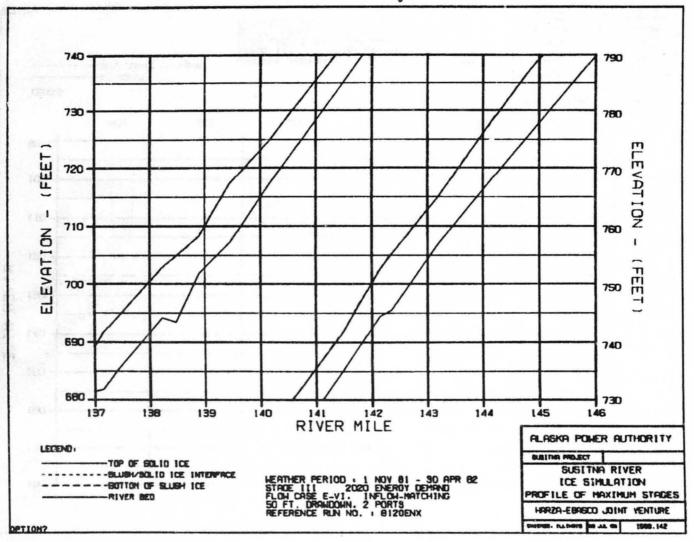


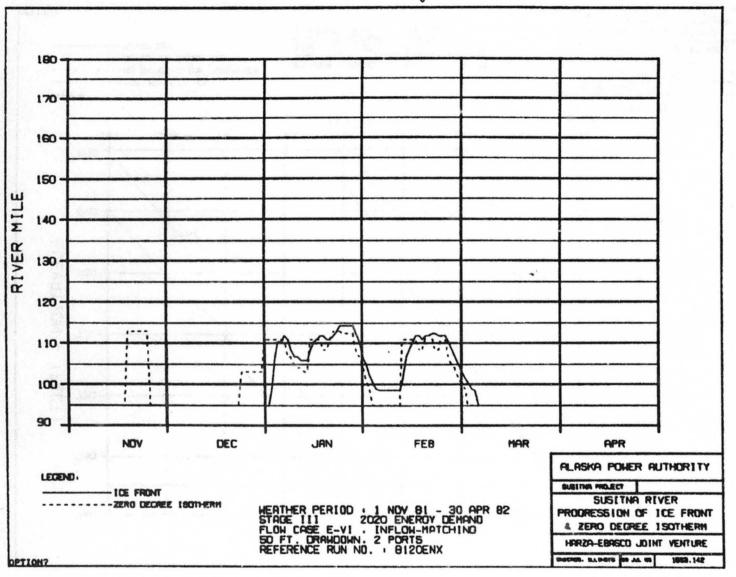




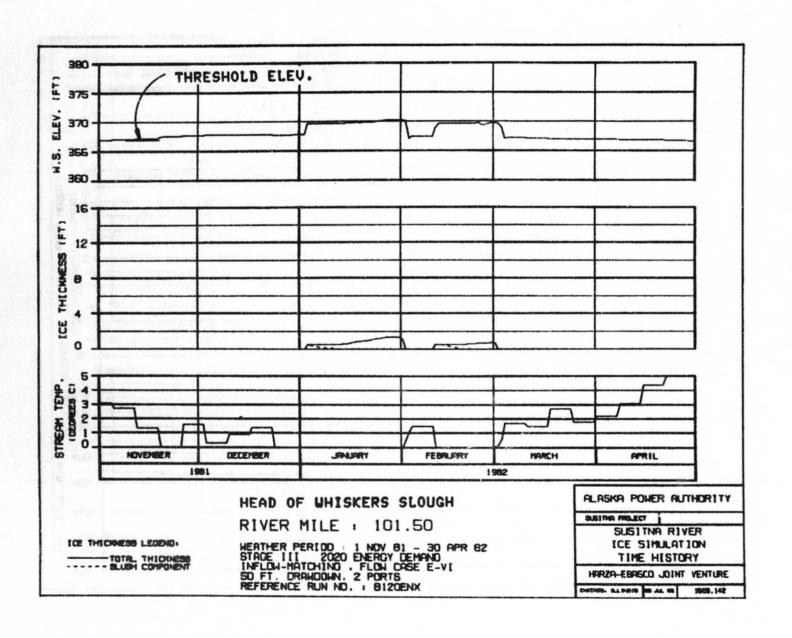


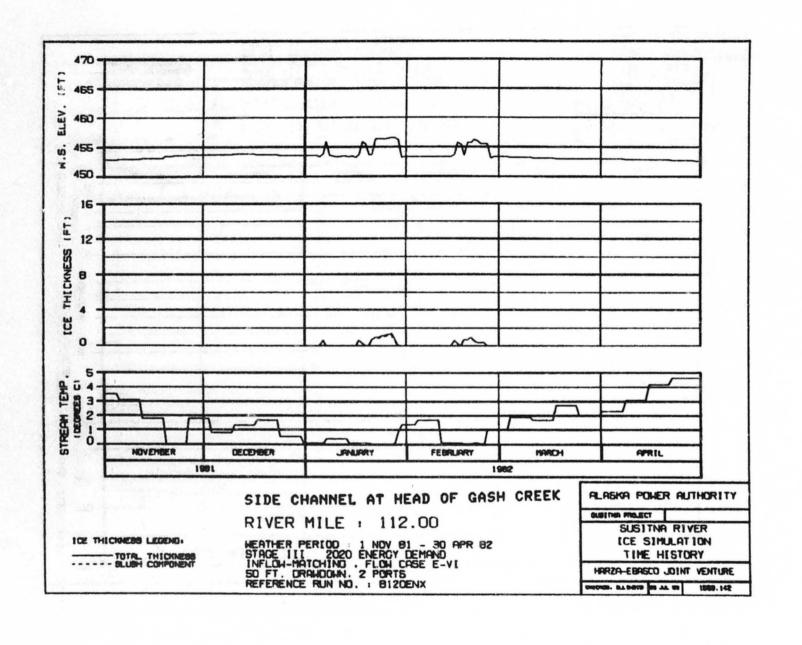


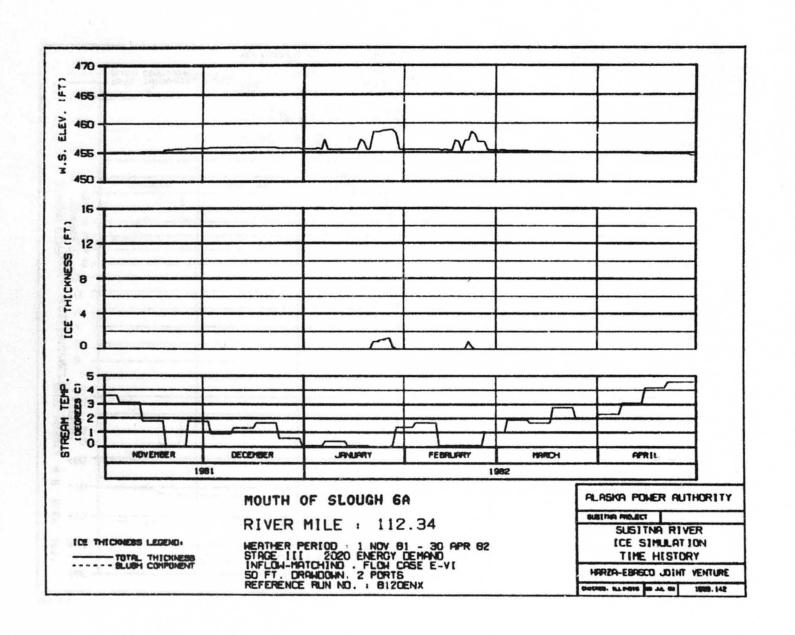




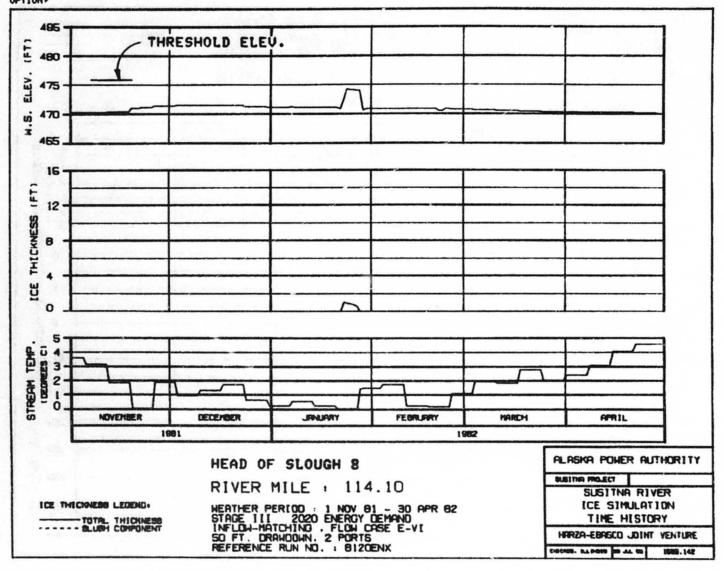
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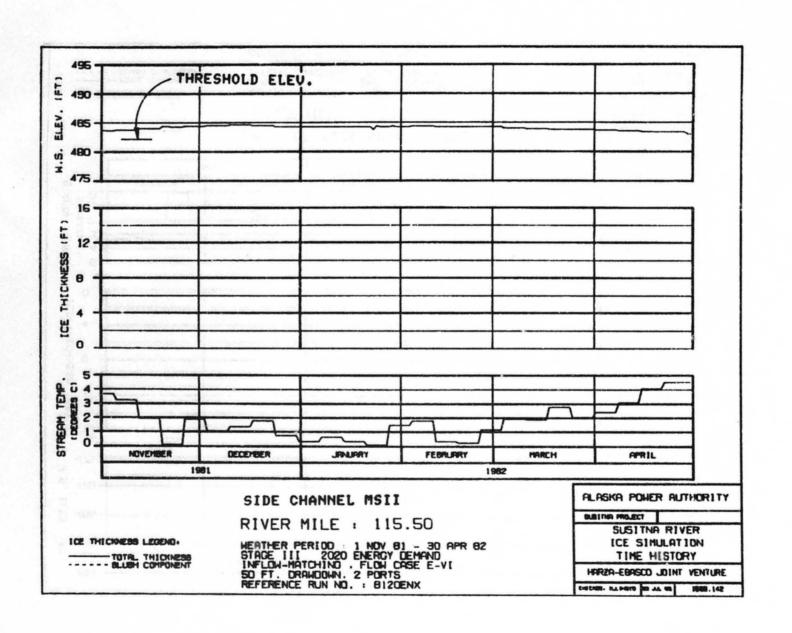


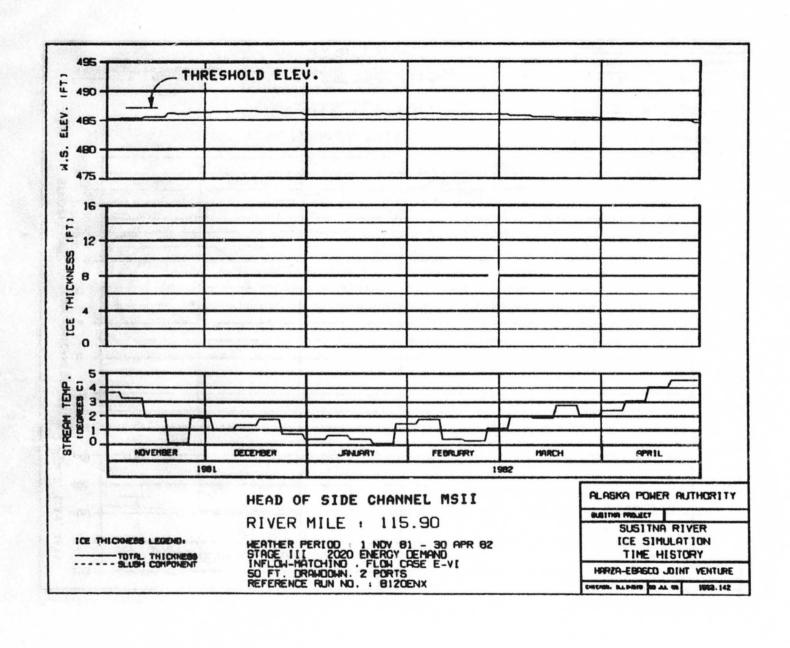


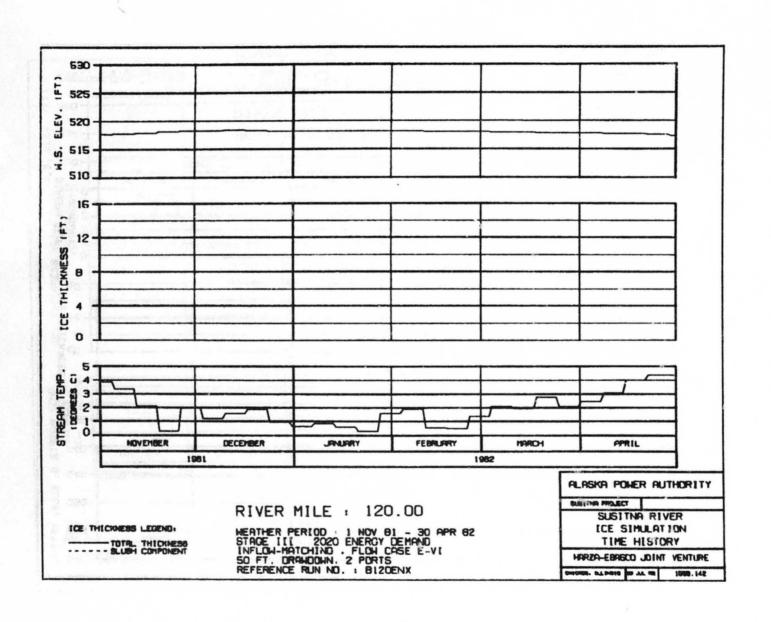


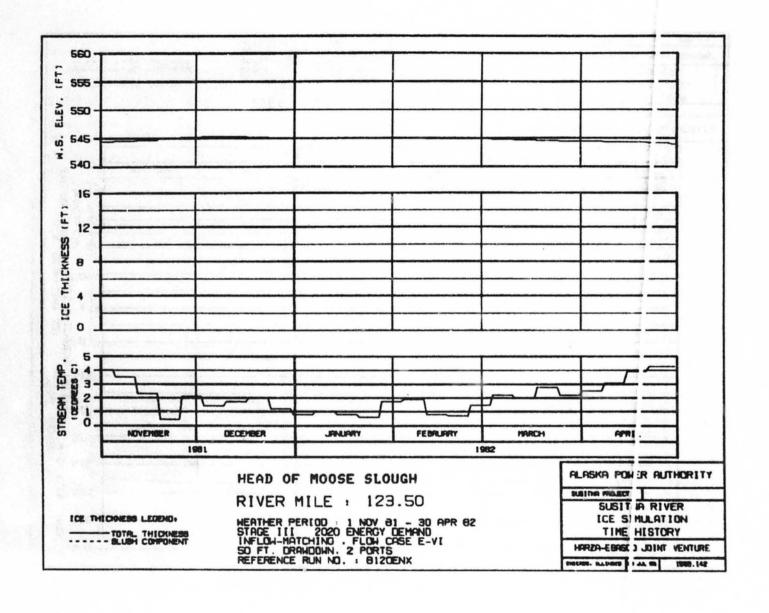




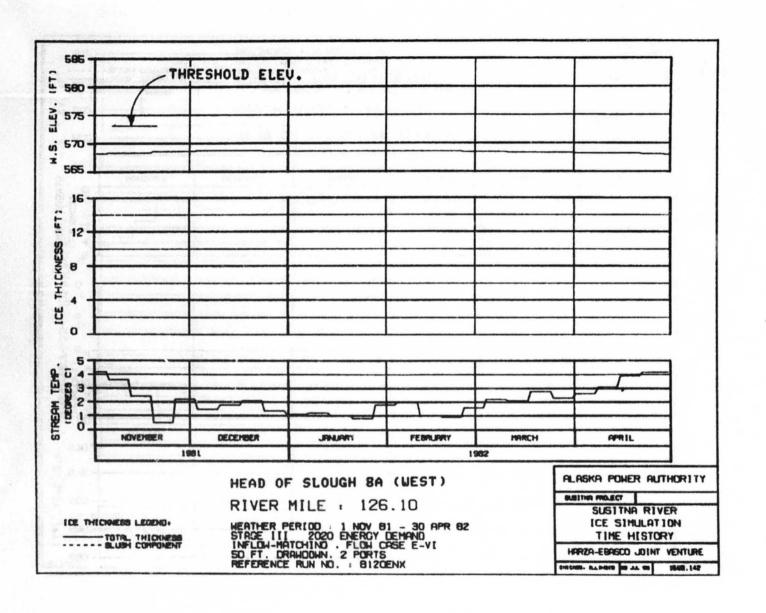


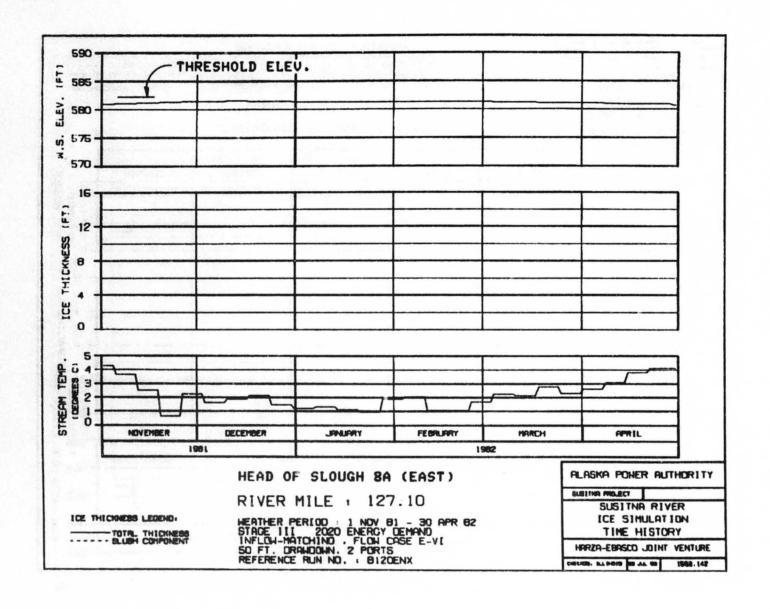




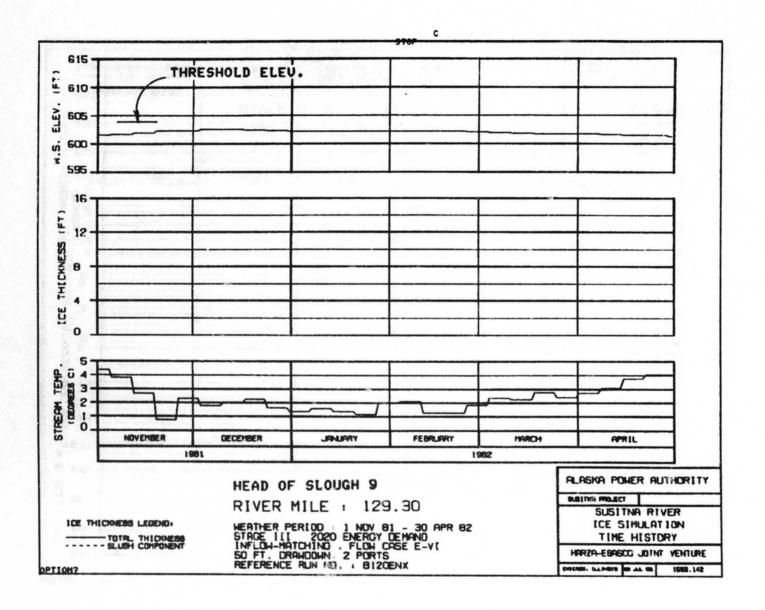


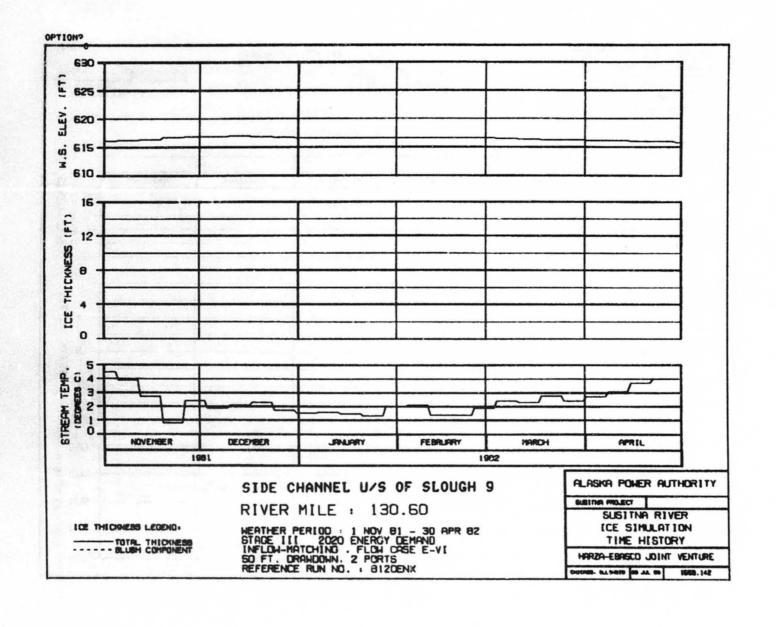
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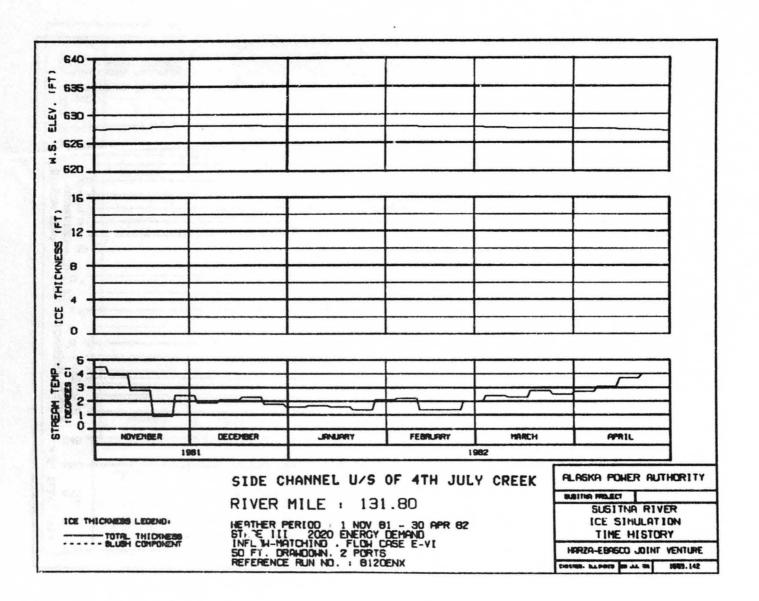


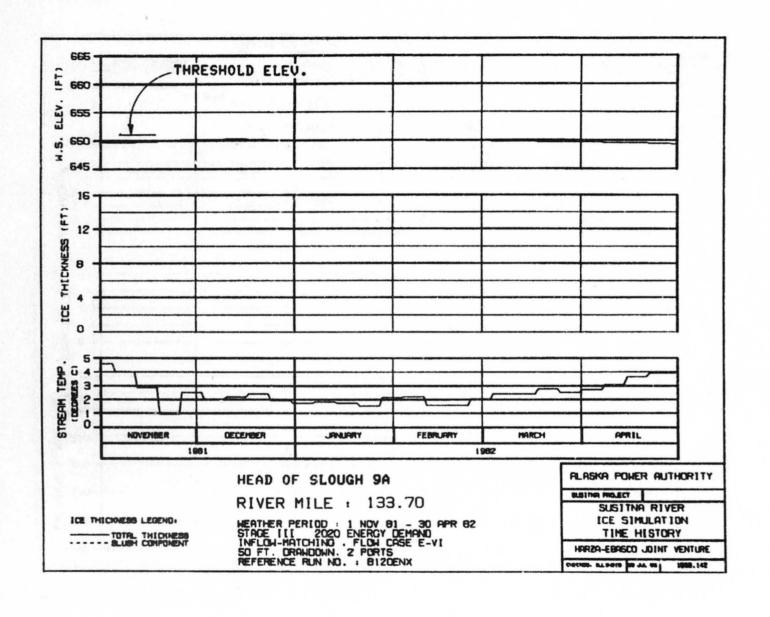


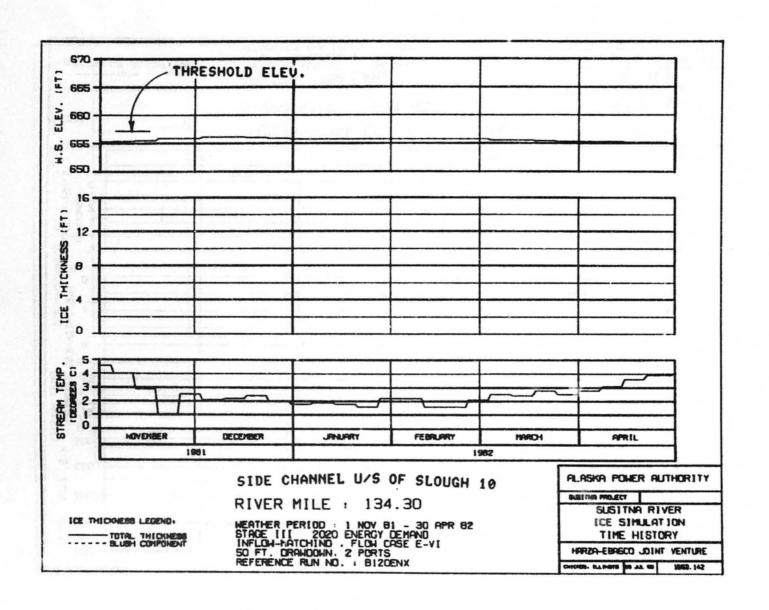
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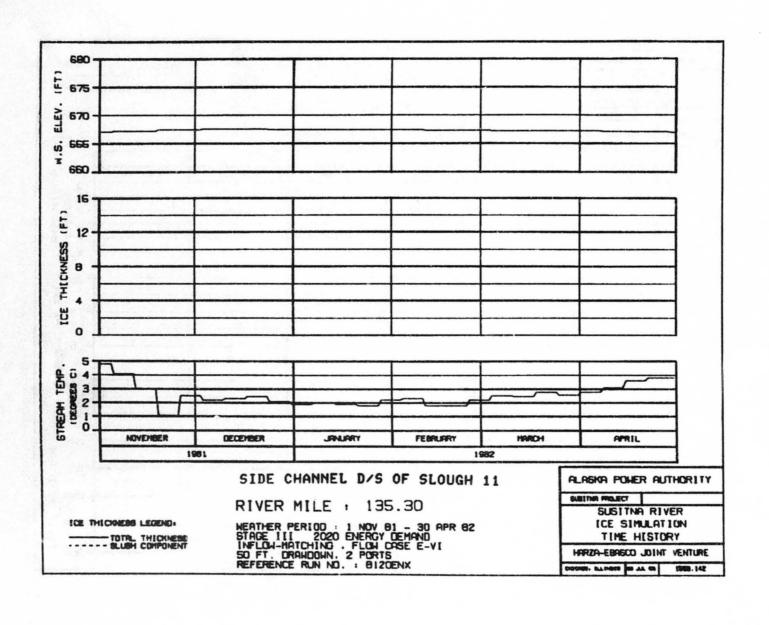


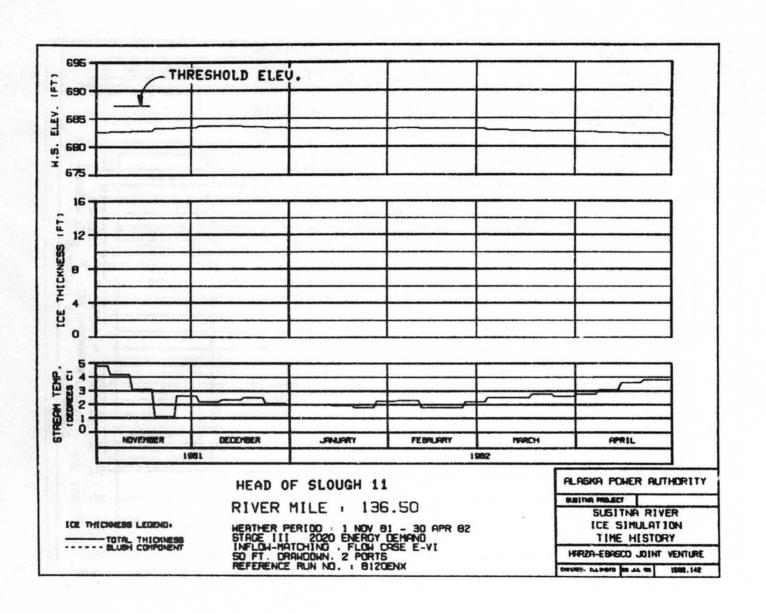


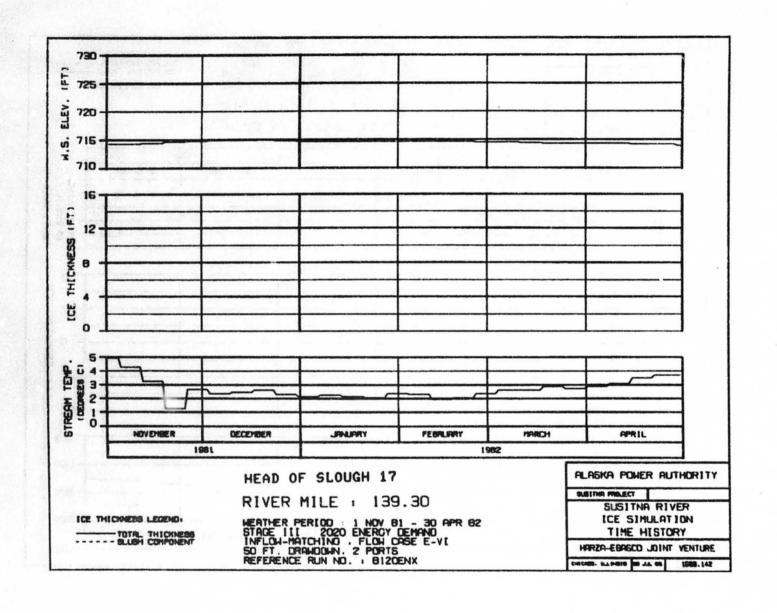


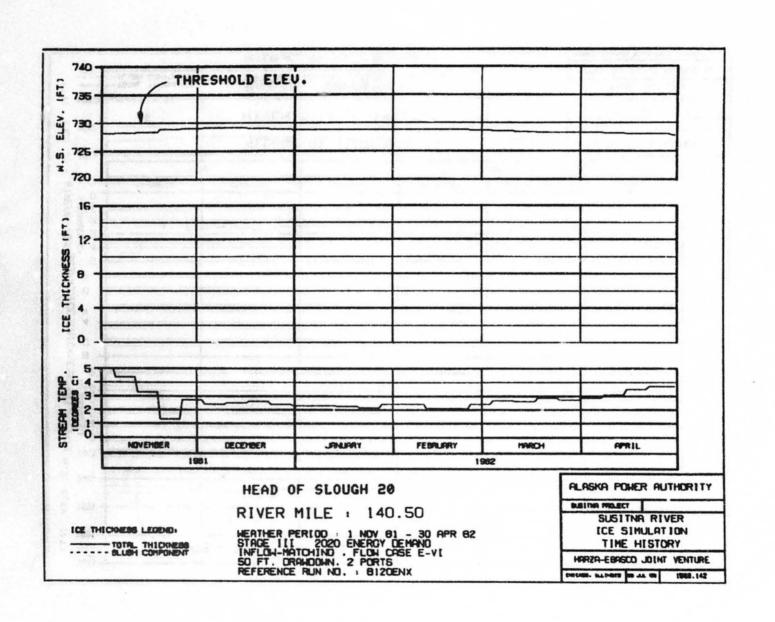


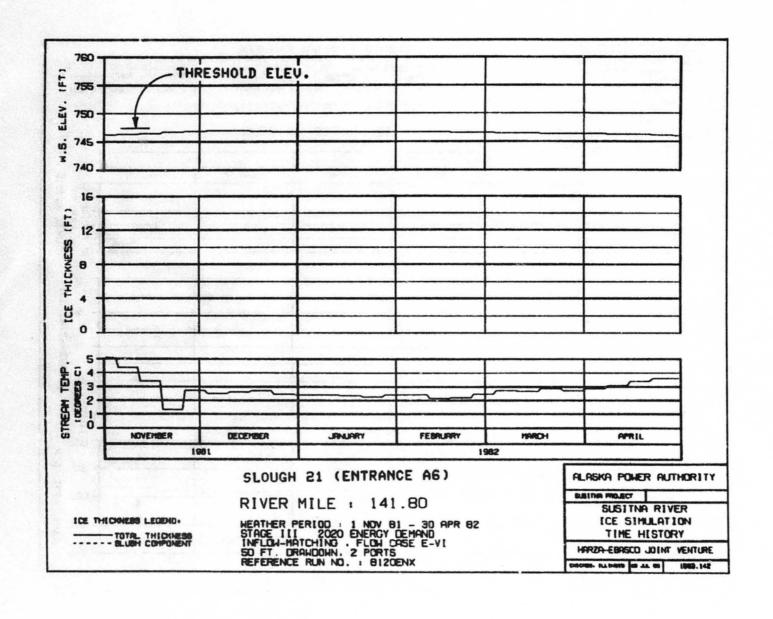


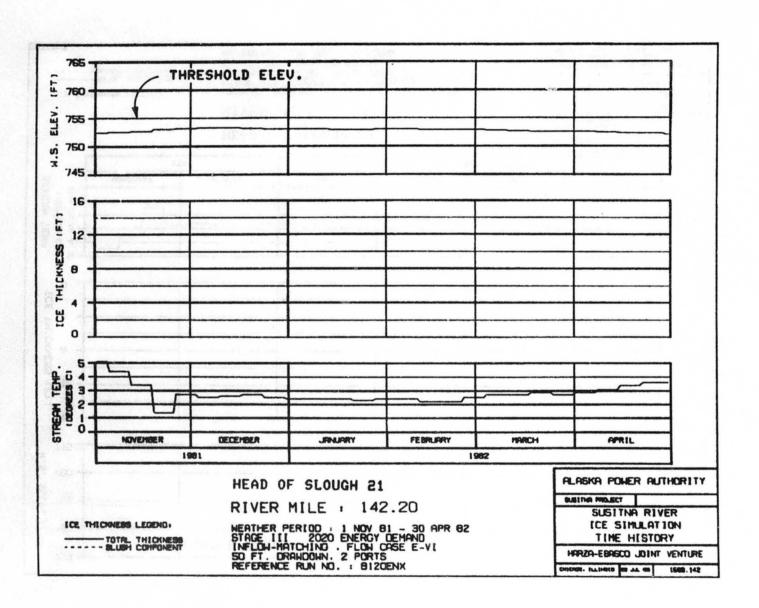




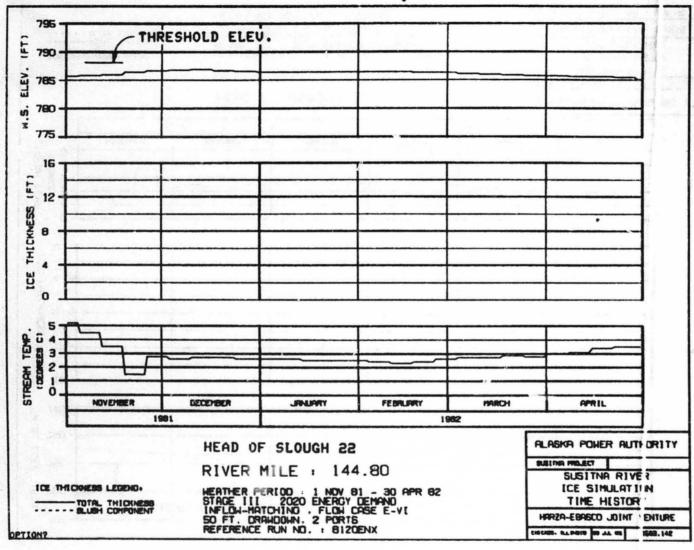








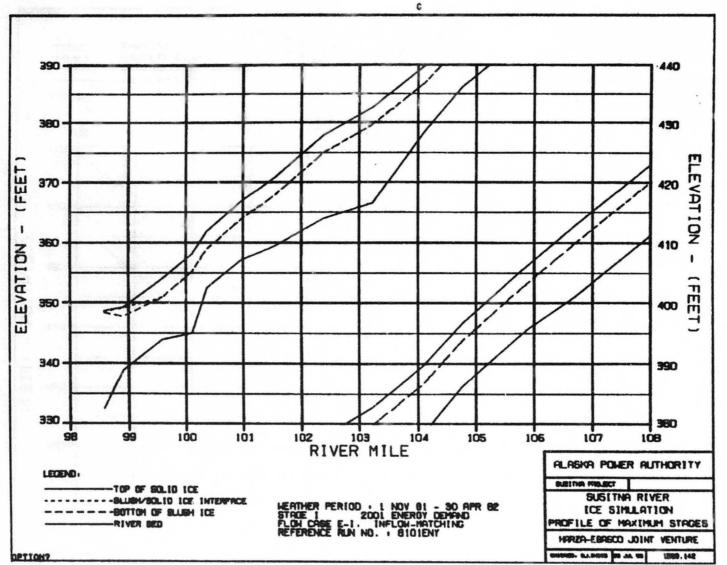


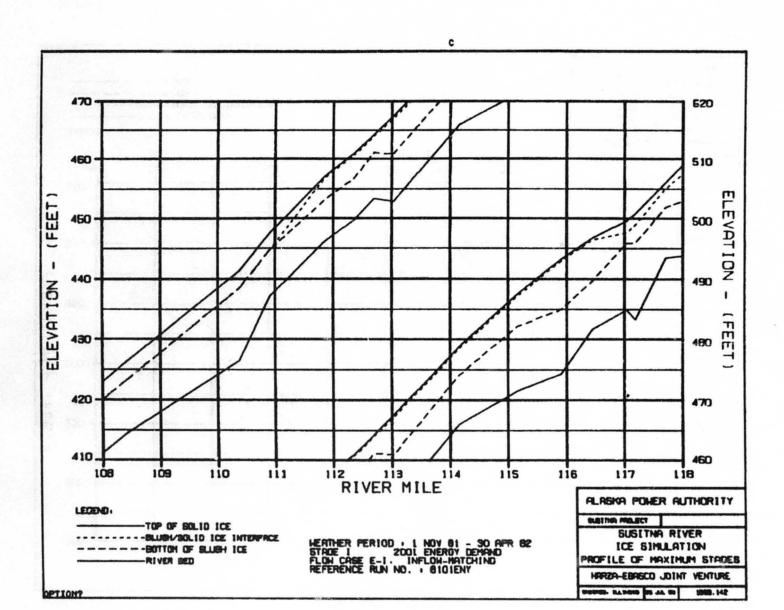


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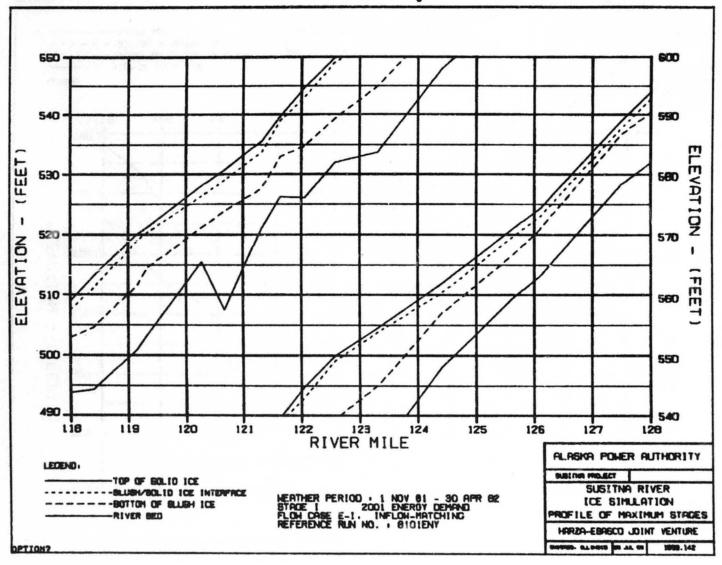
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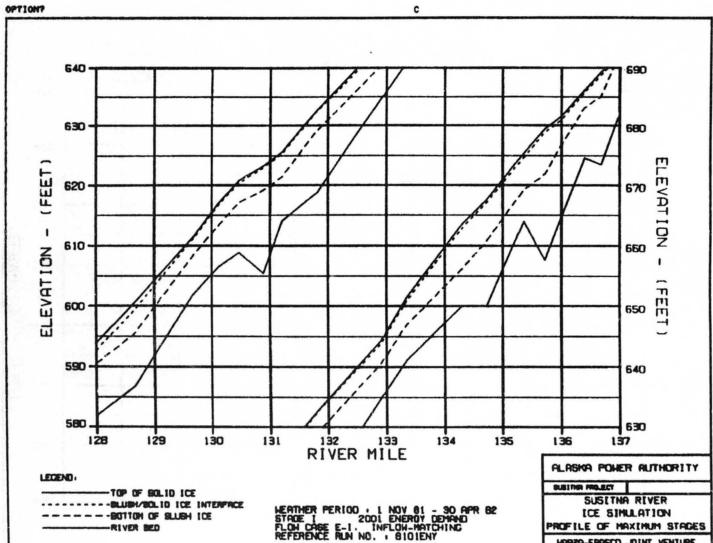










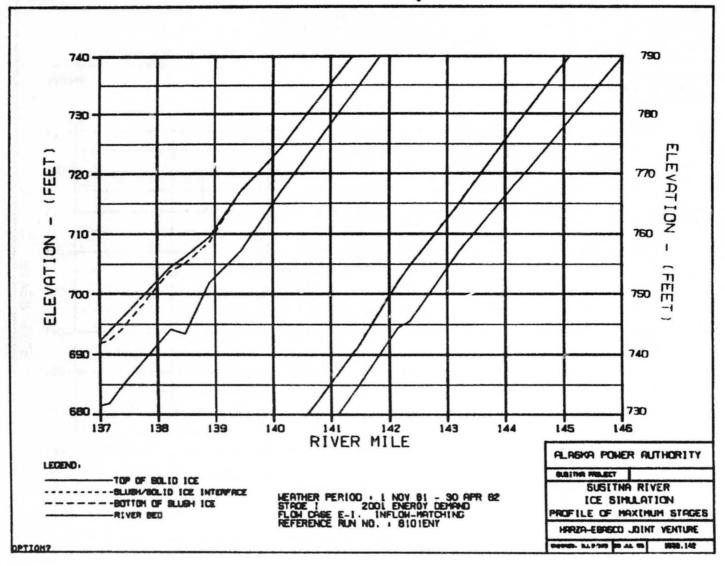


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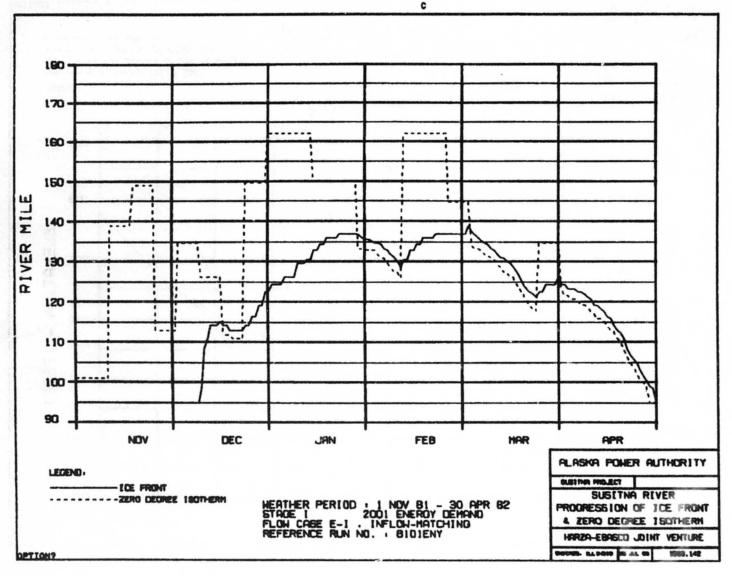
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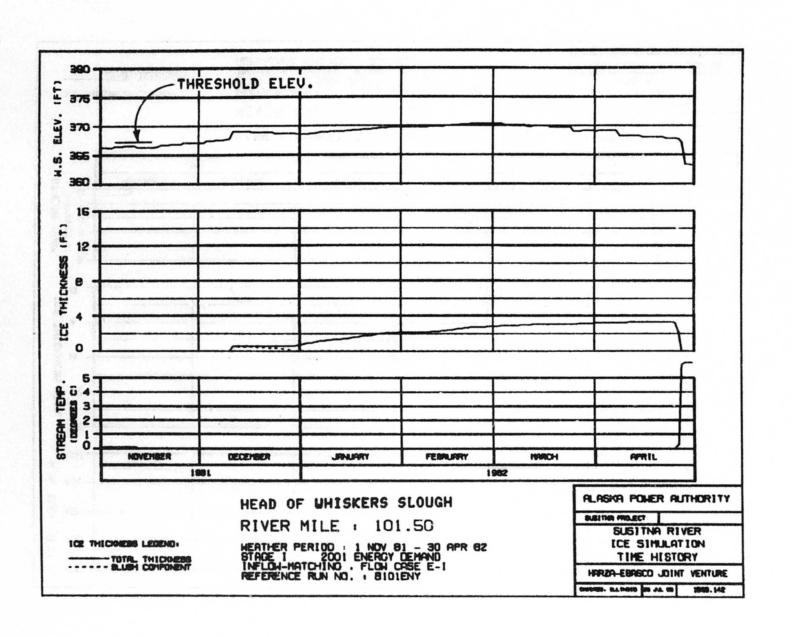
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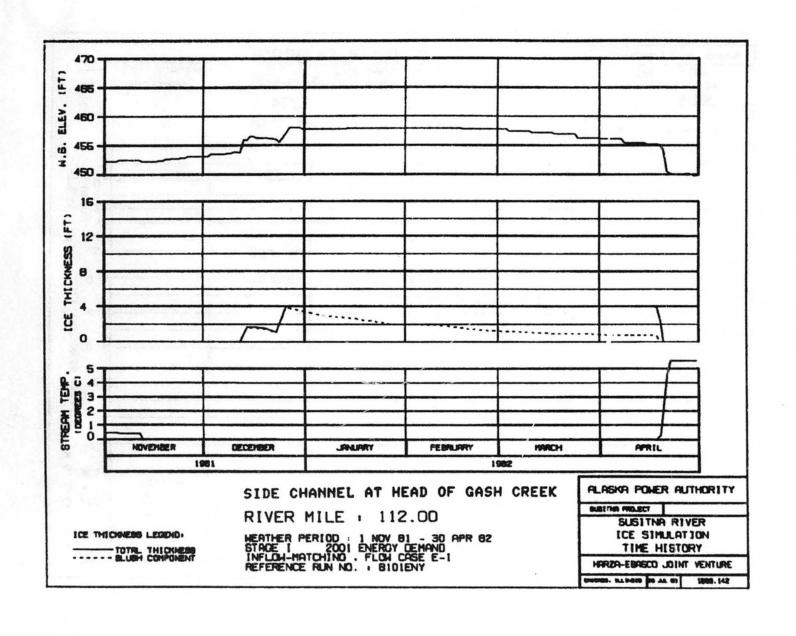


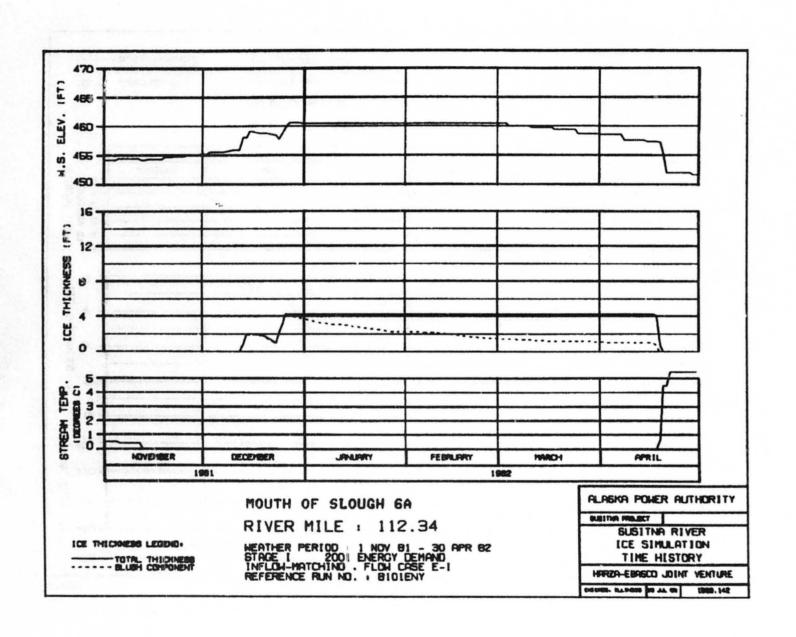


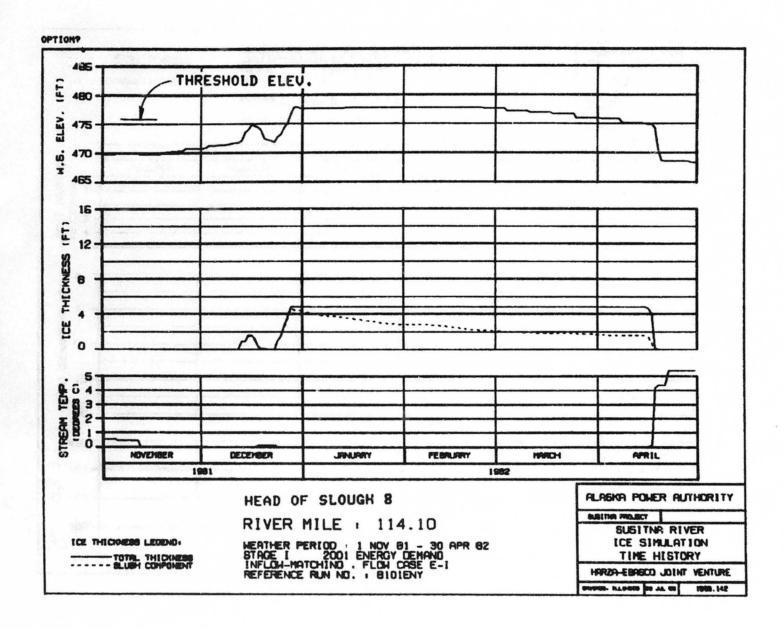


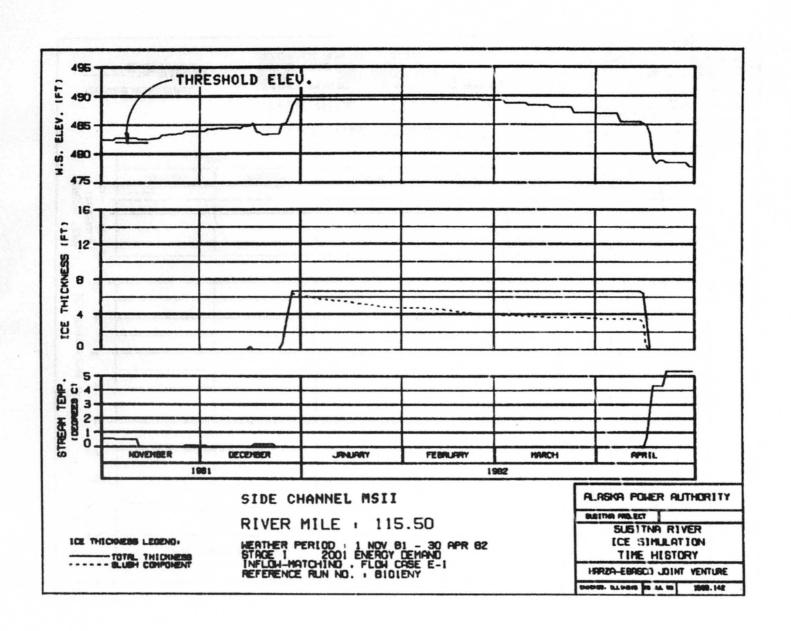




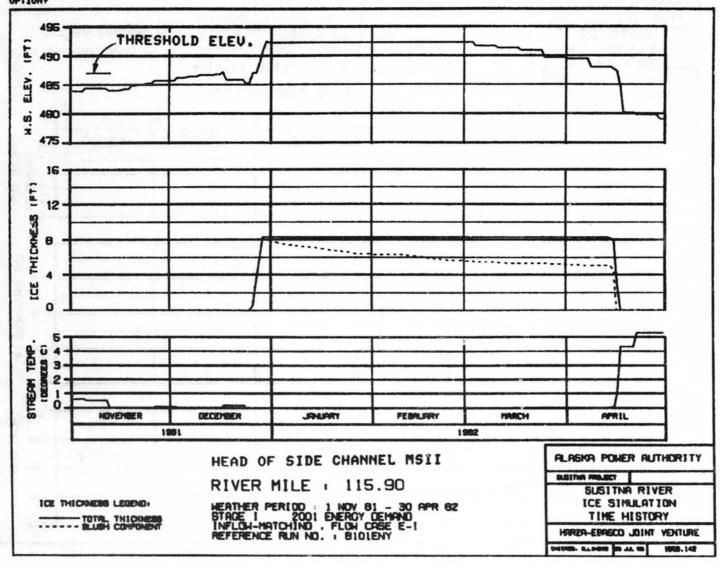




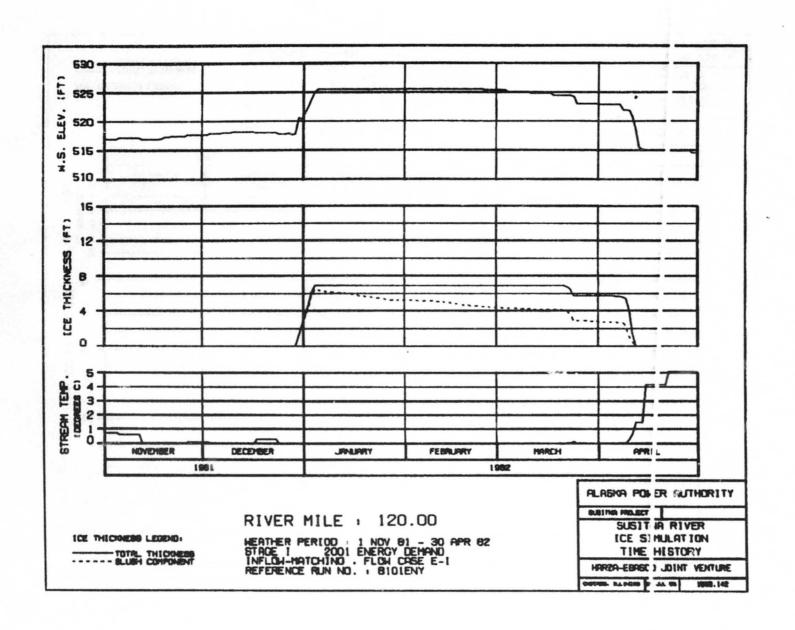


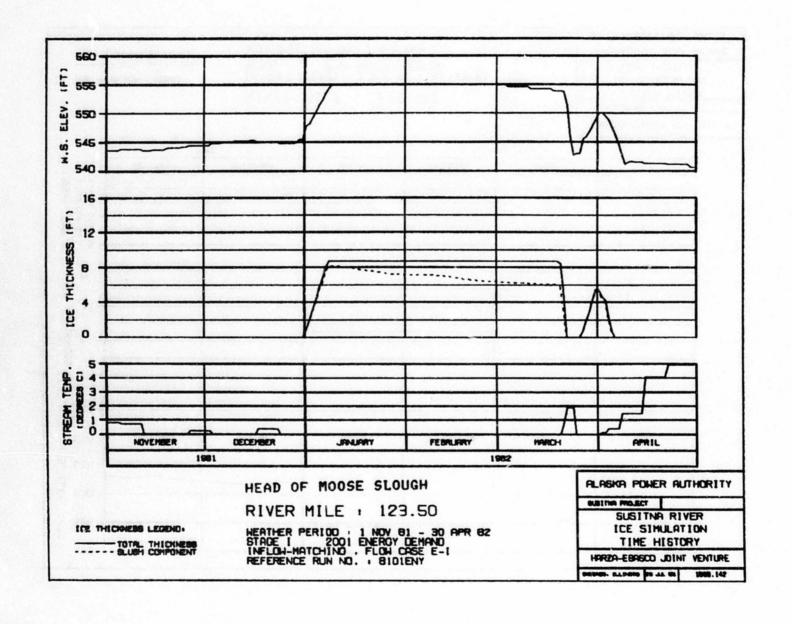


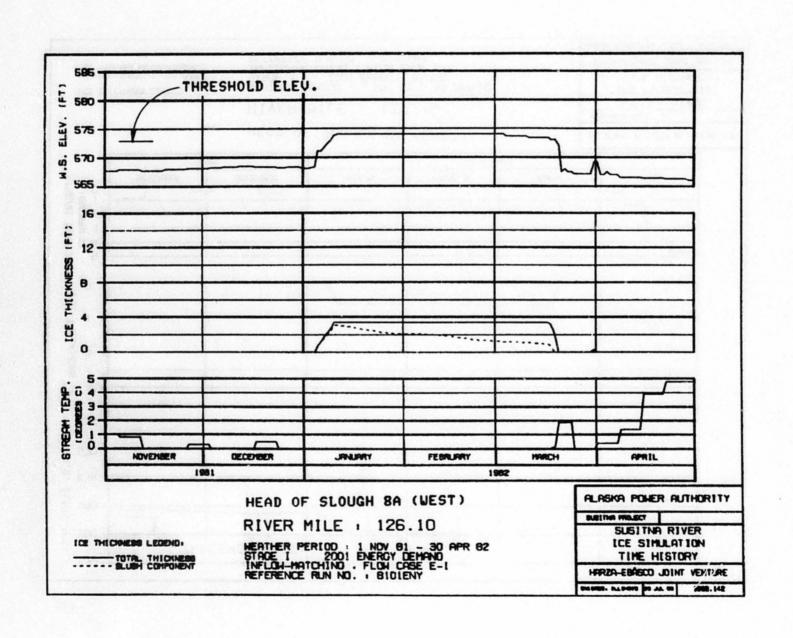


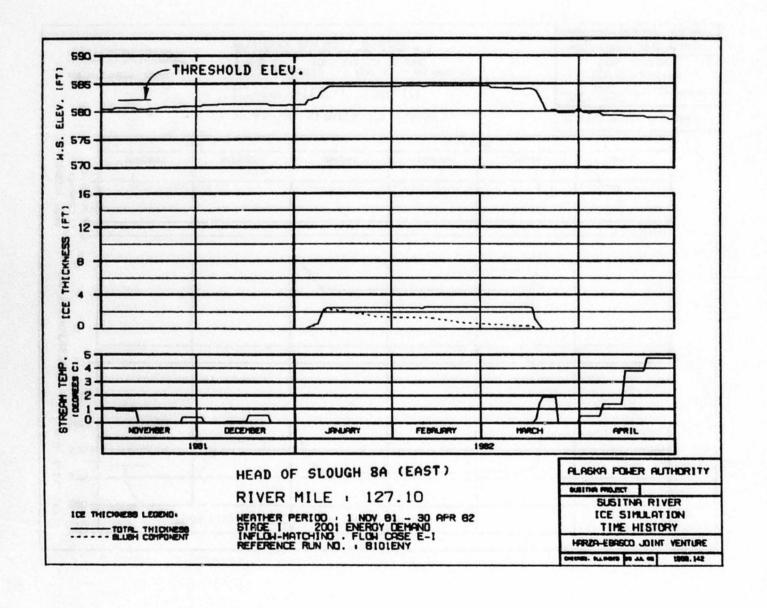


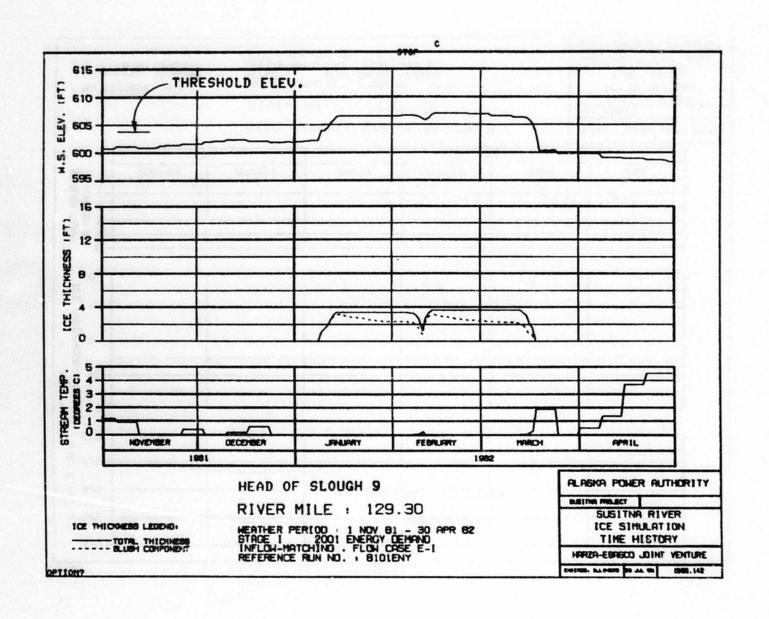
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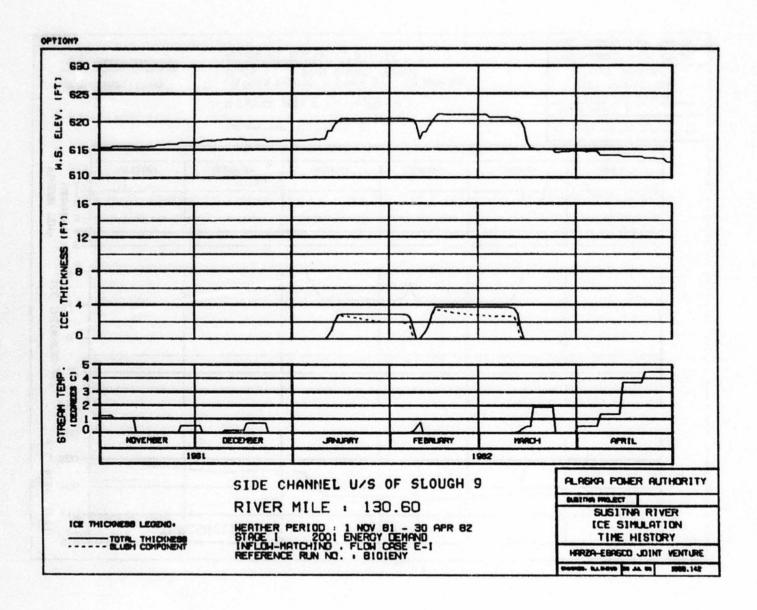


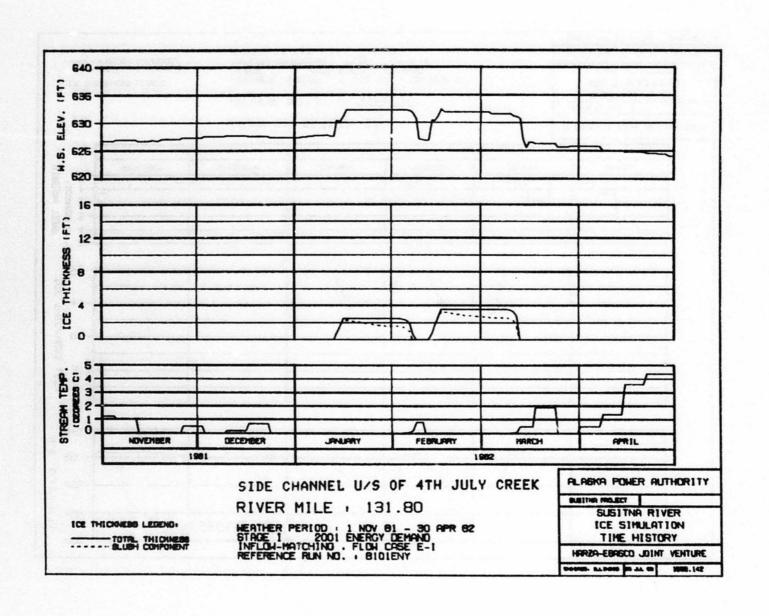


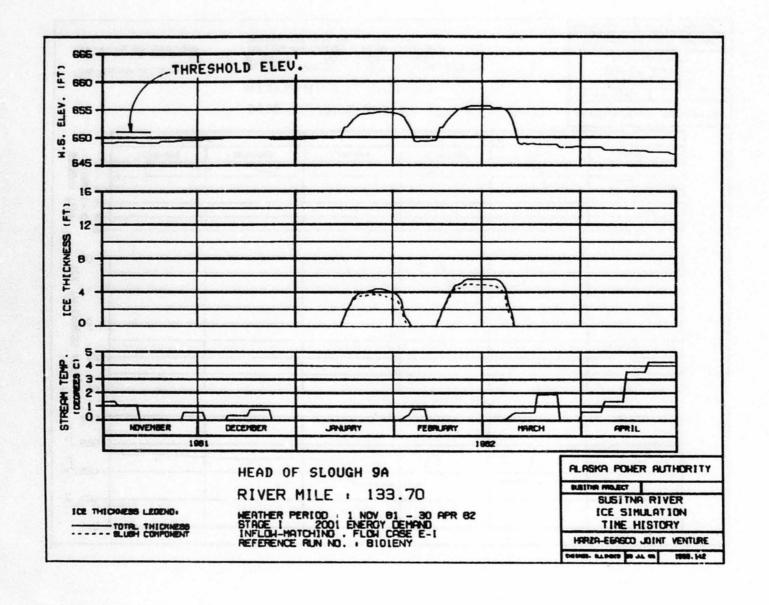


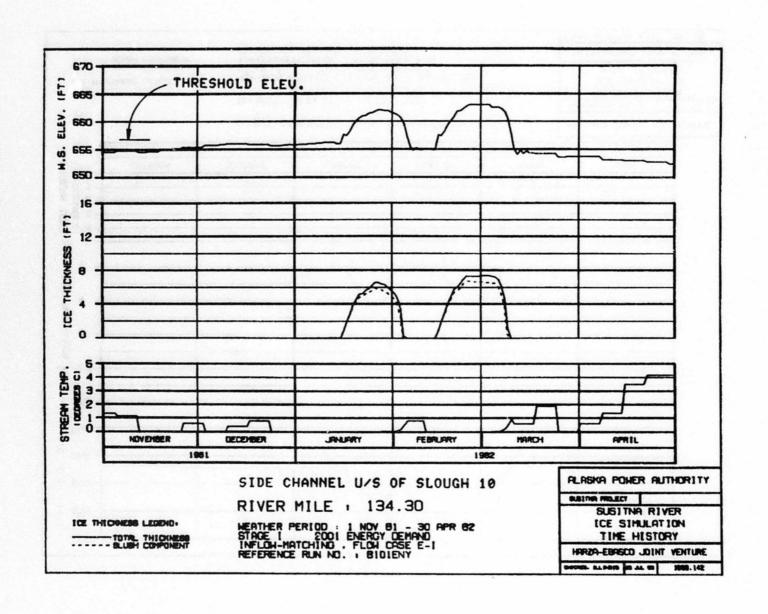


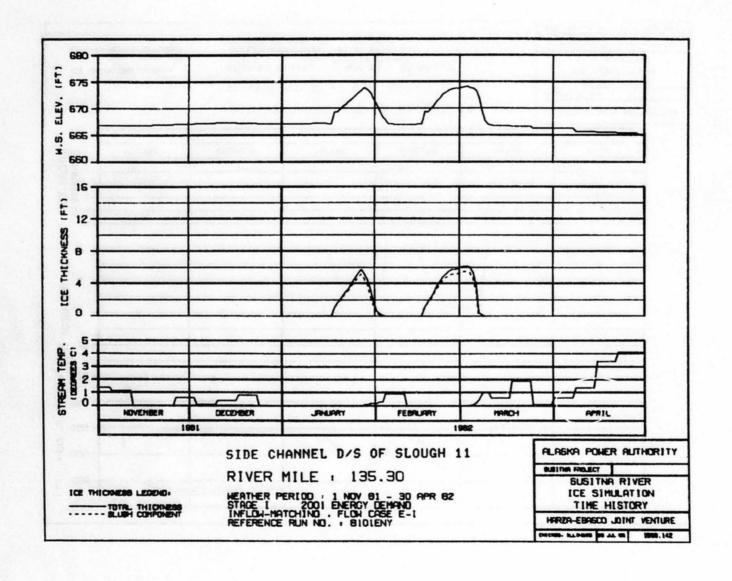


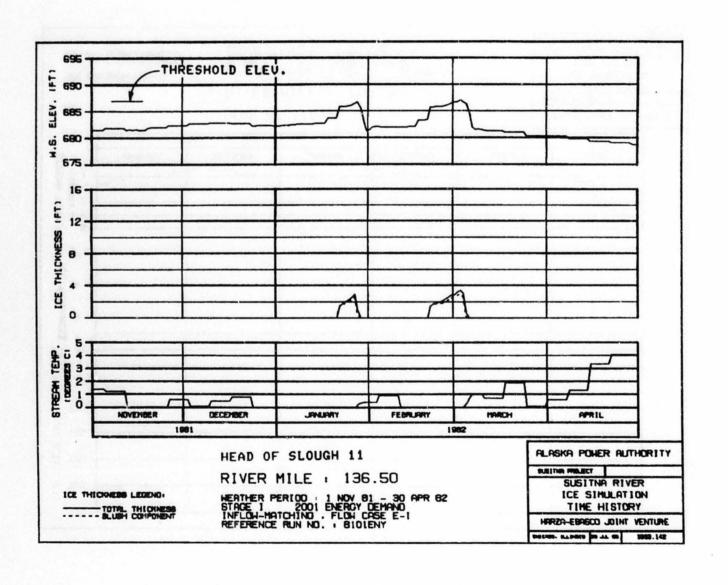


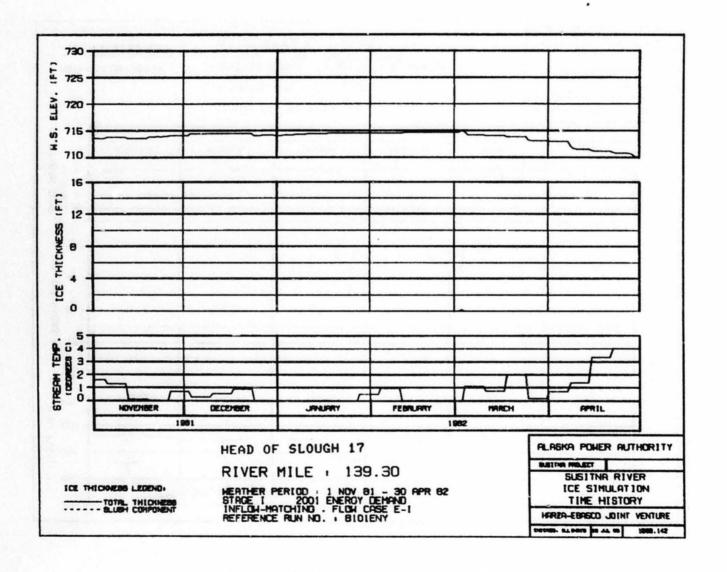


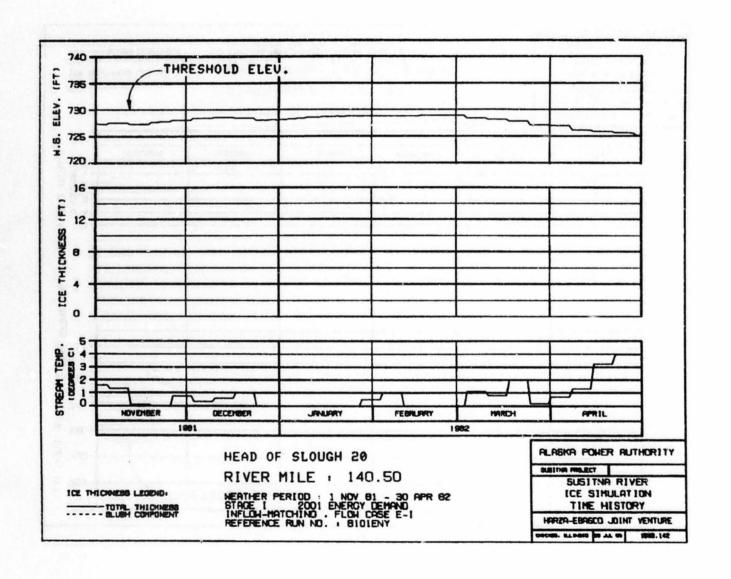


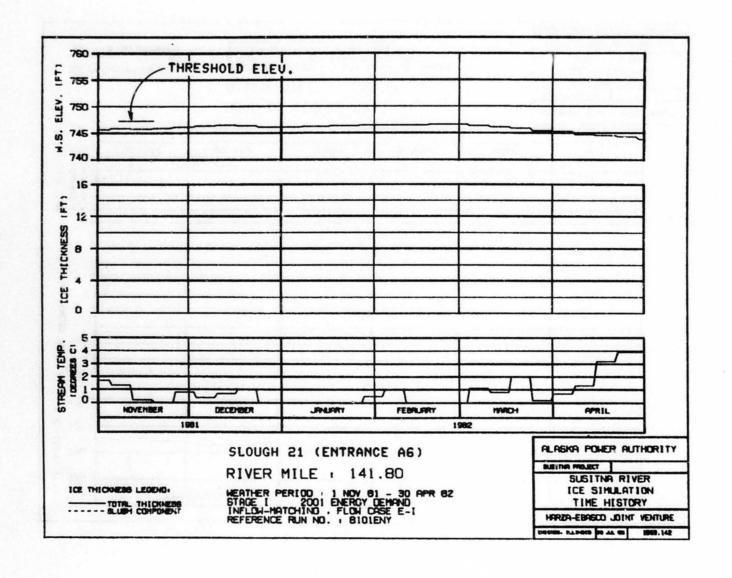


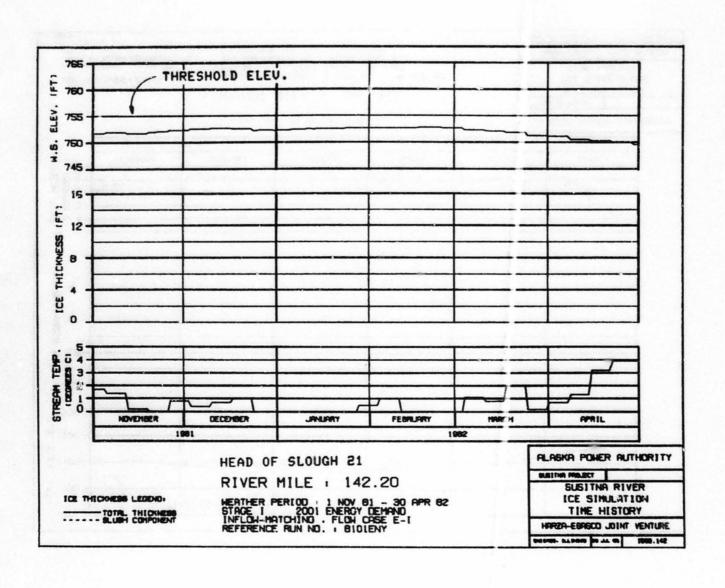


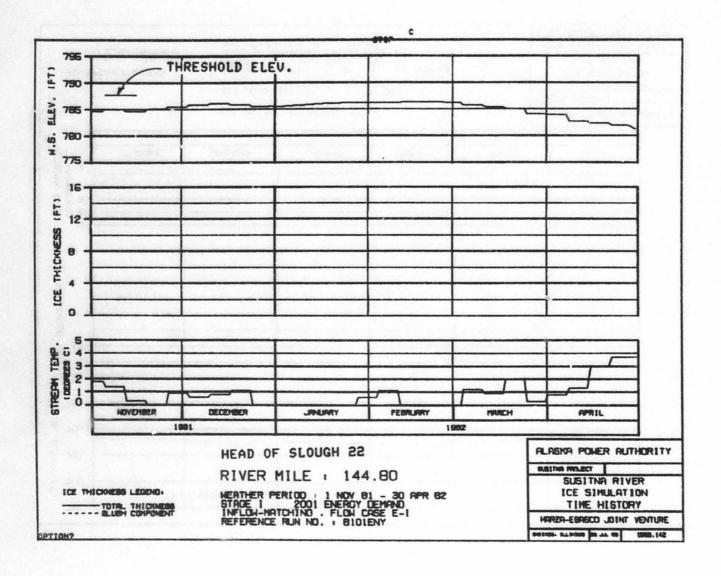






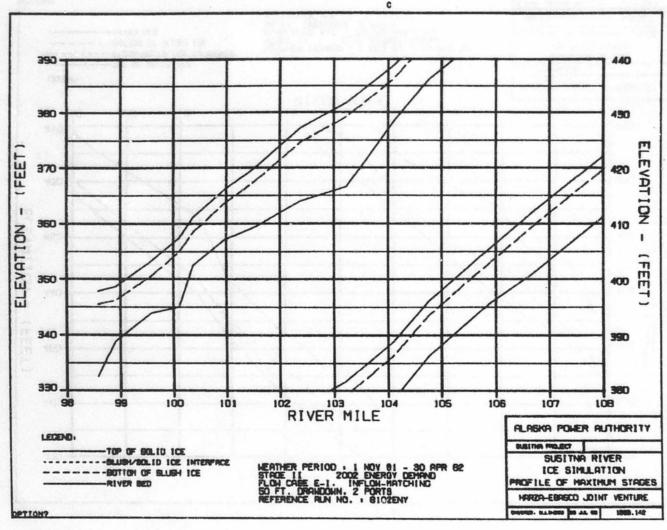




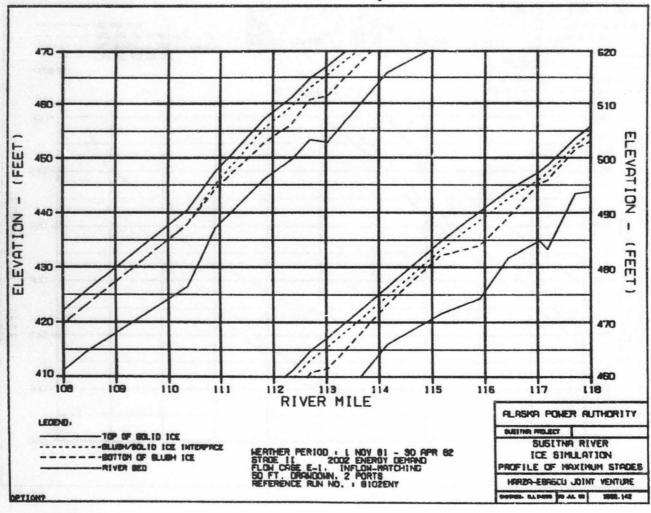


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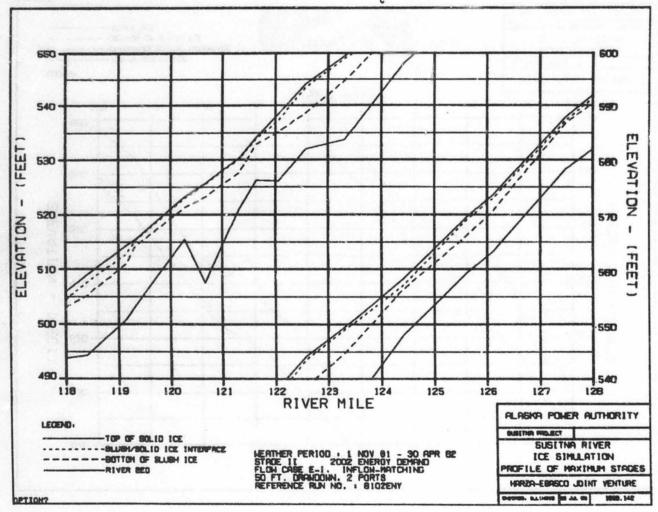




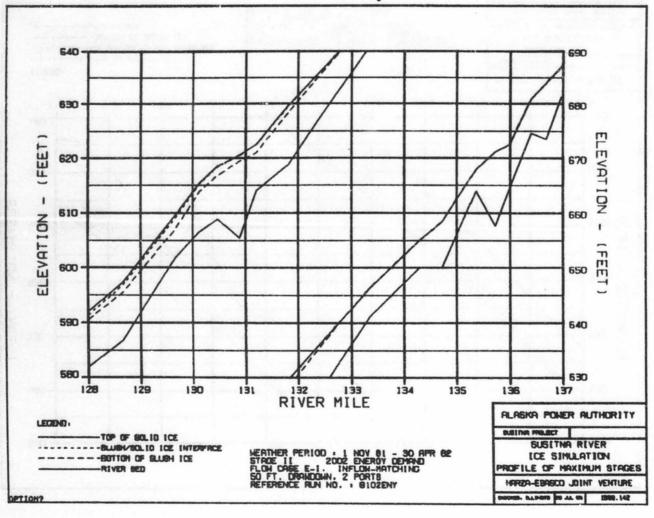




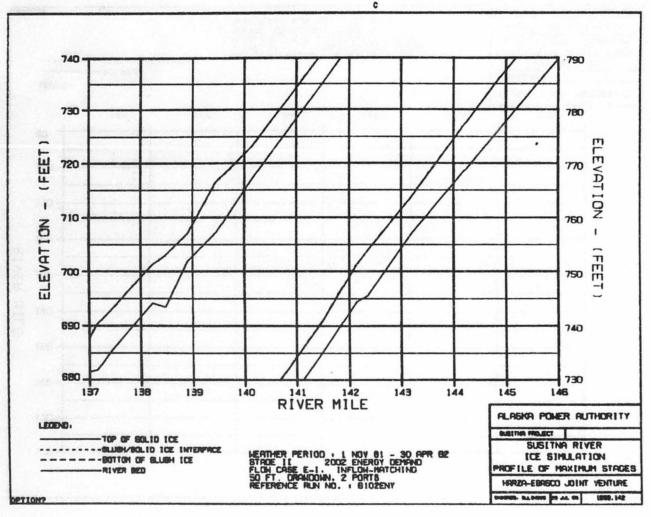


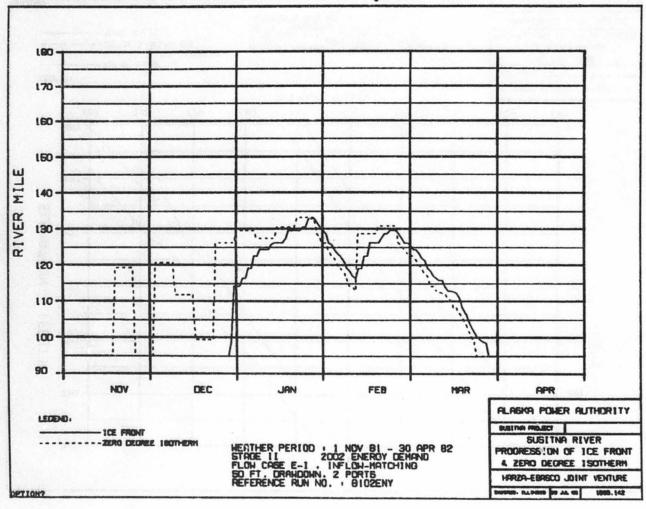


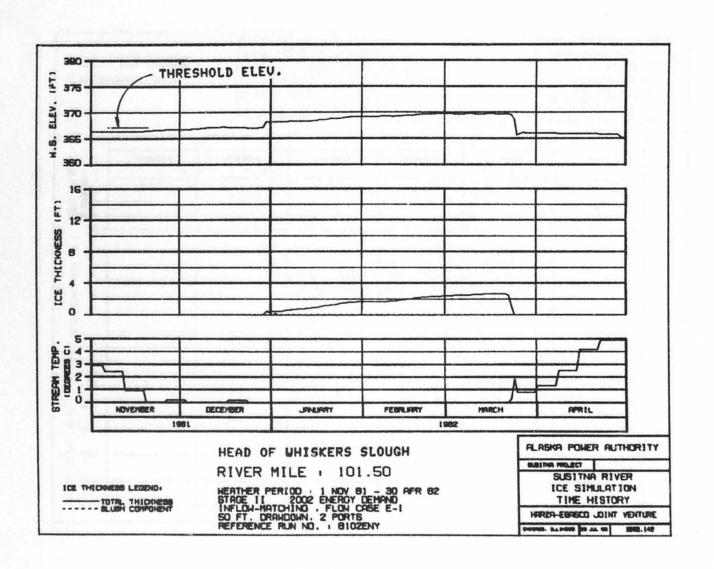


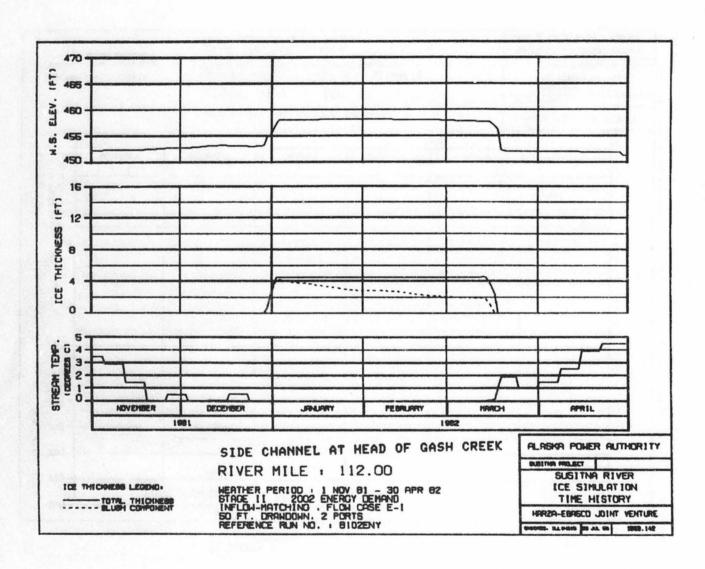


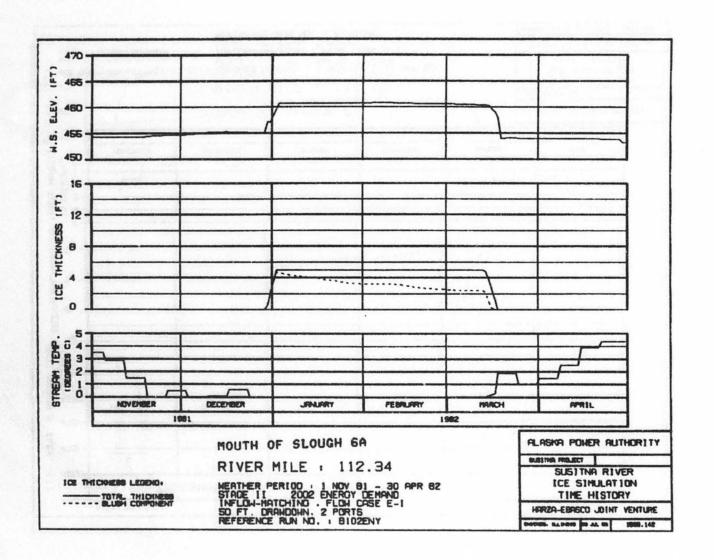


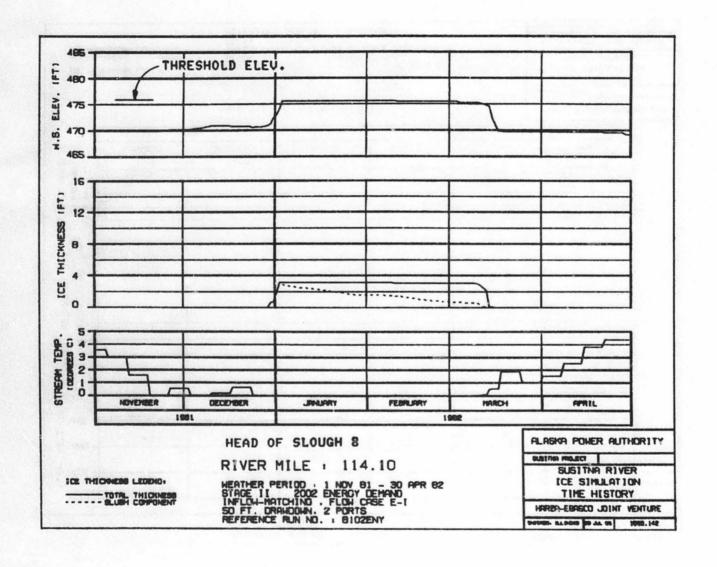


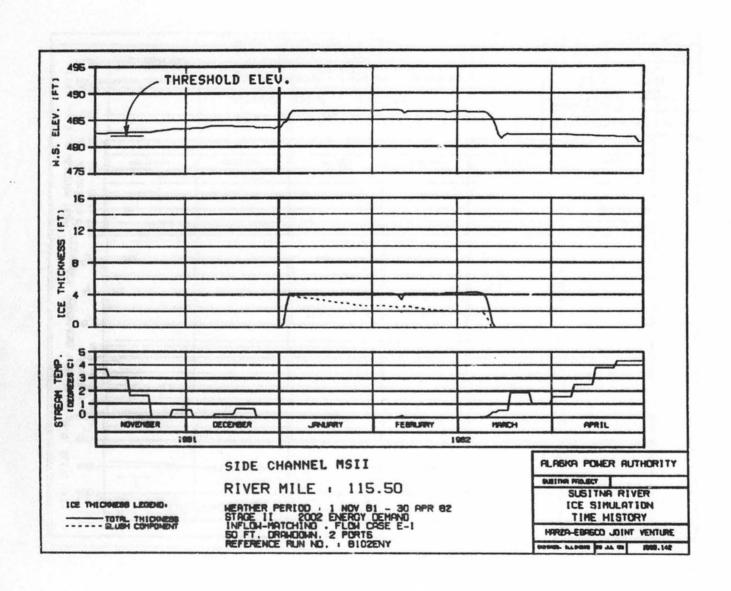


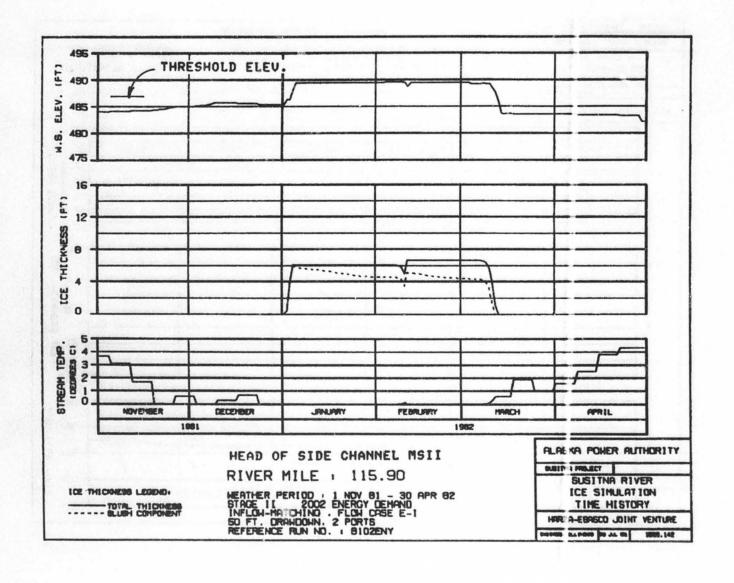


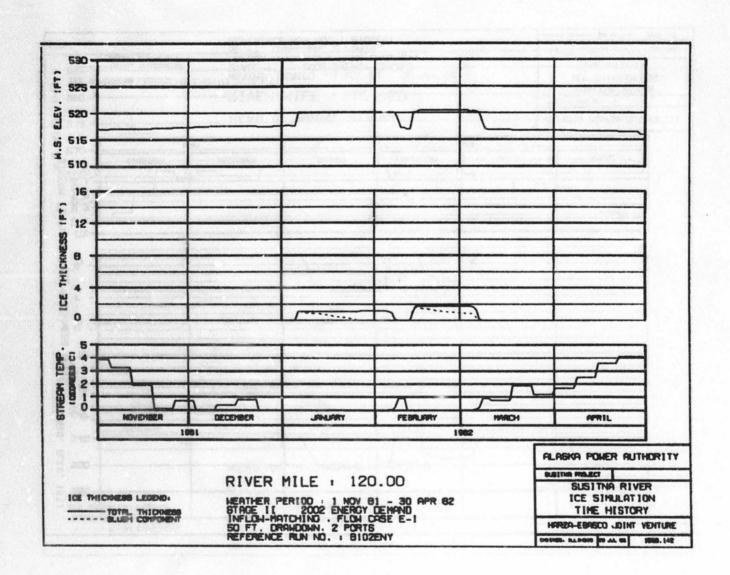


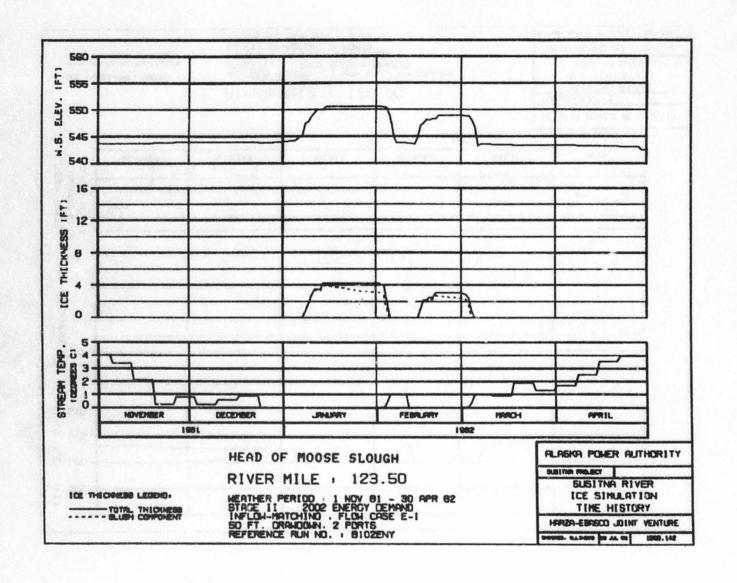




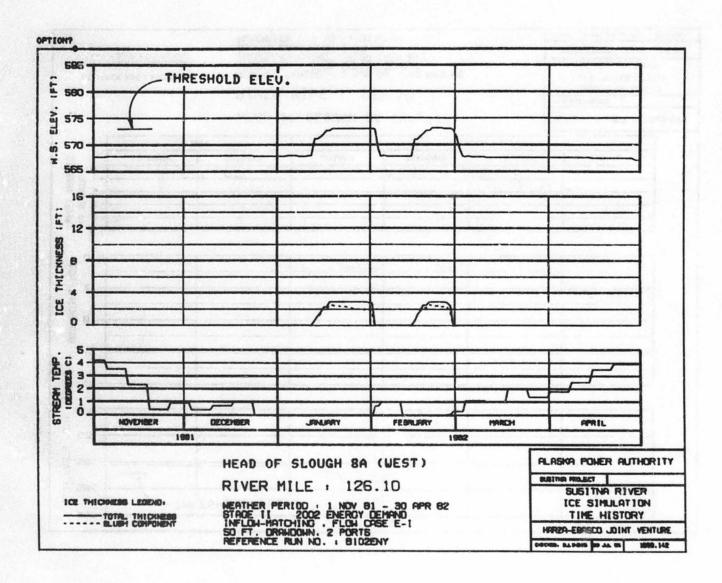


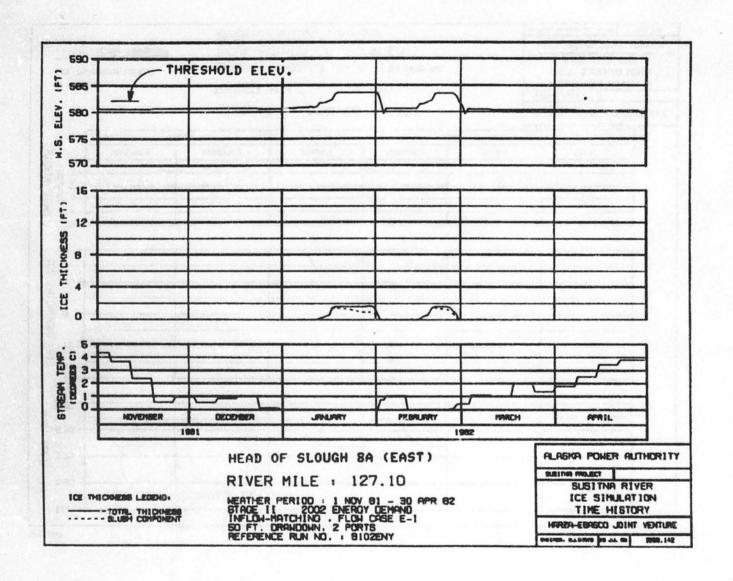


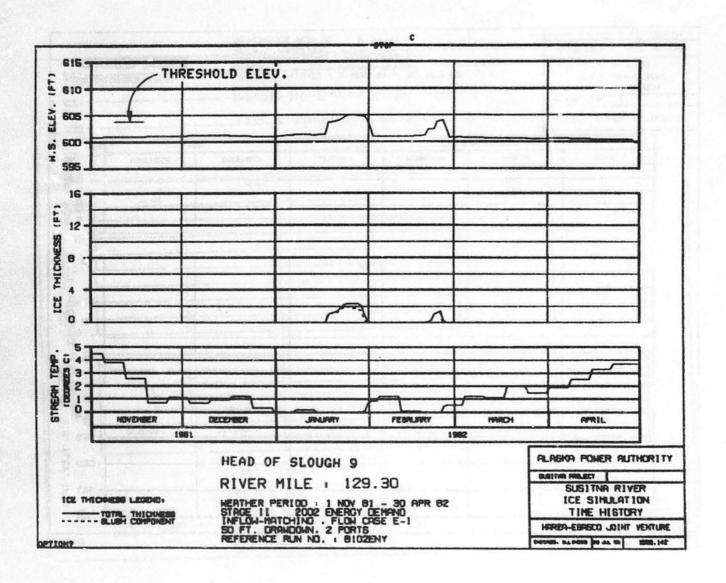


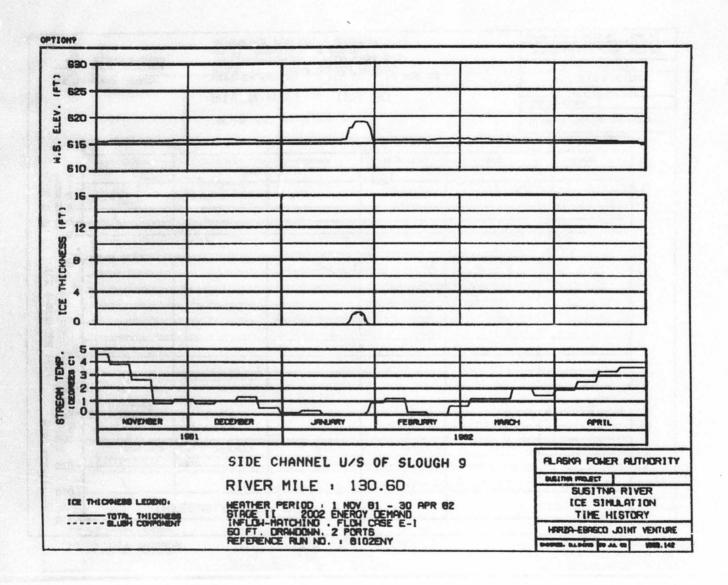


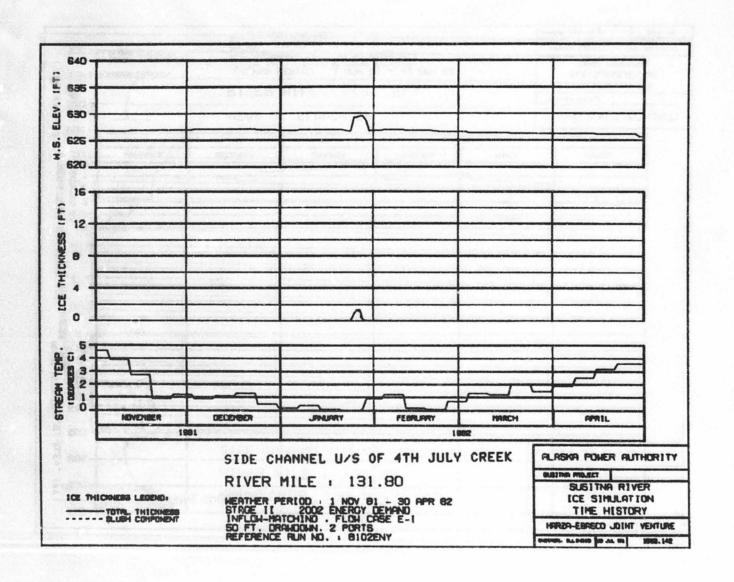
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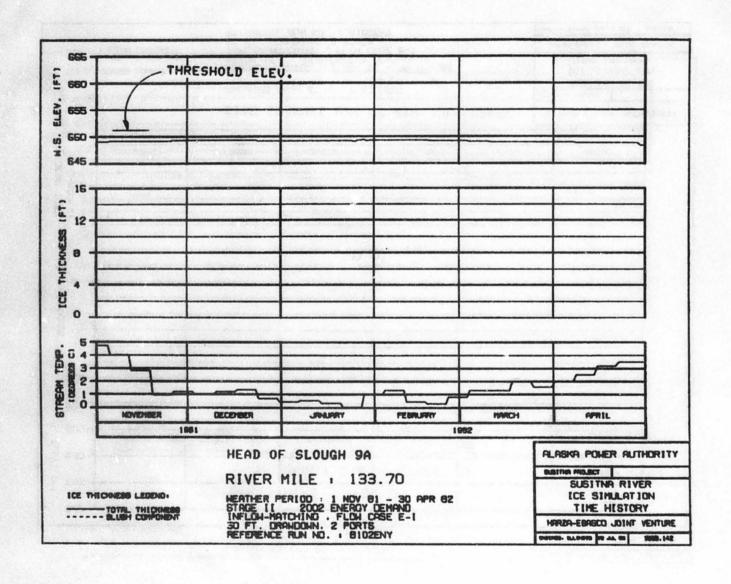


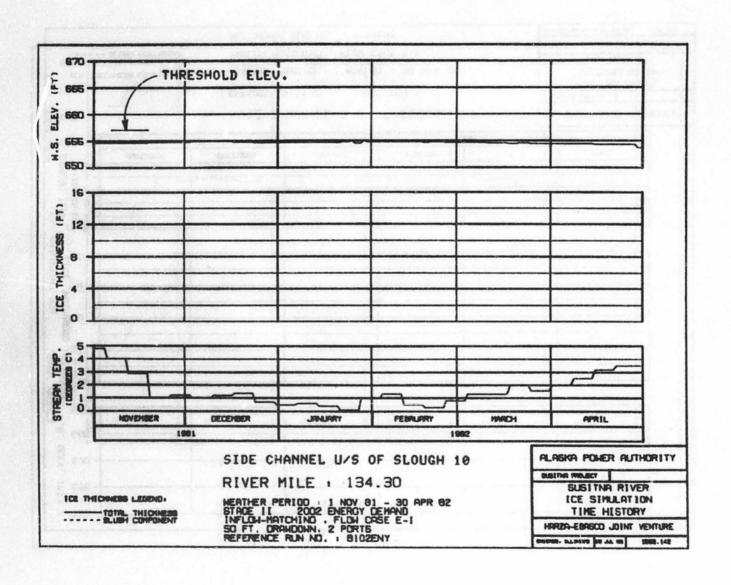


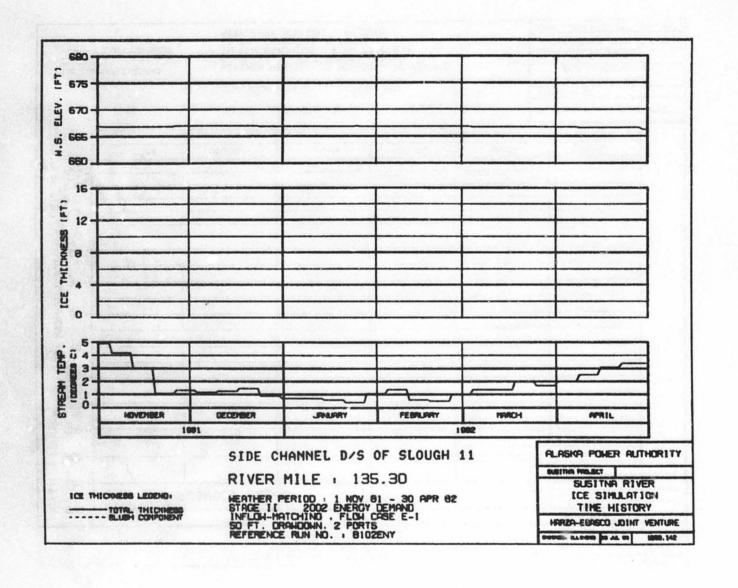




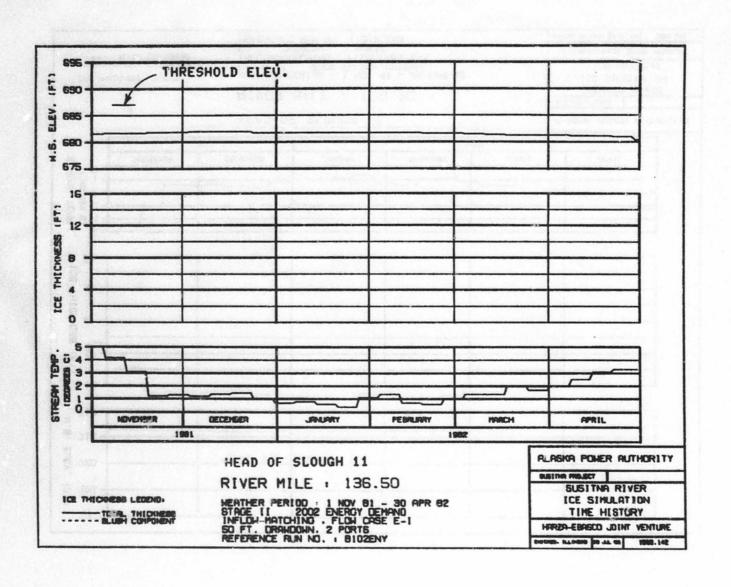


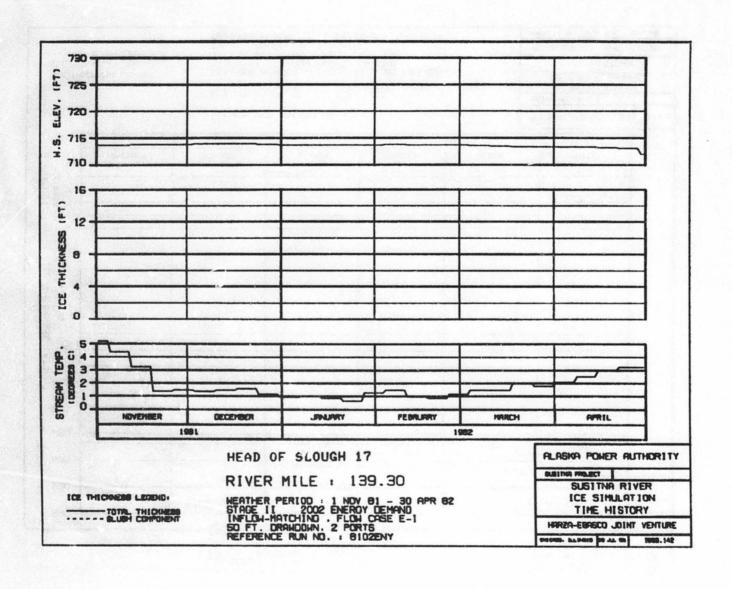


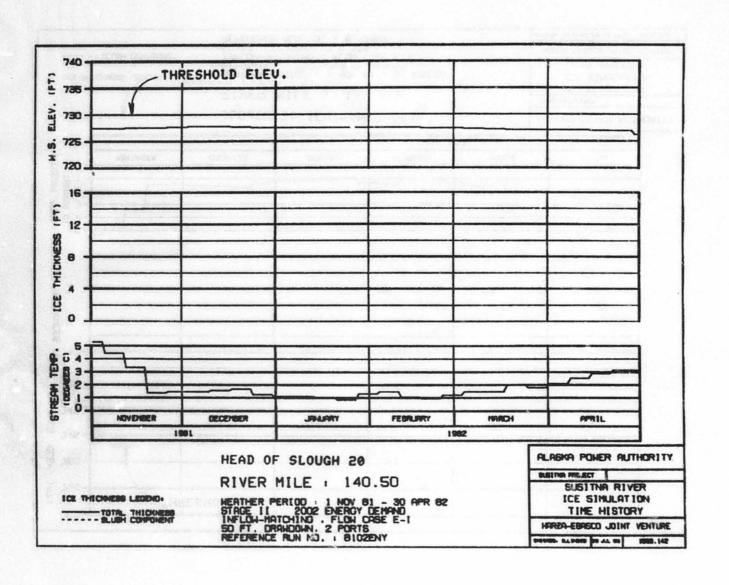


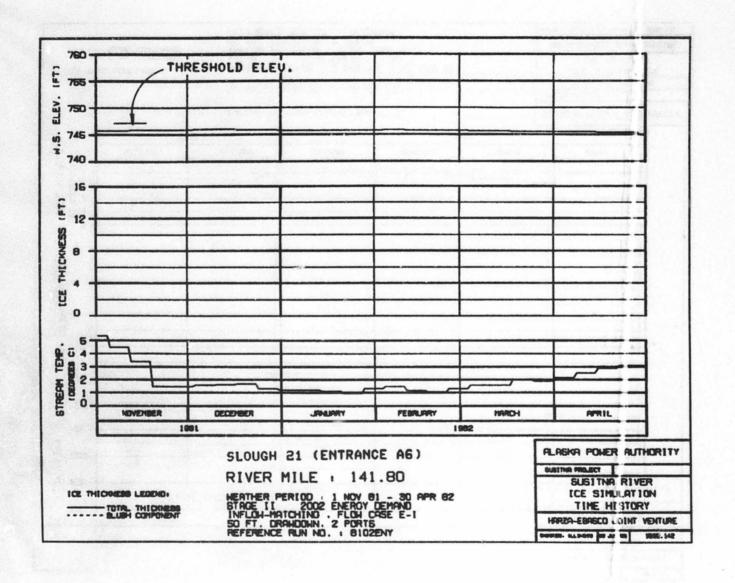


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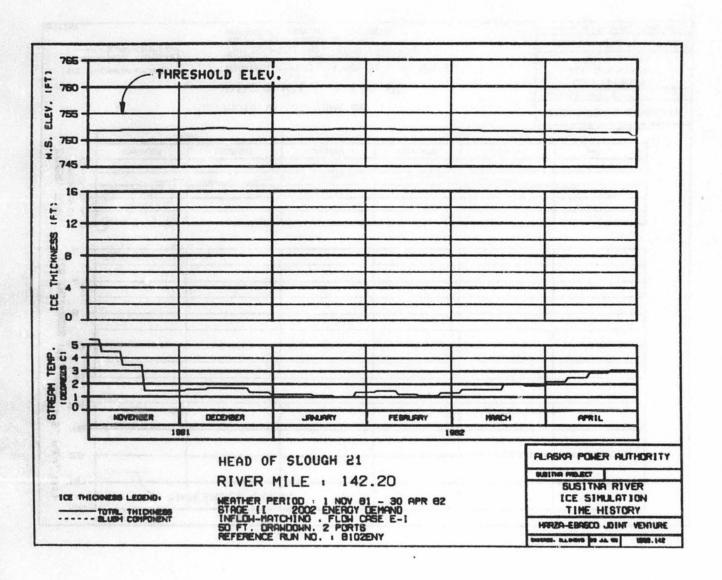


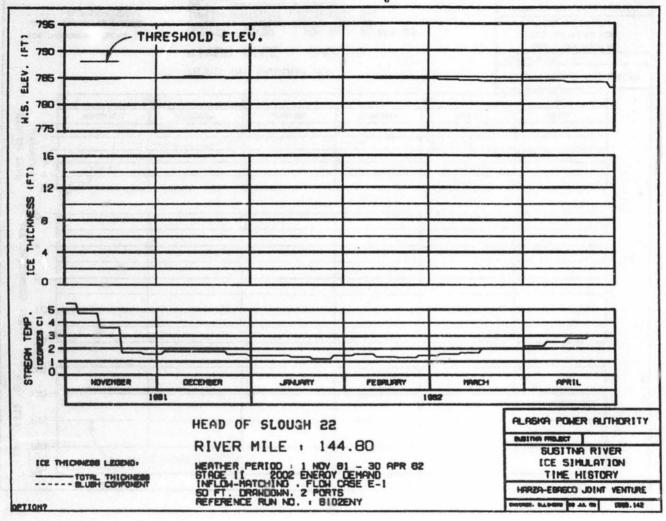






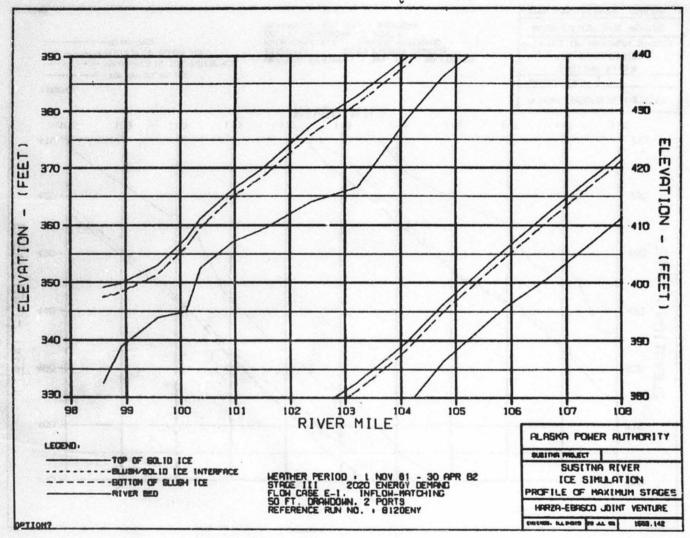
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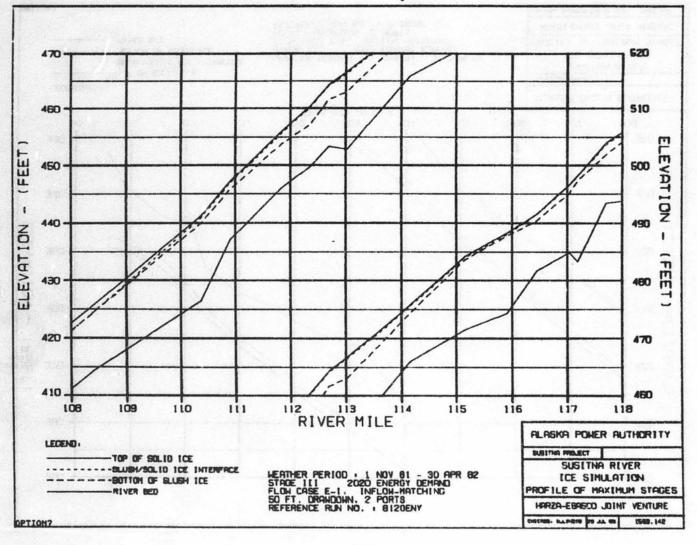
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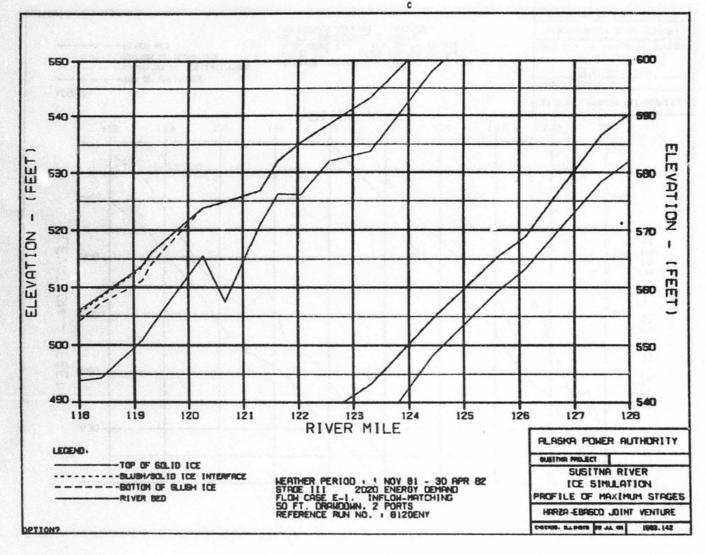


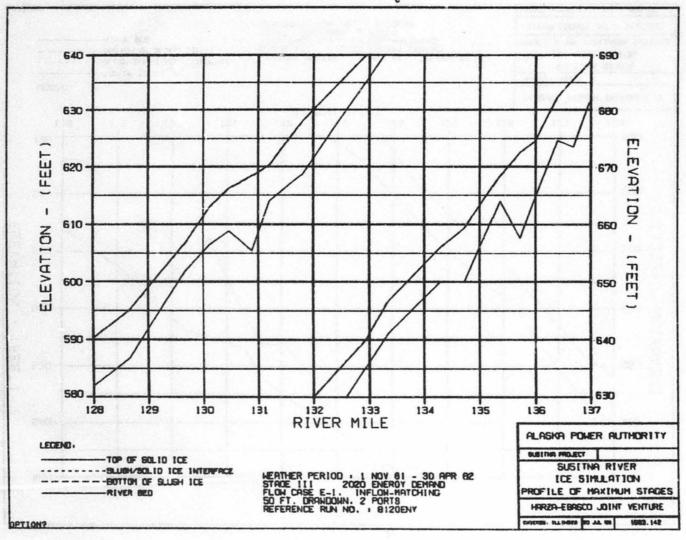
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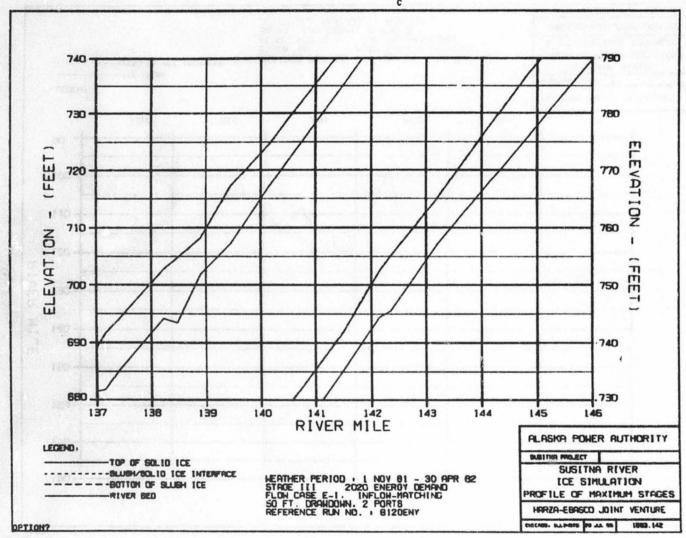




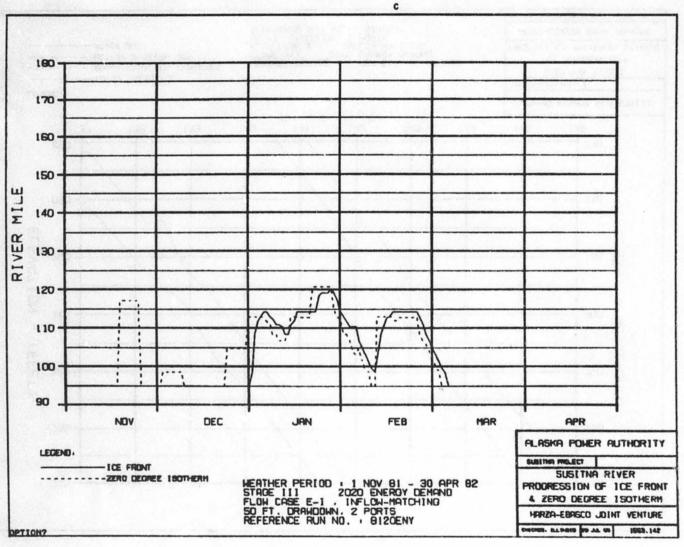


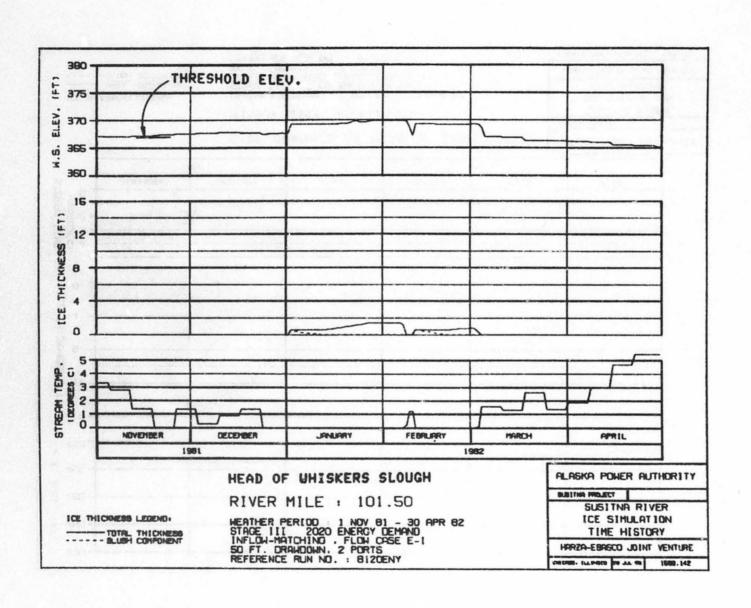


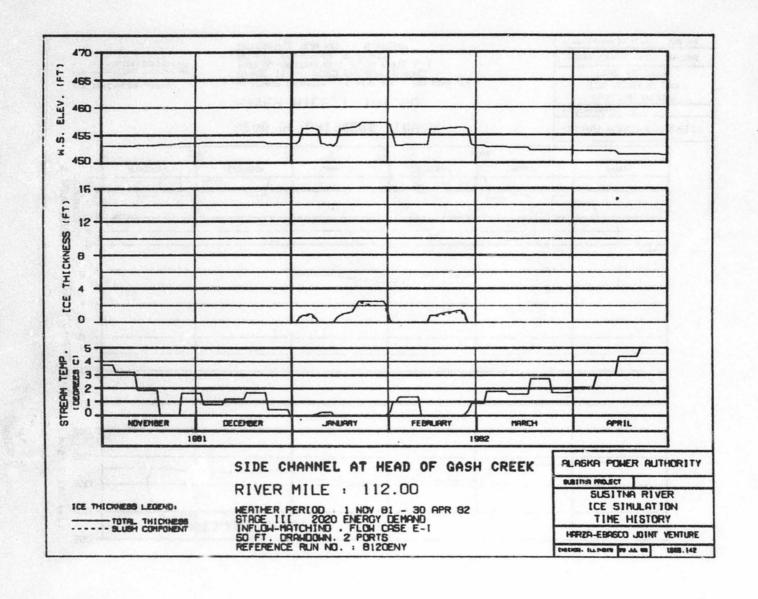


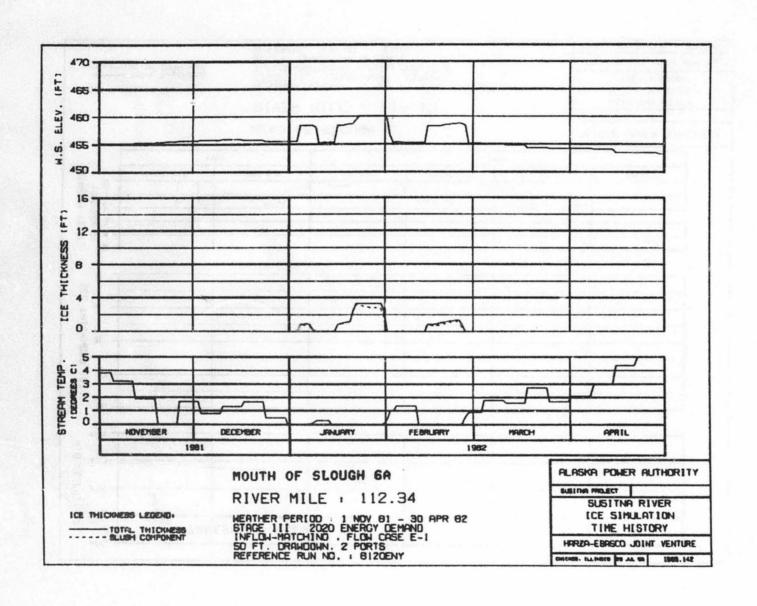


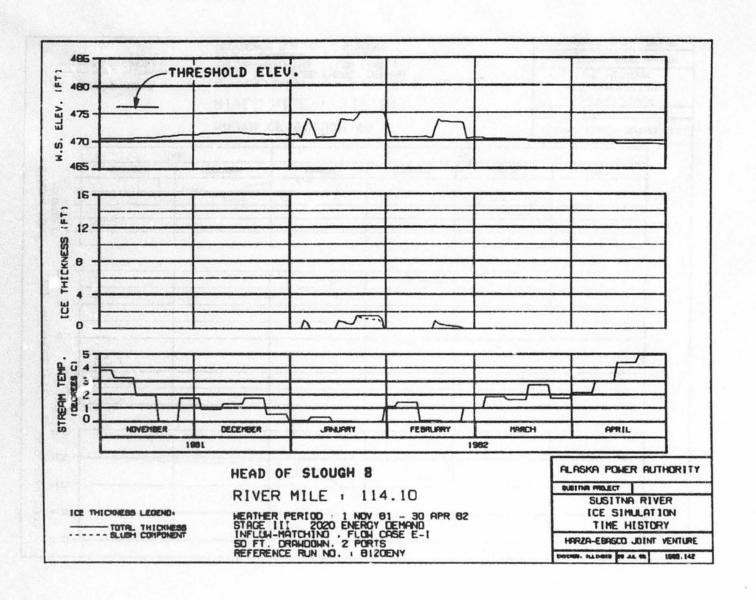


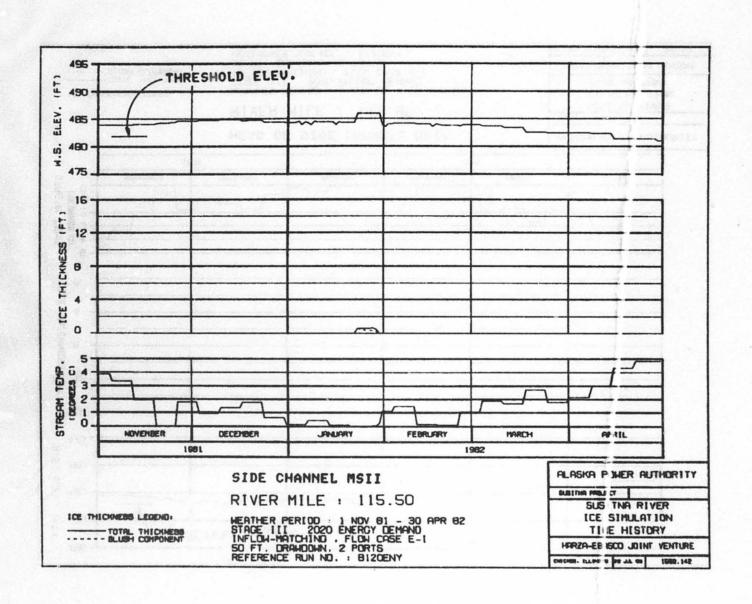


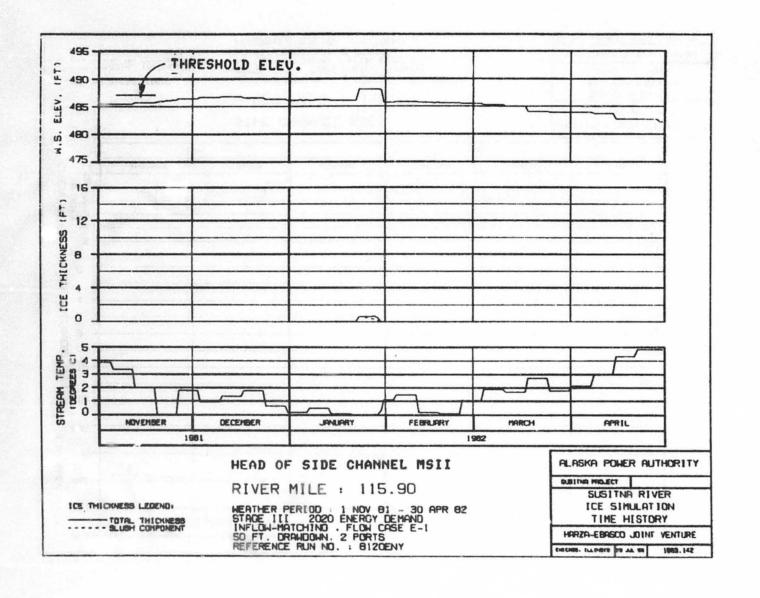


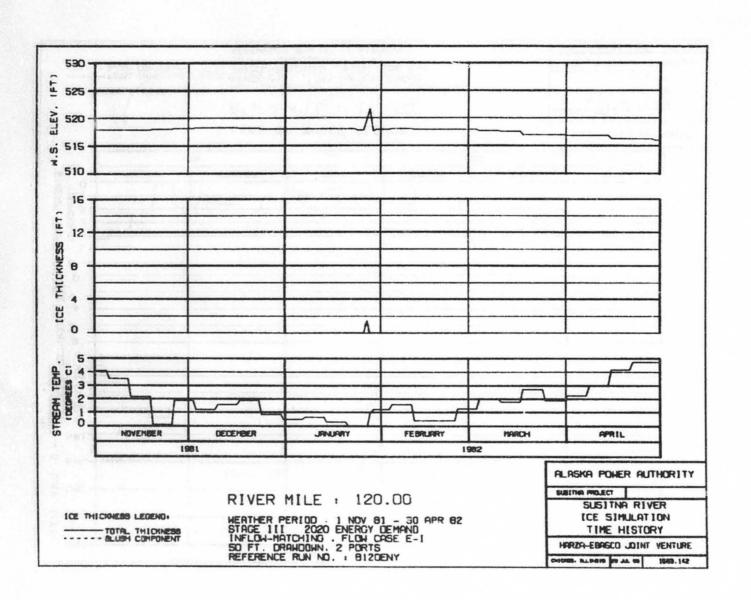


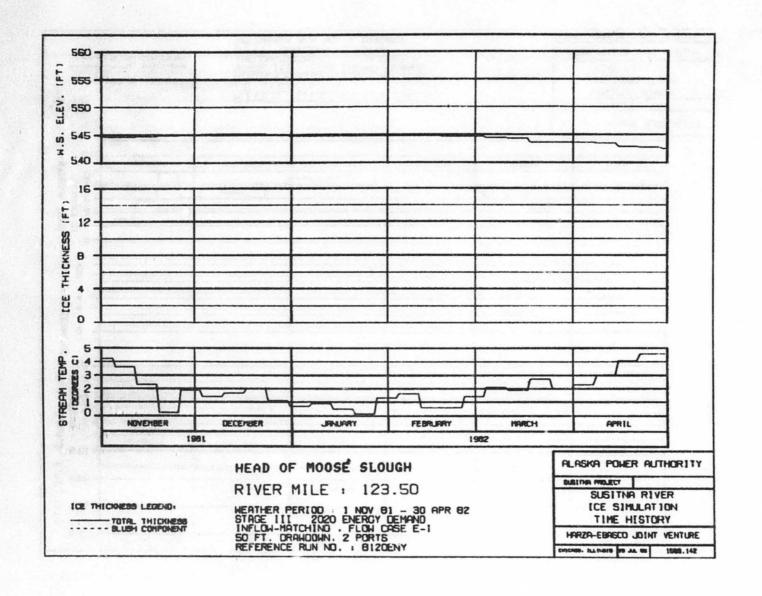


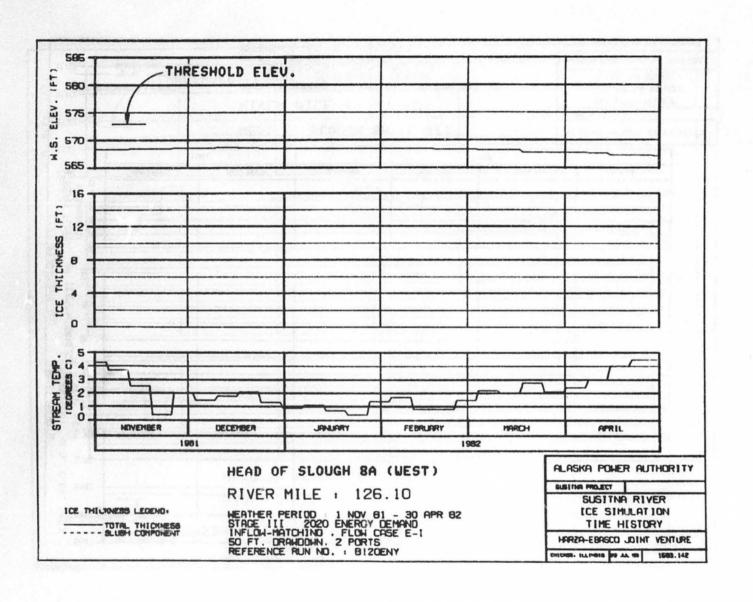


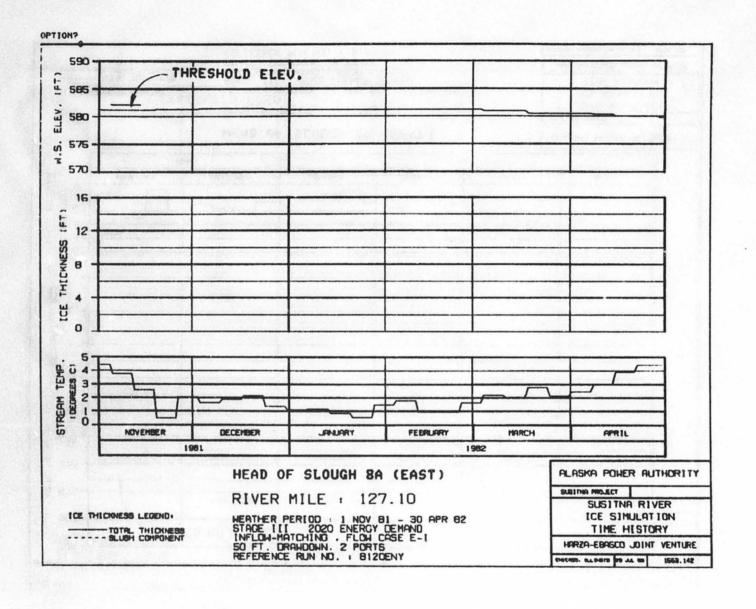


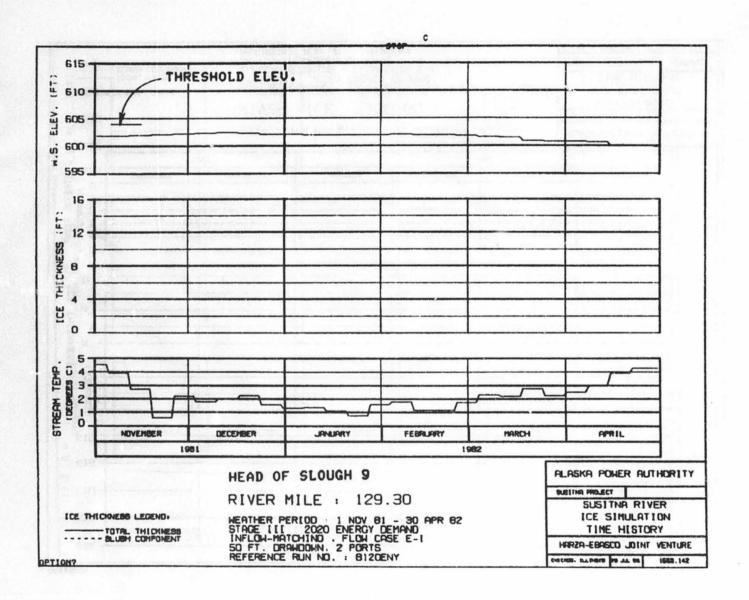


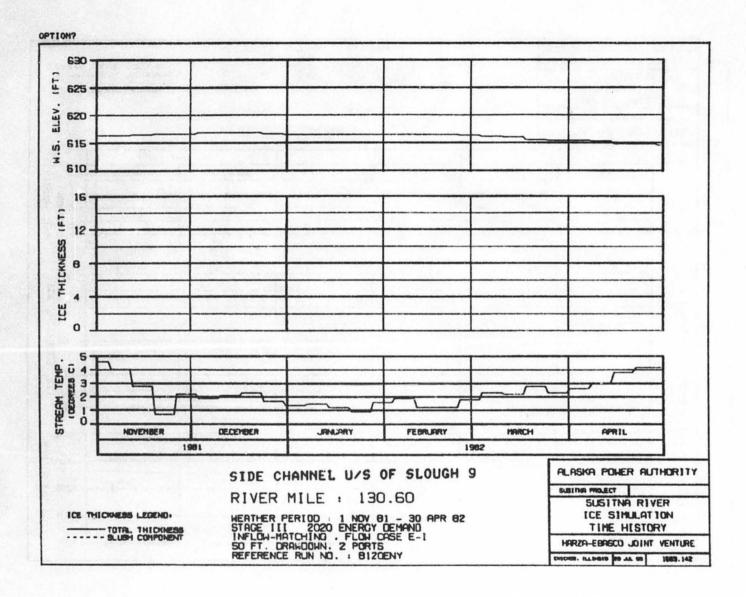




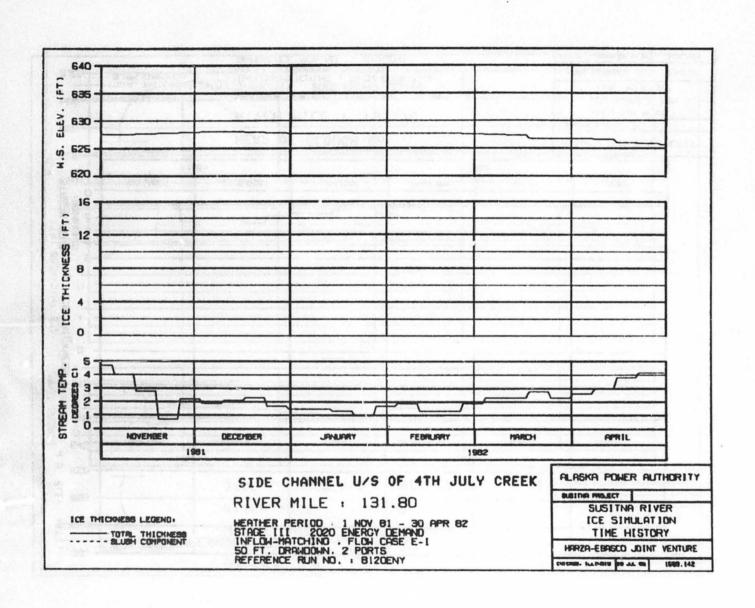


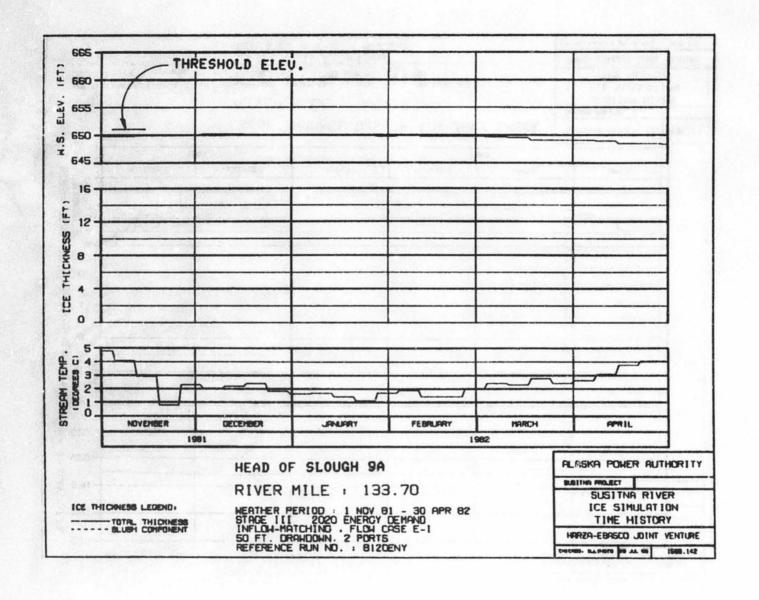


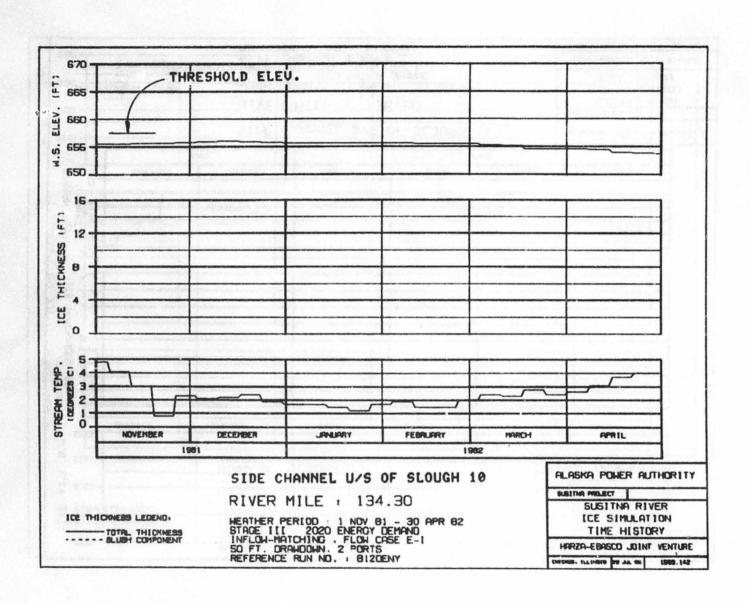


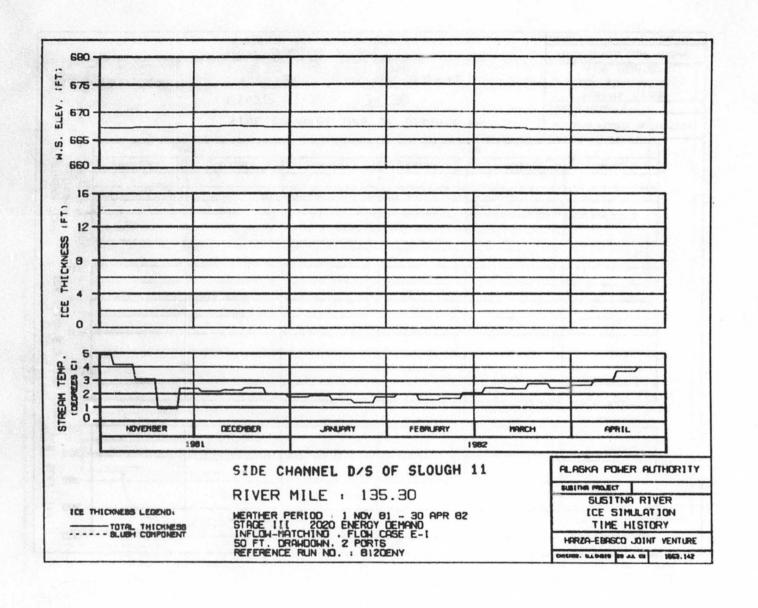


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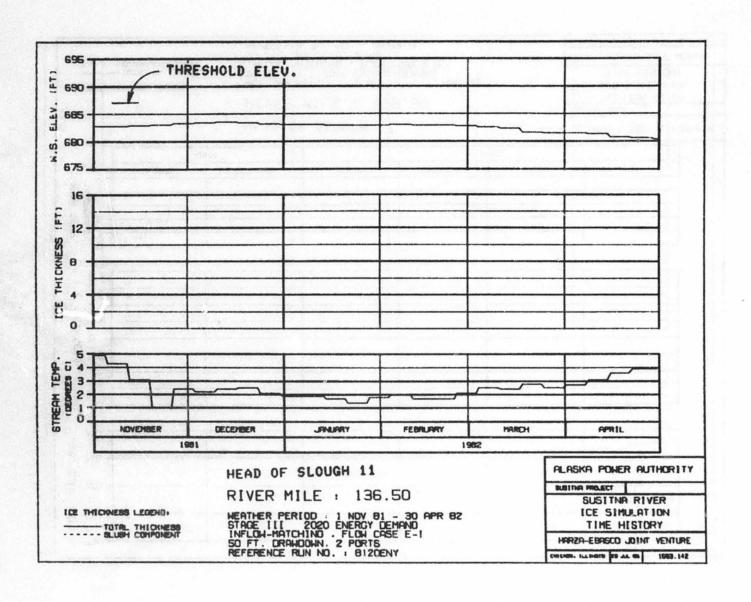


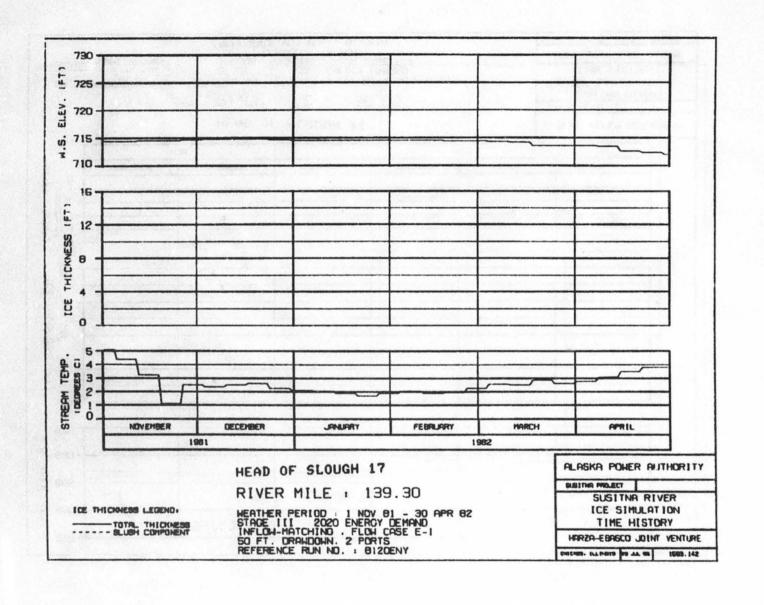




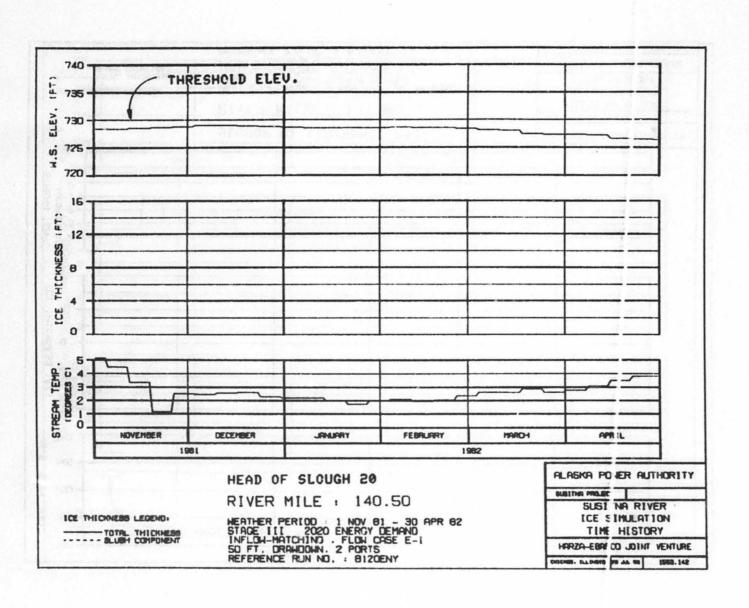


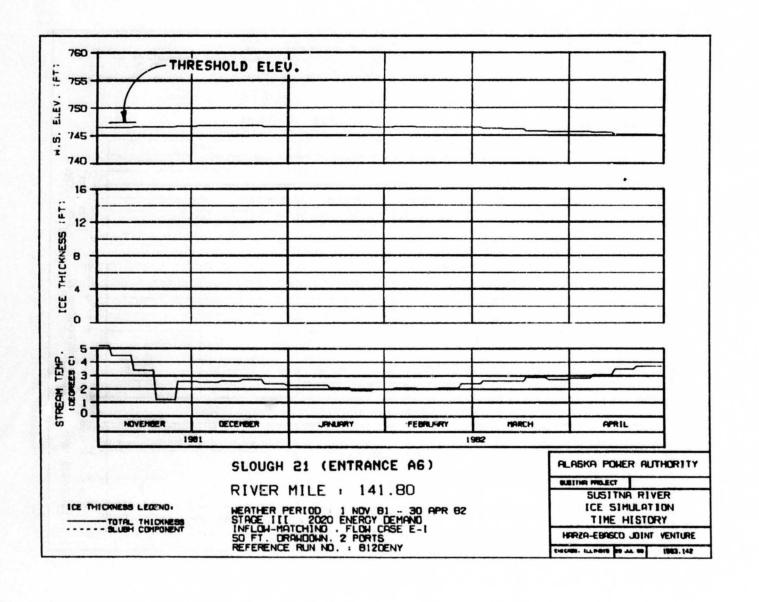
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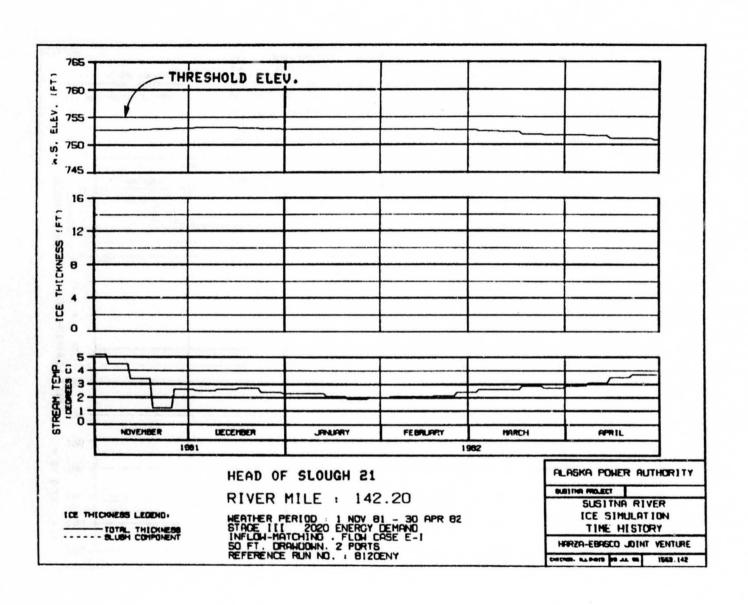


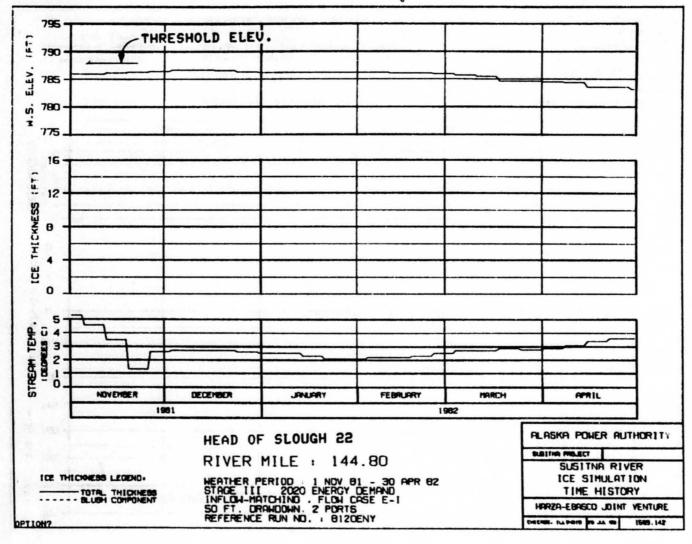
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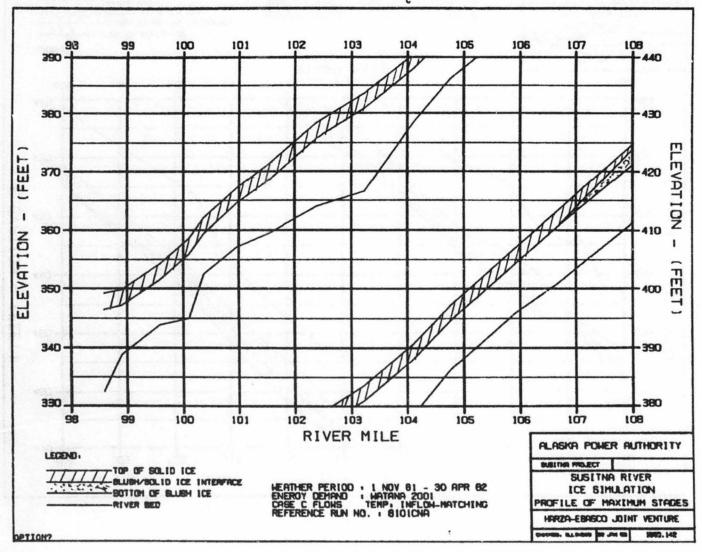
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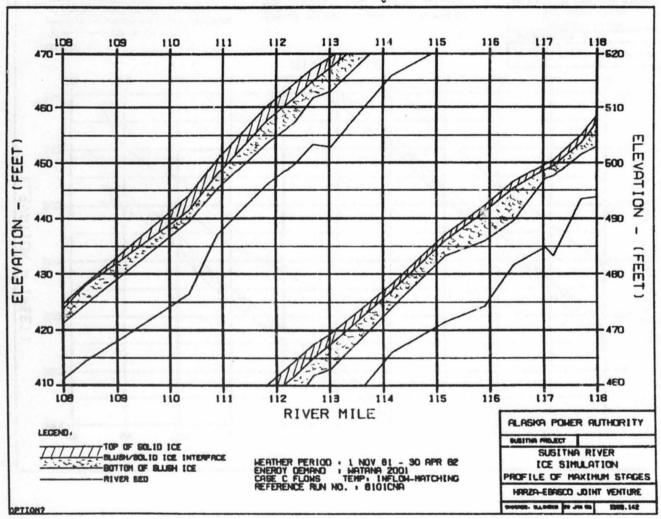


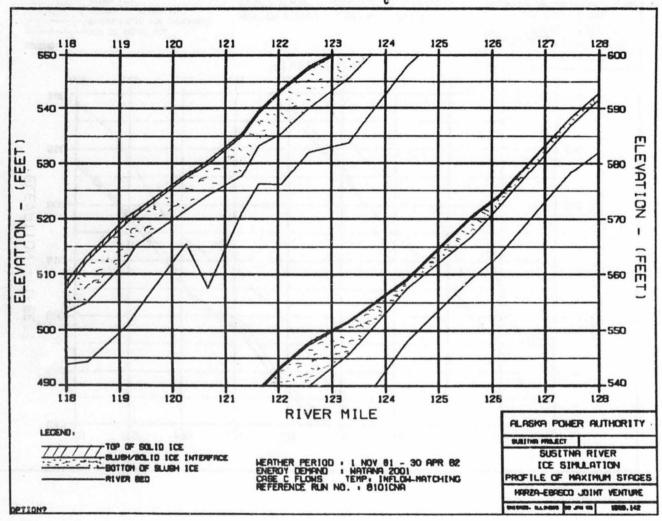
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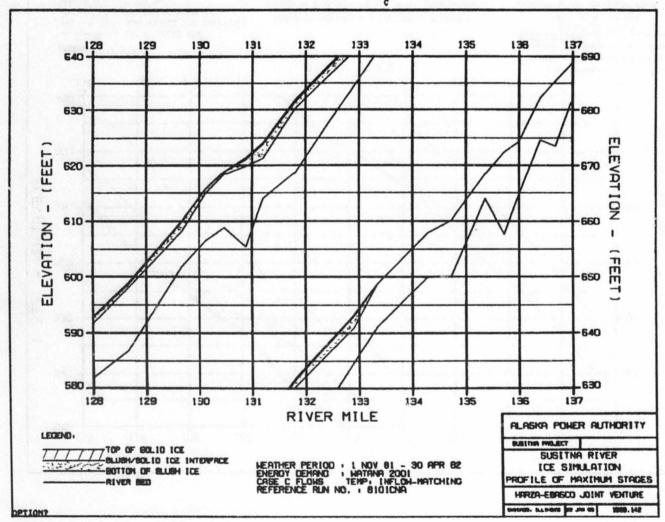
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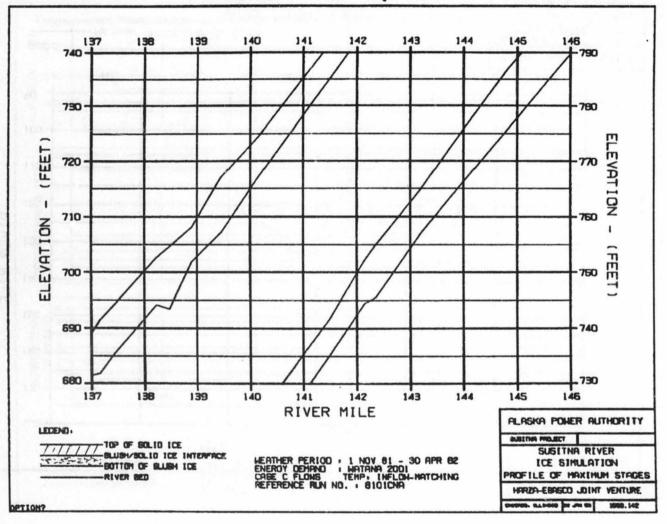




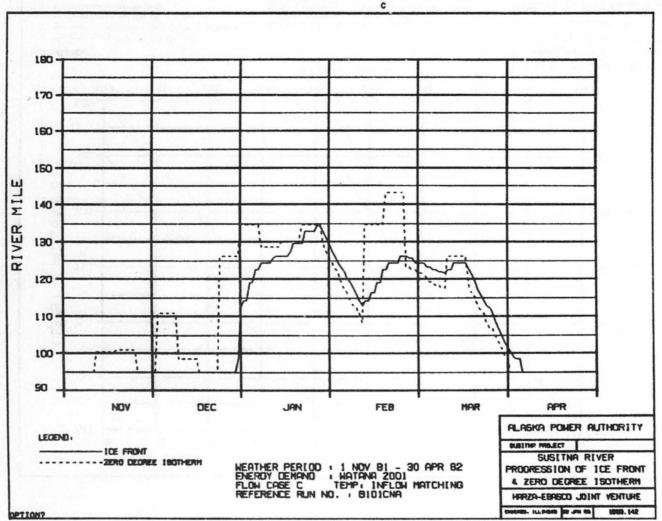


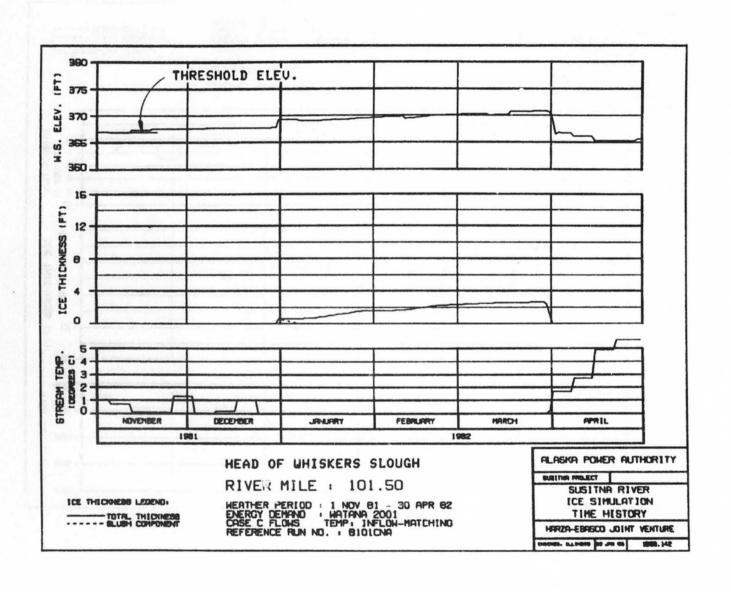
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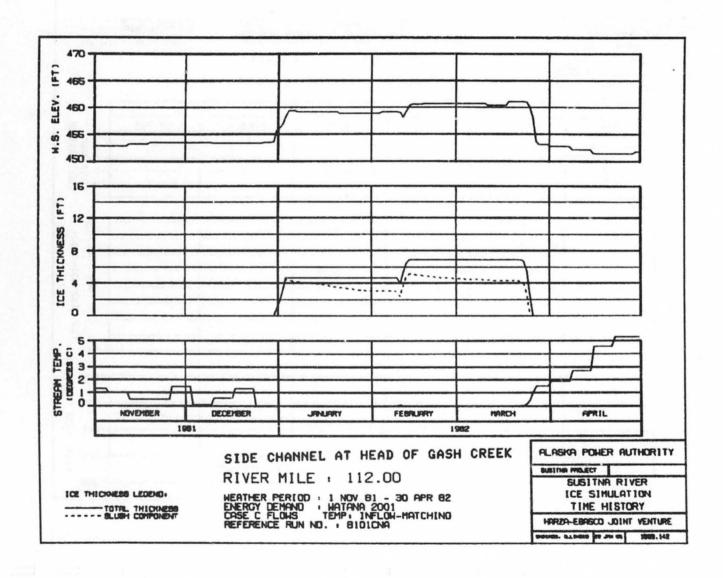


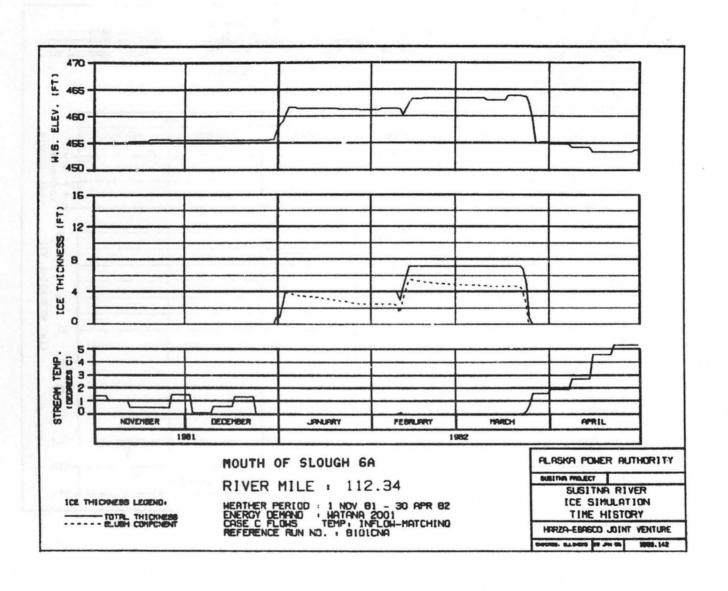


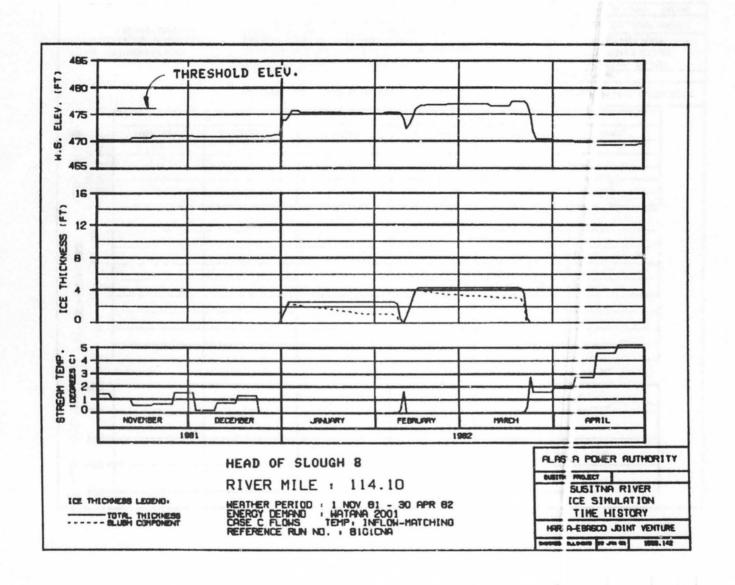


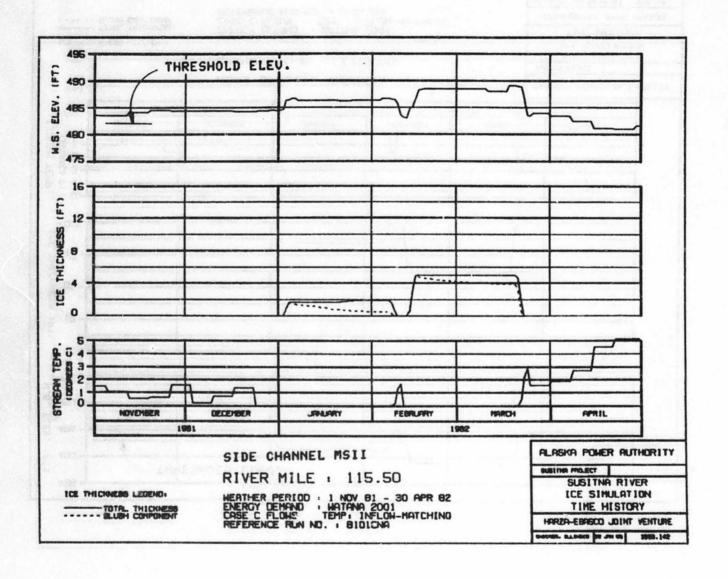


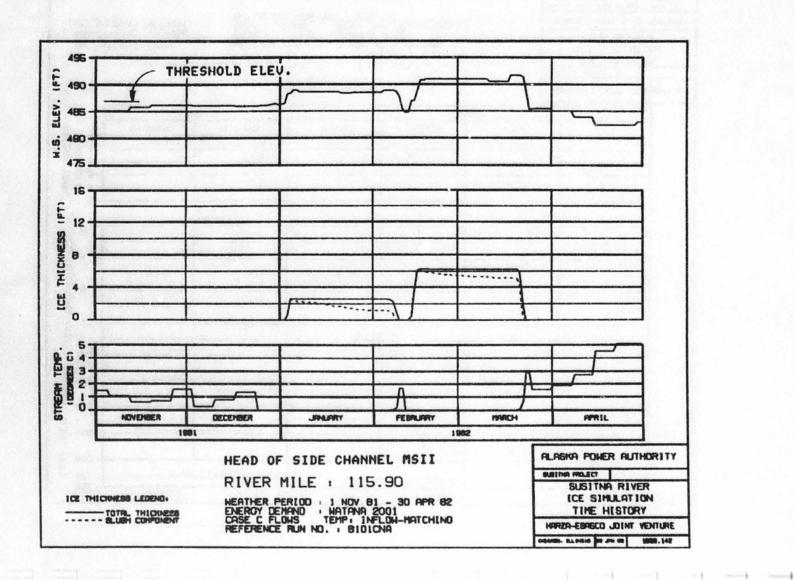


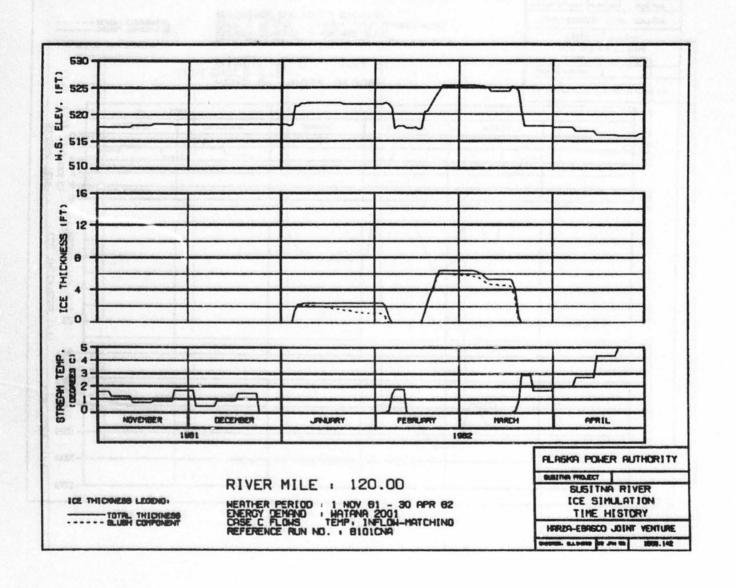


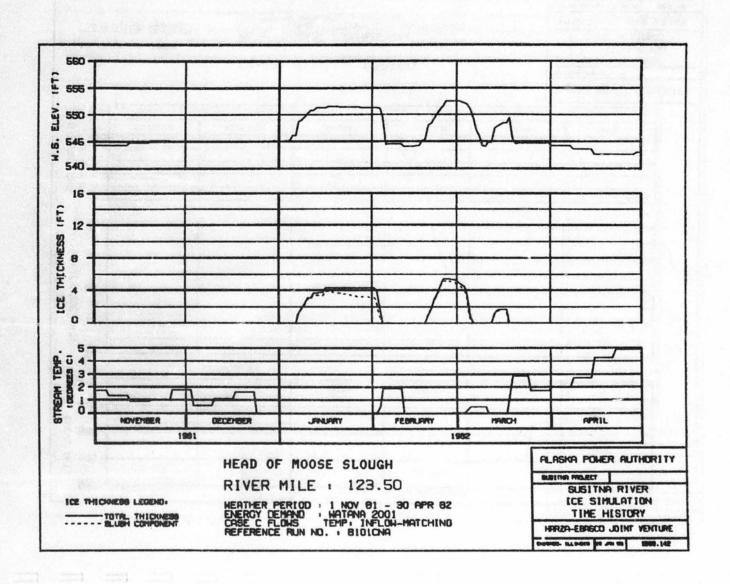


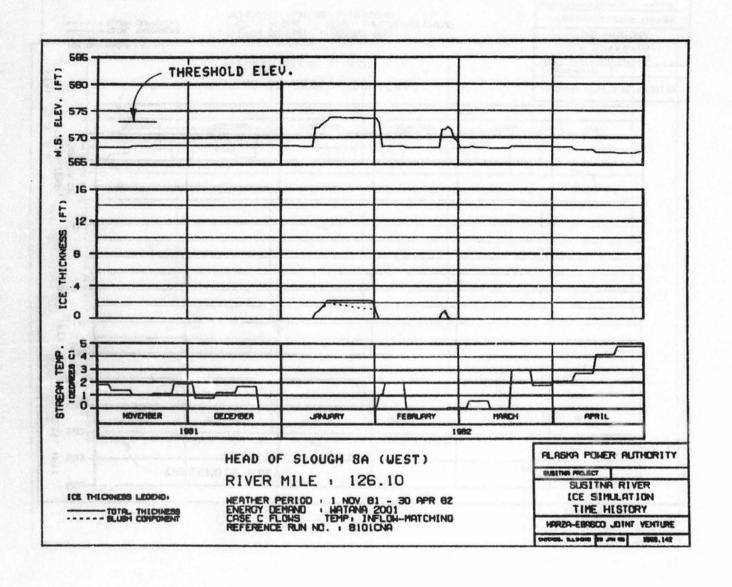


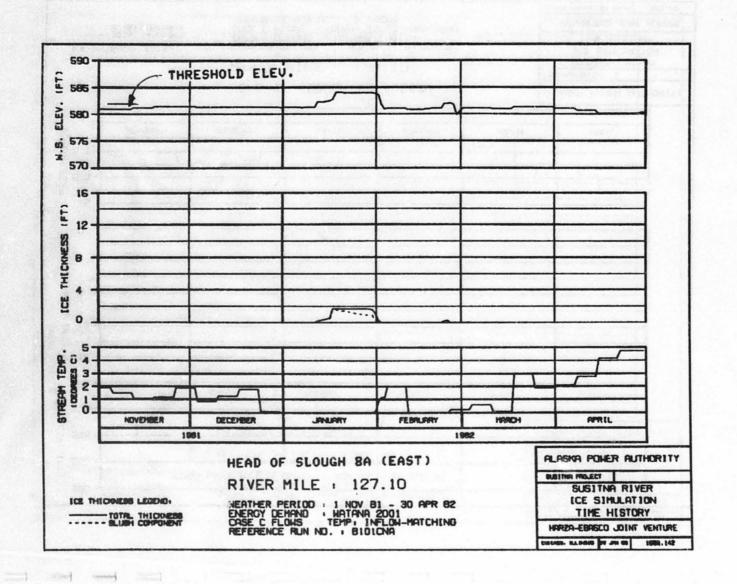


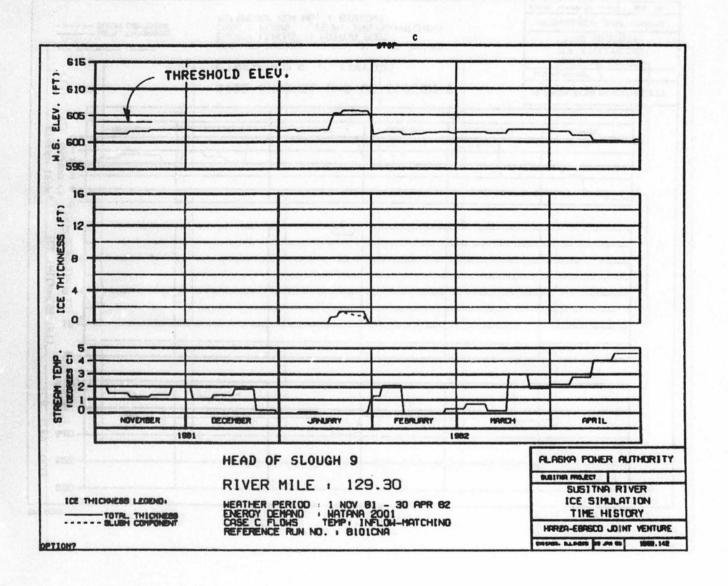


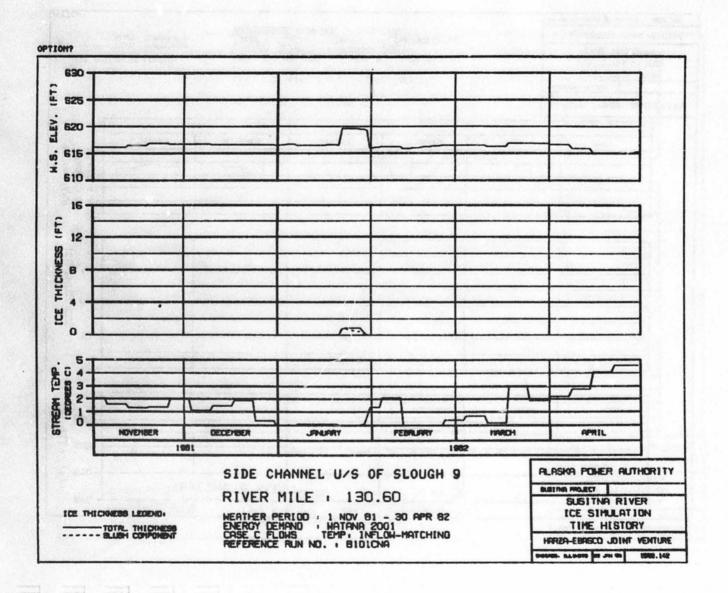


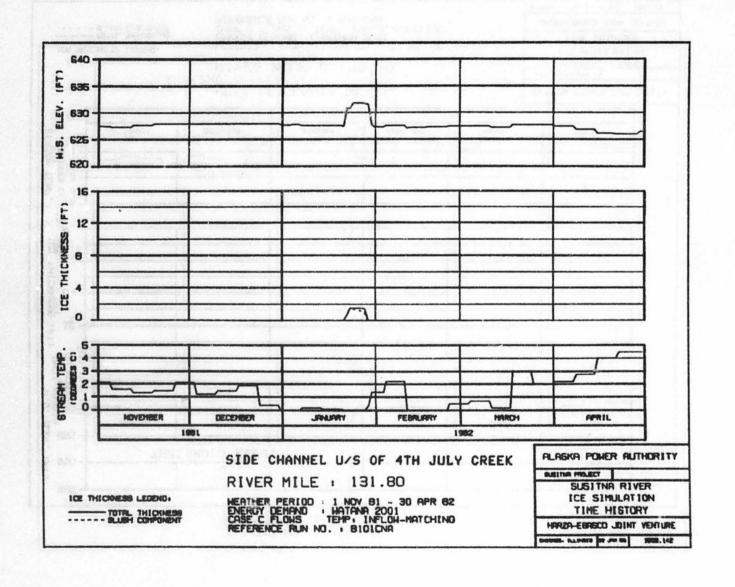


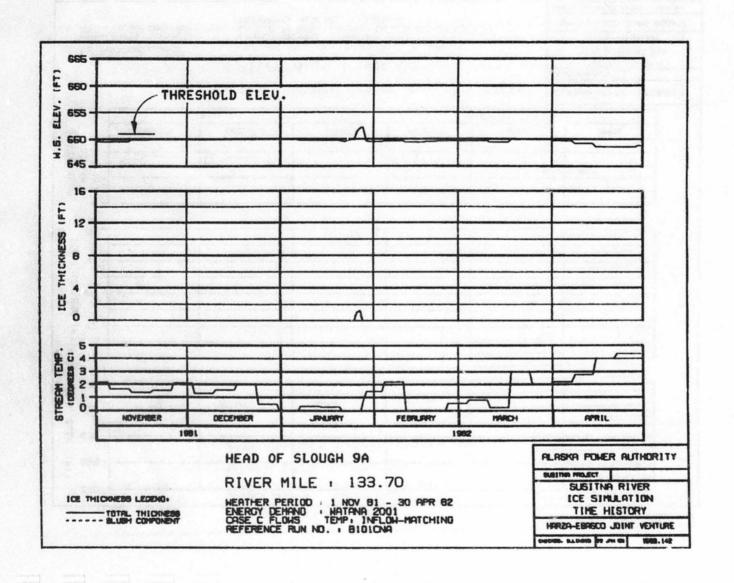


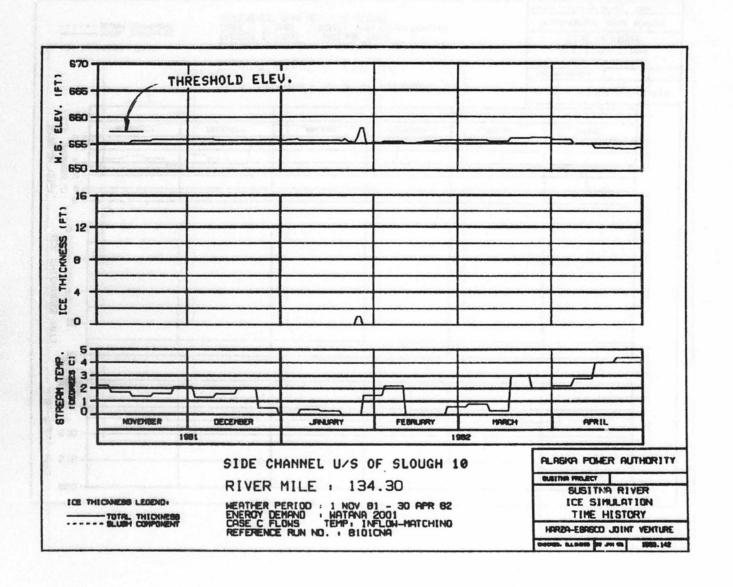


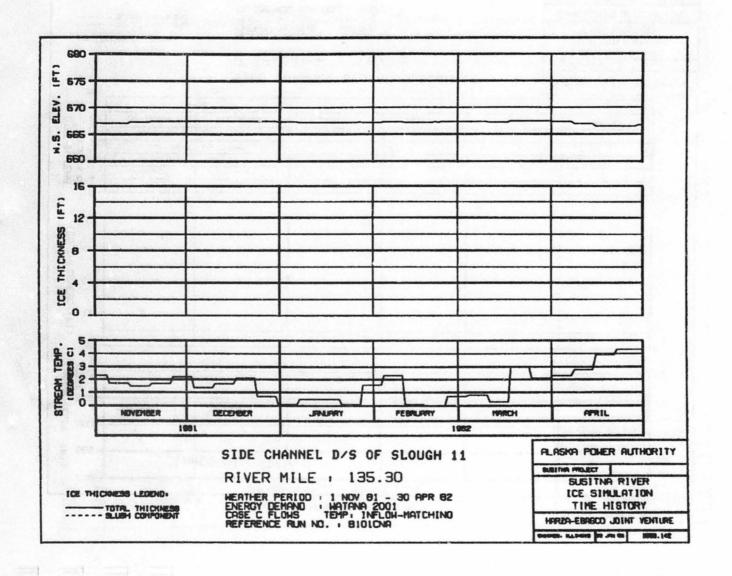


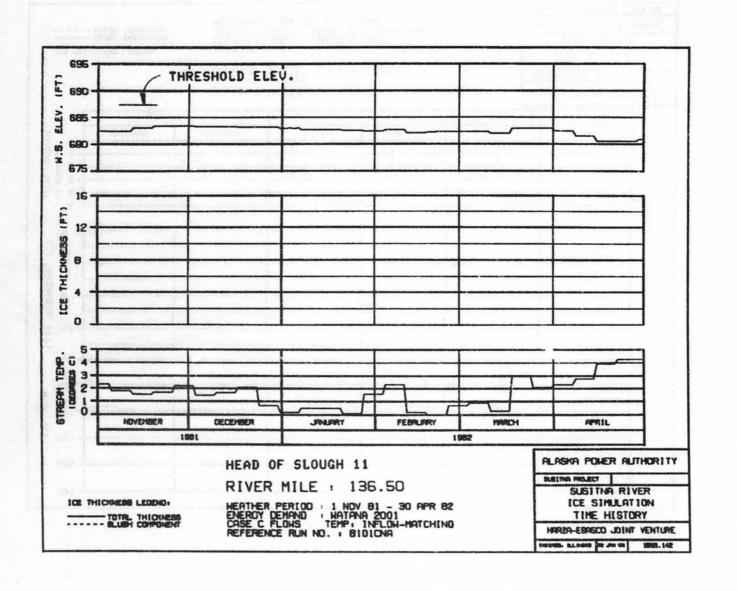


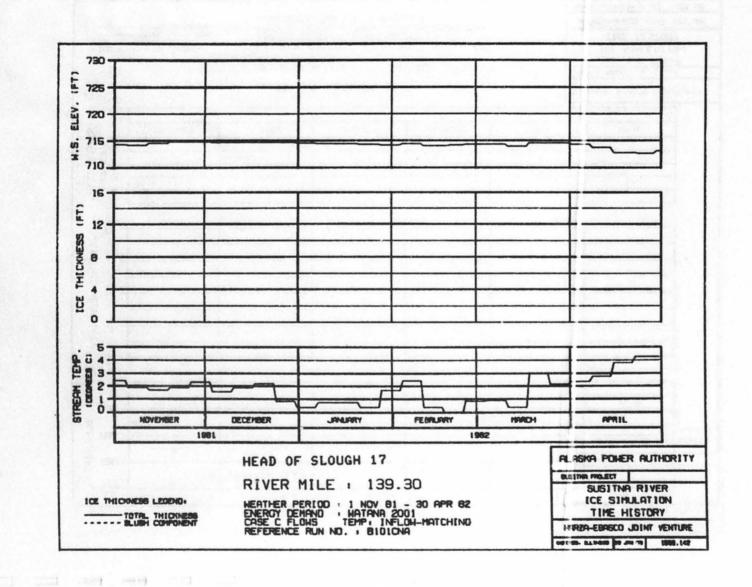


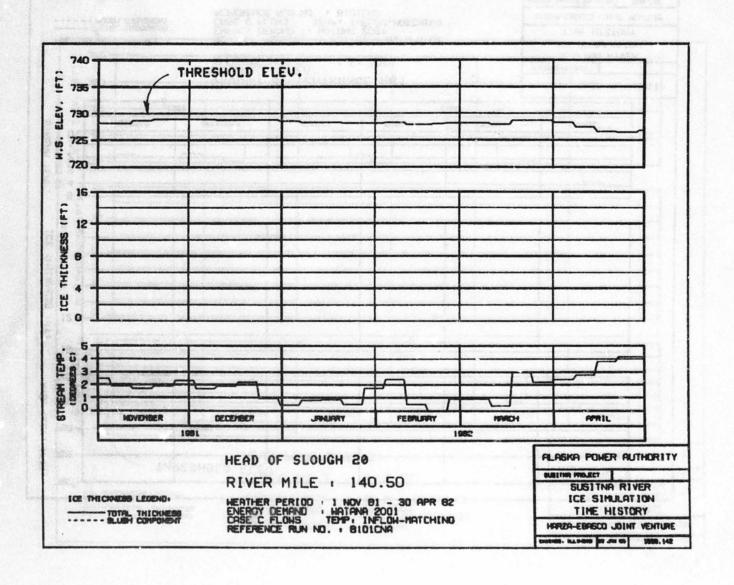


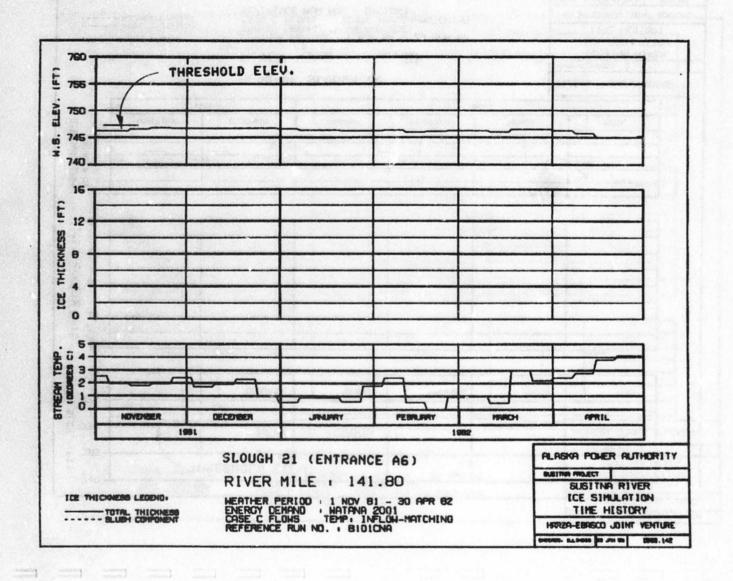


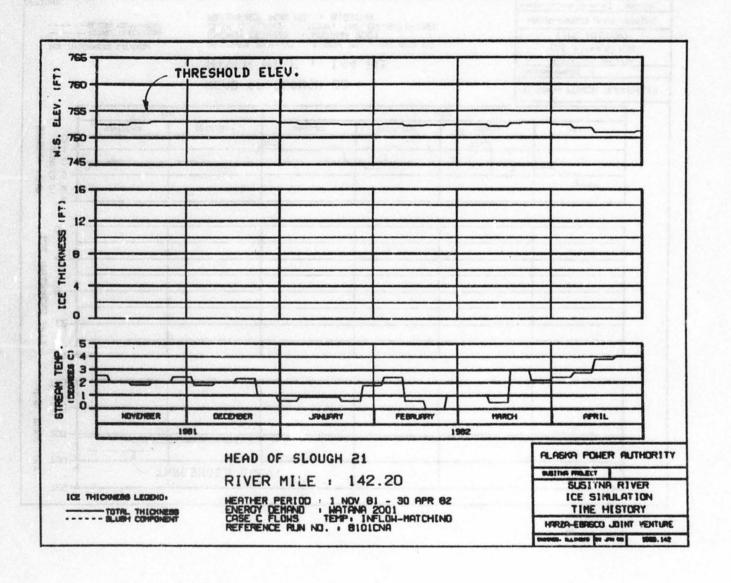


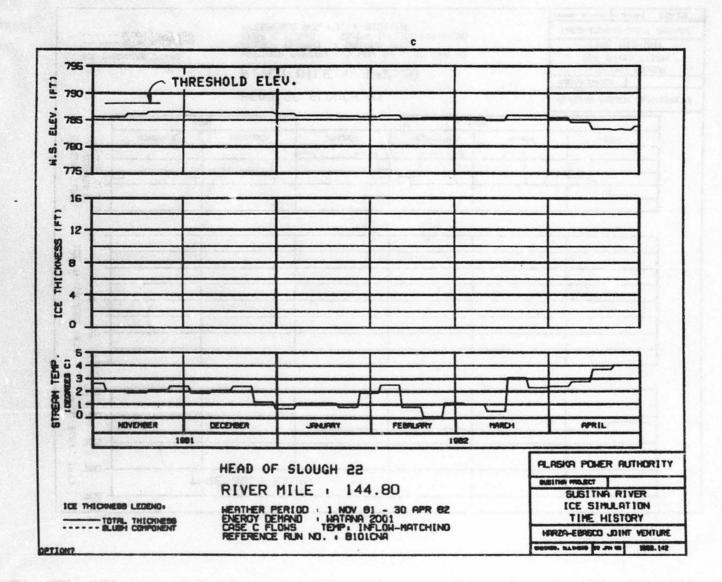




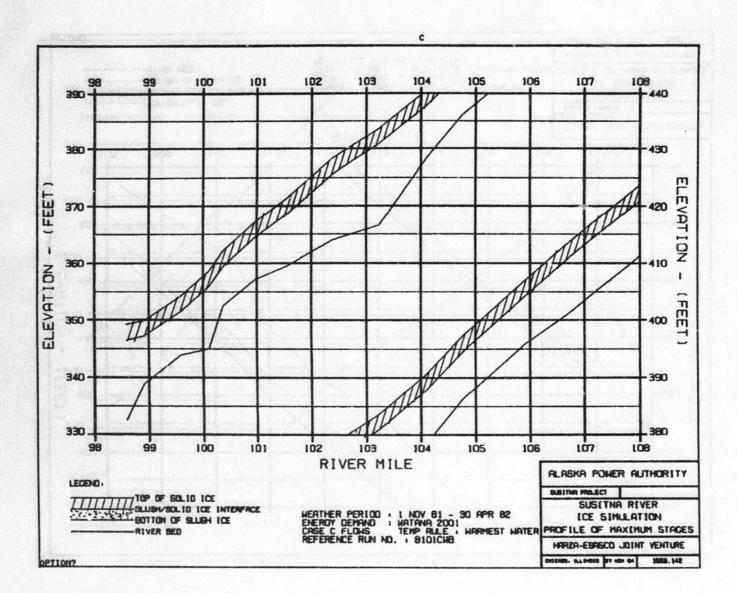




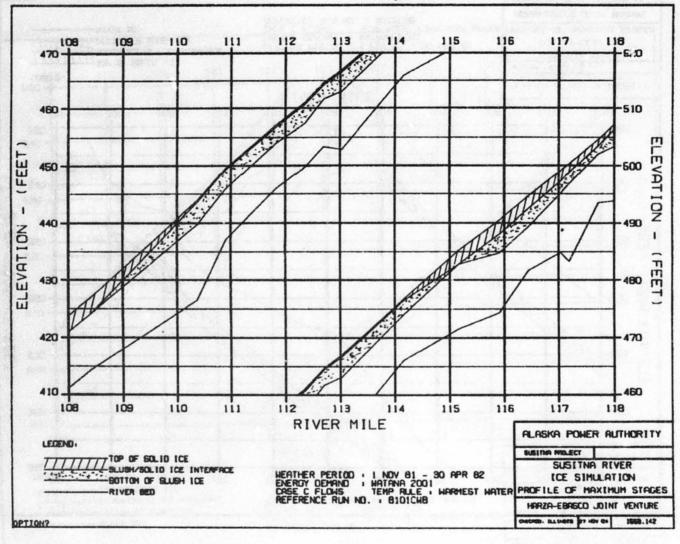




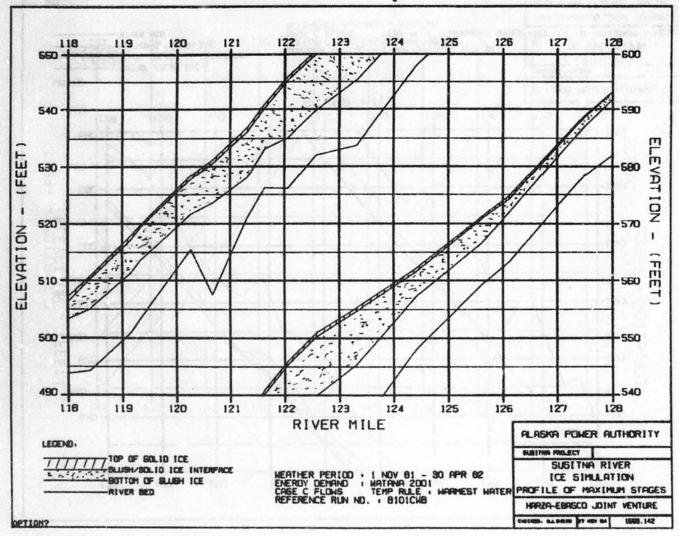
## EXHIBIT H



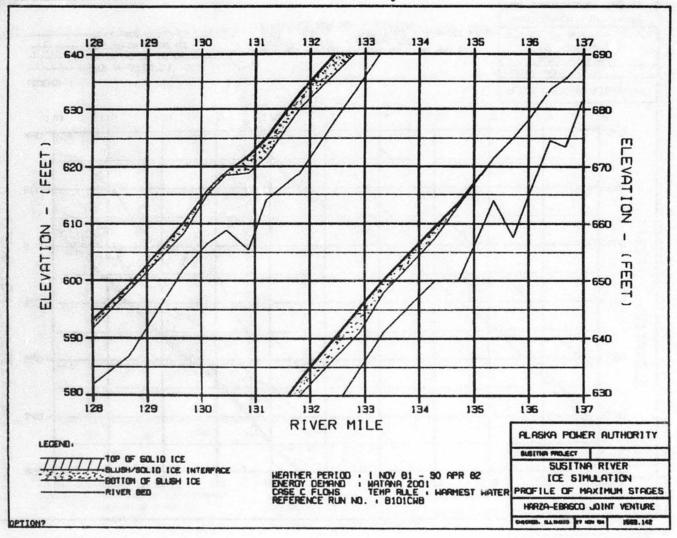




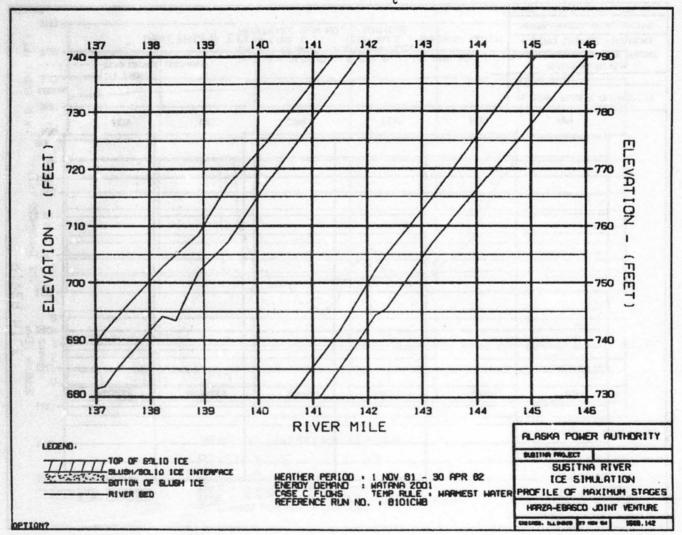


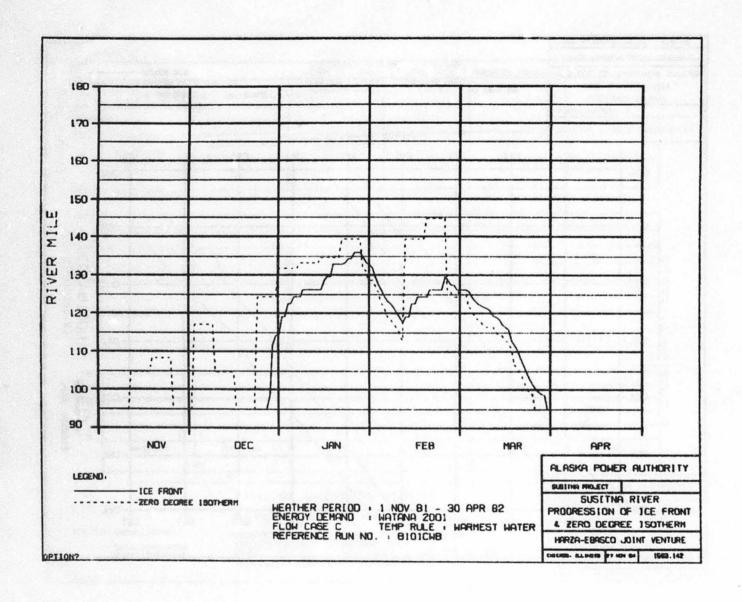


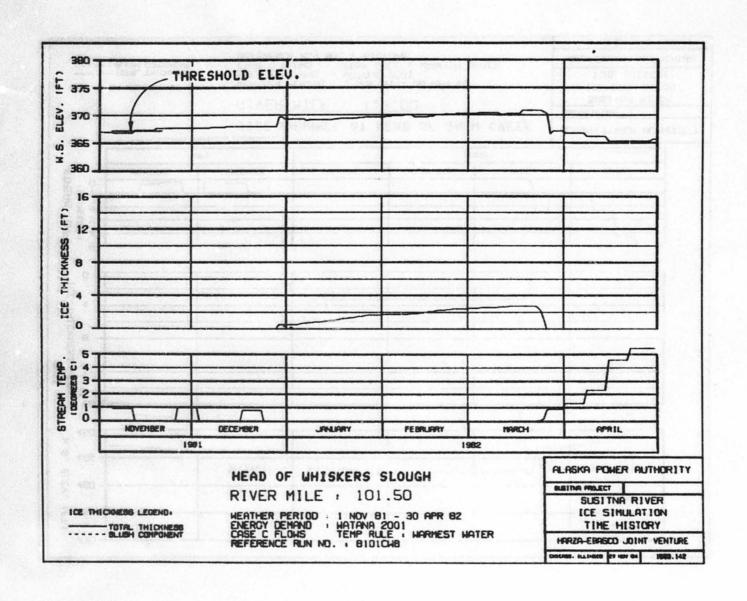


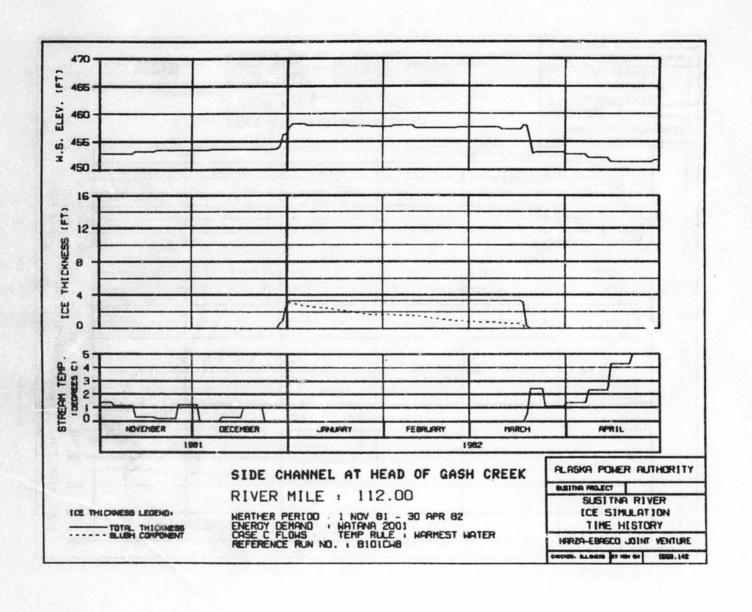


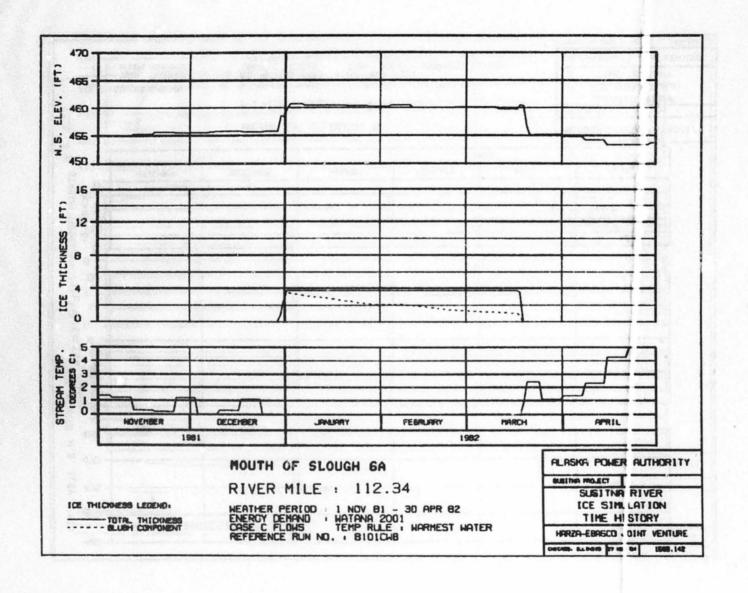


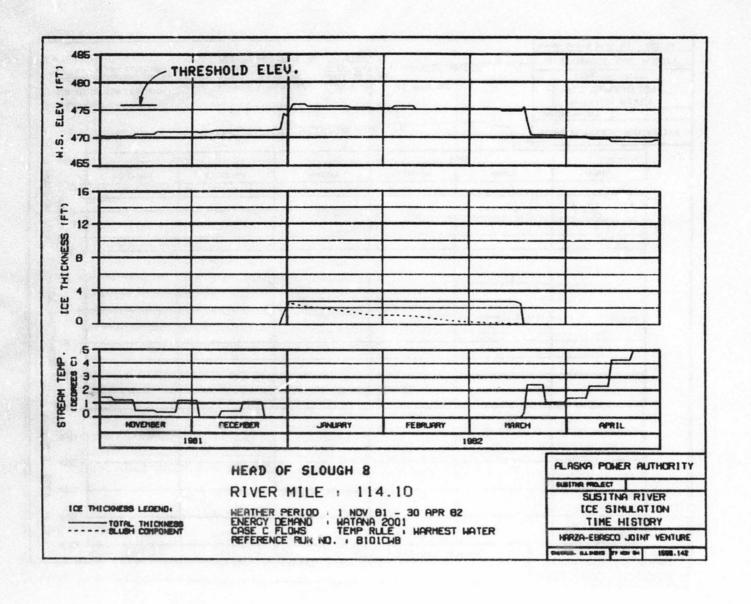


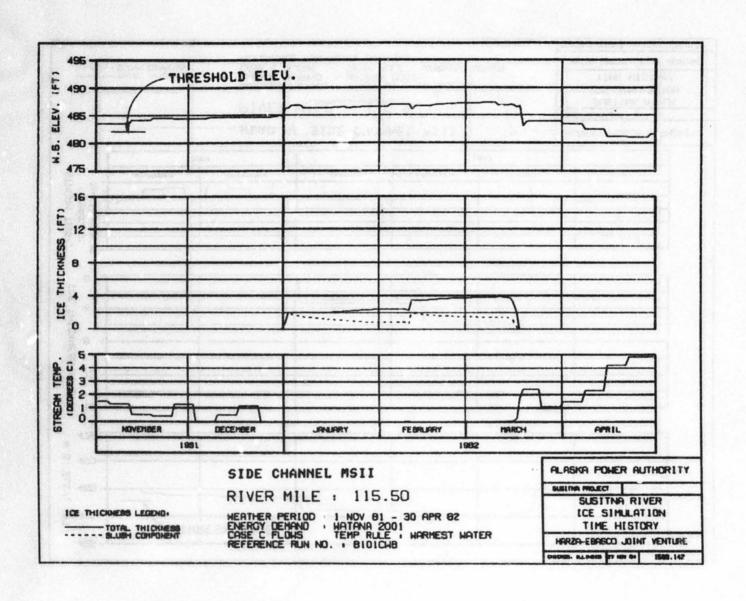


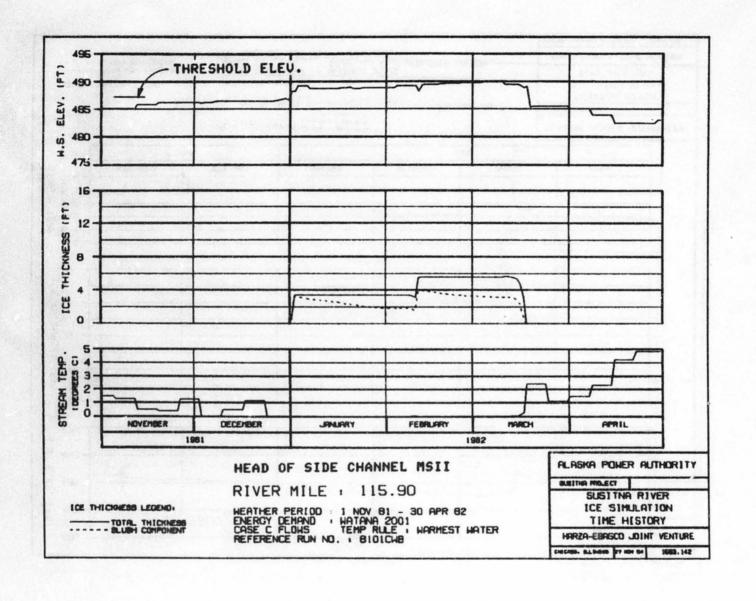


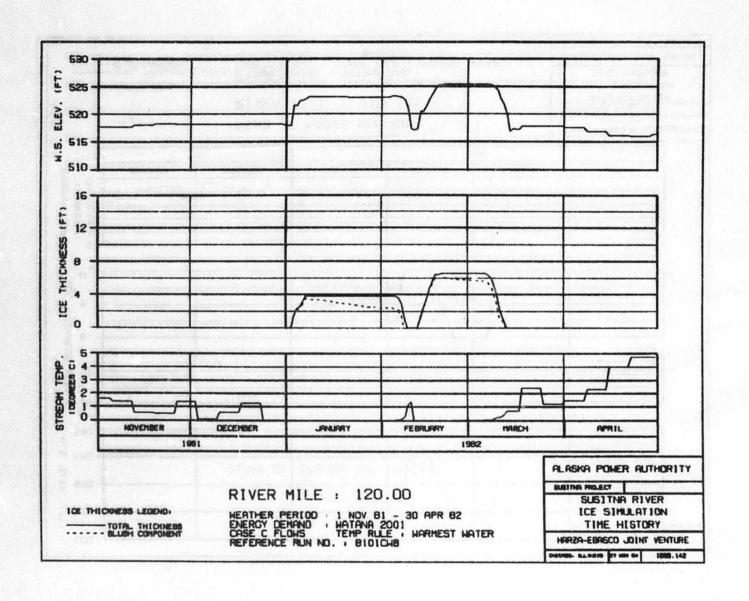


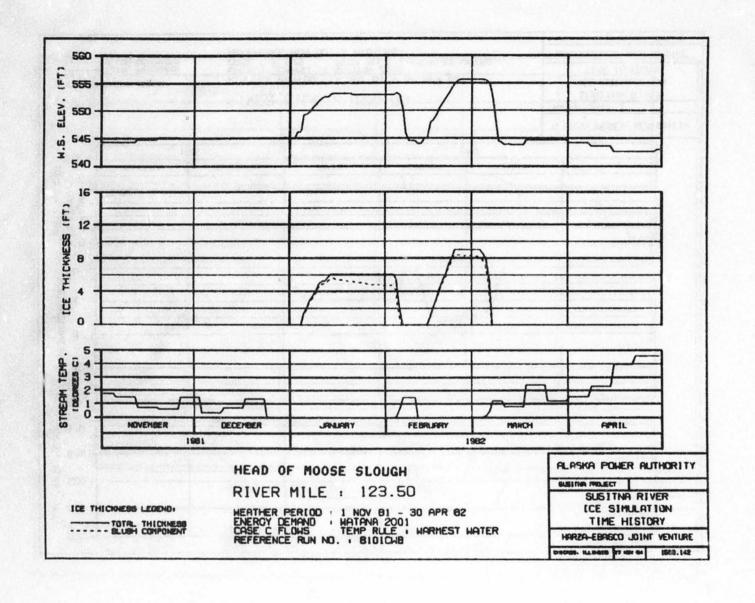


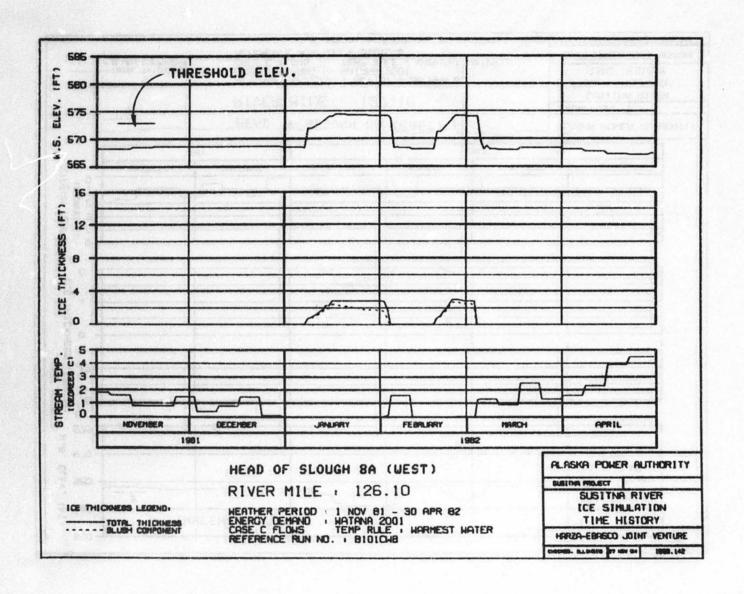


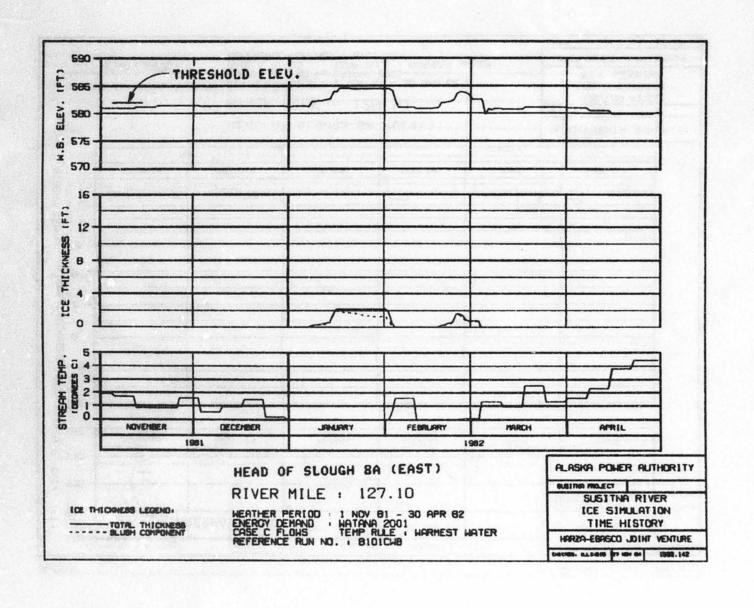


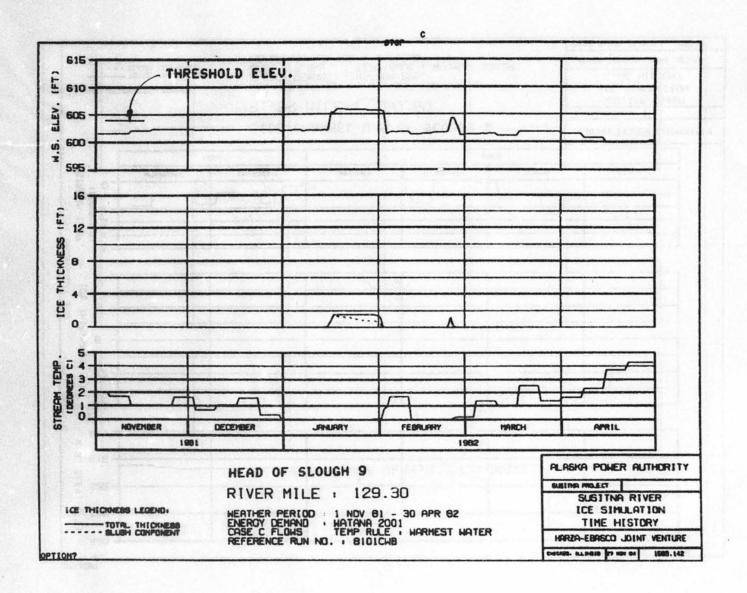


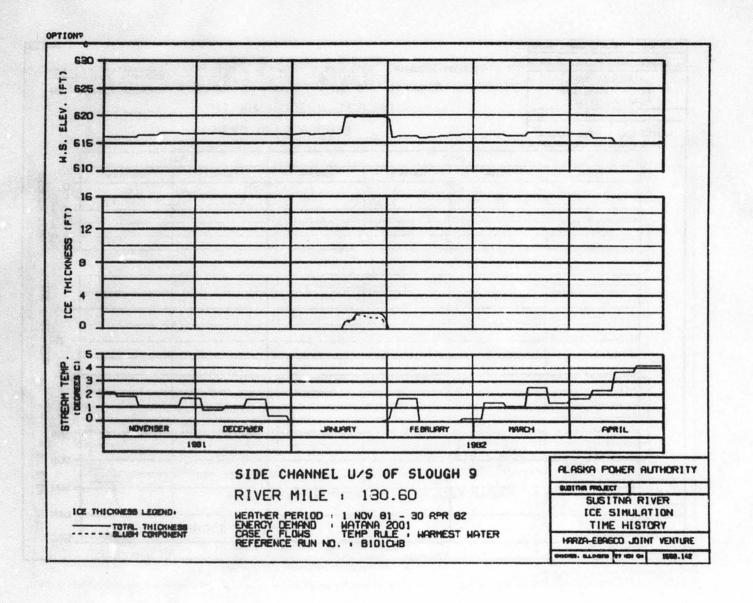


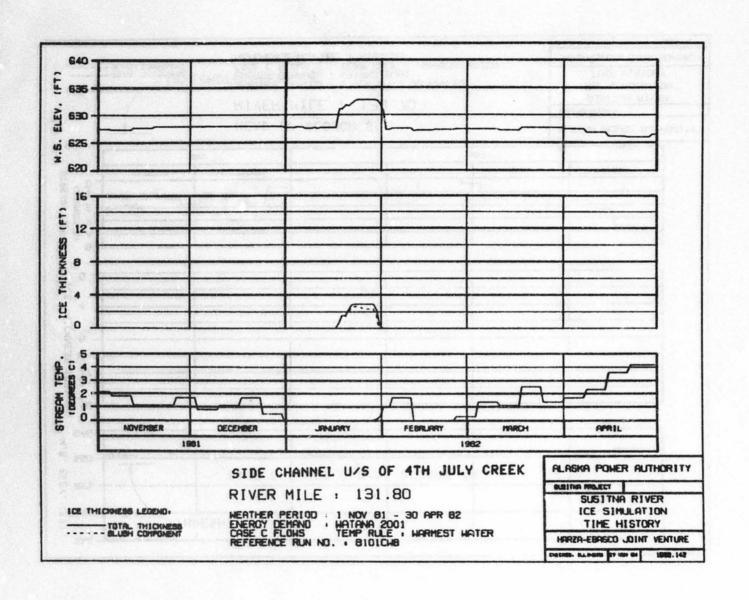


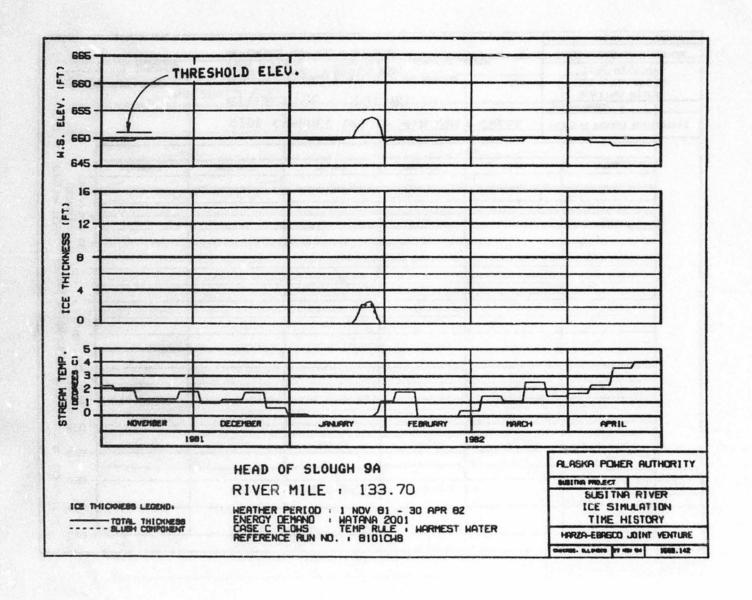


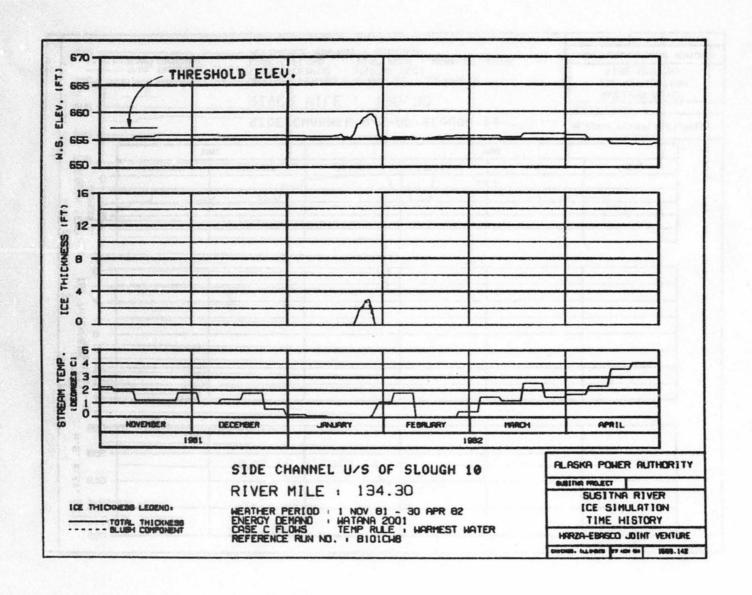


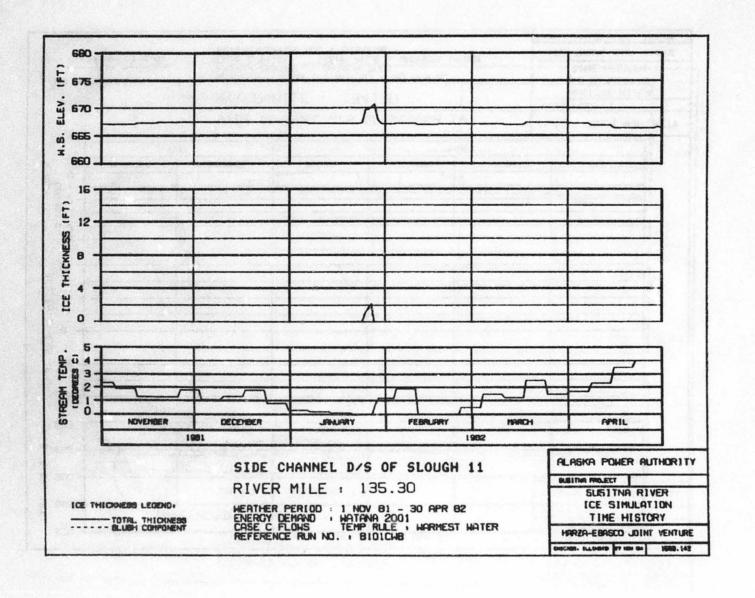


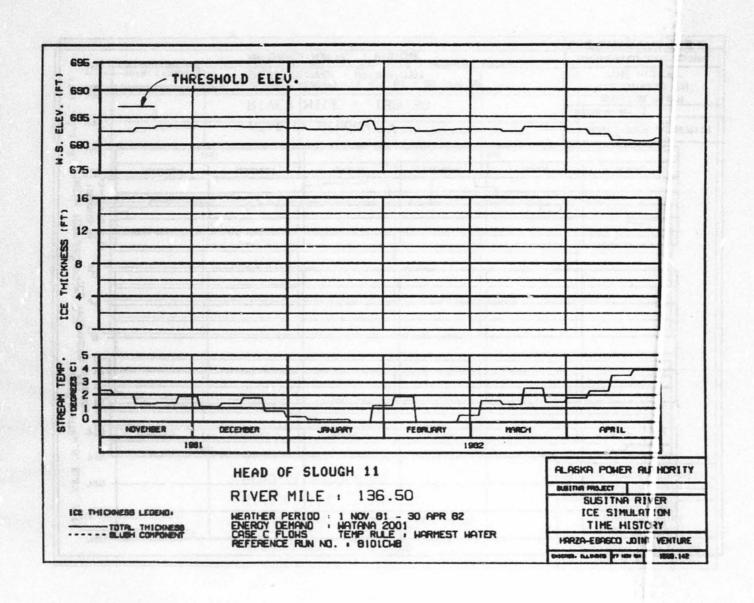


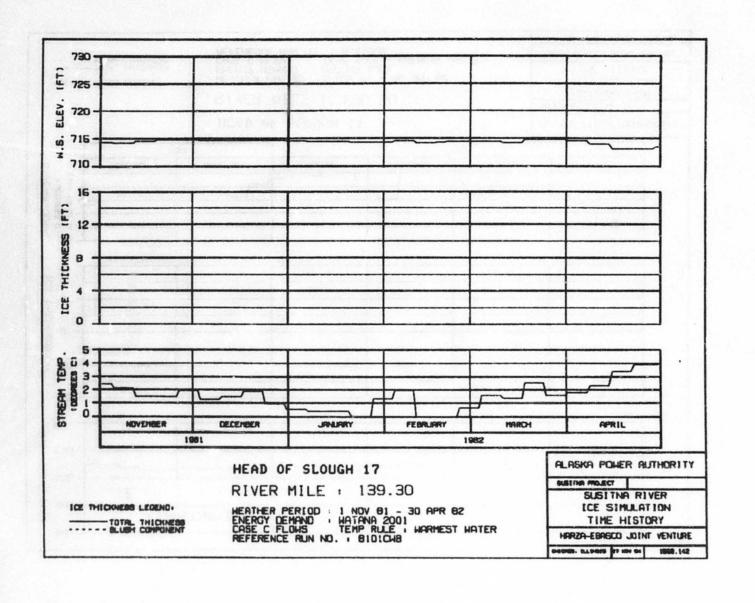


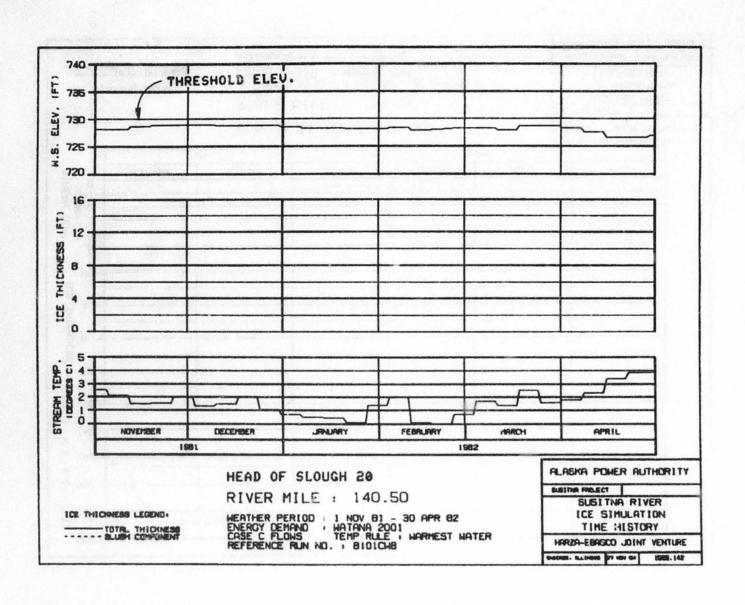


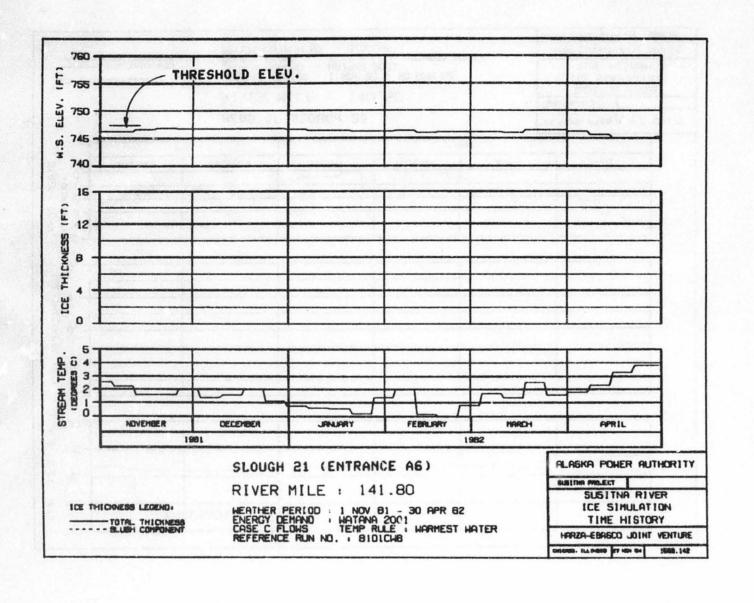


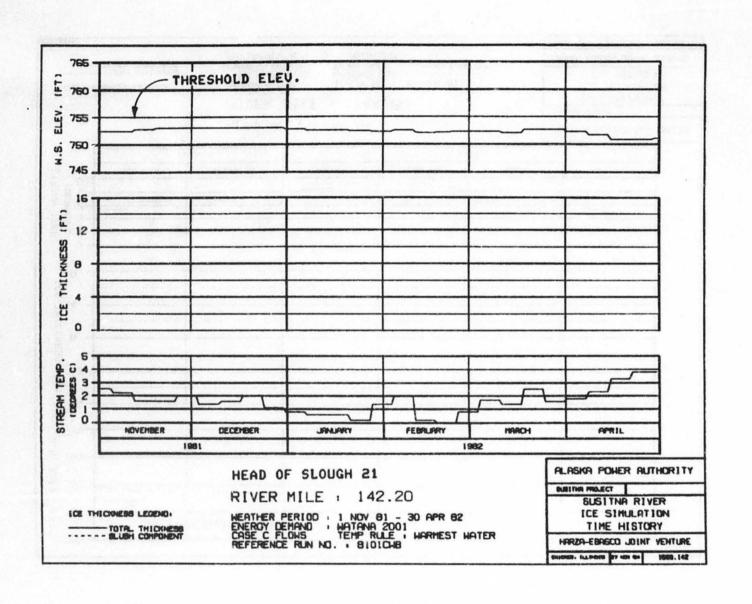


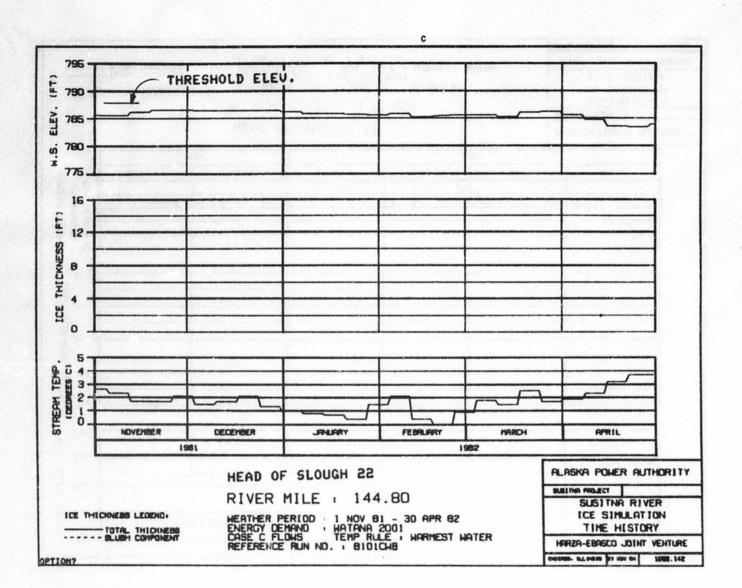






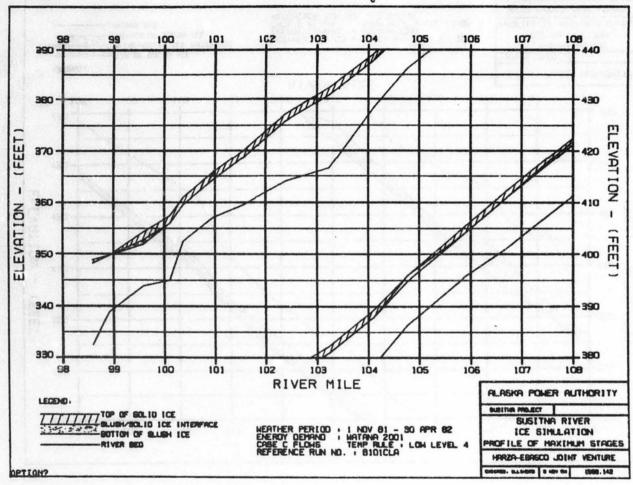




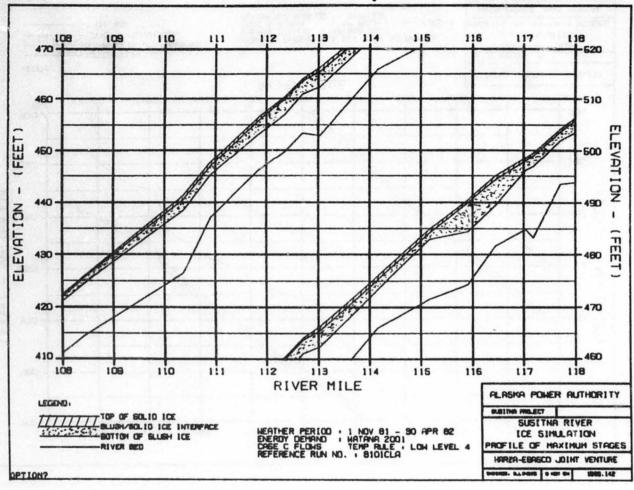


## EXHIBIT I

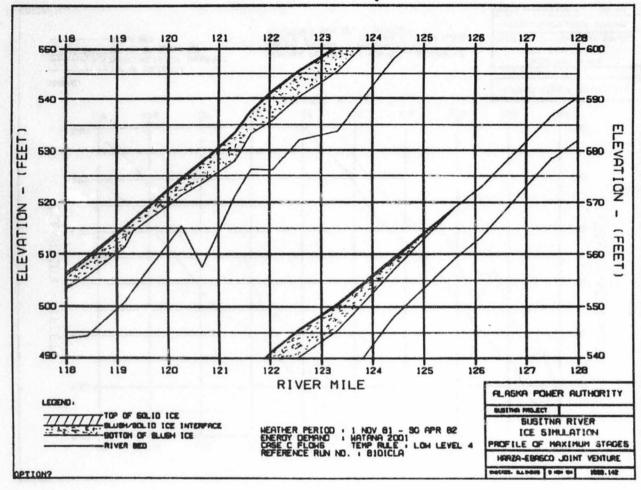


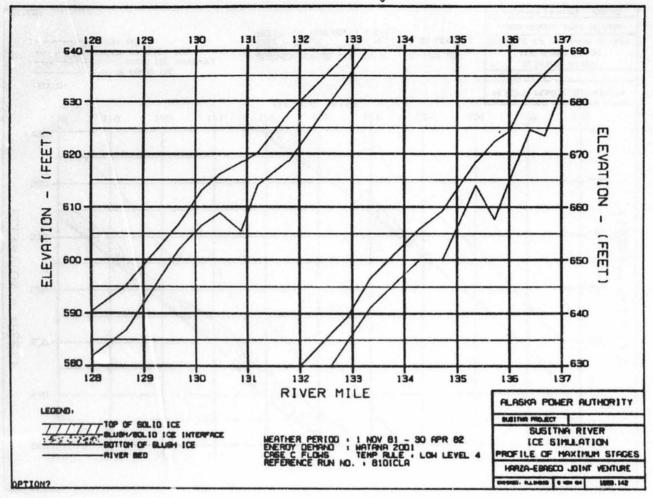


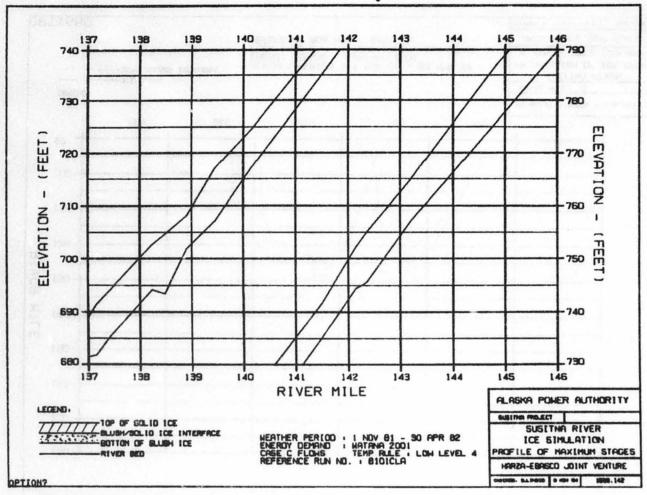


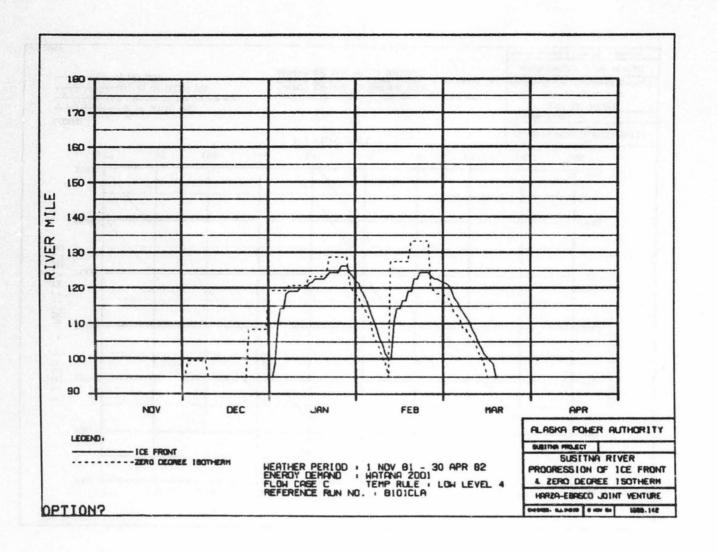


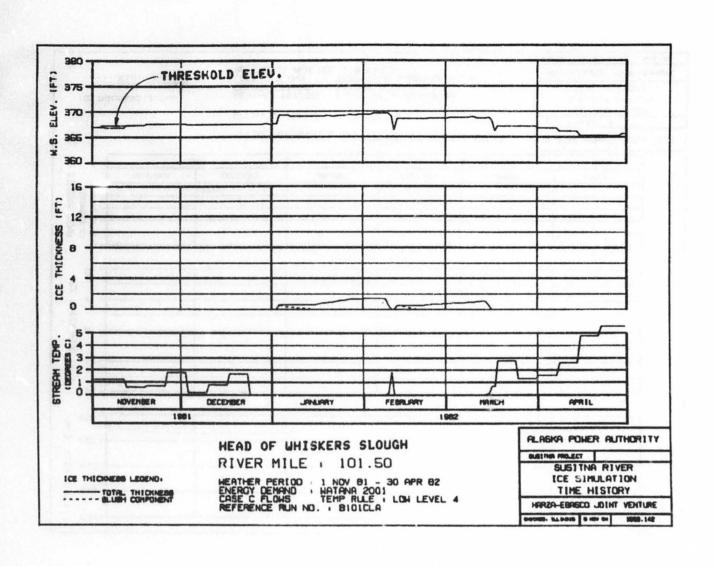


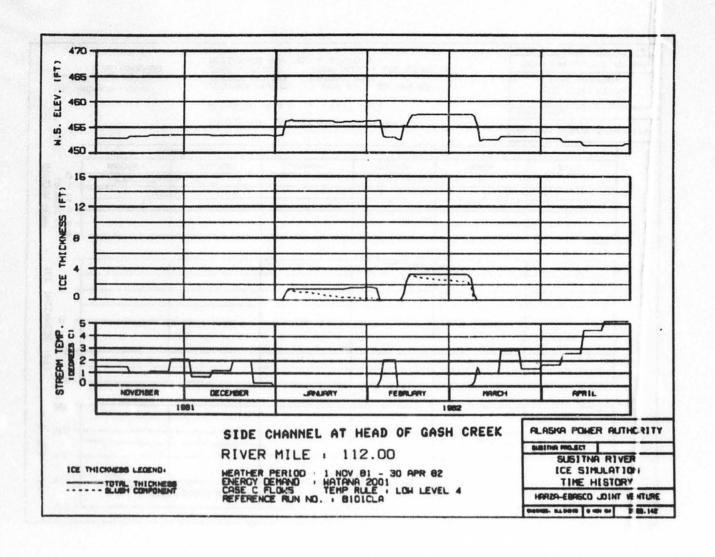


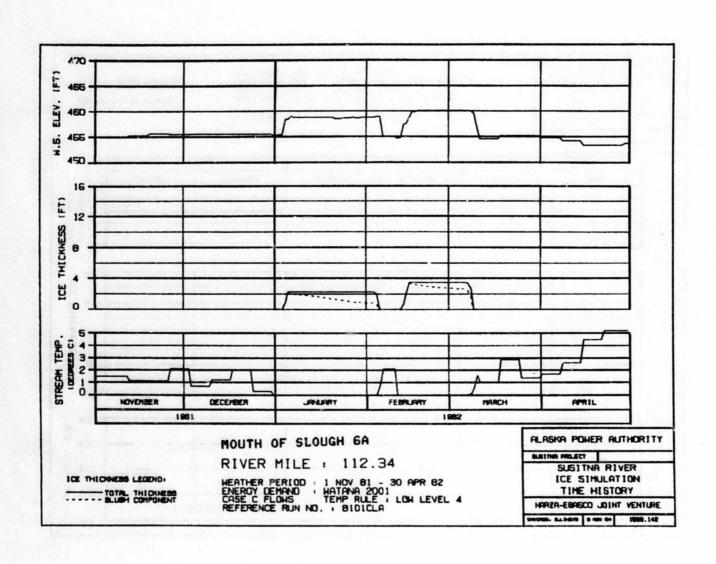


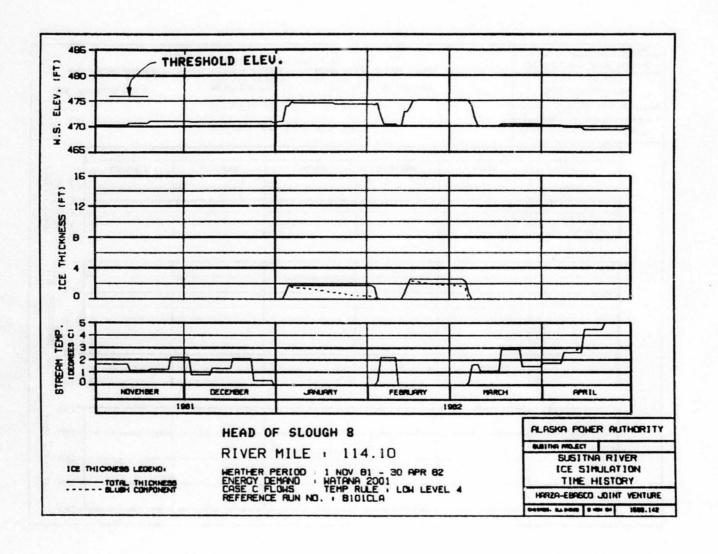


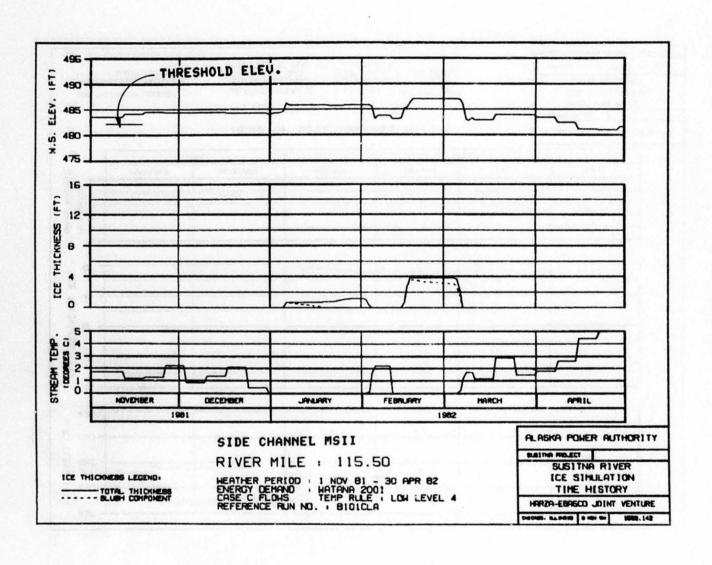


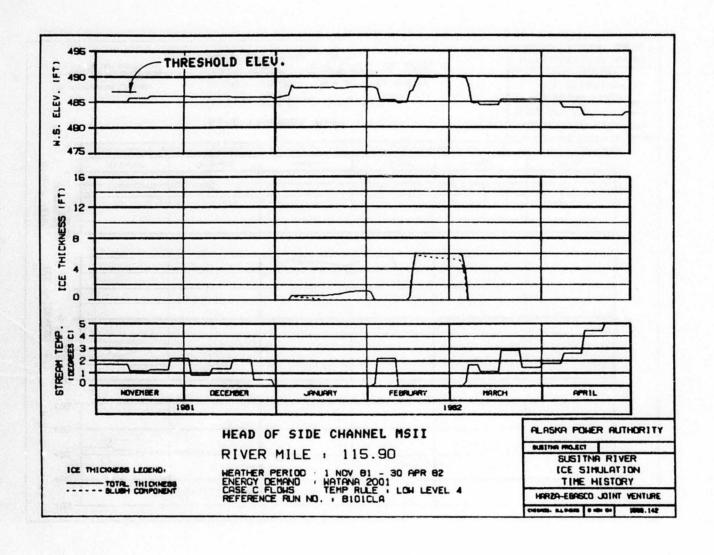




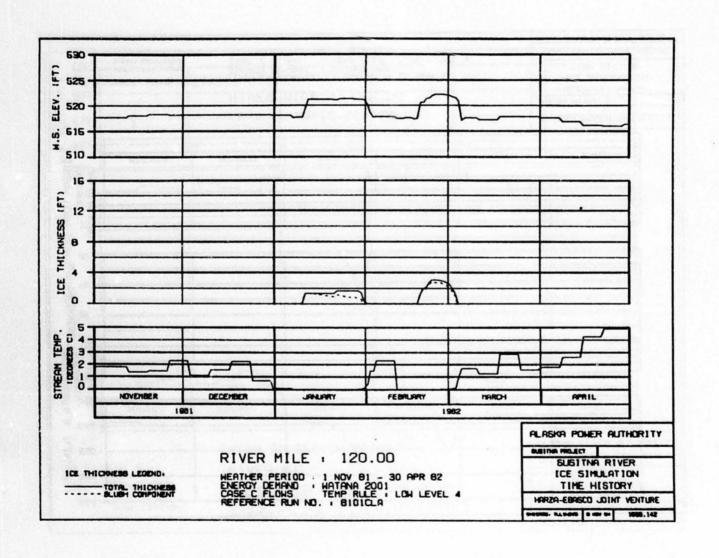


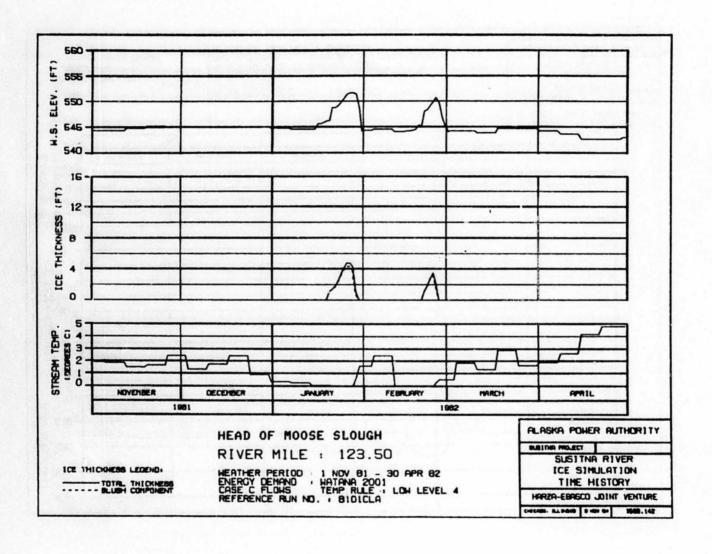


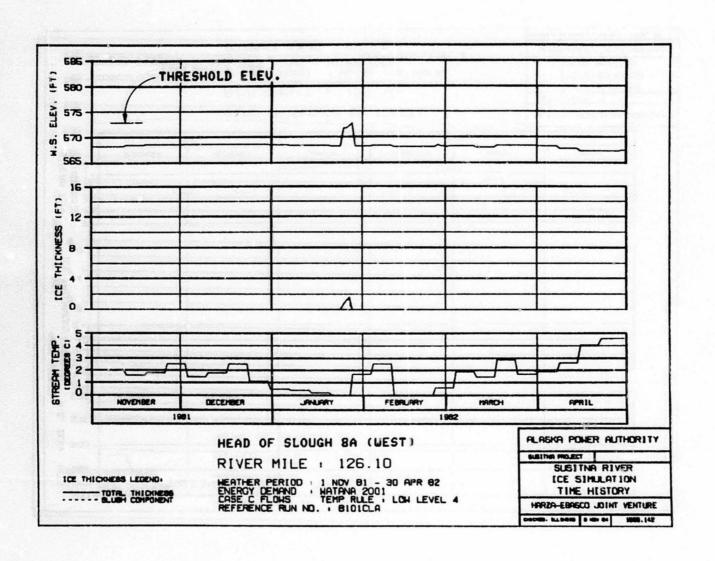


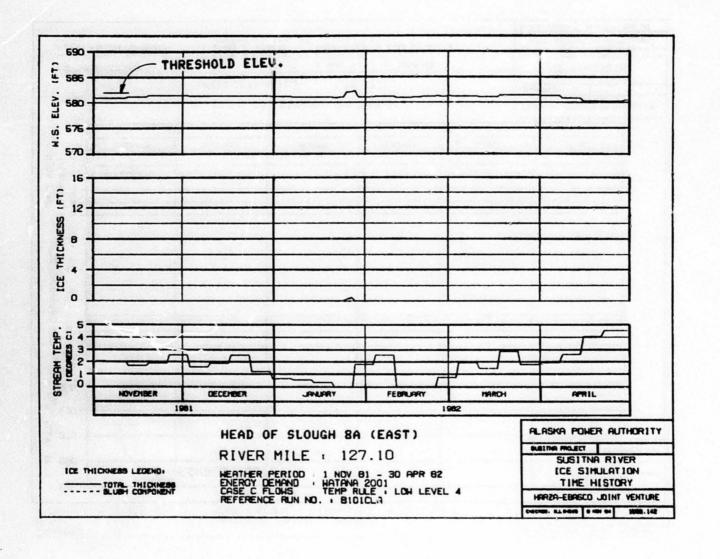


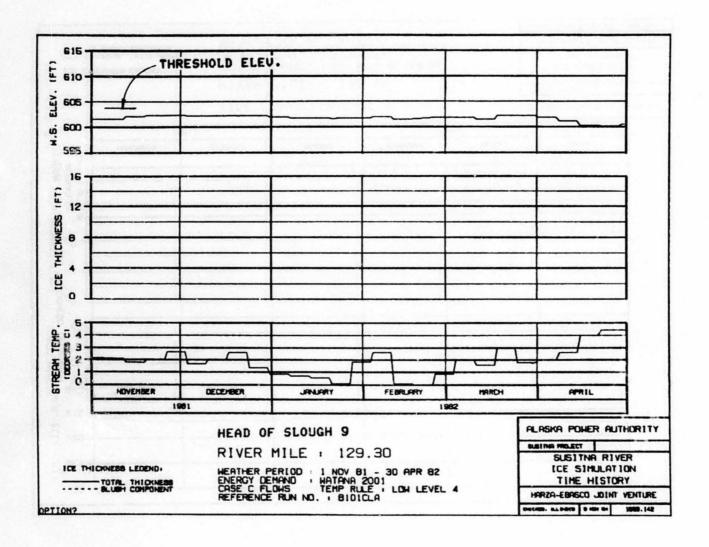
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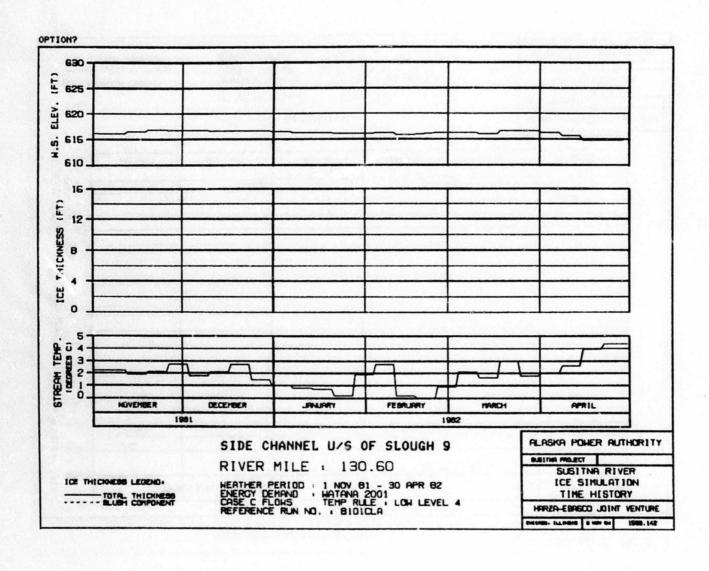


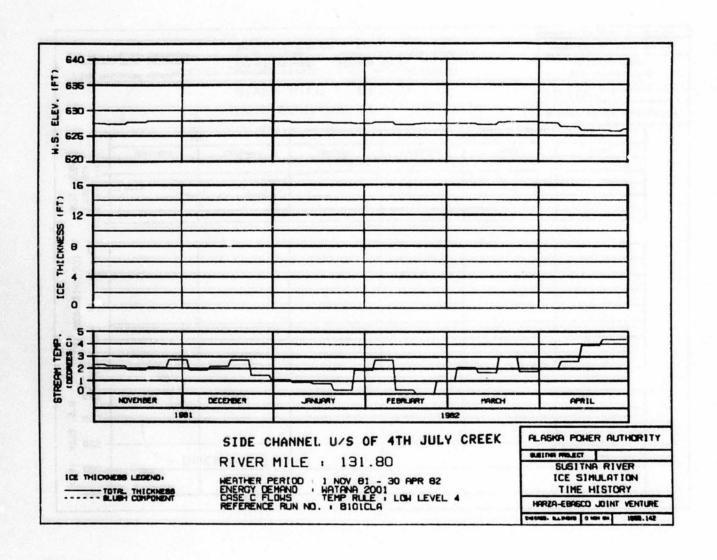


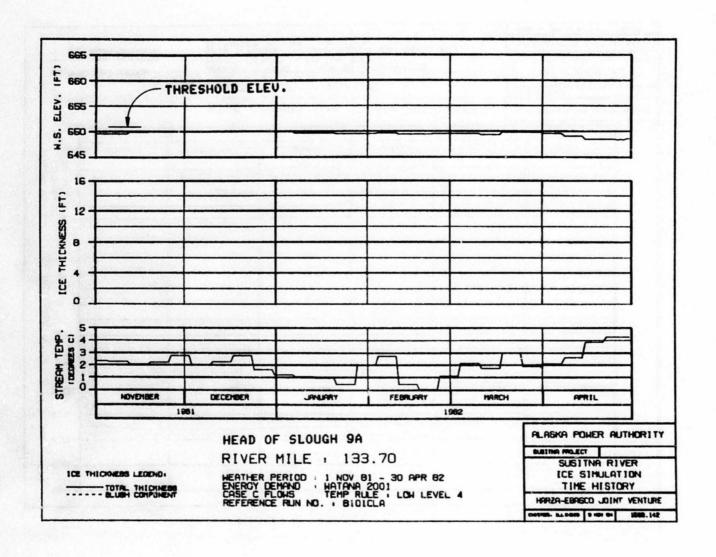


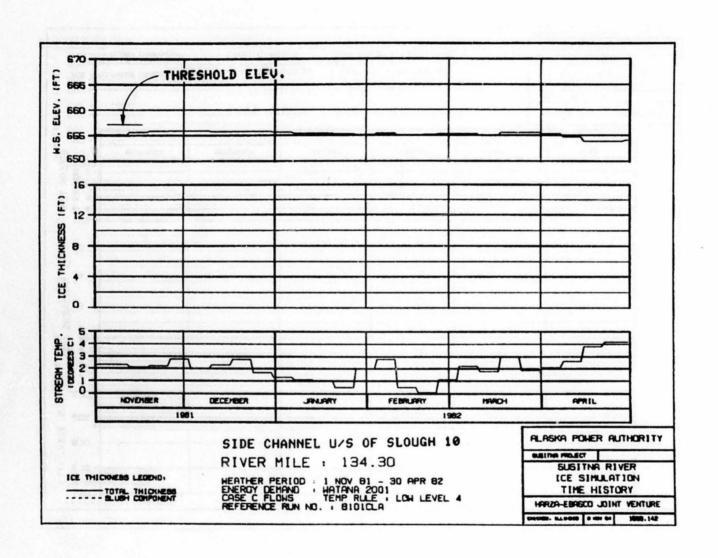


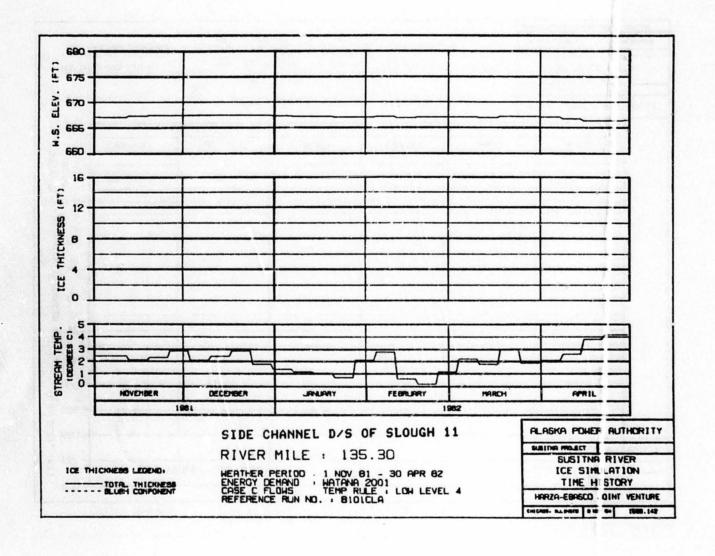


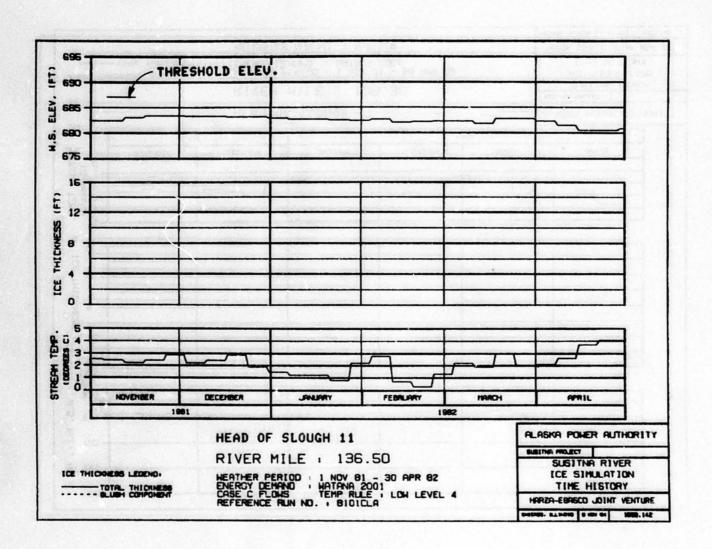


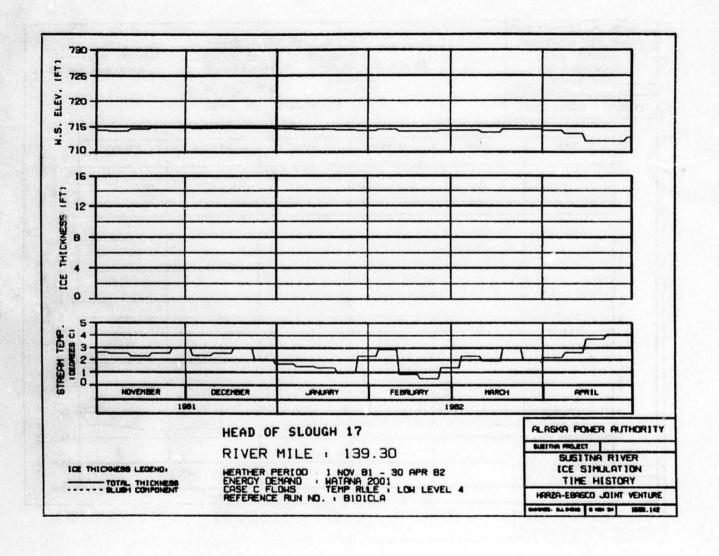




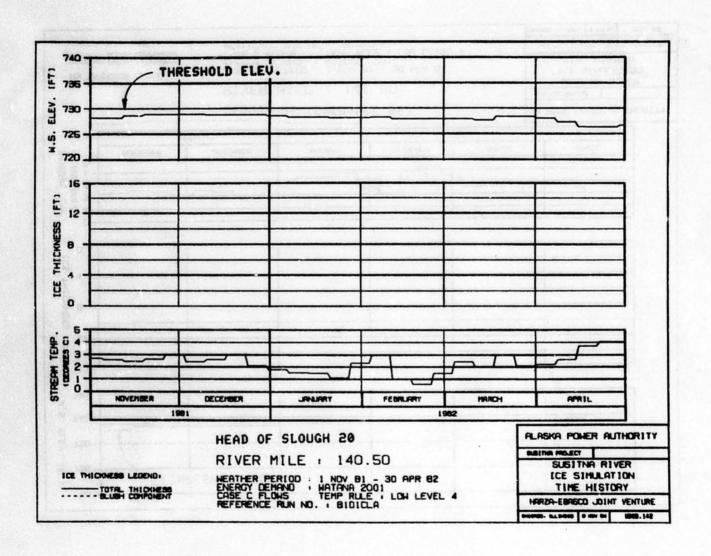


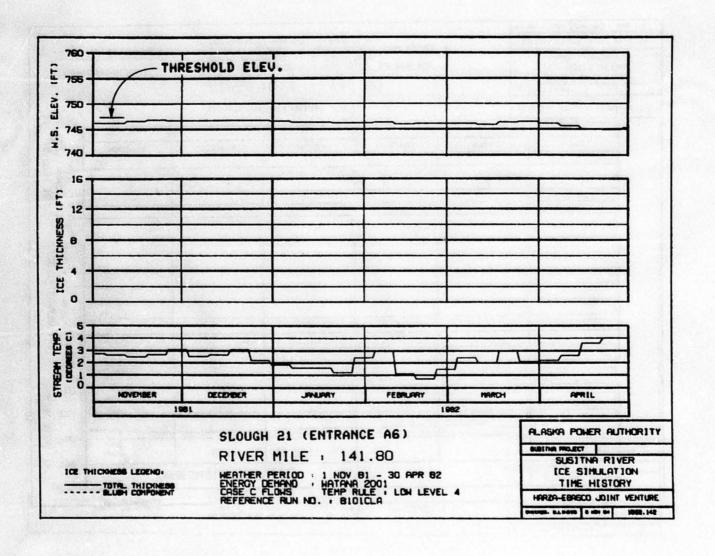


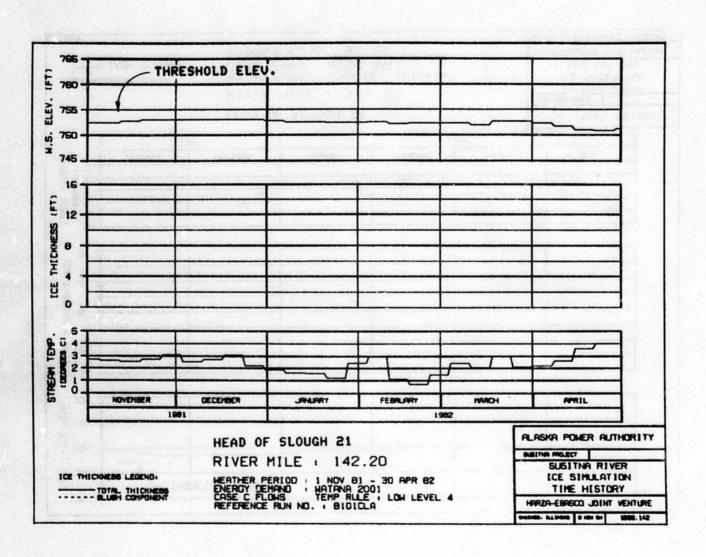




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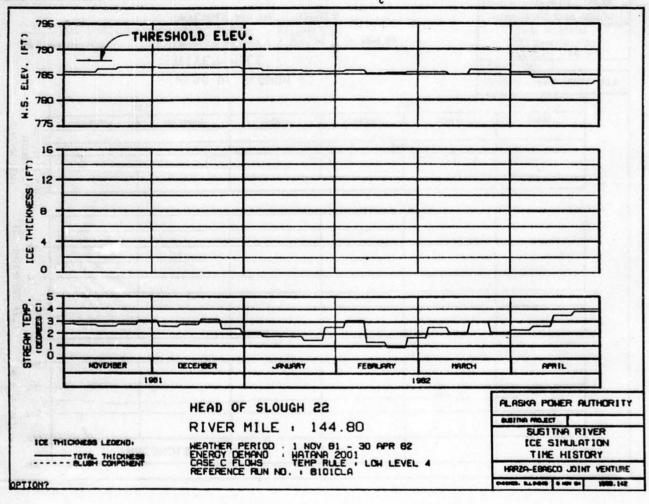
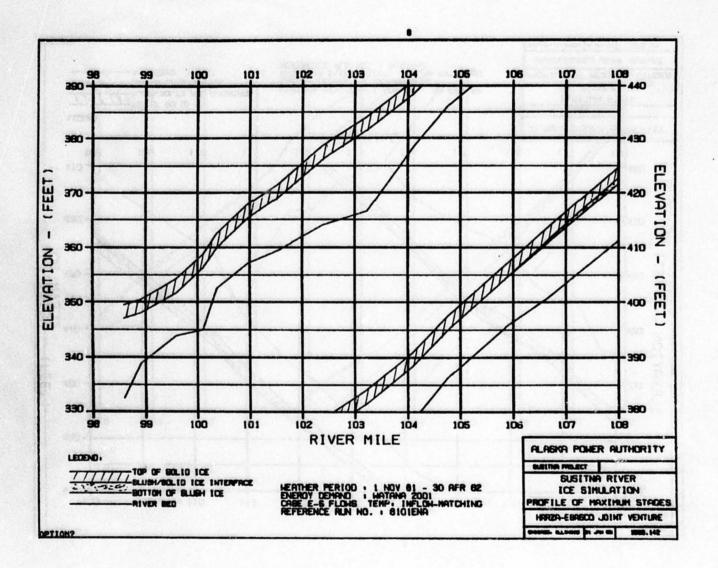
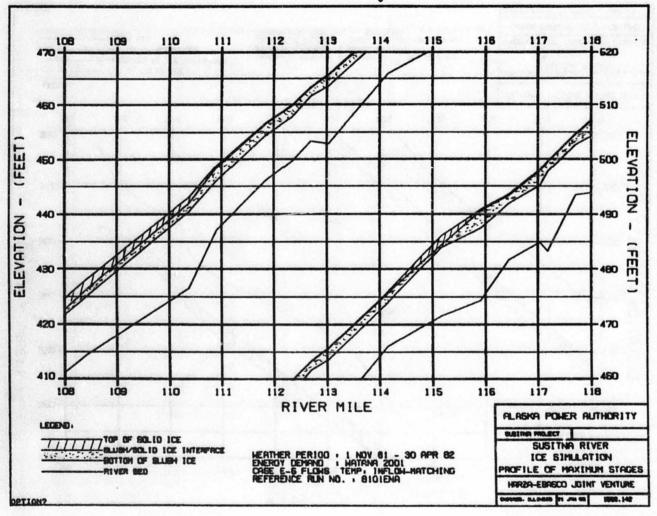
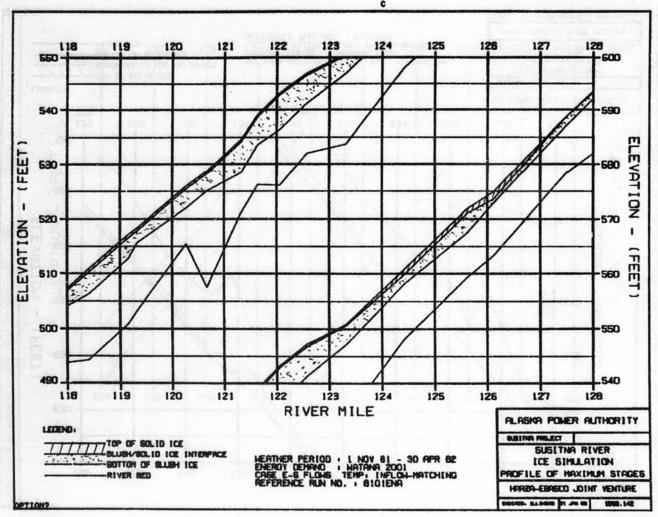


EXHIBIT J

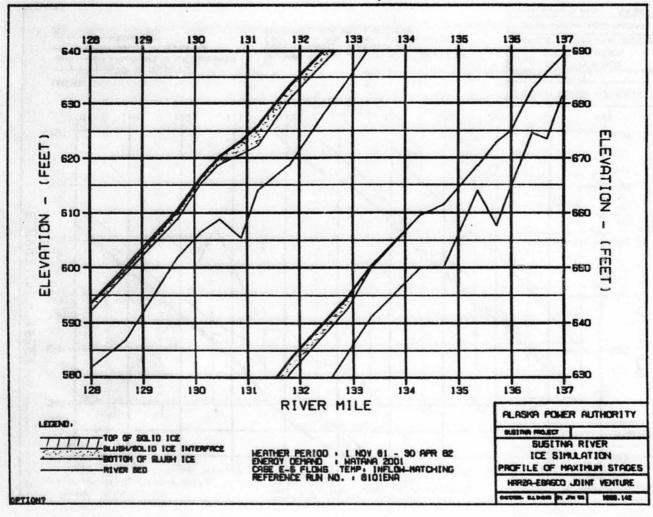




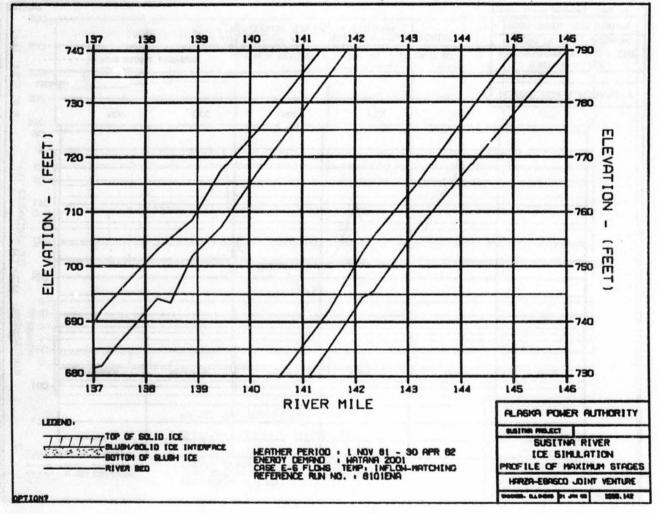


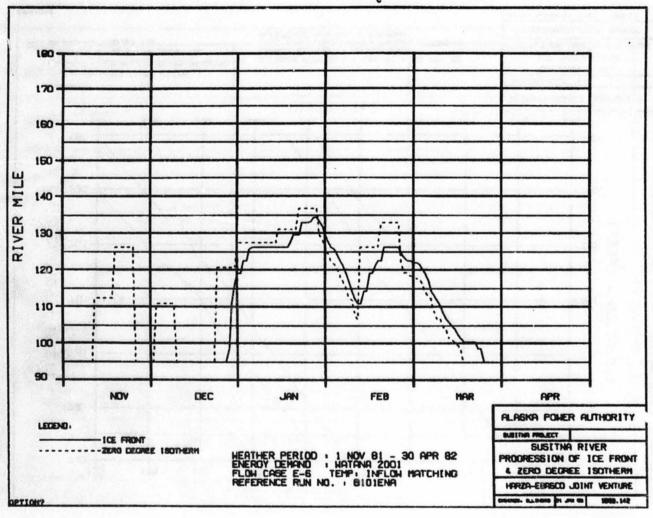


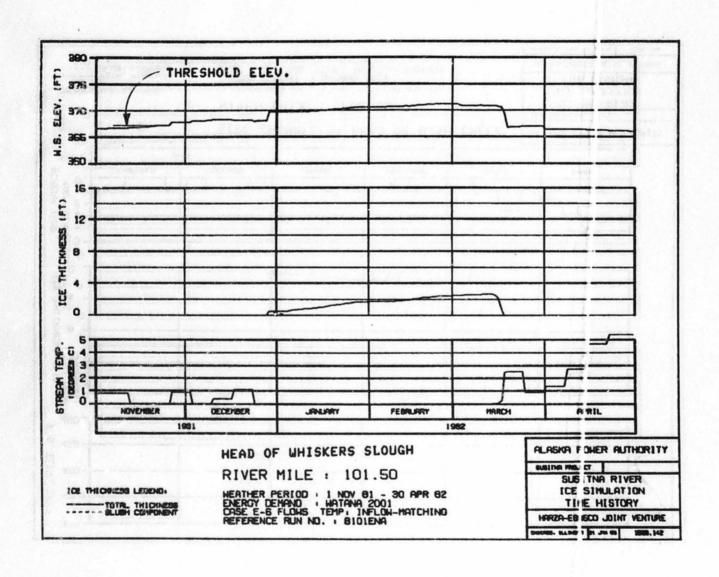


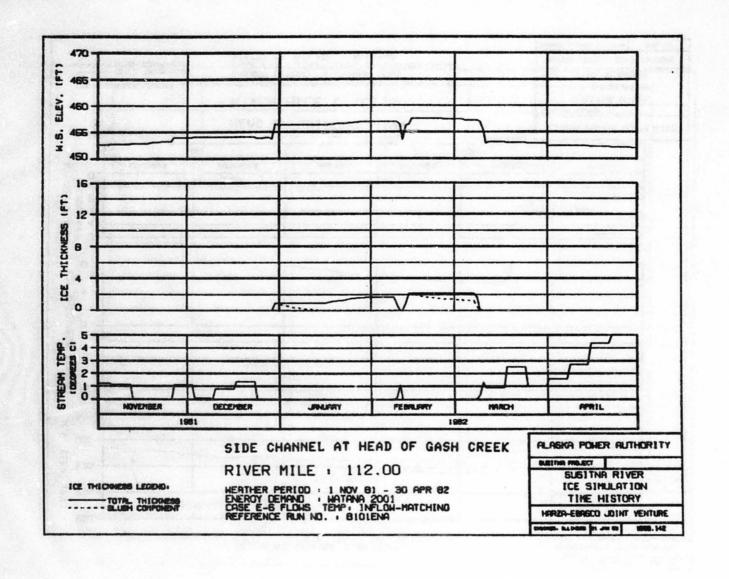


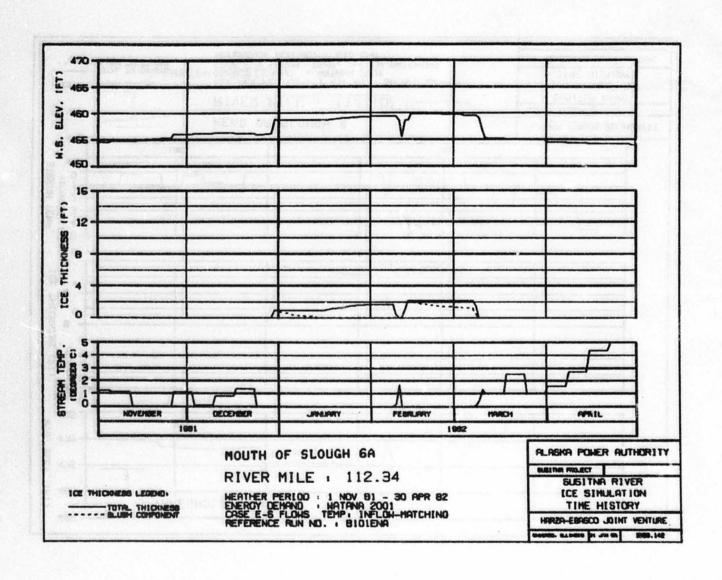


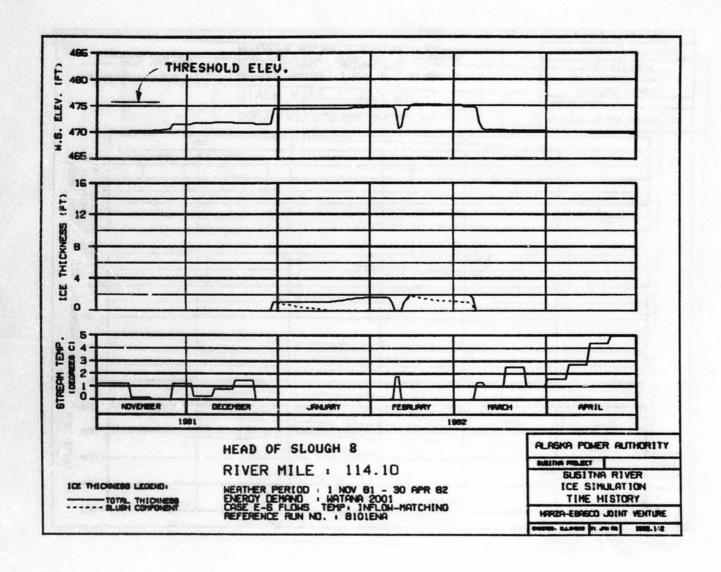




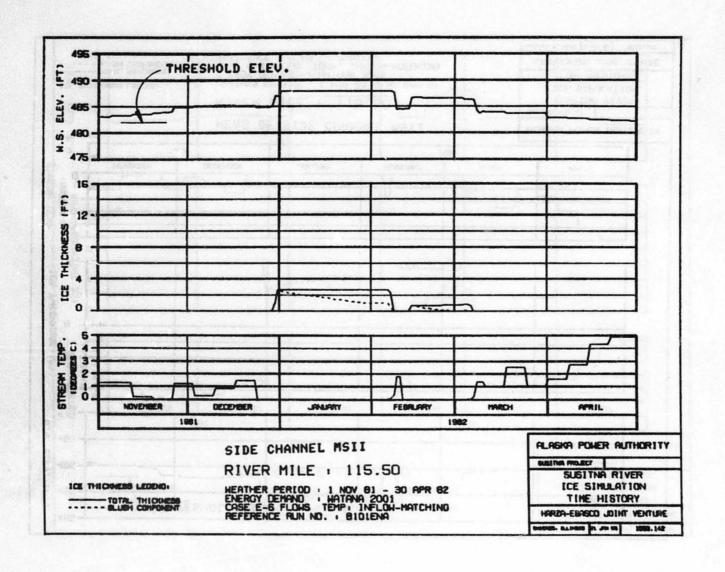


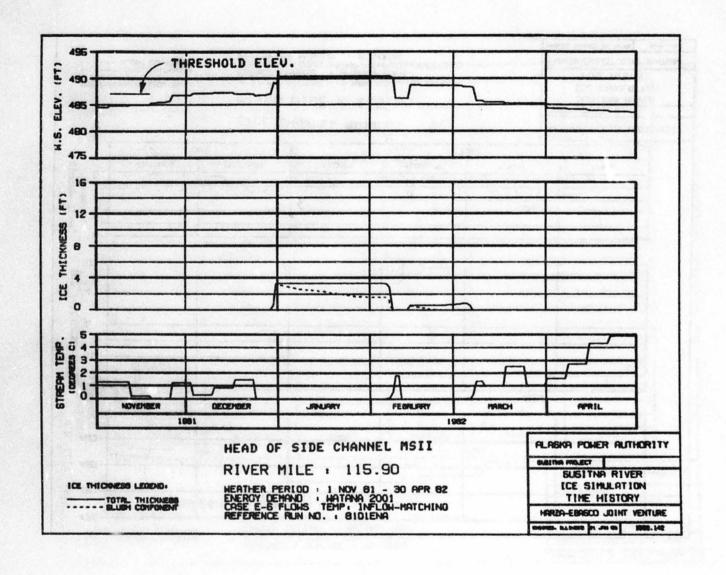




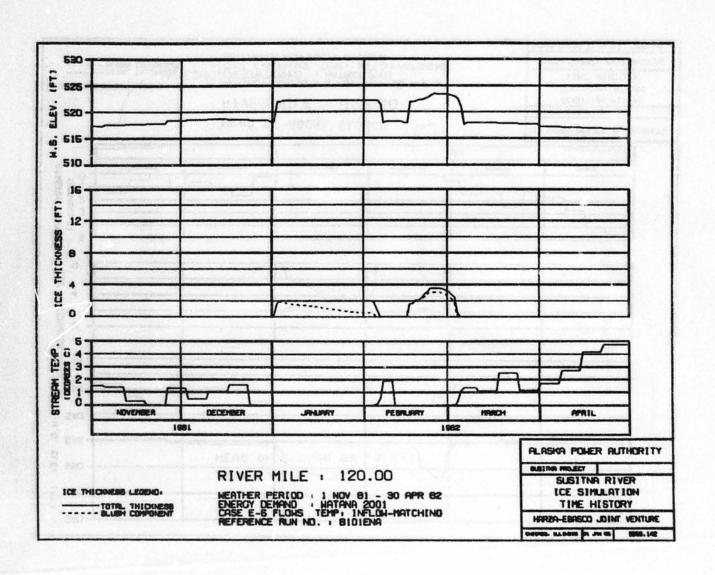


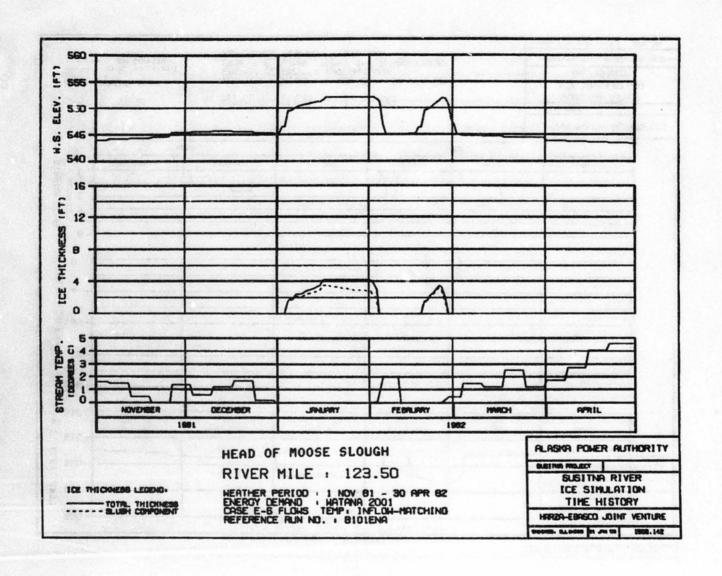
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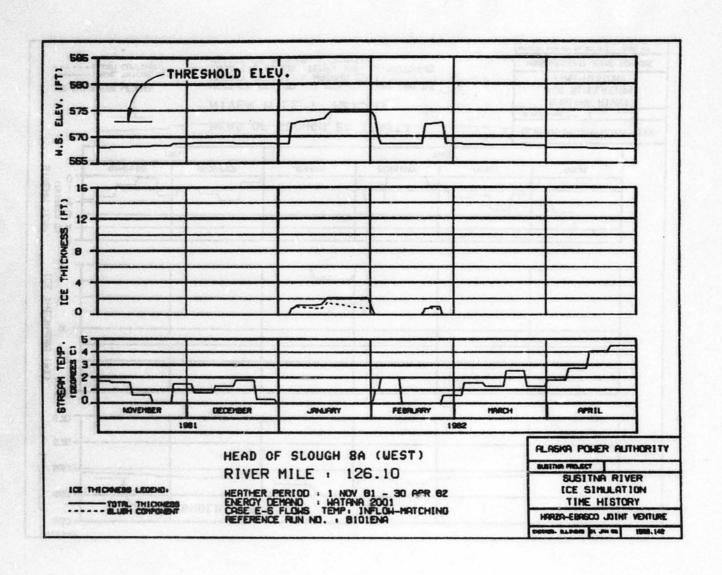
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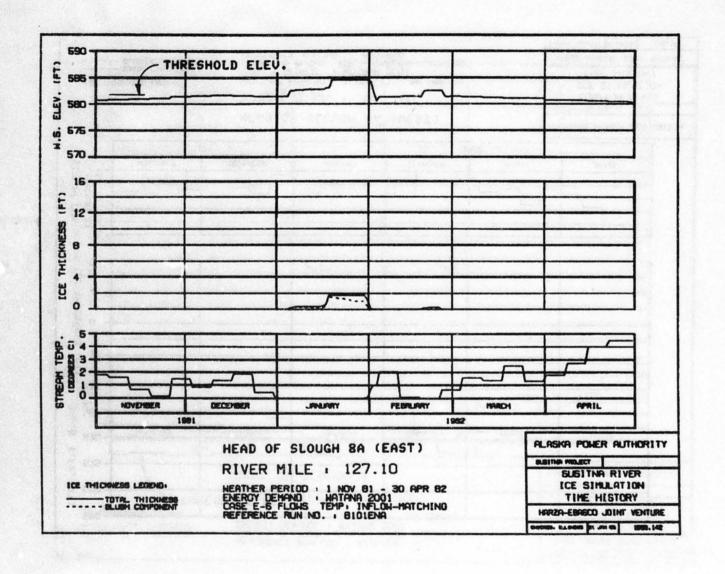


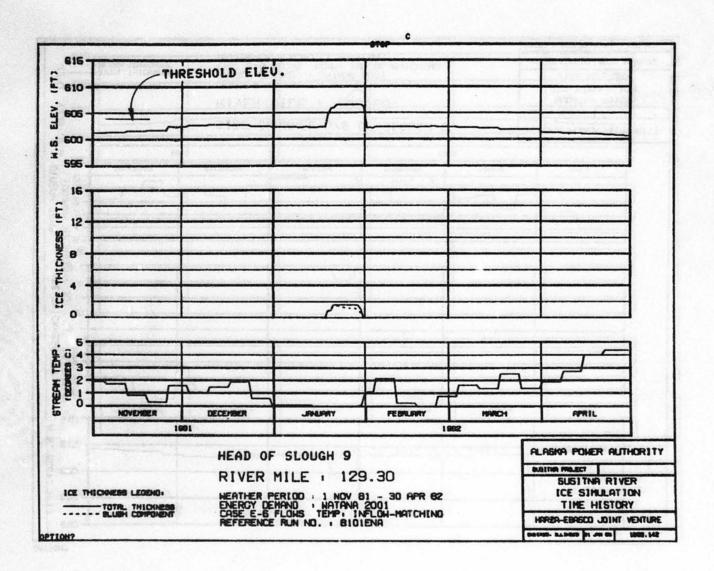


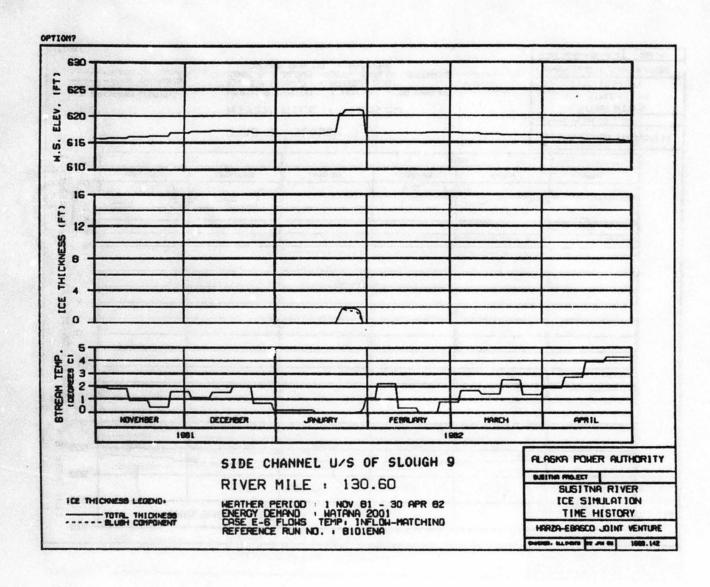
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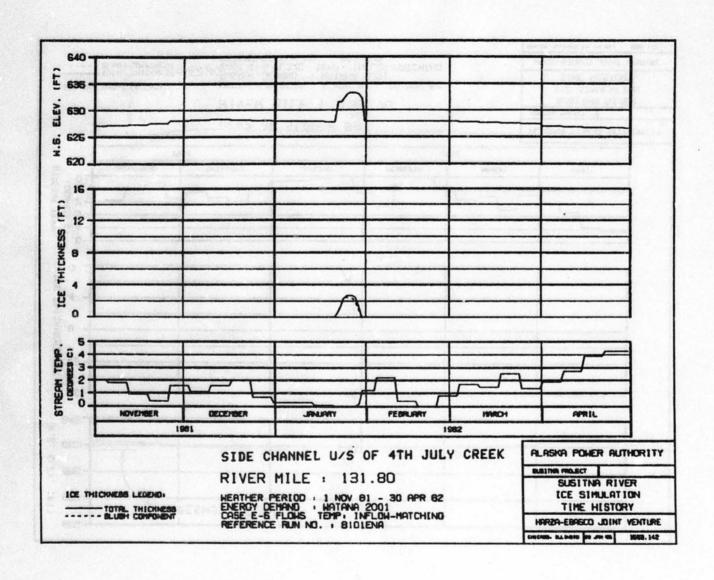
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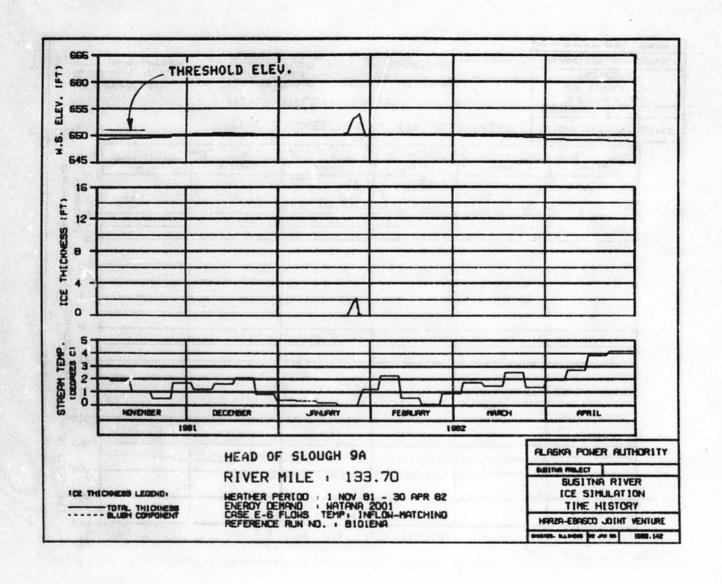


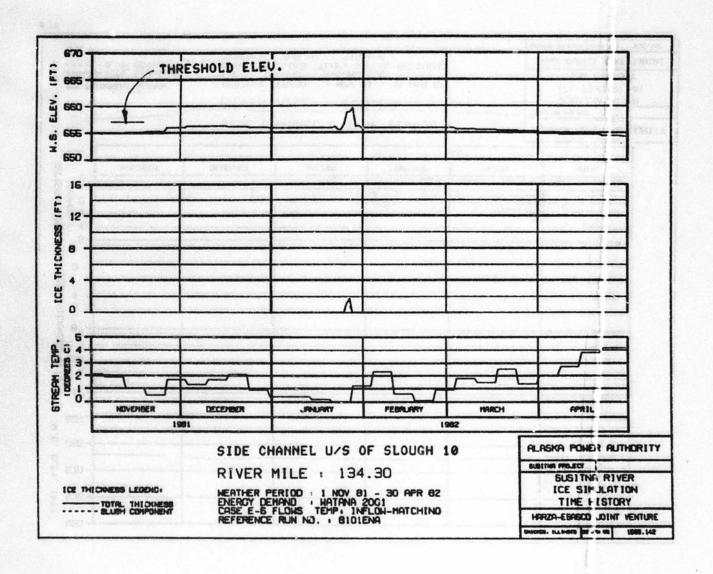


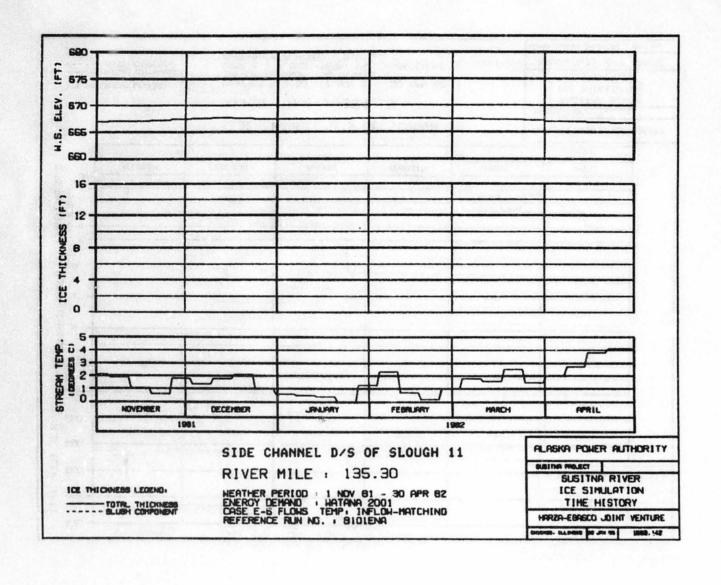




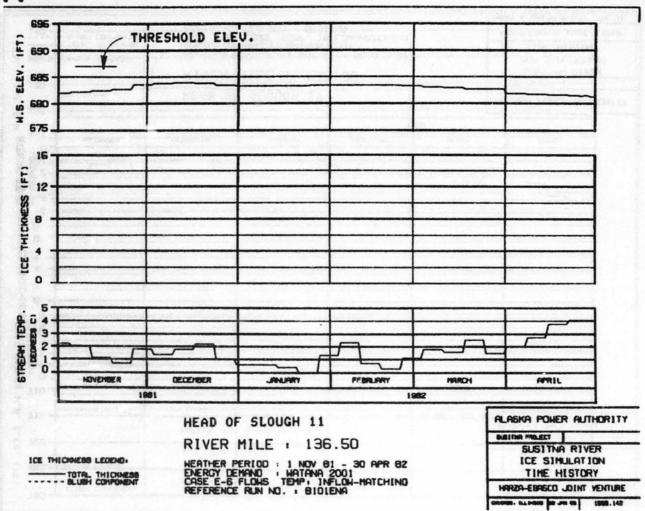


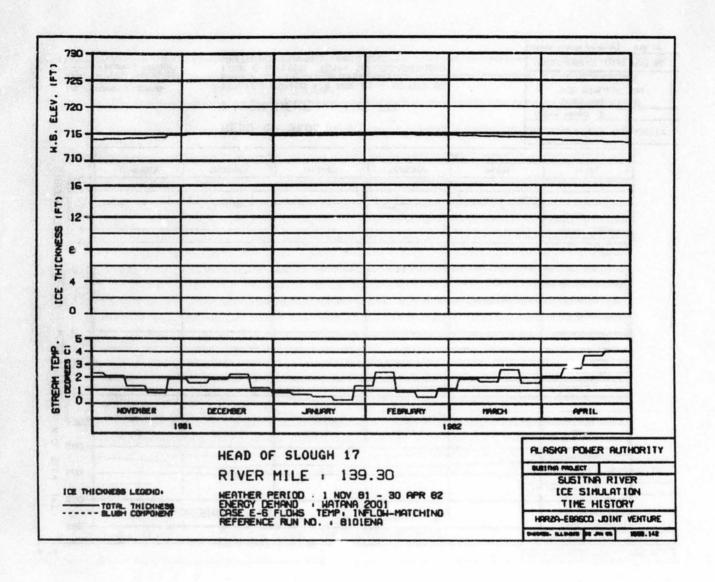




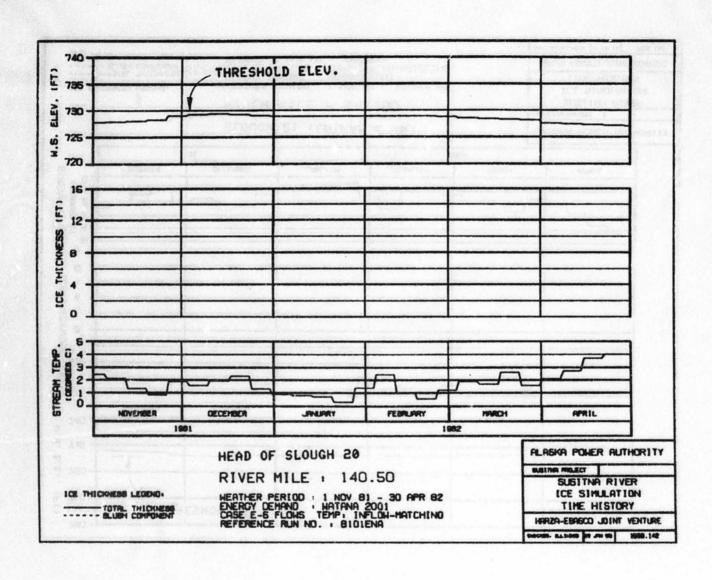


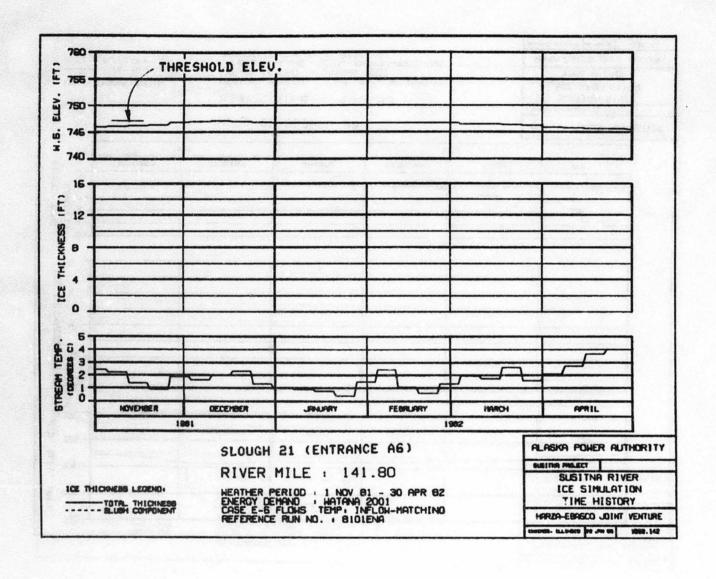
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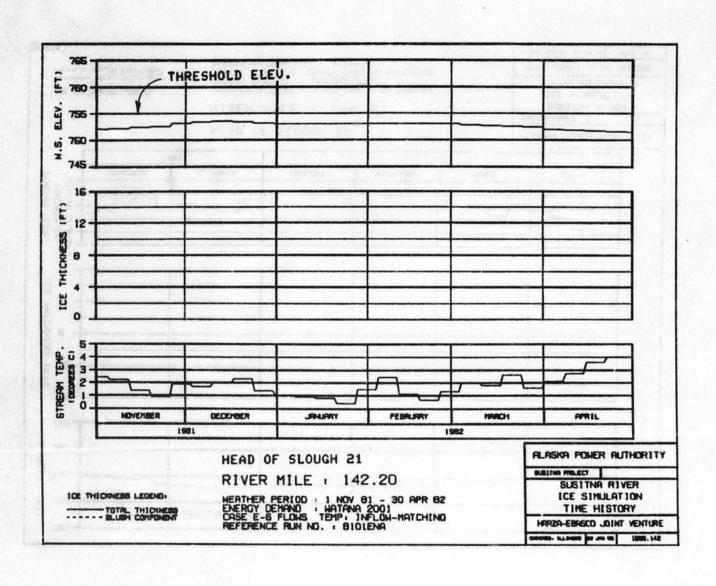




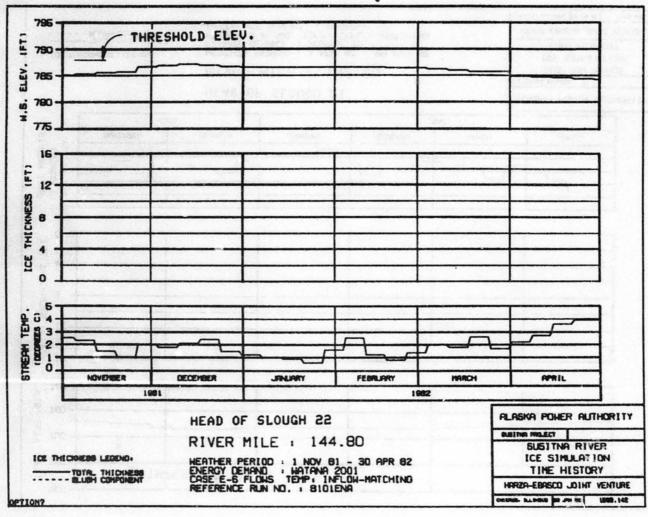
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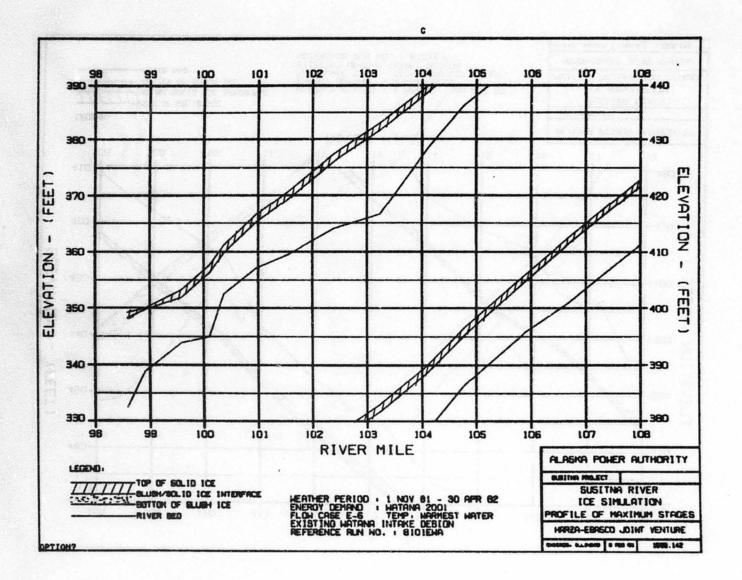




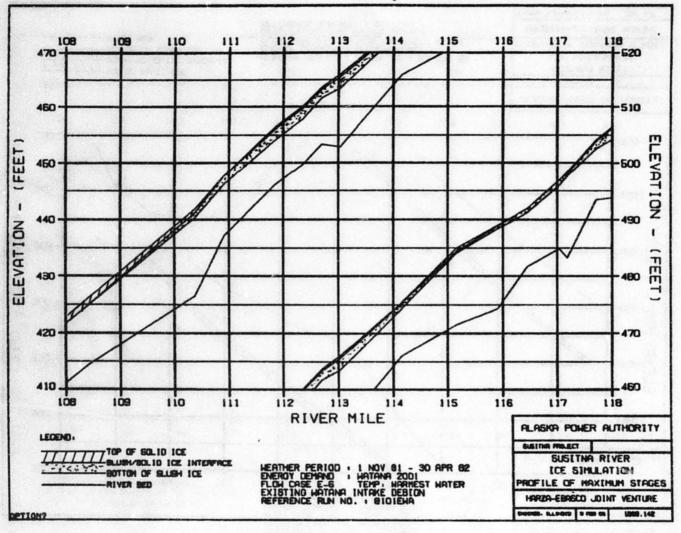


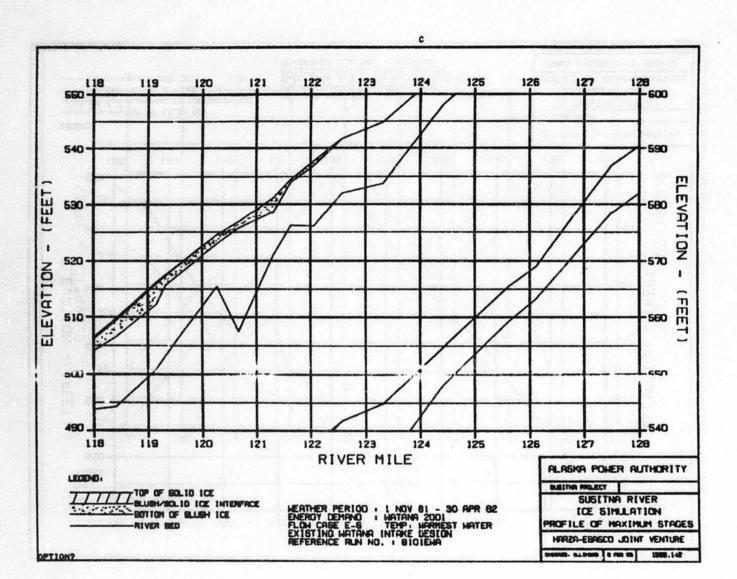


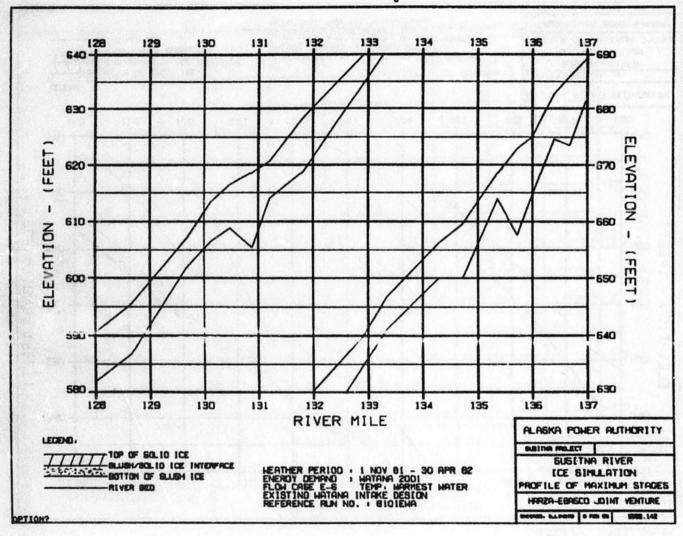
## EXHIBIT K



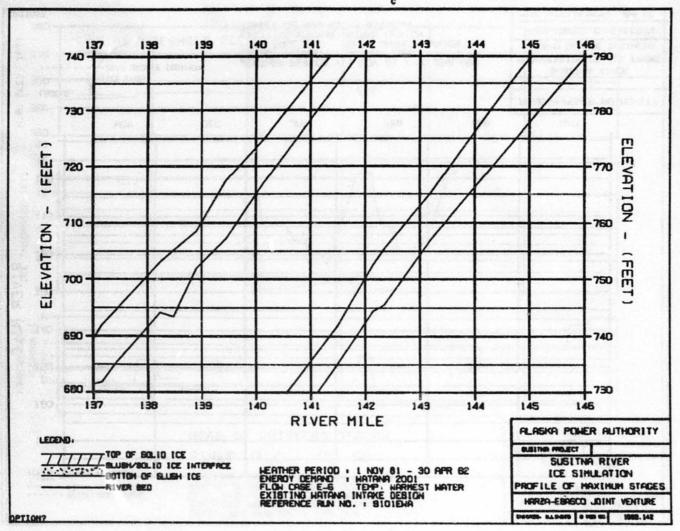




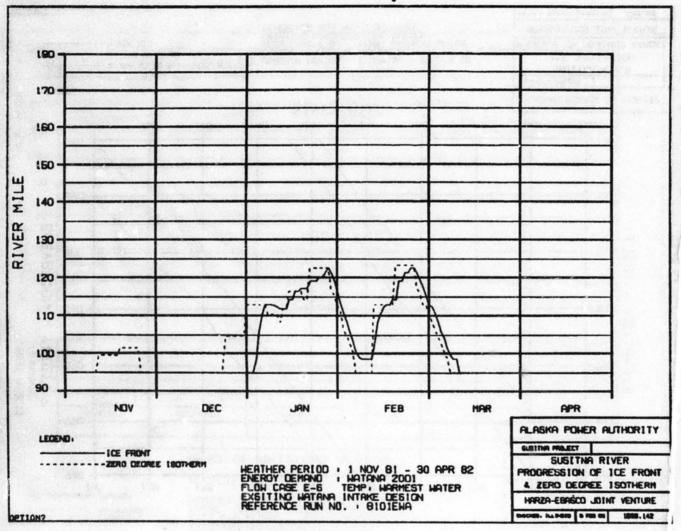


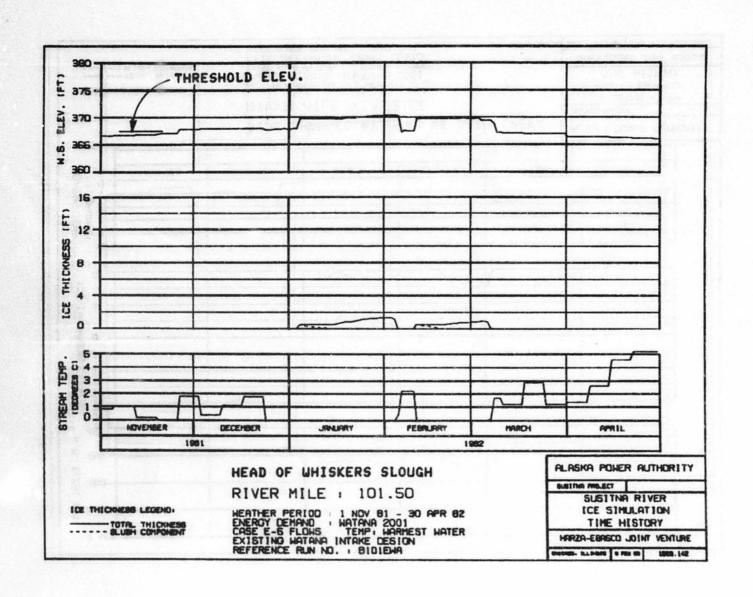


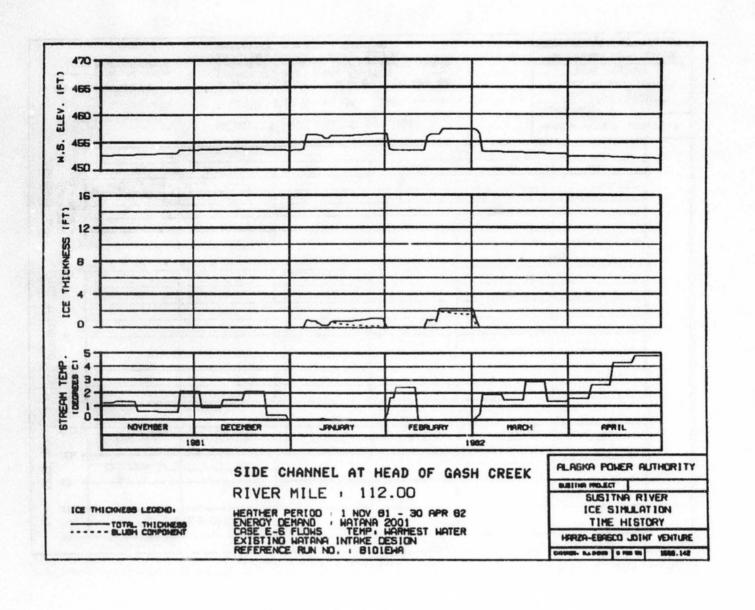


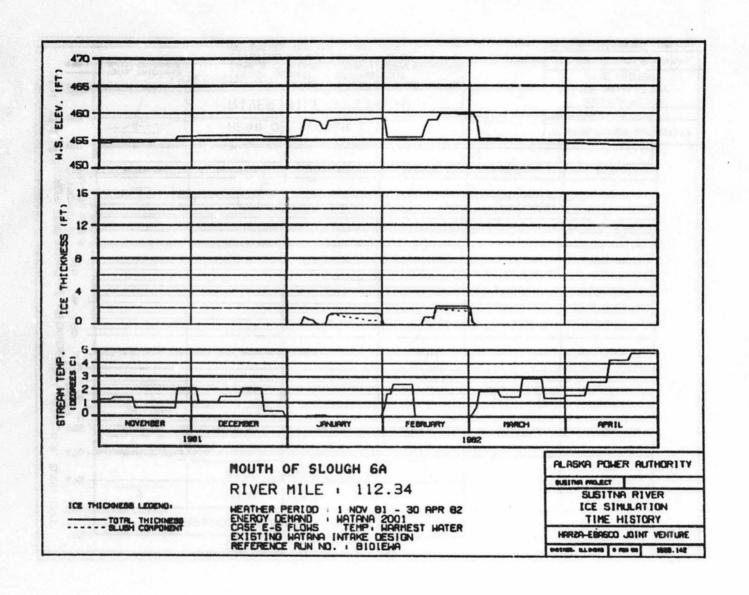


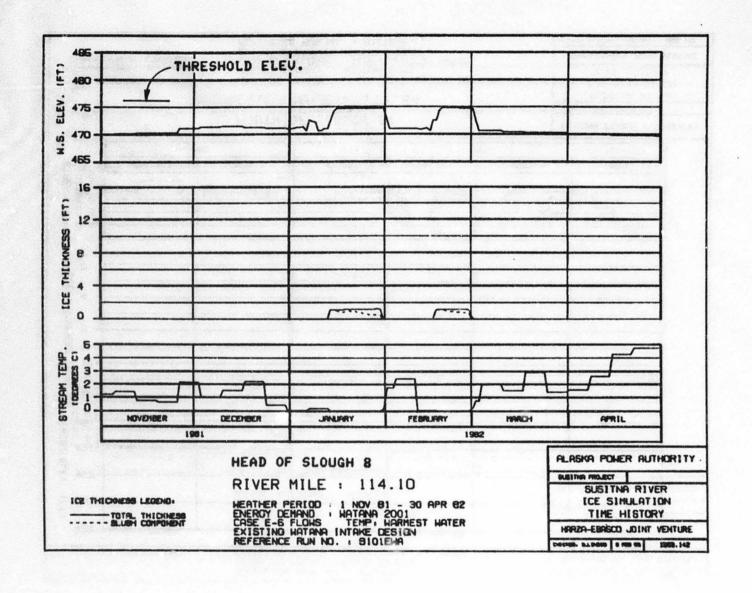


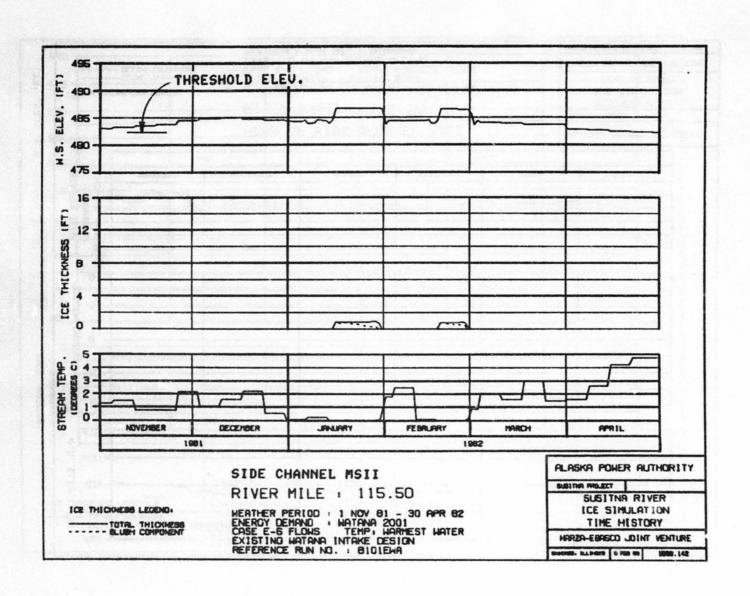


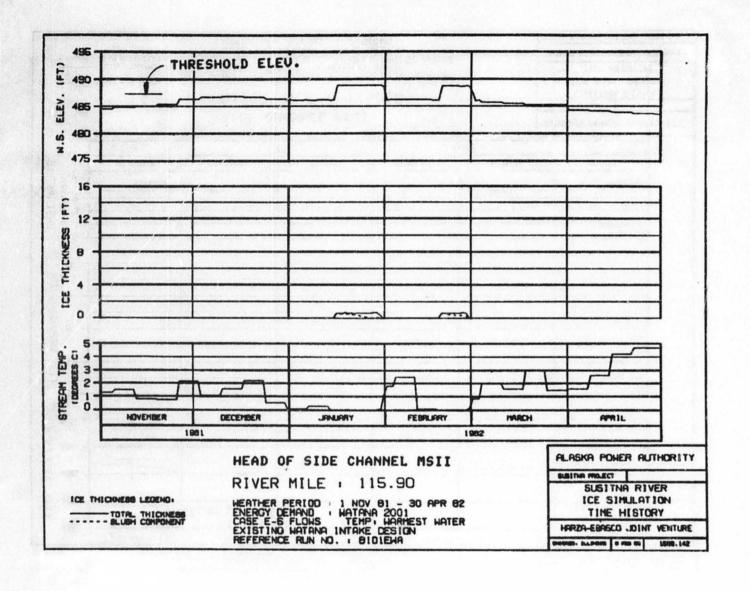


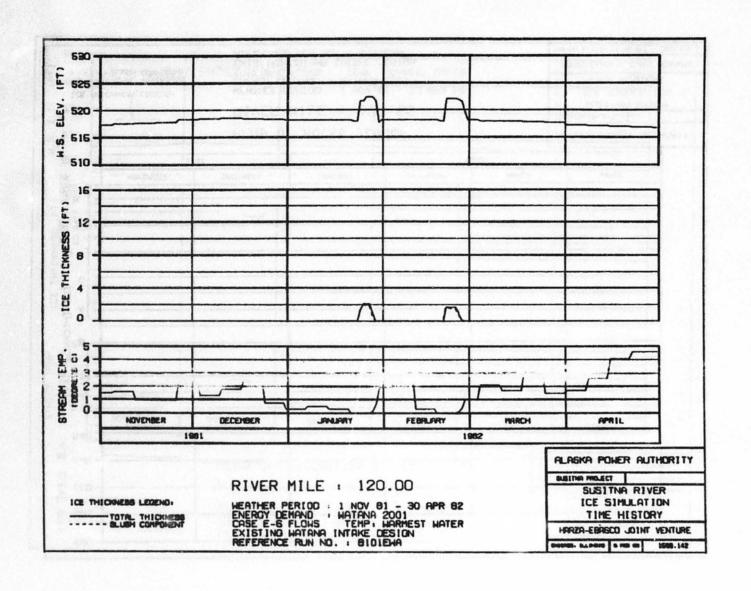


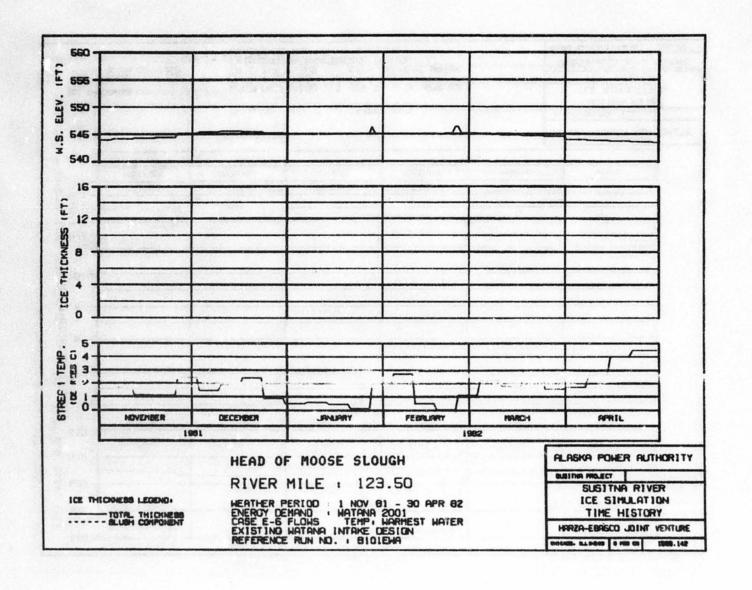


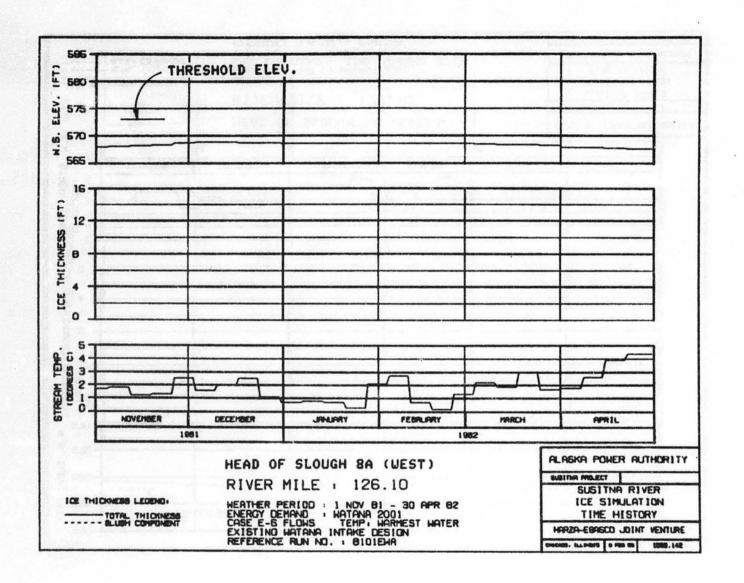


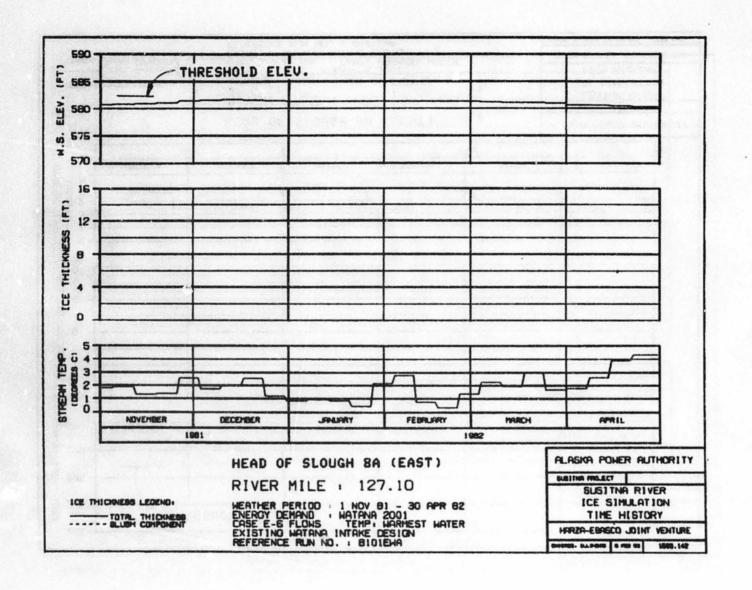


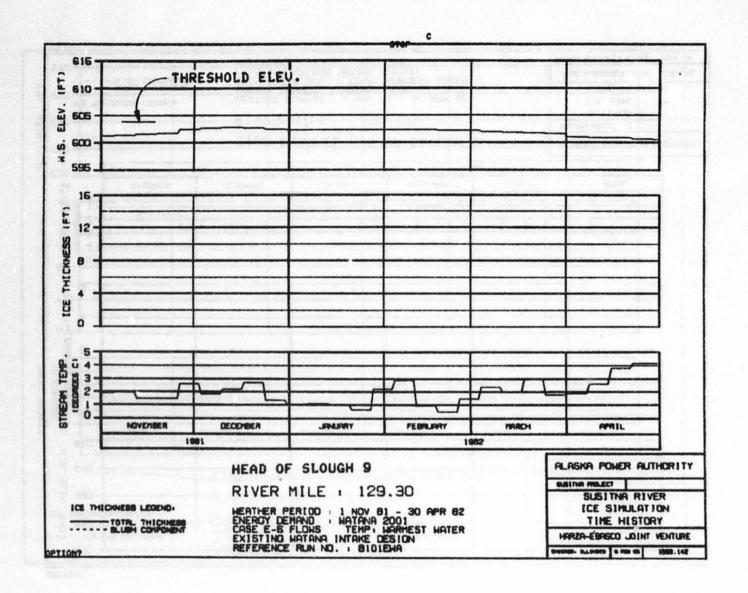


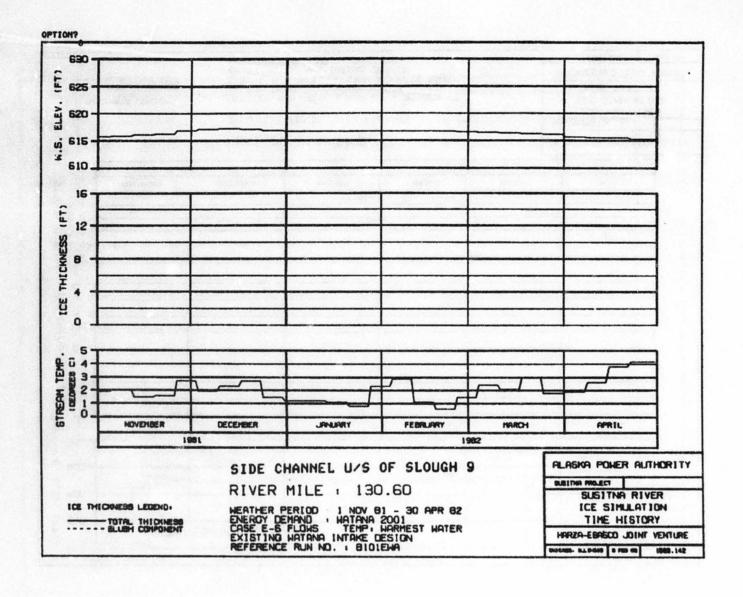


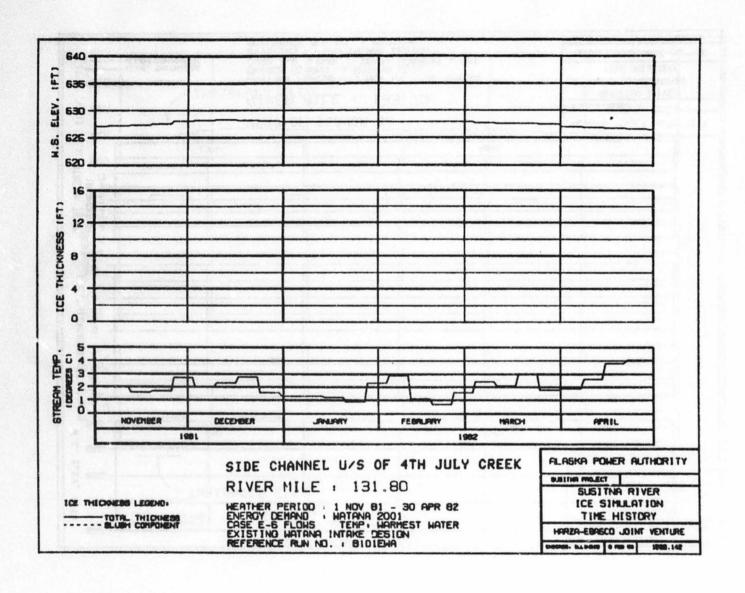


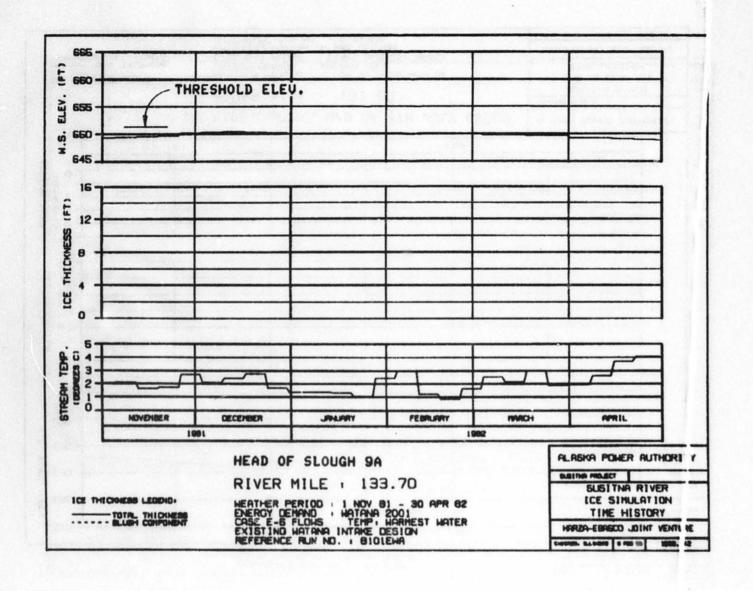


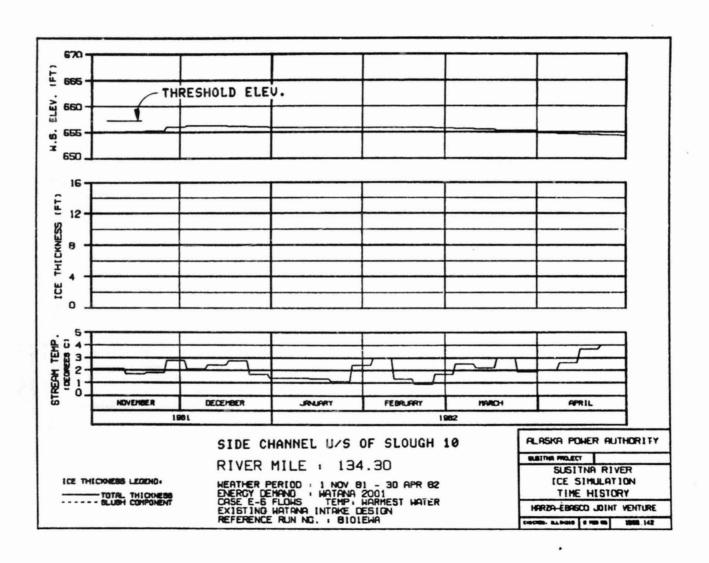


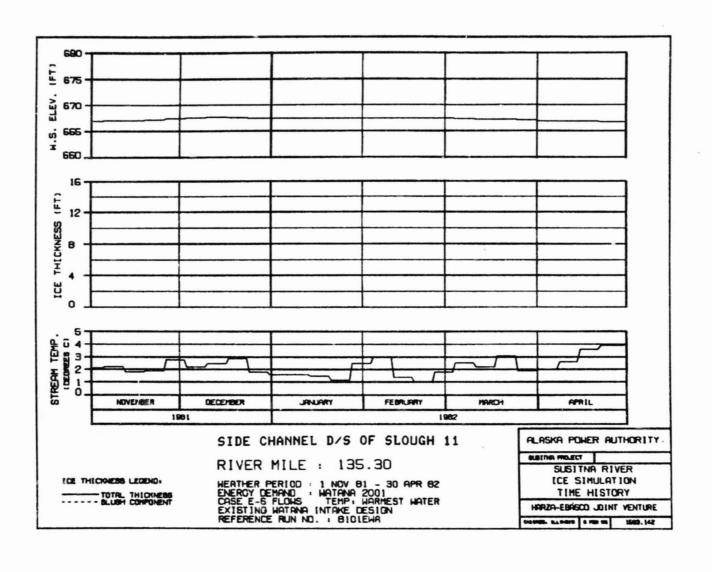


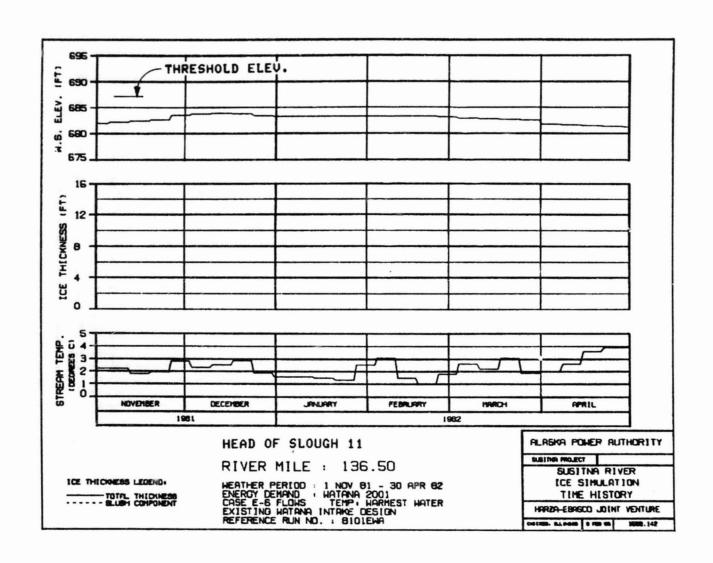


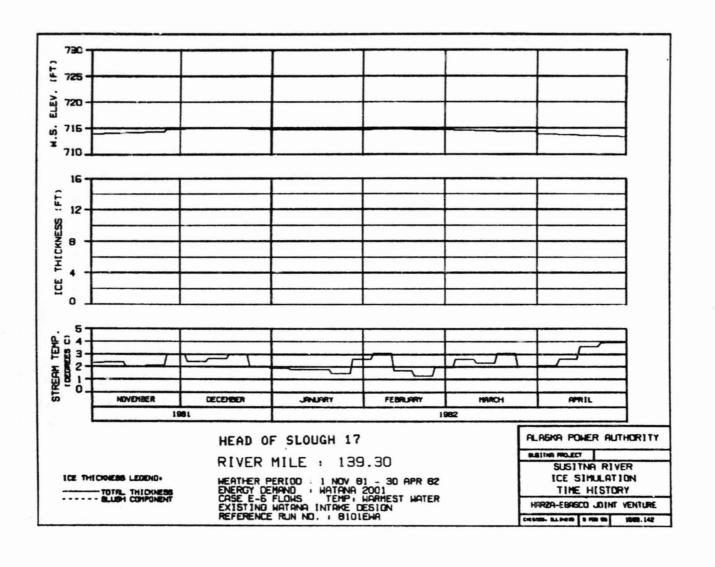


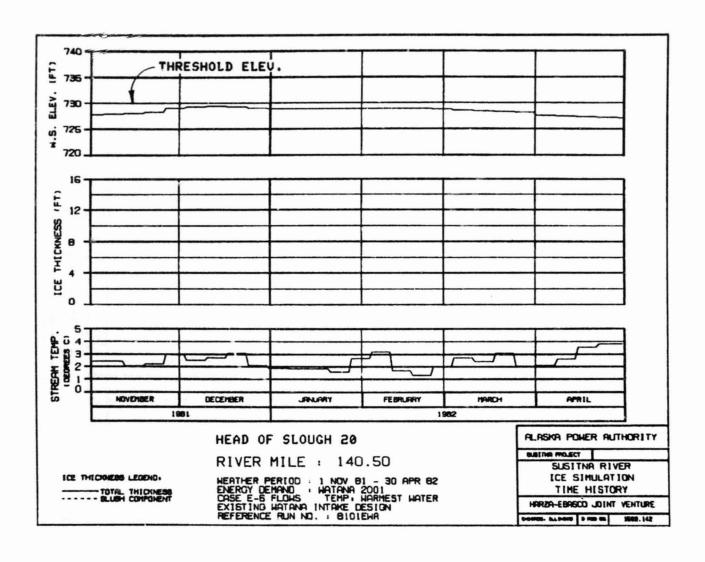


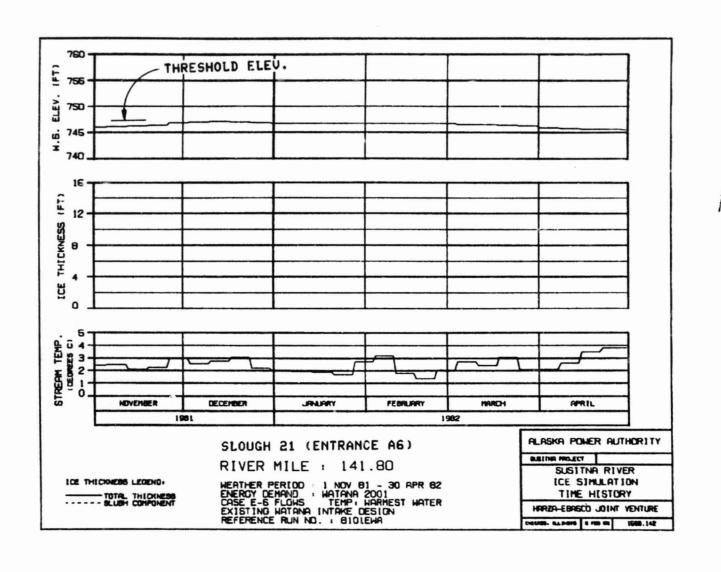


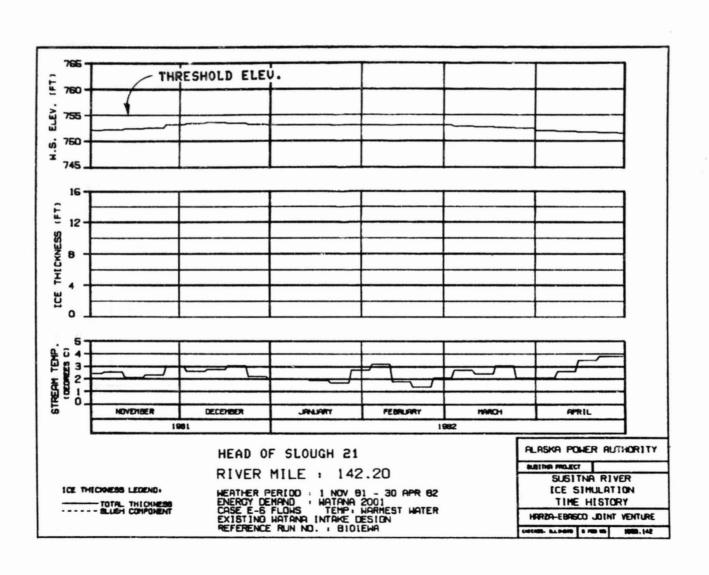


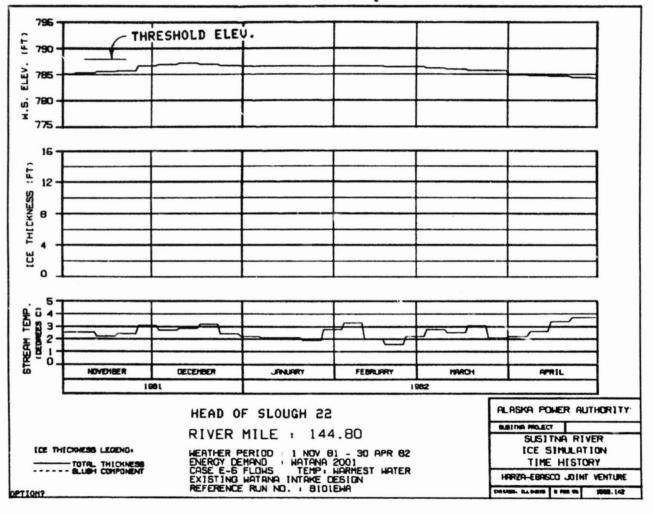


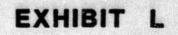


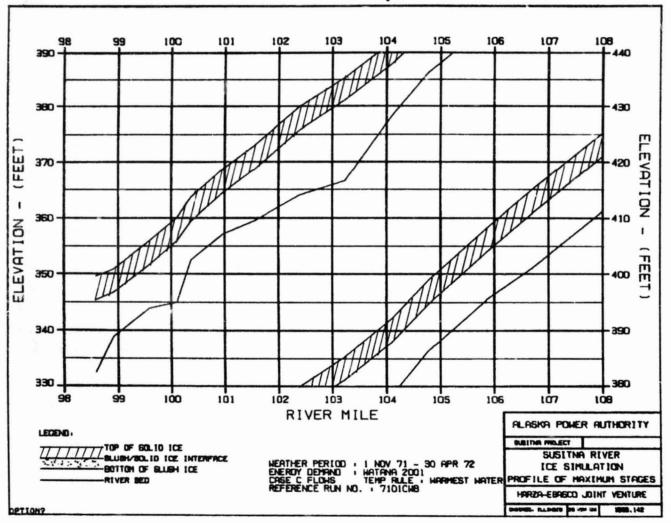


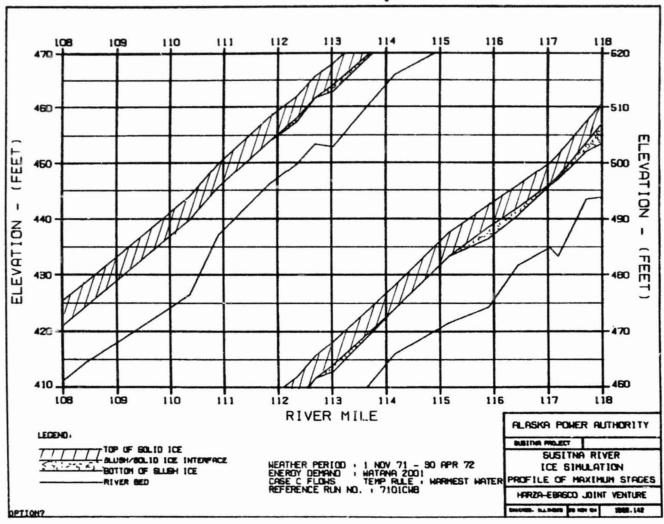




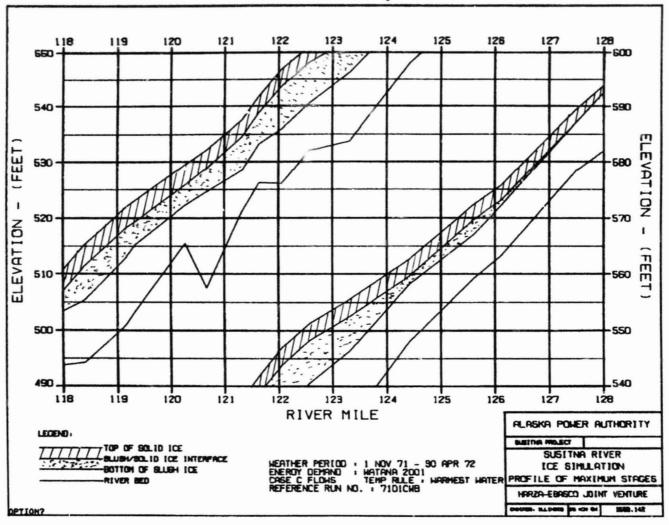




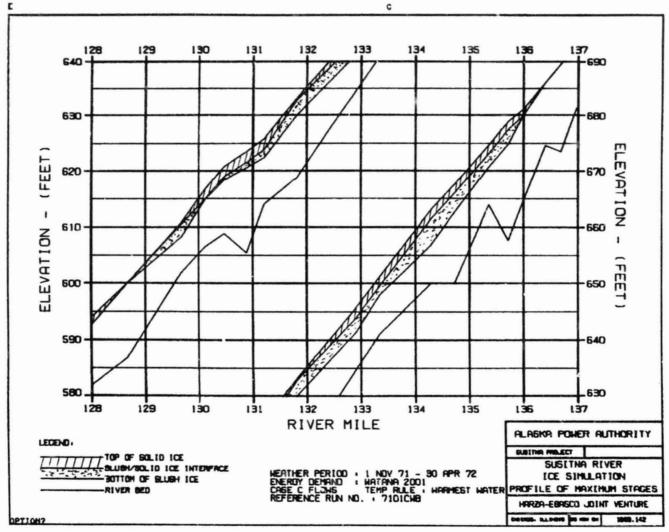




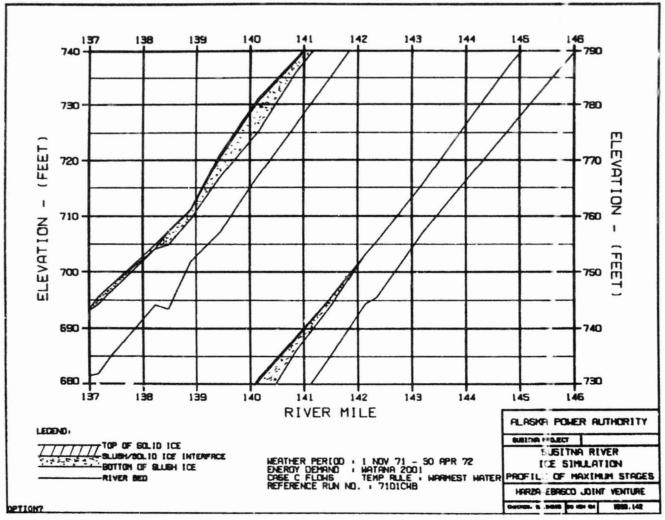


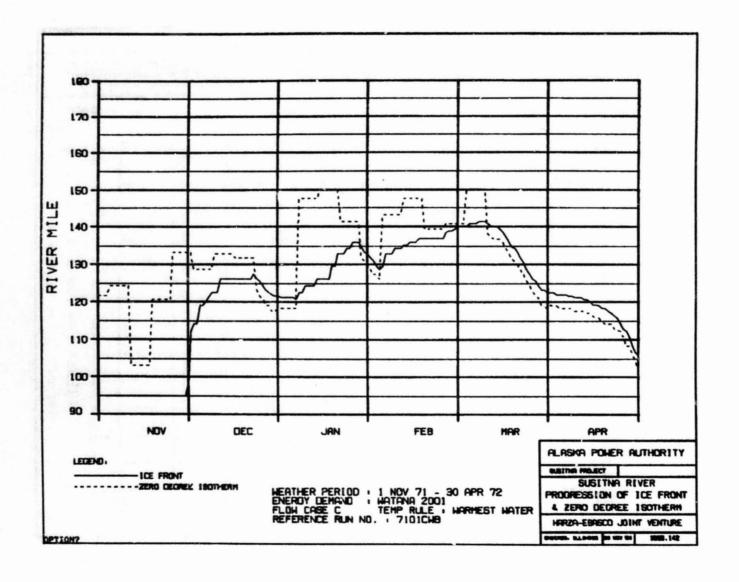


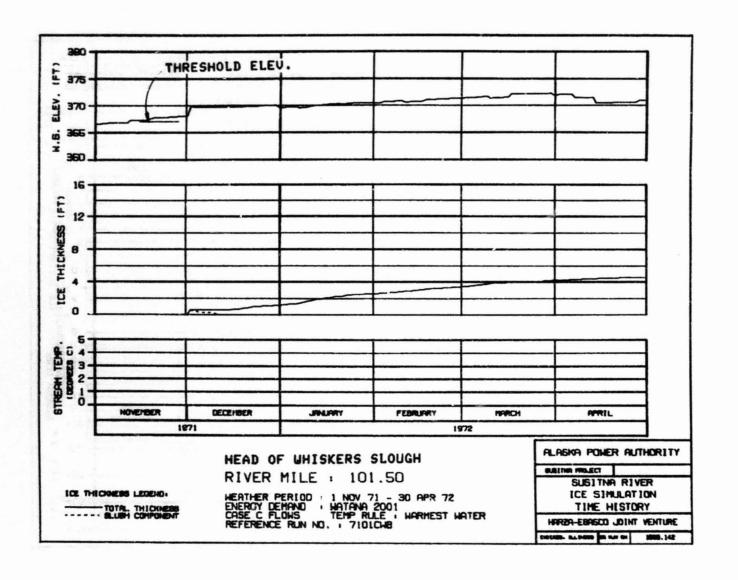


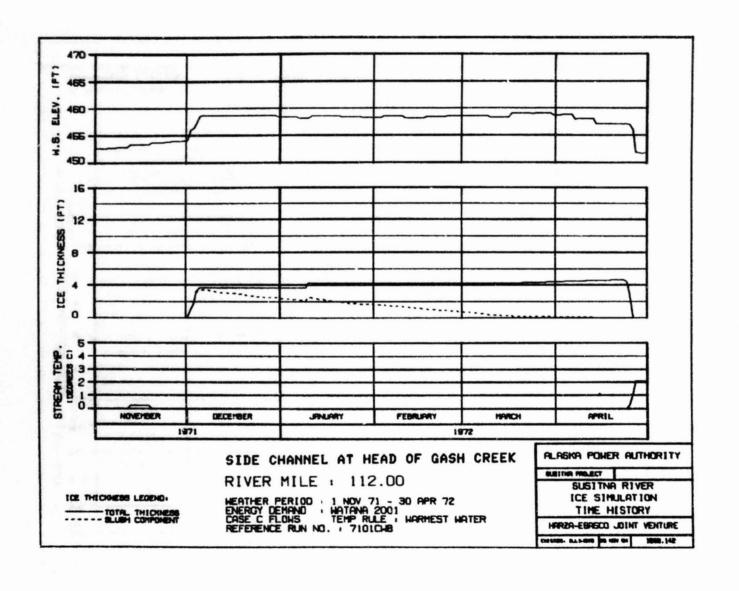


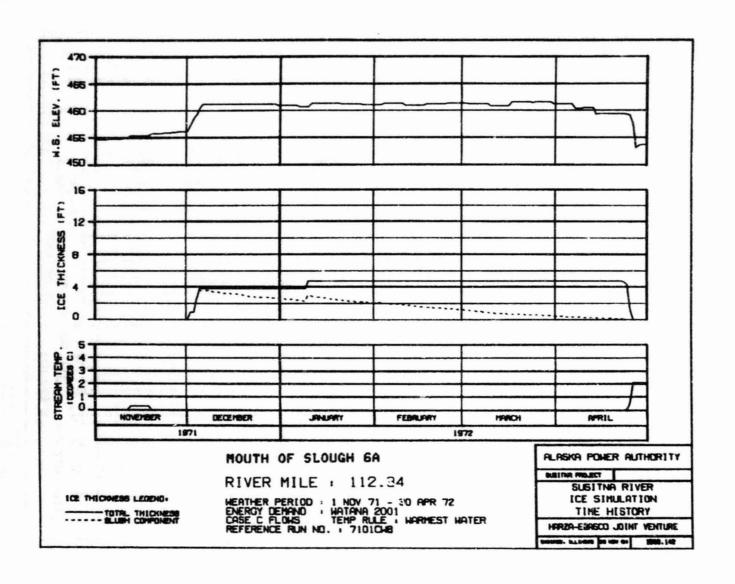


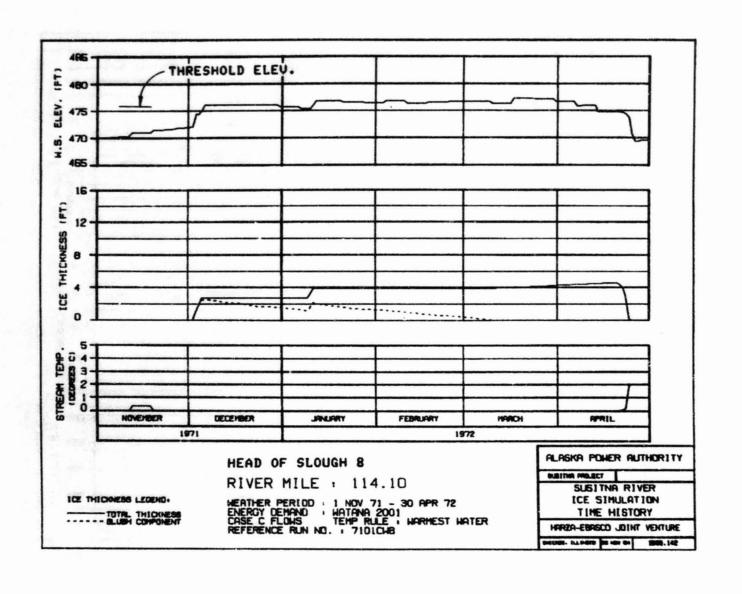


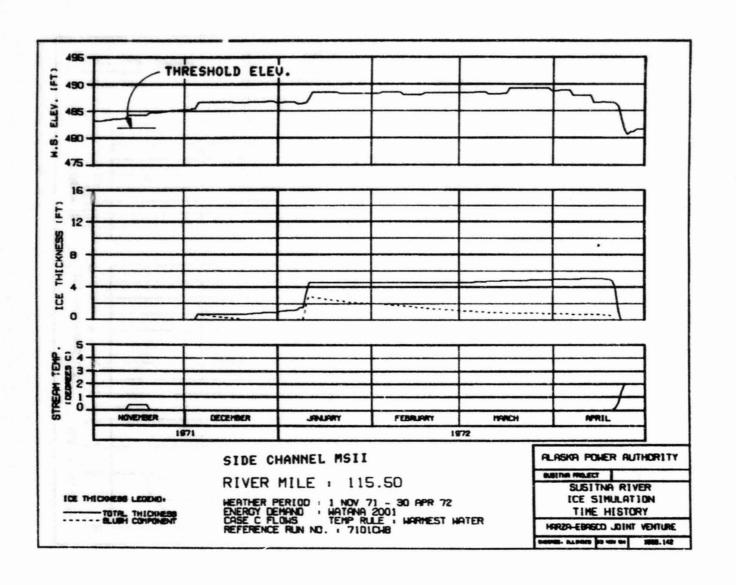


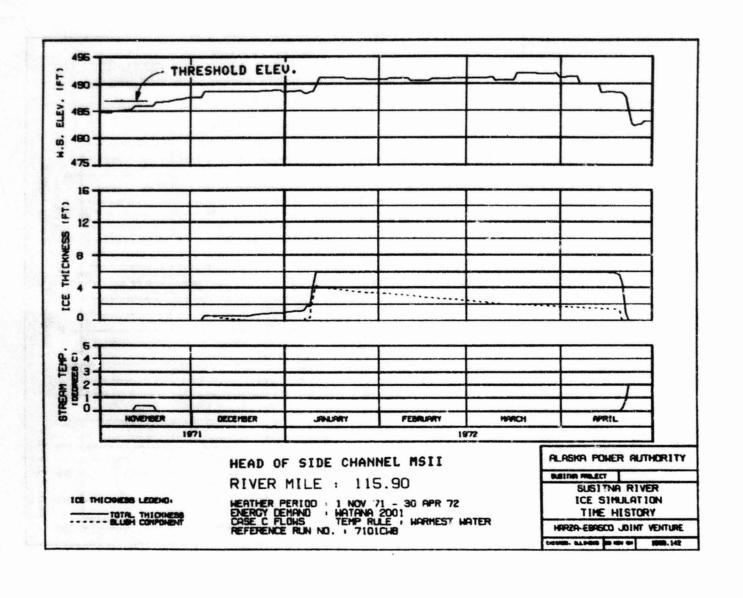


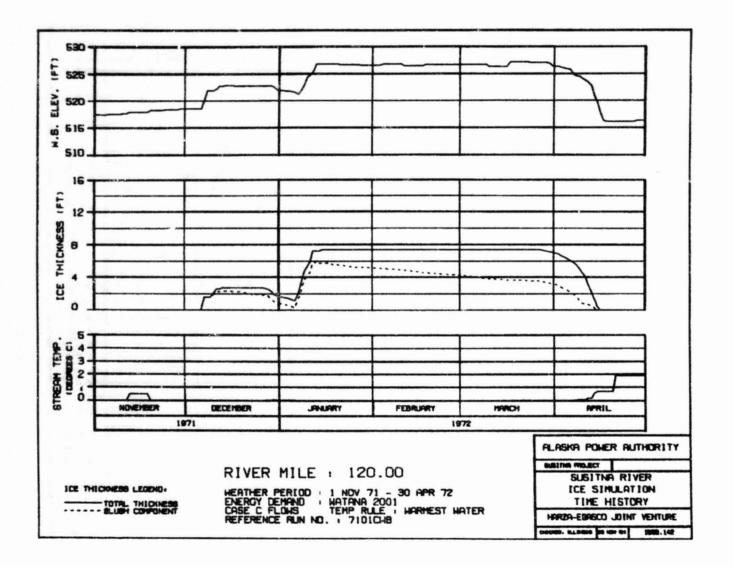


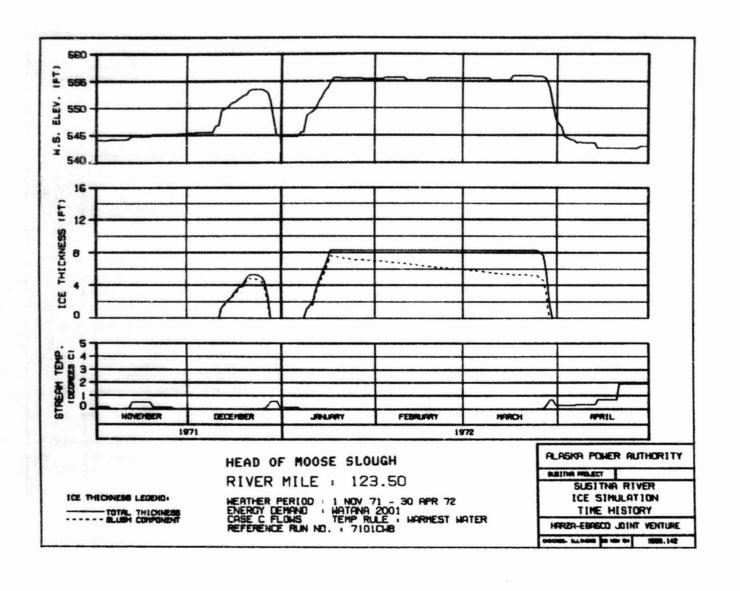


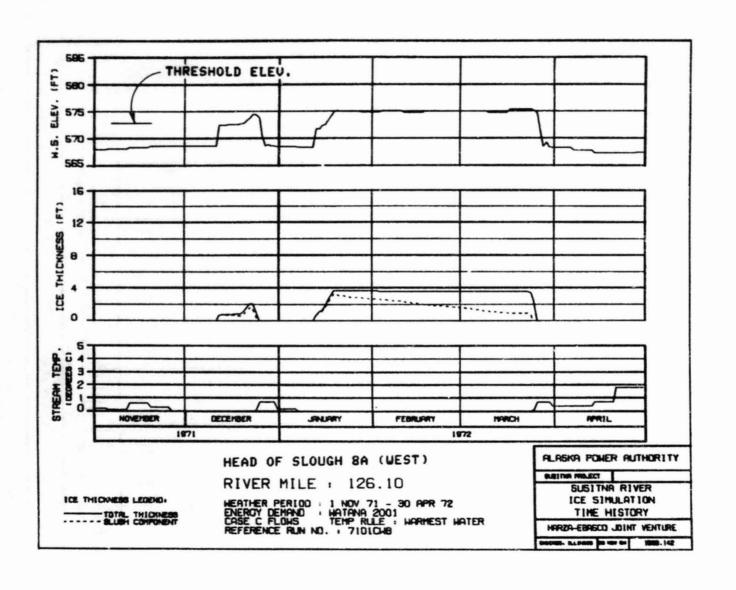


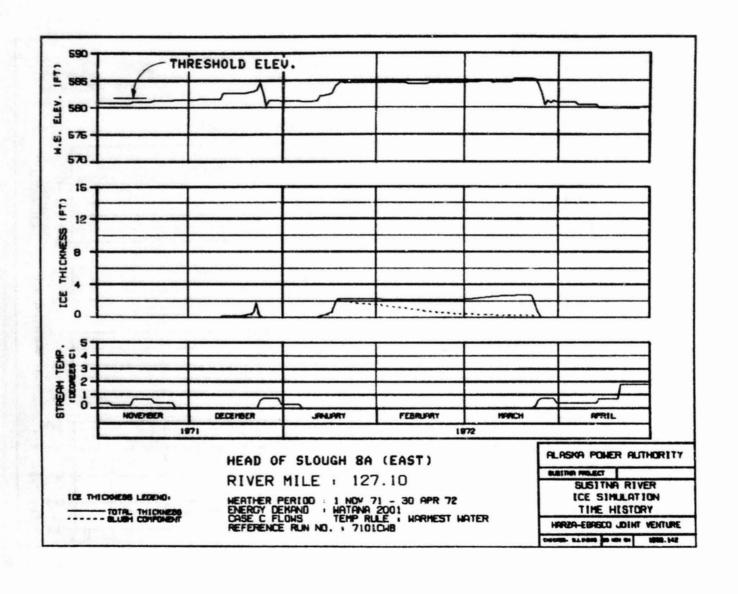


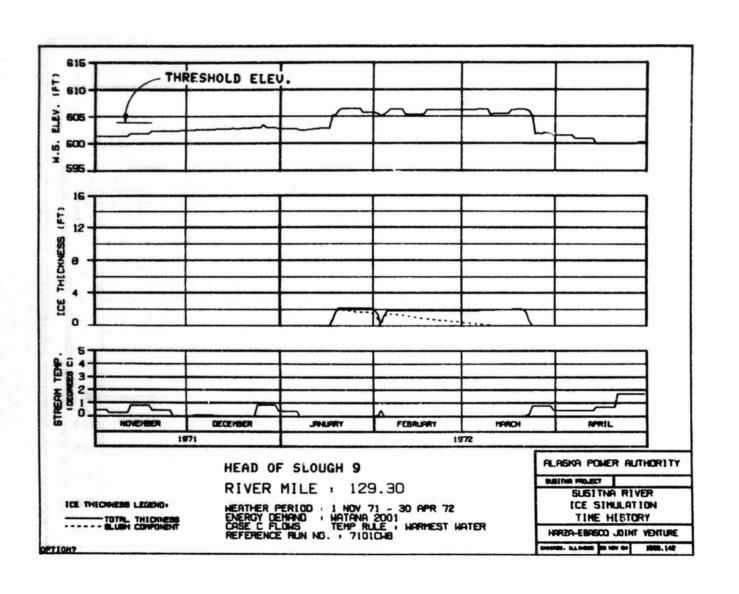


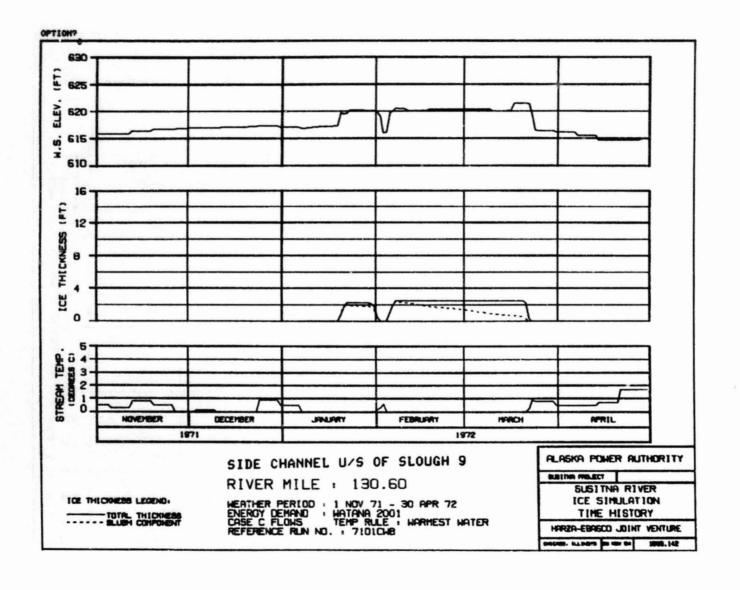


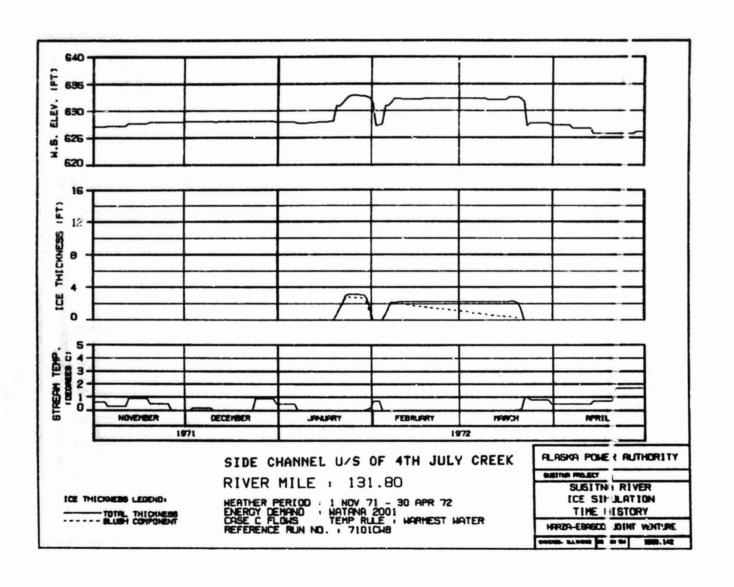


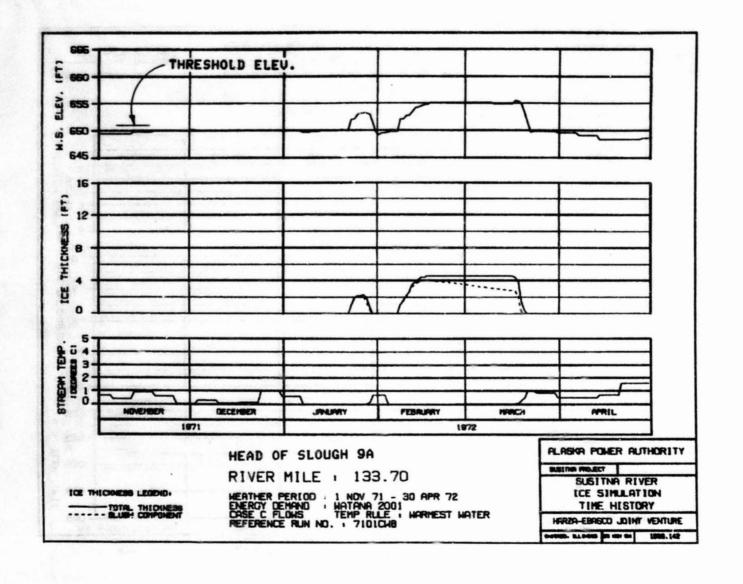


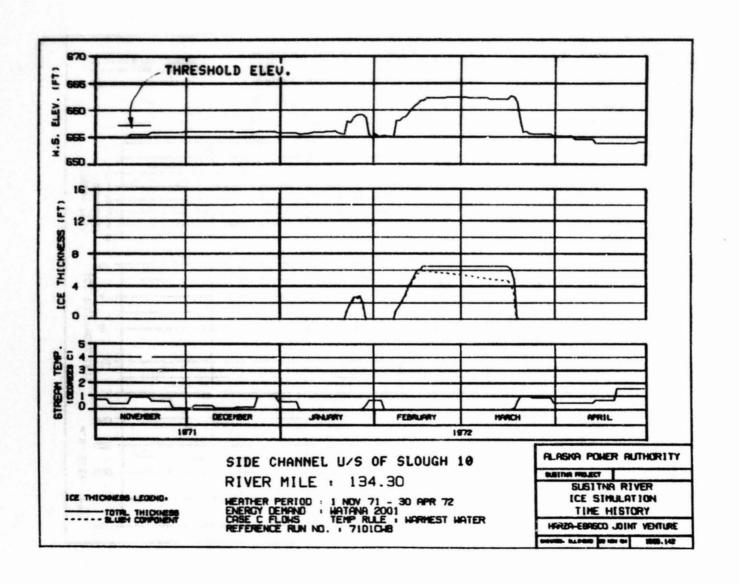


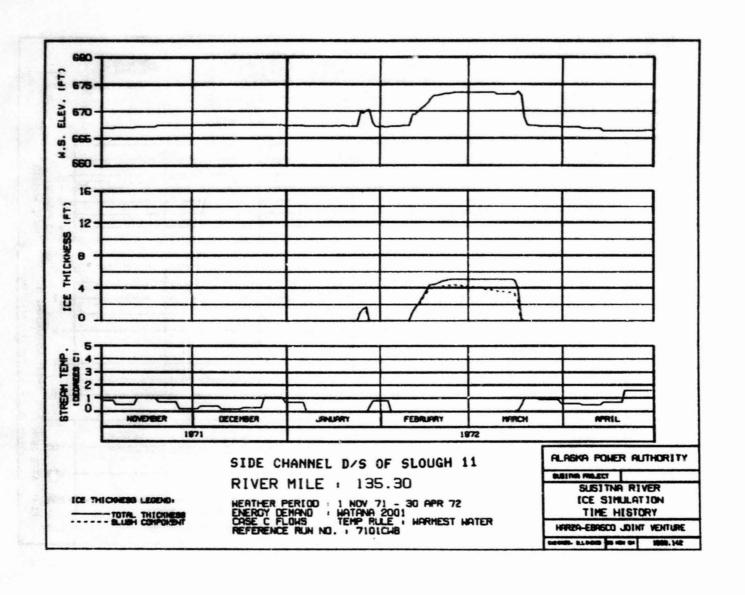


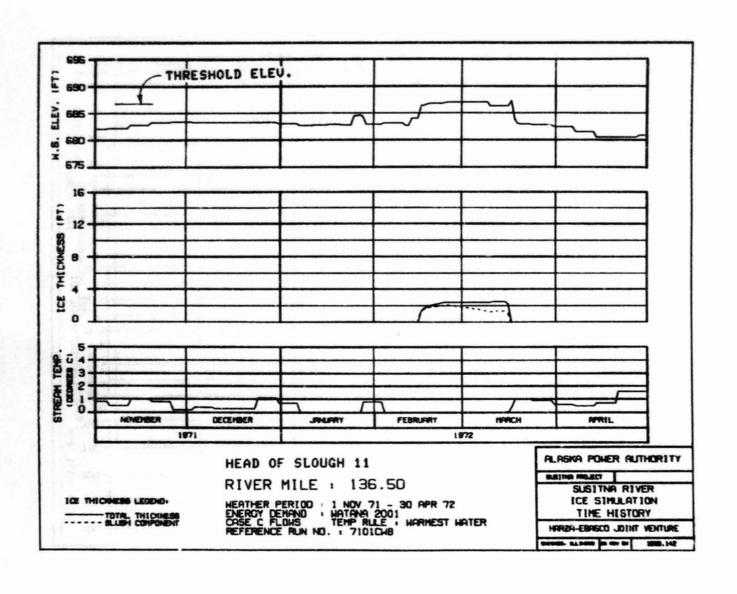


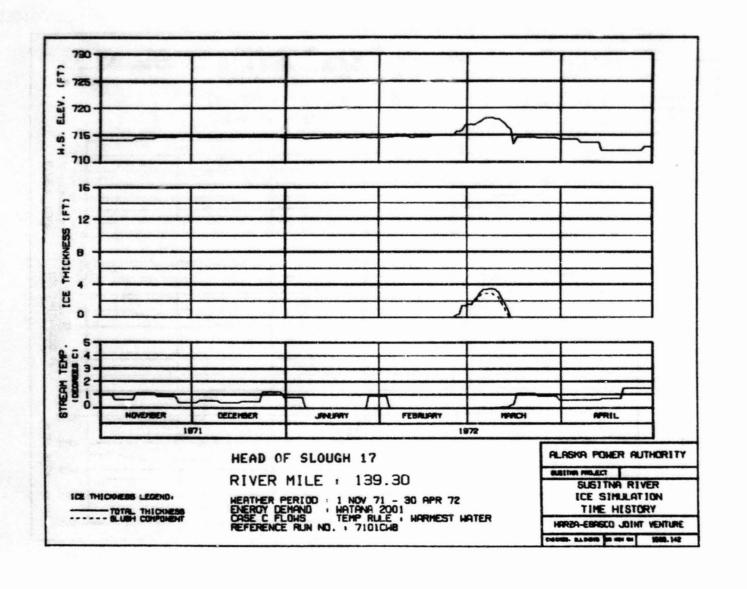


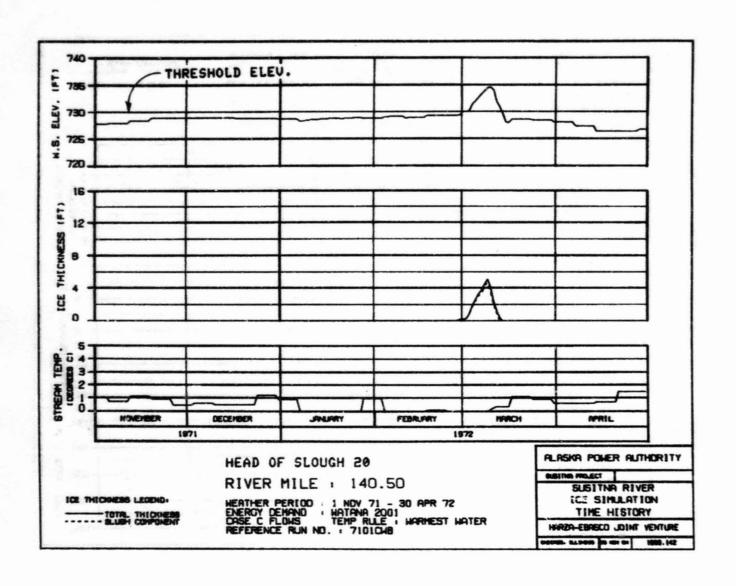


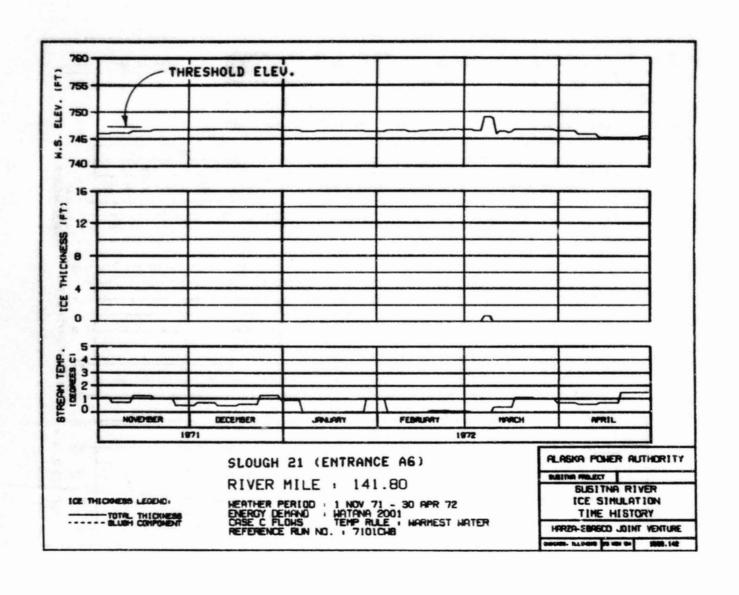


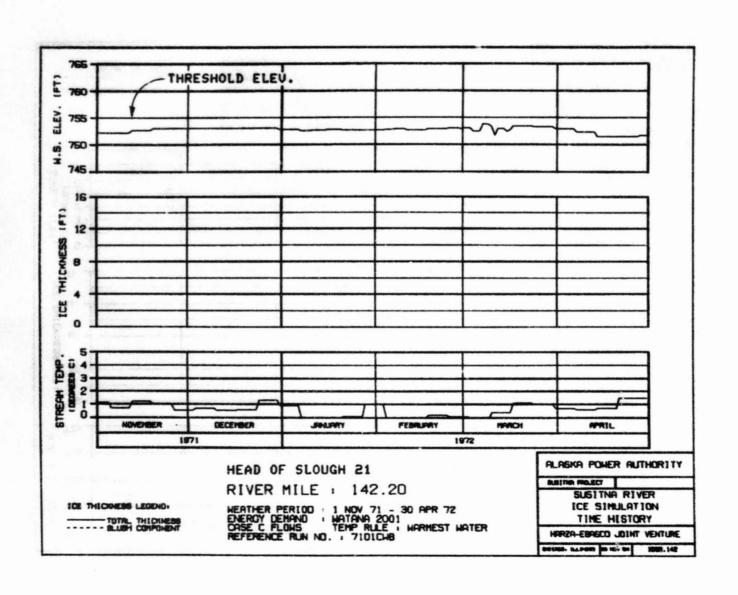














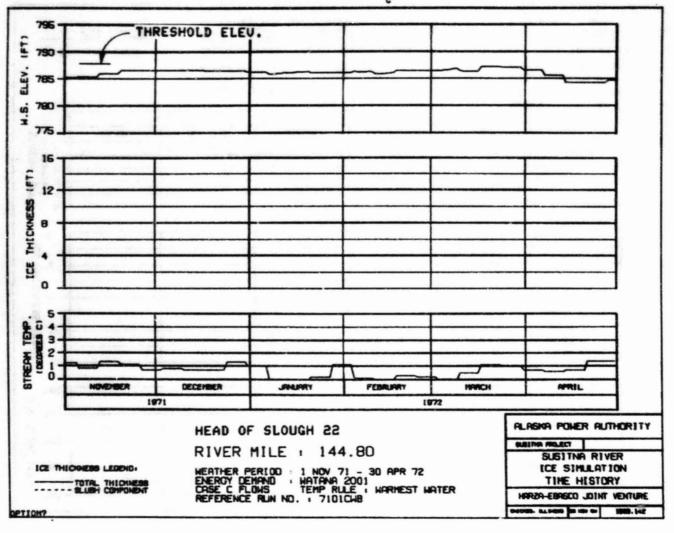
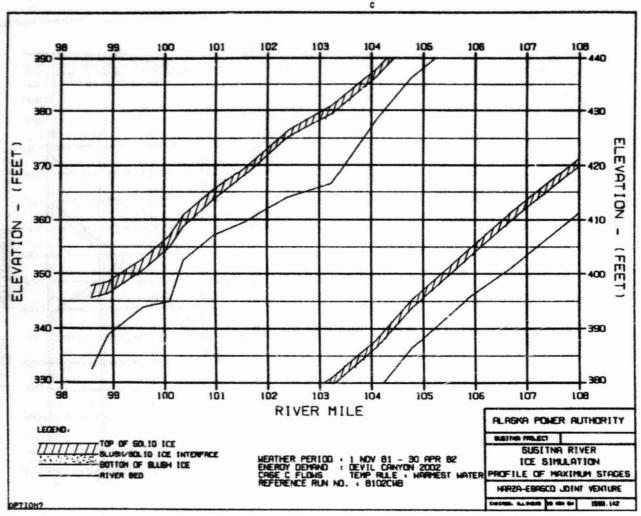
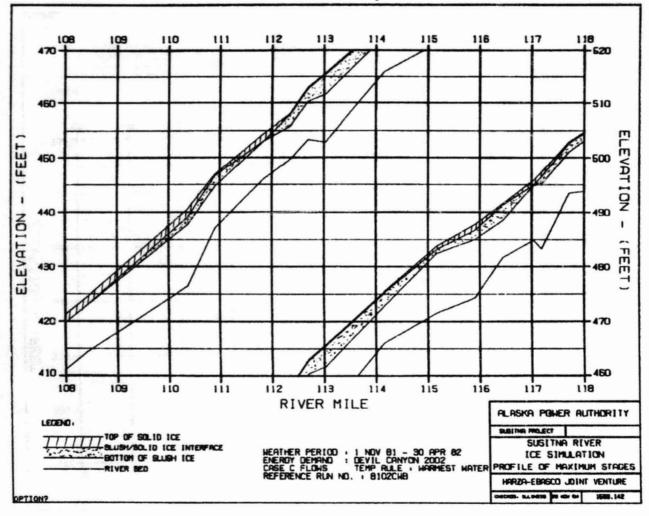
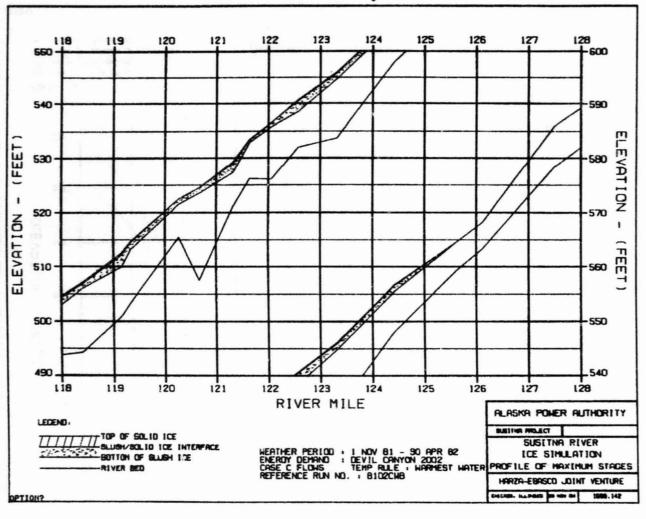


EXHIBIT M

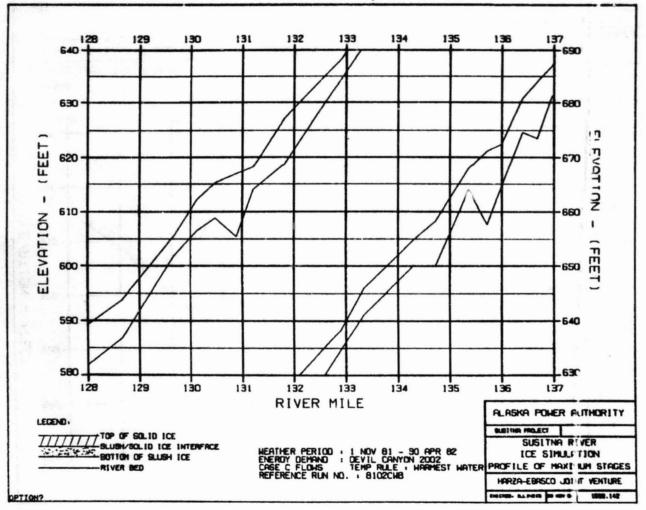




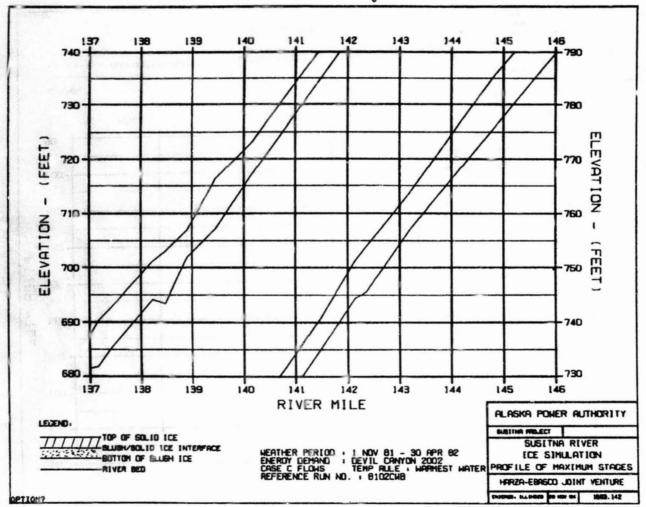


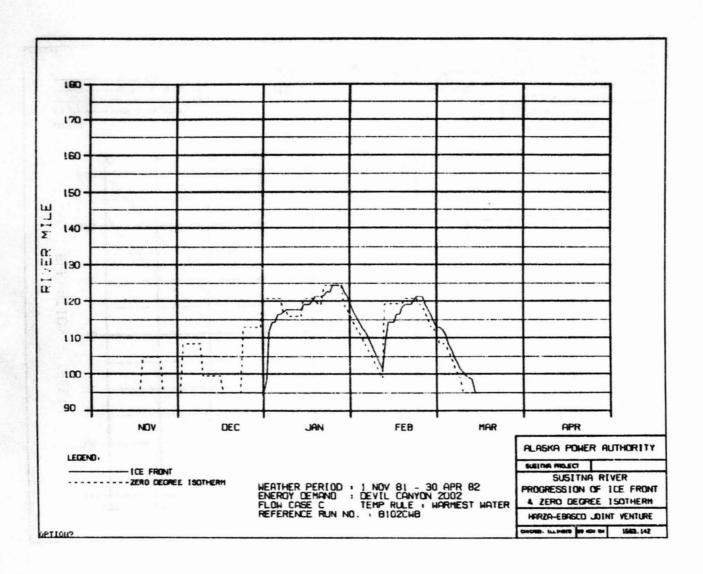


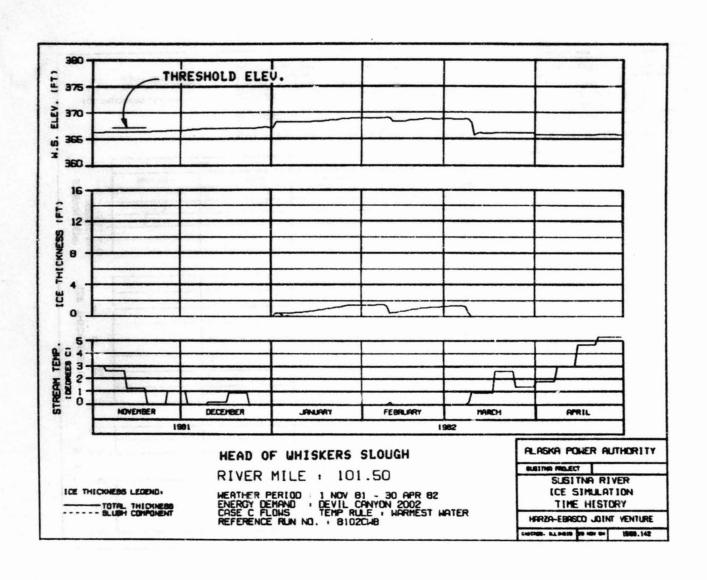


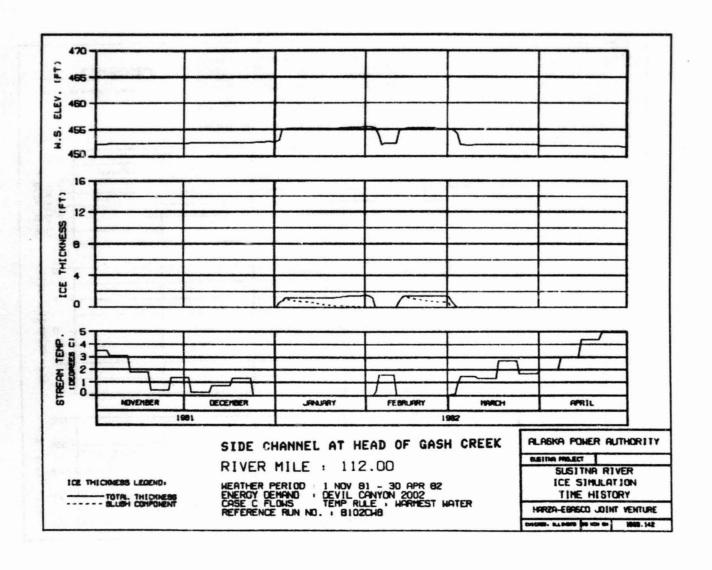


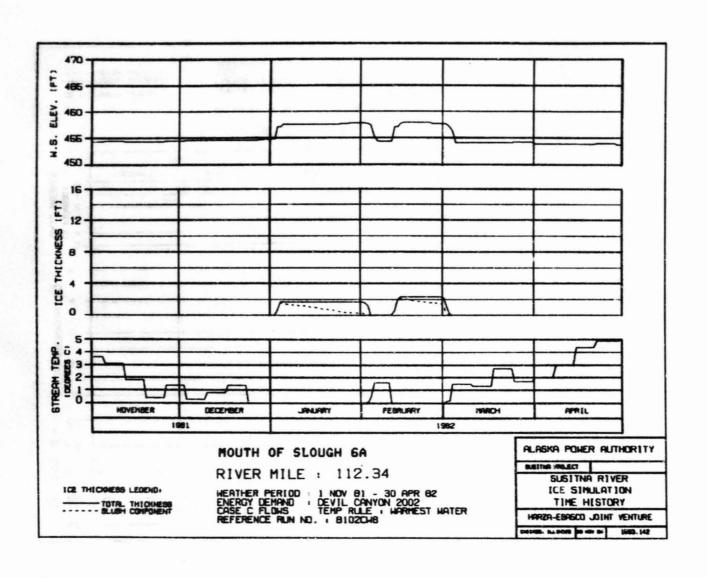


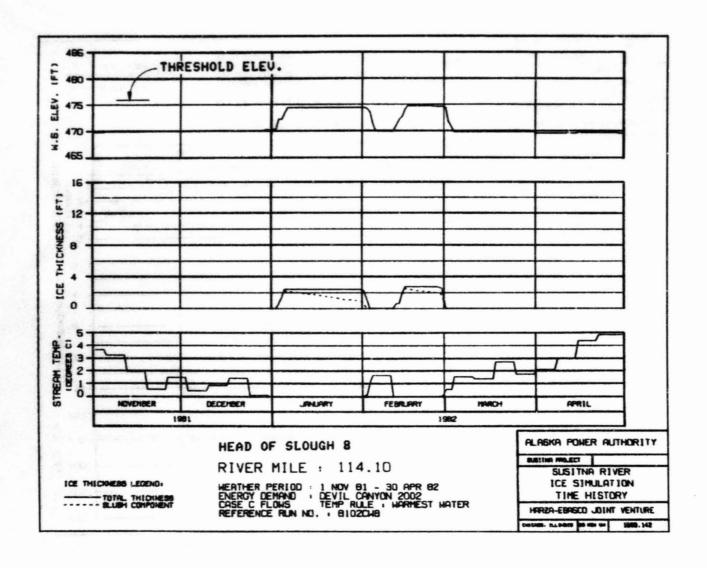


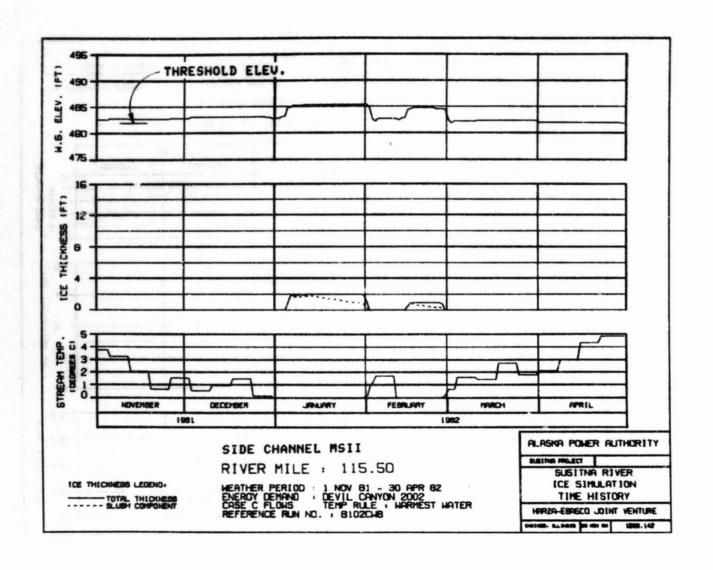


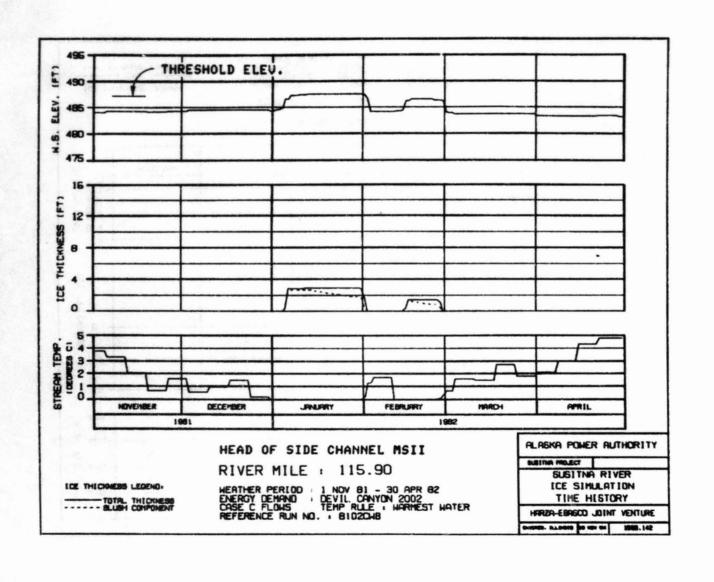


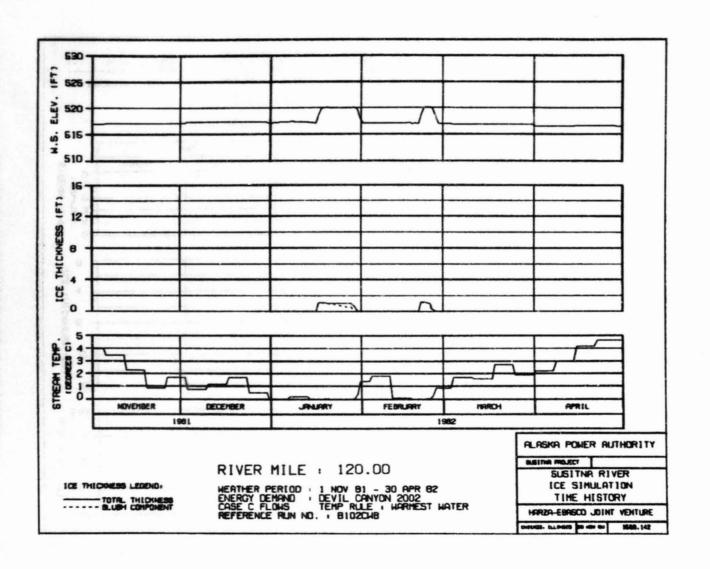


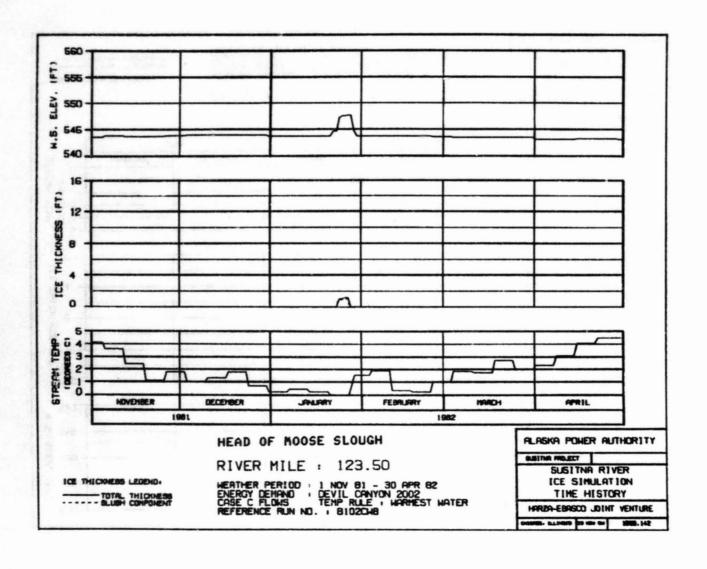


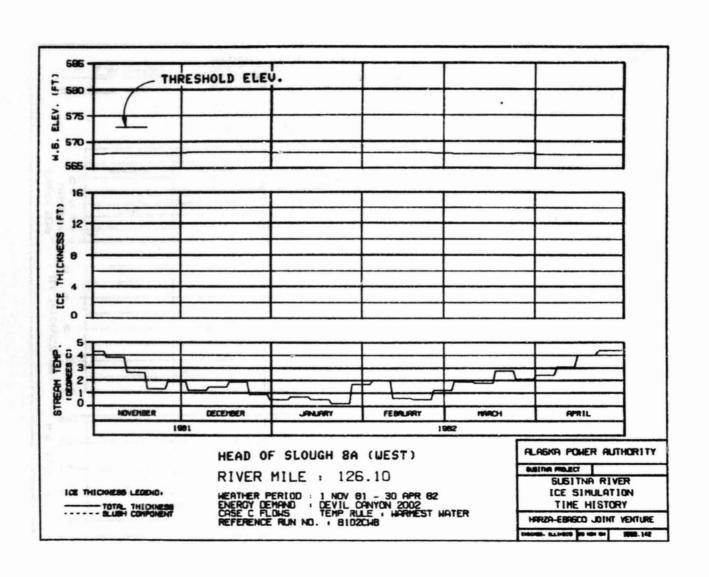


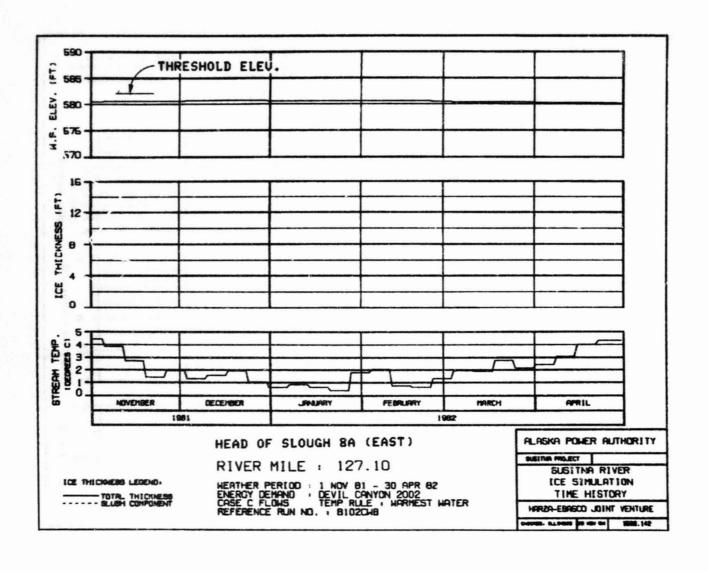


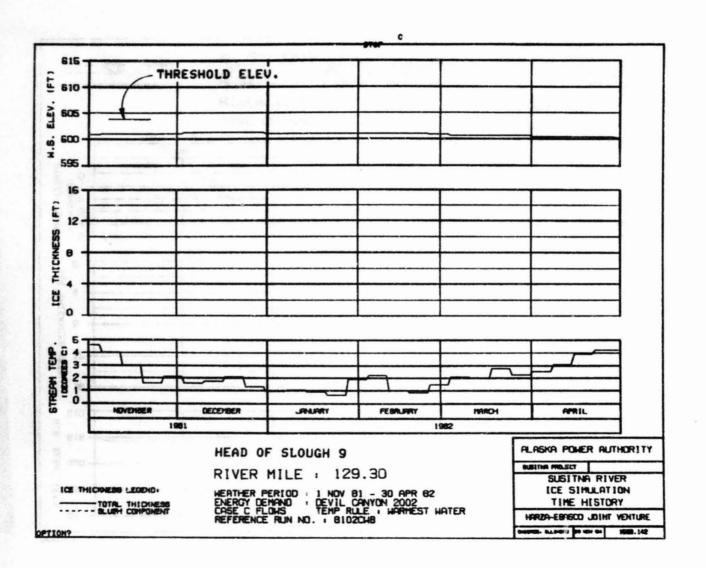


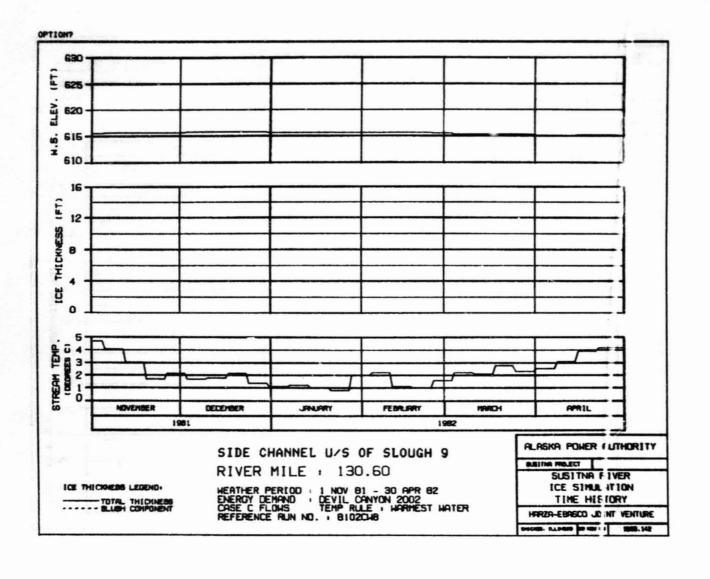


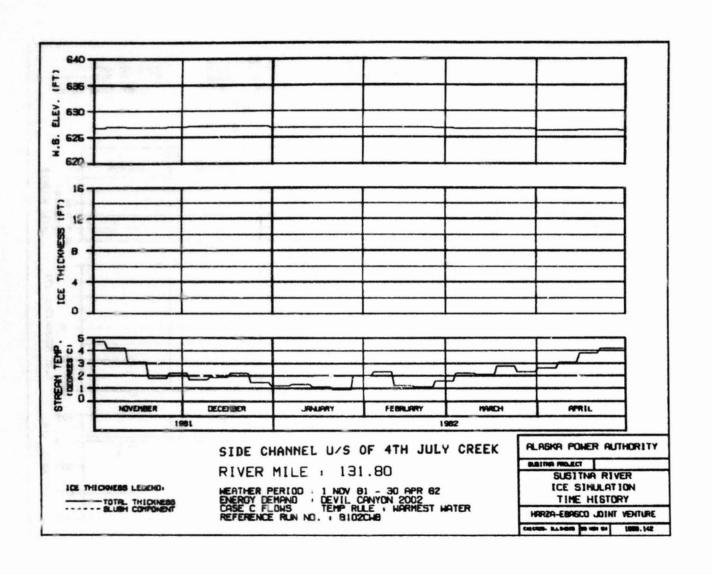


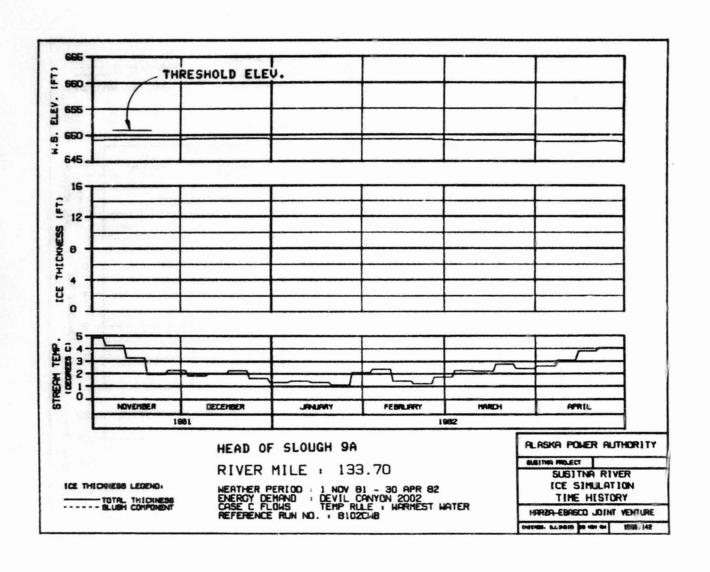


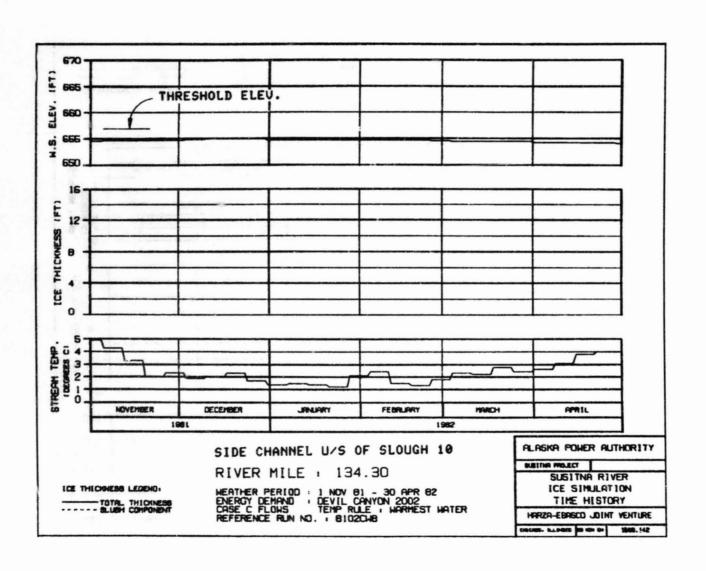


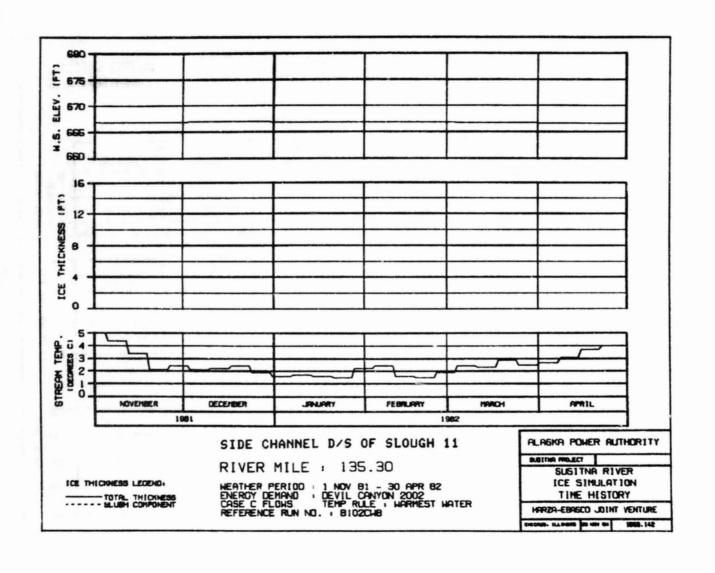


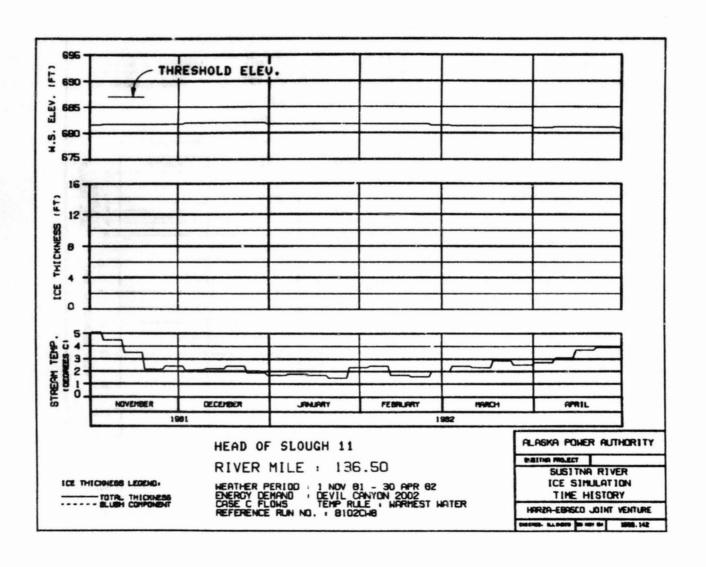


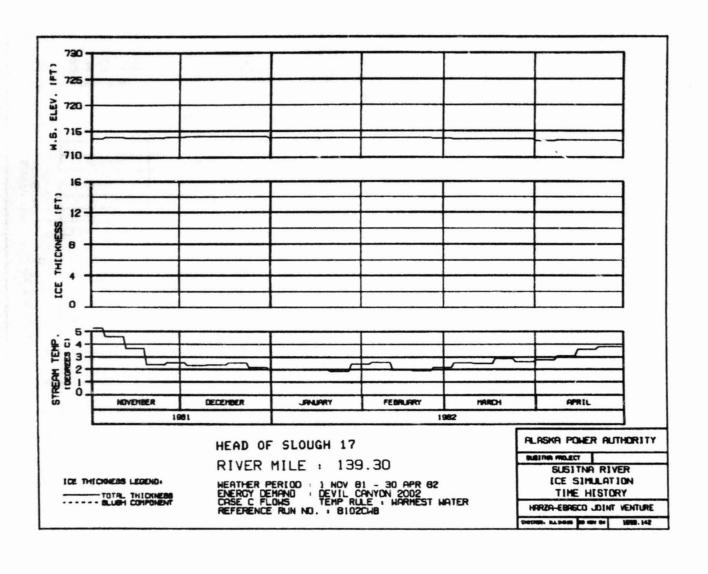


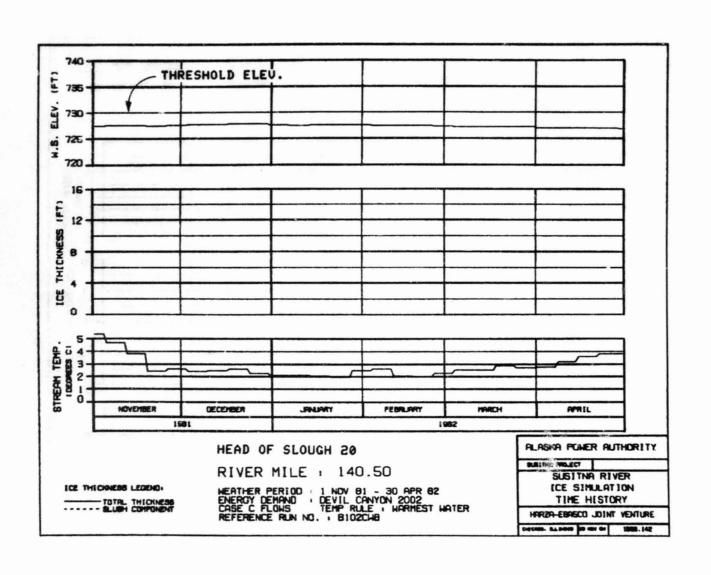


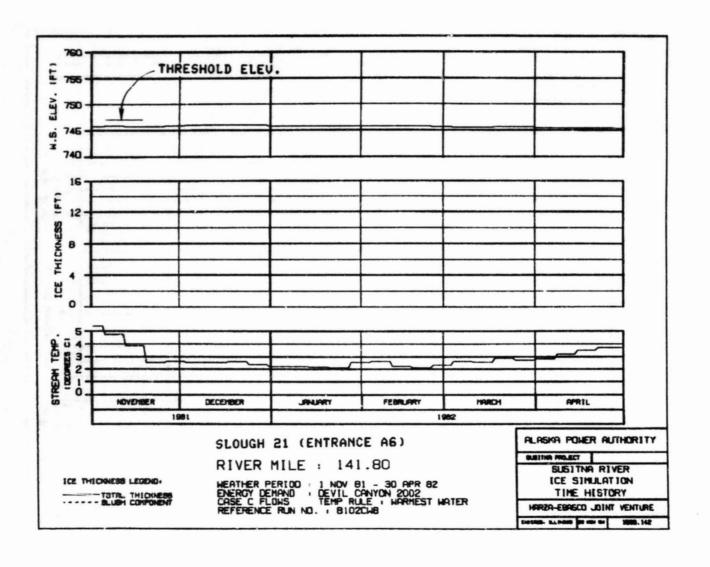


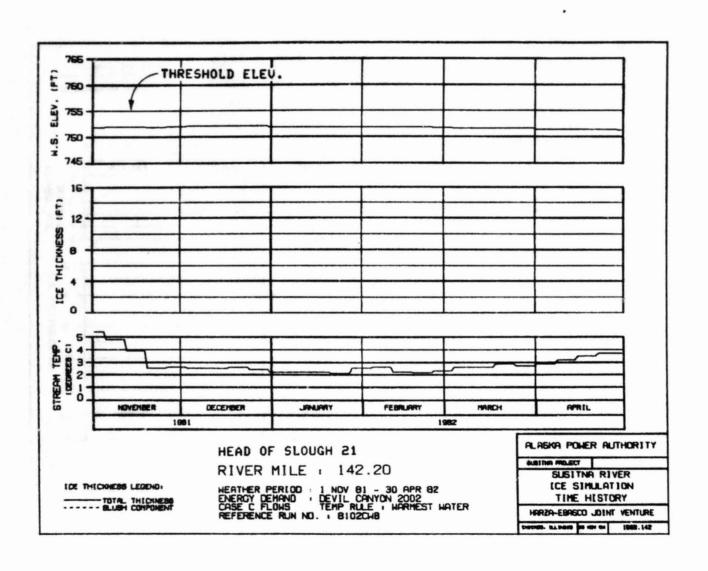












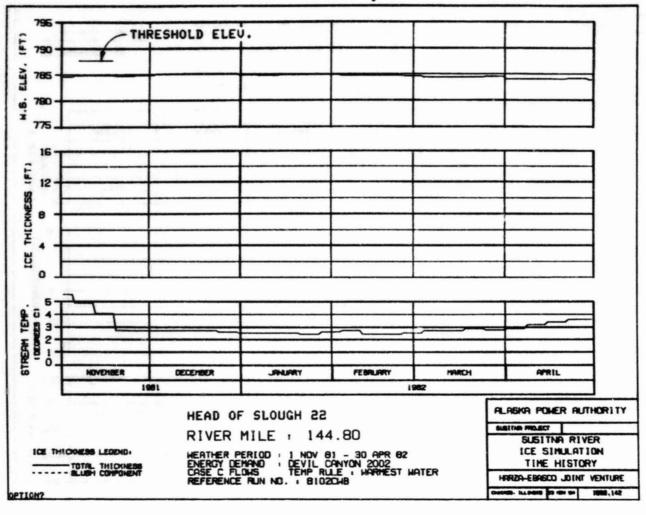
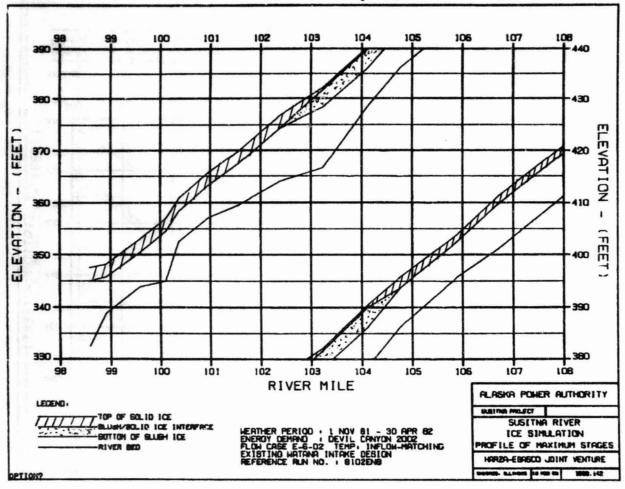
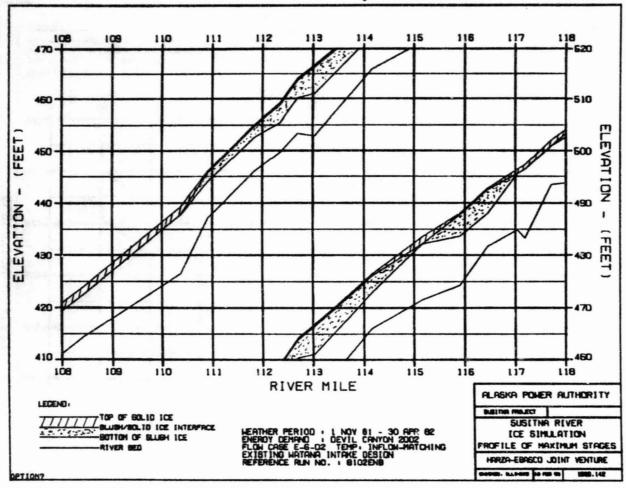


EXHIBIT N

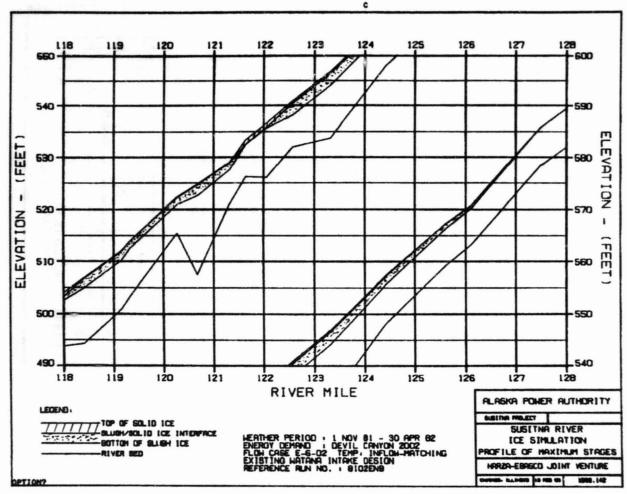




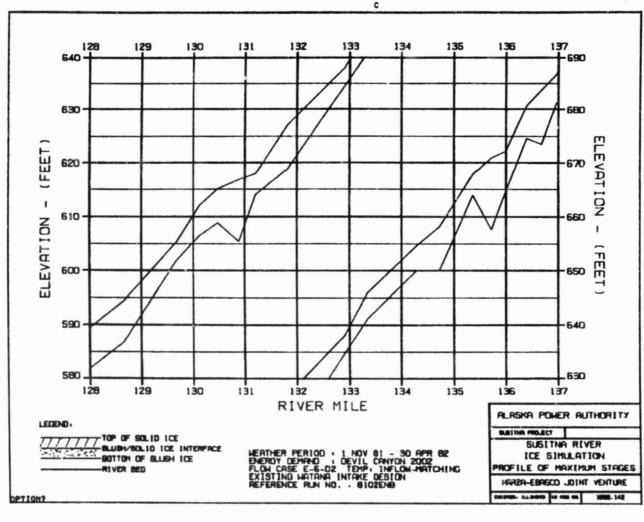




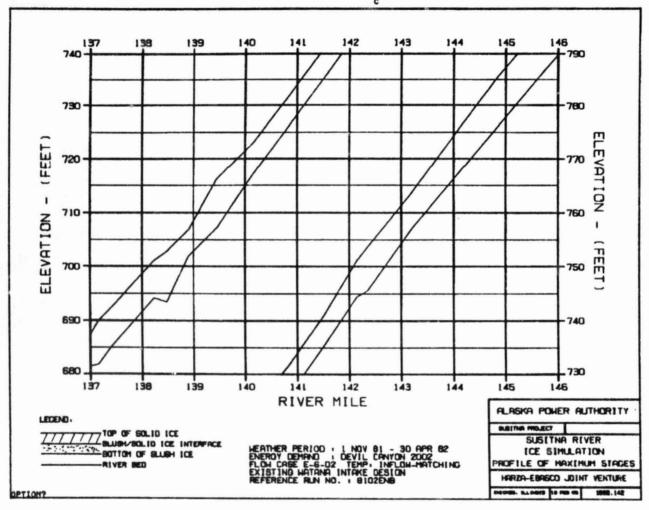


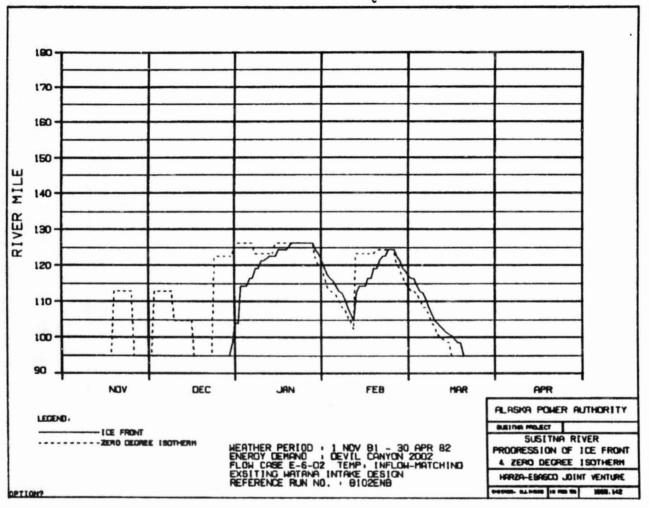


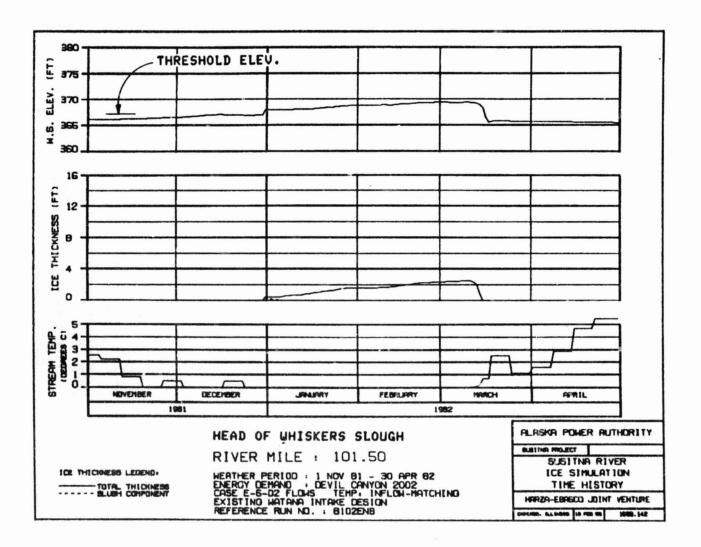


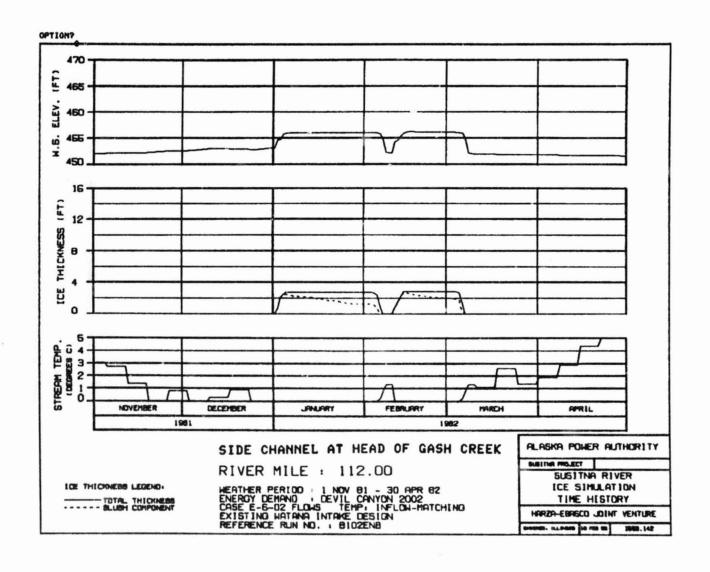


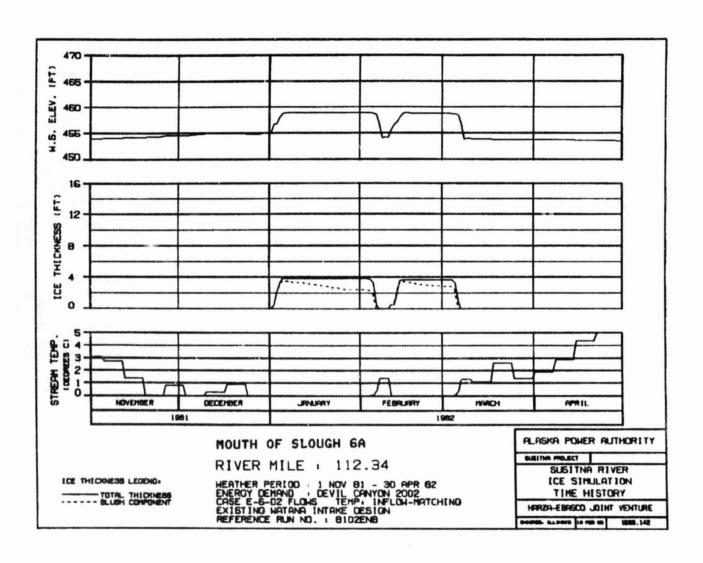


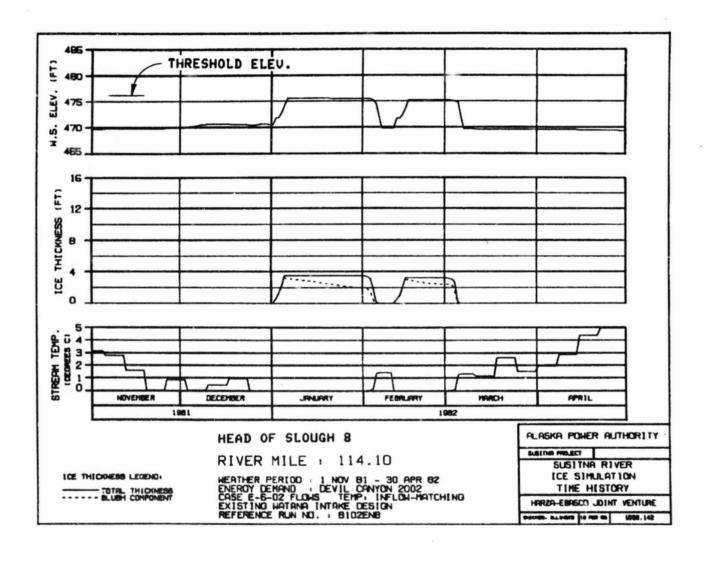




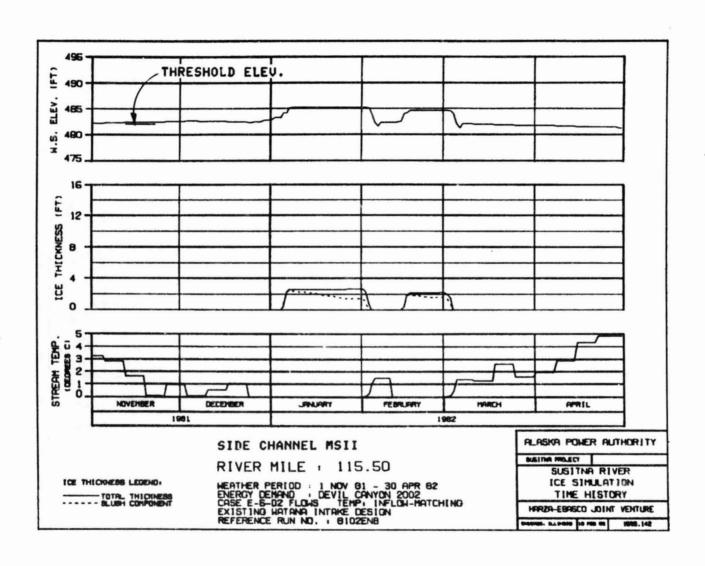


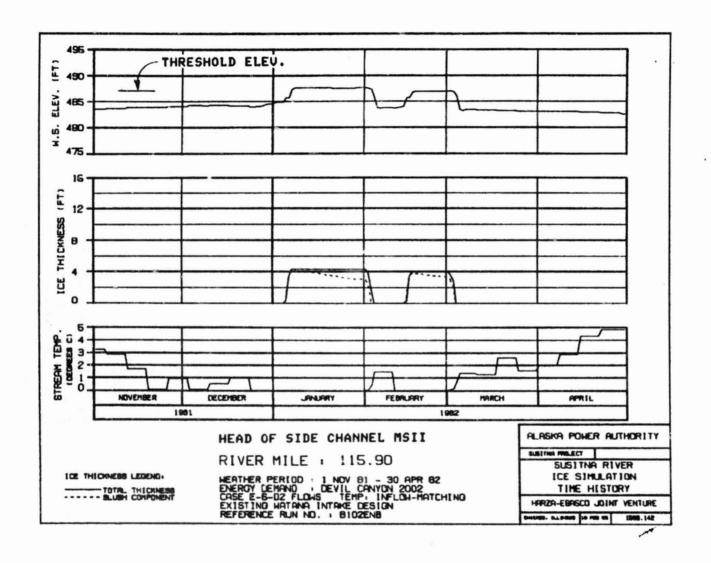


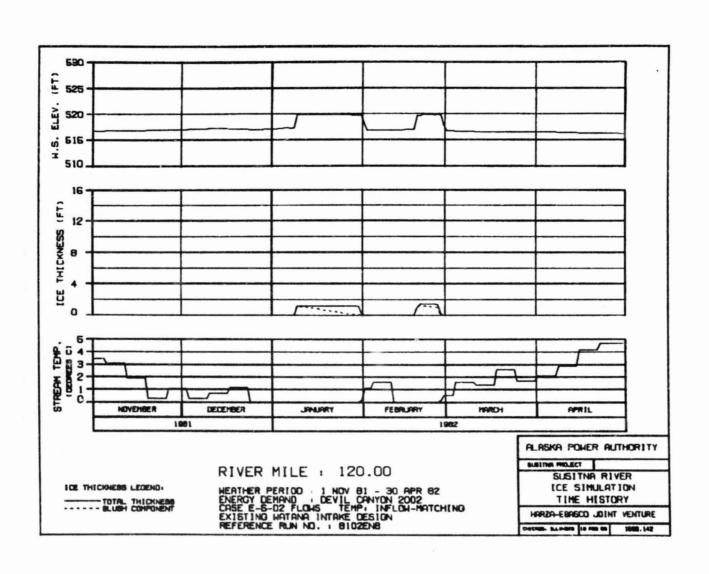


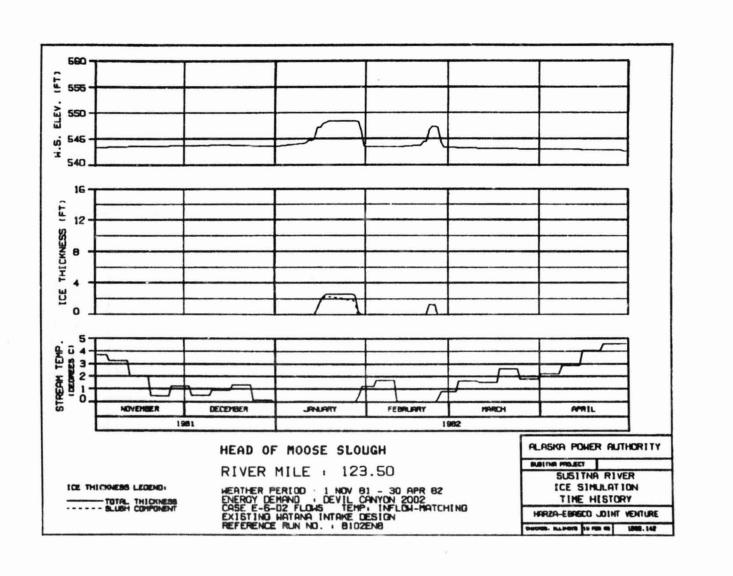


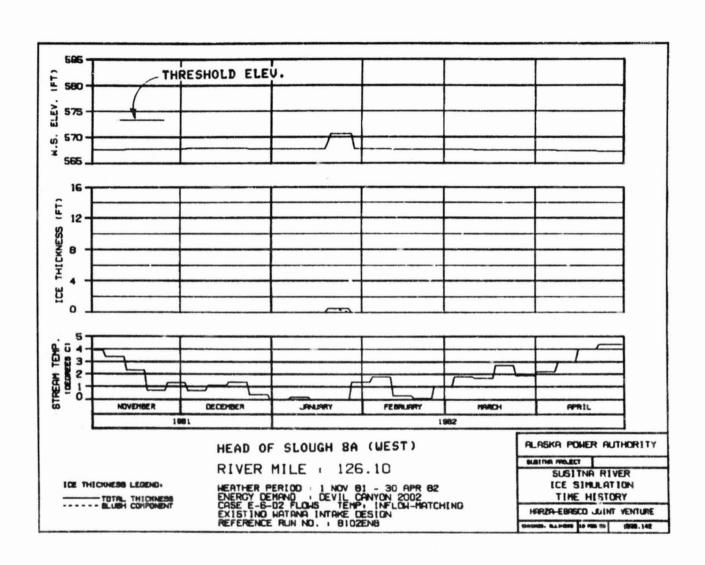
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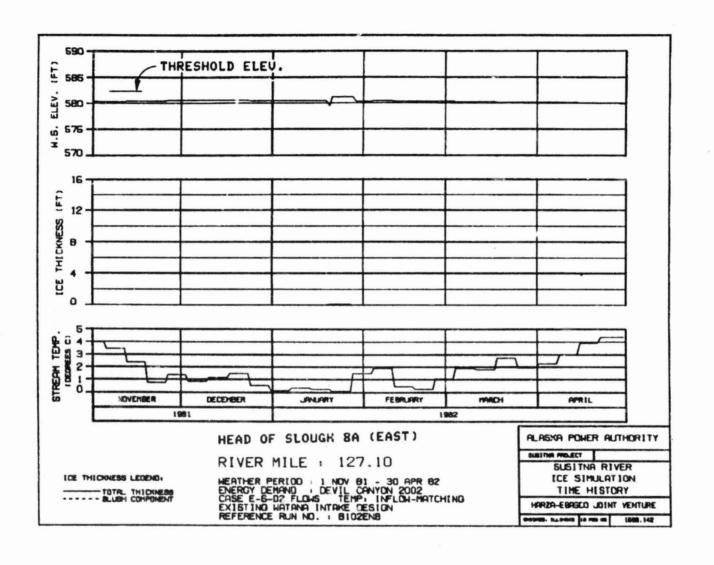


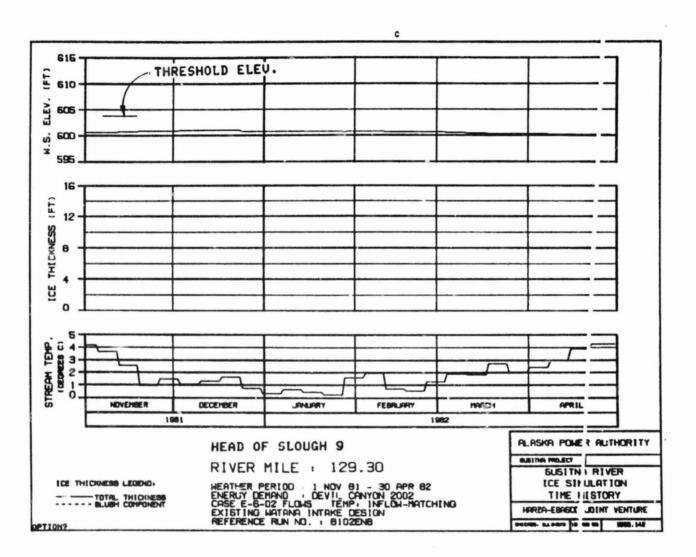


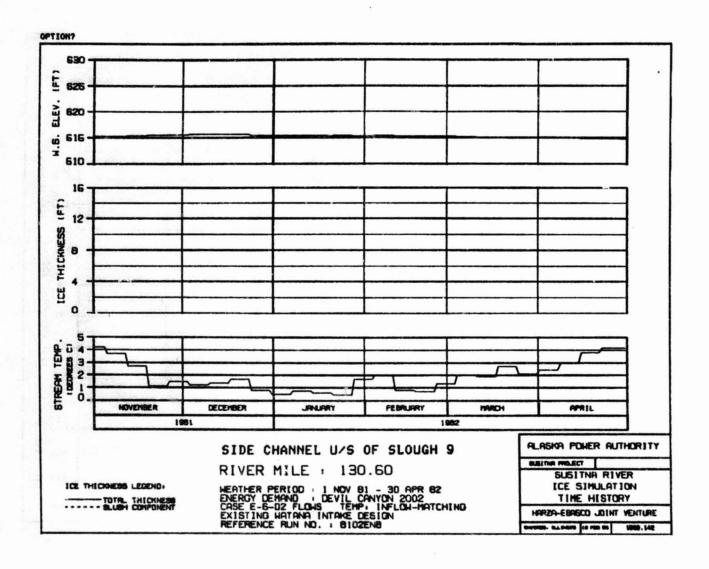


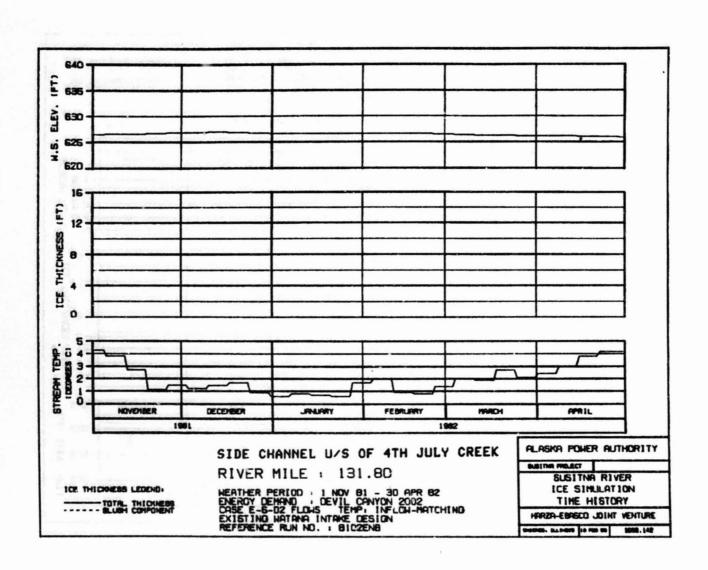


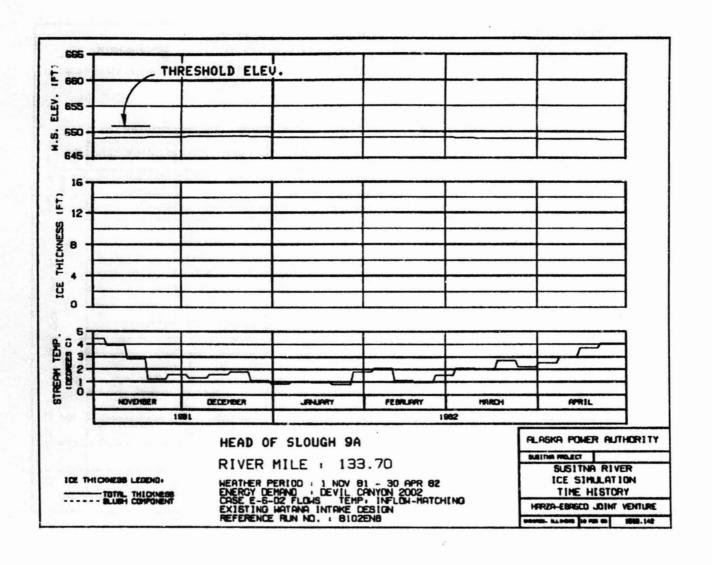


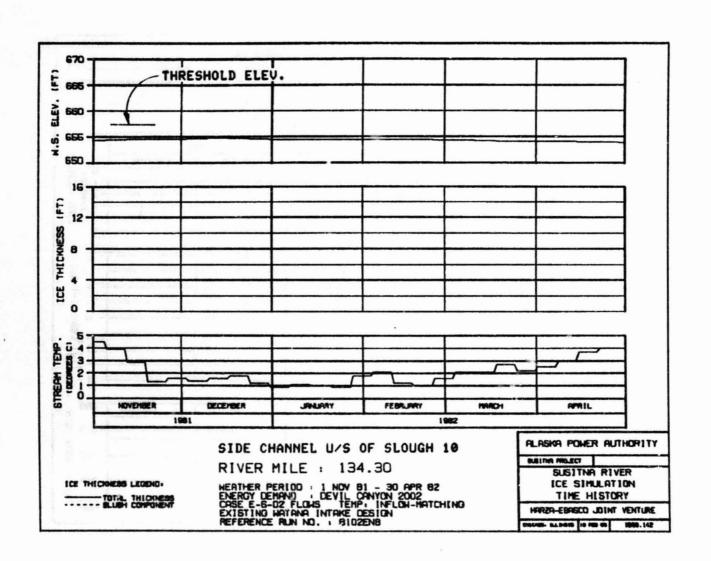


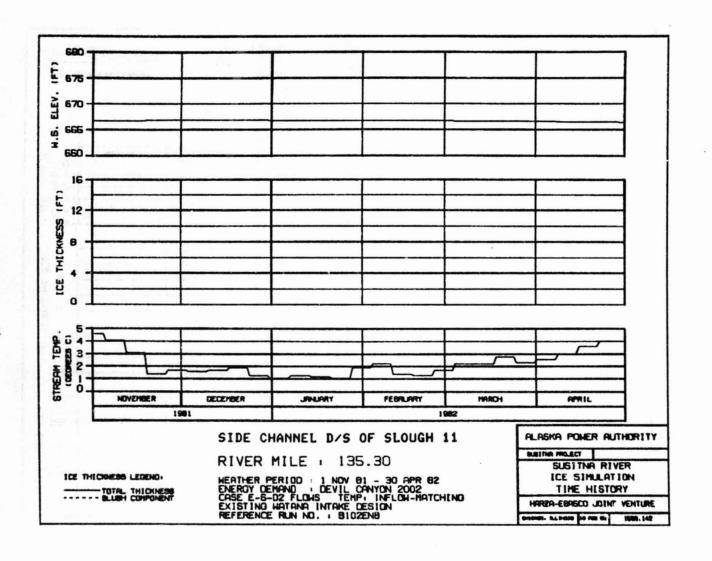


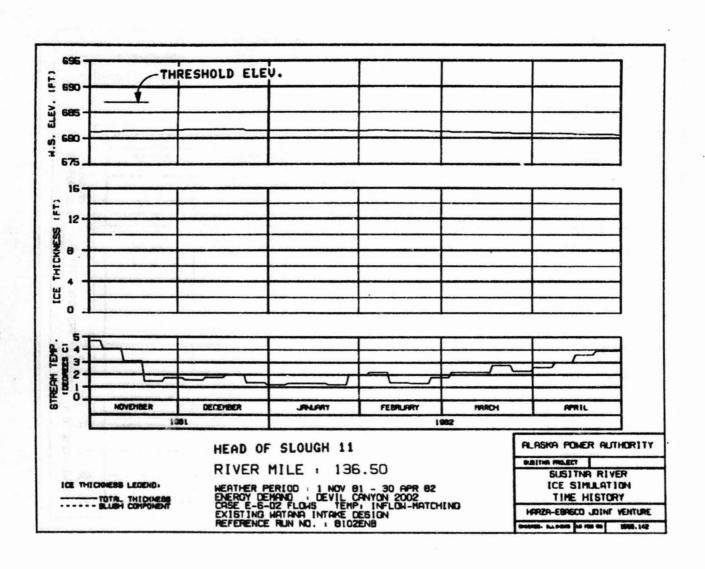


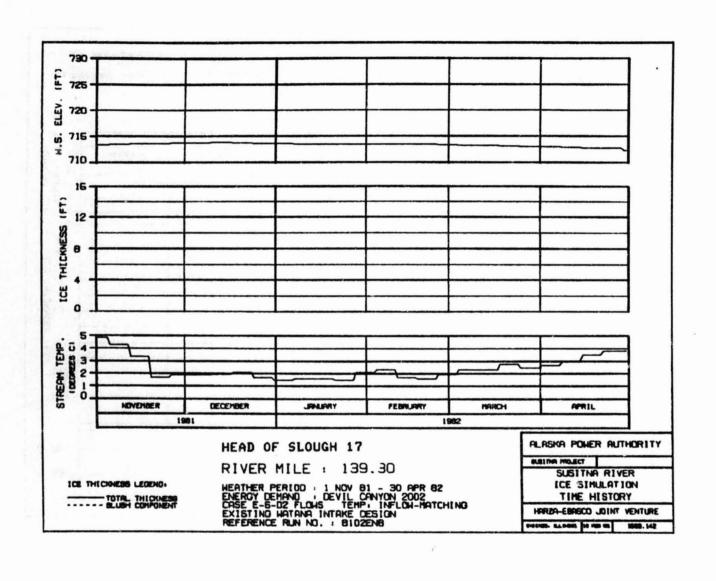


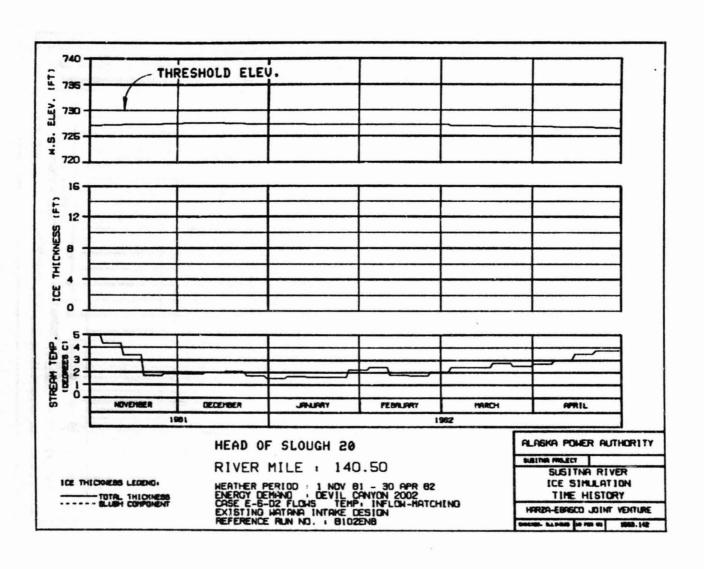


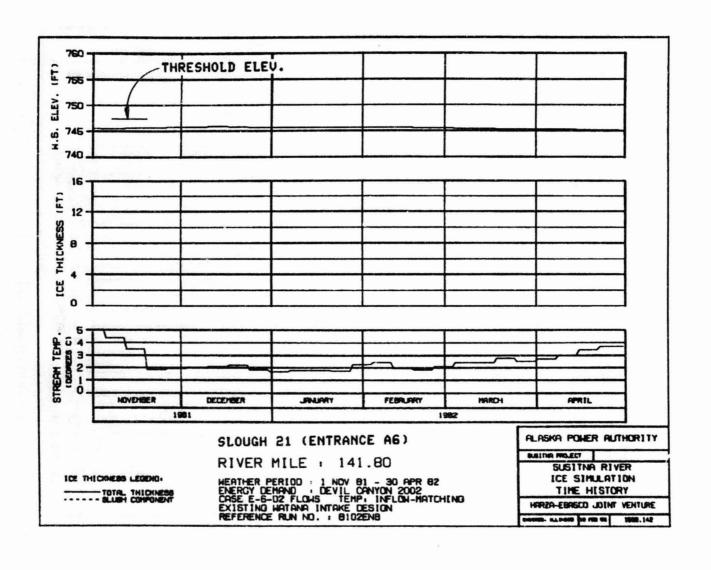


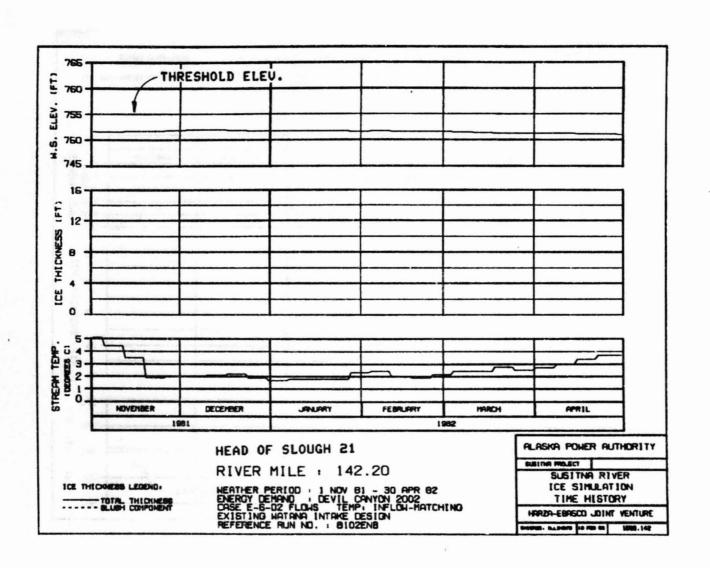


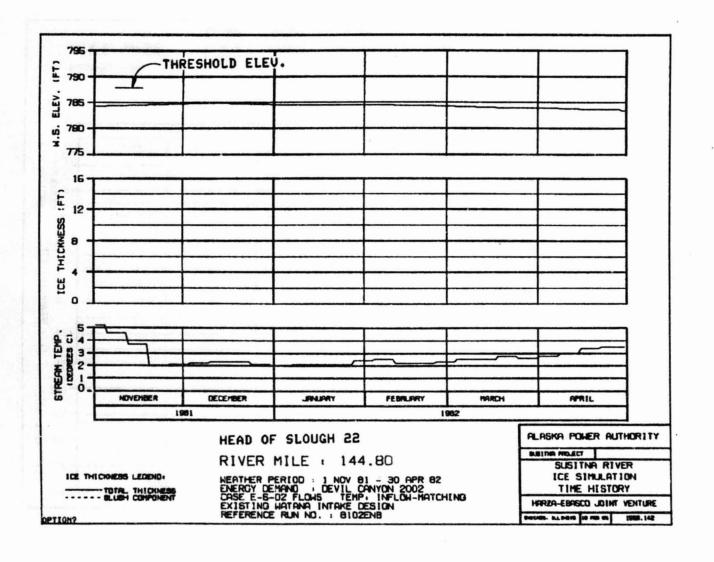




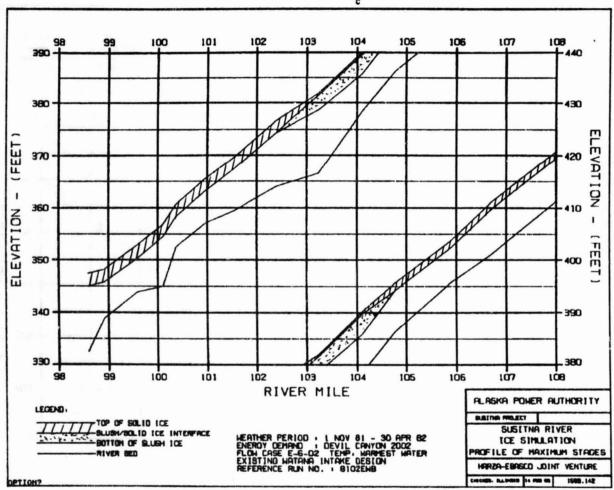




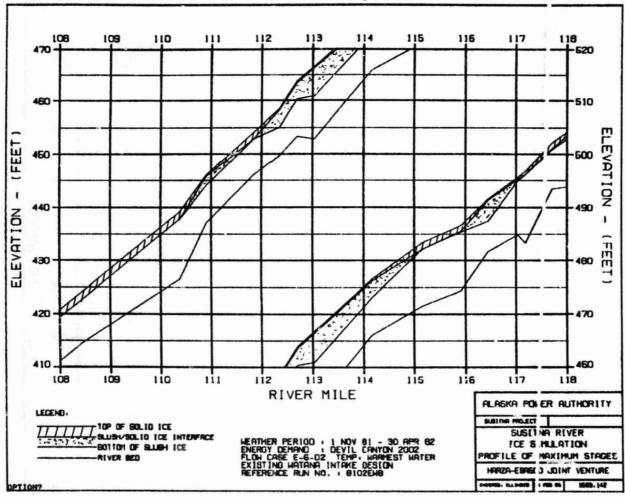




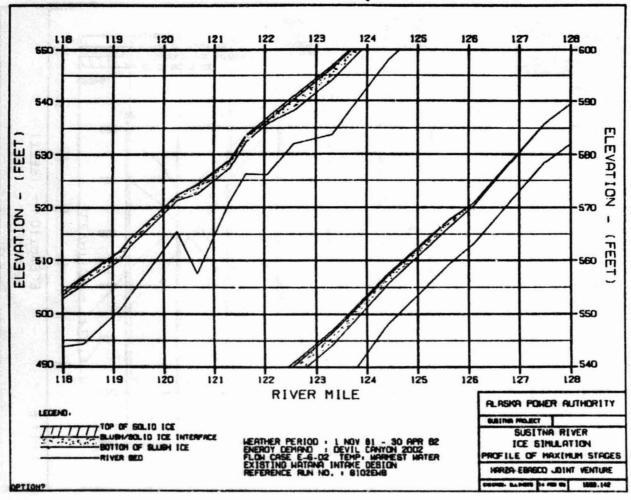
## EXHIBIT O



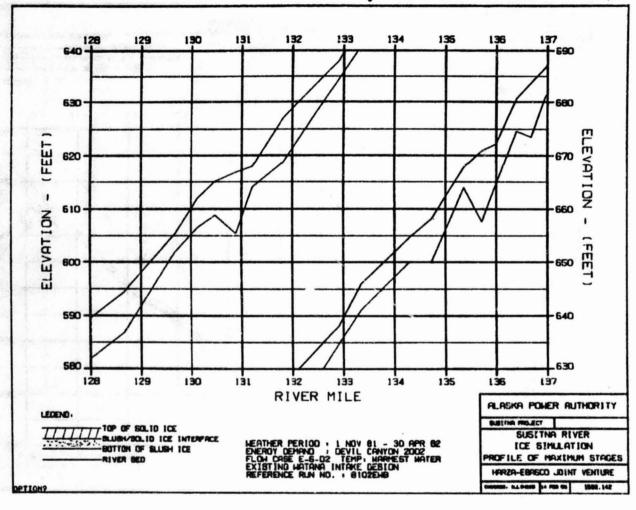


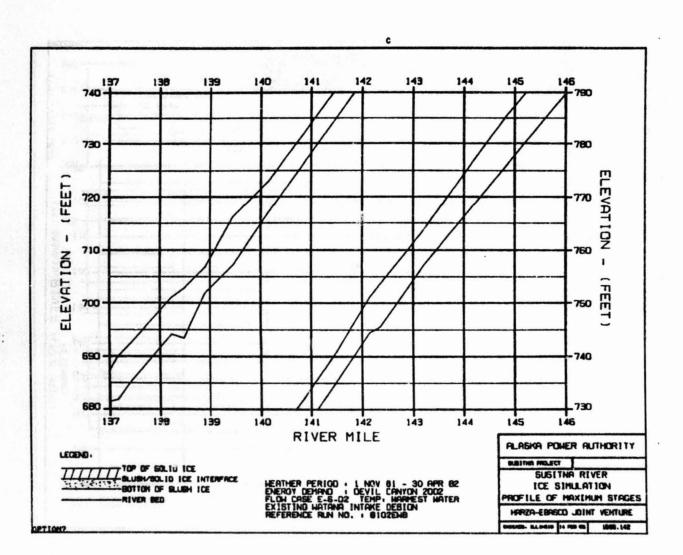


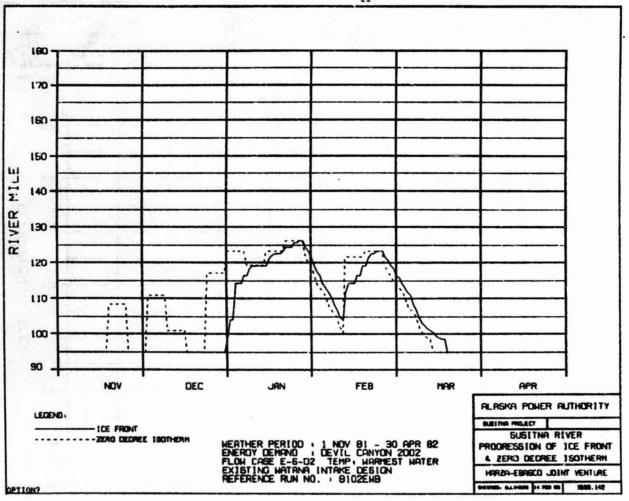


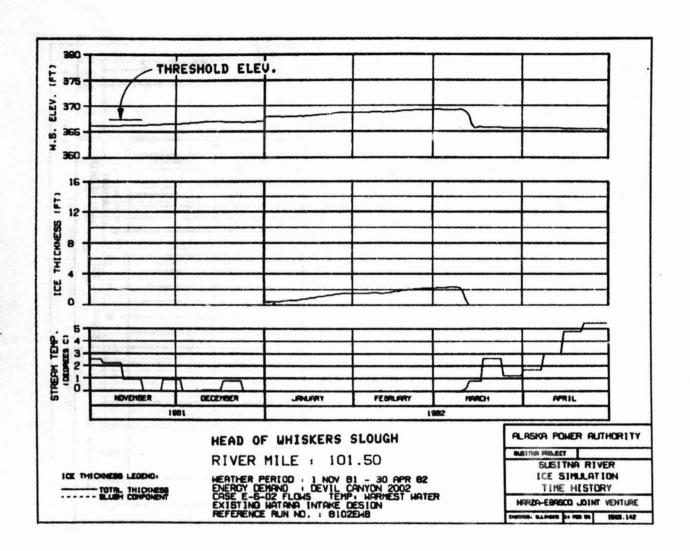


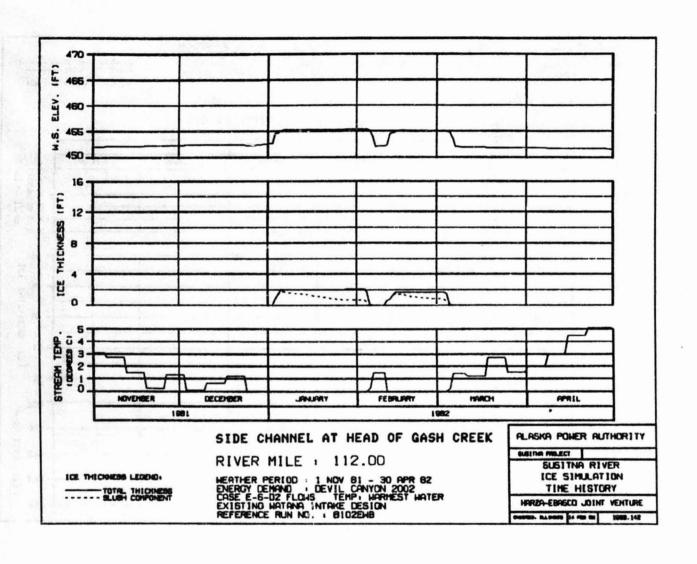


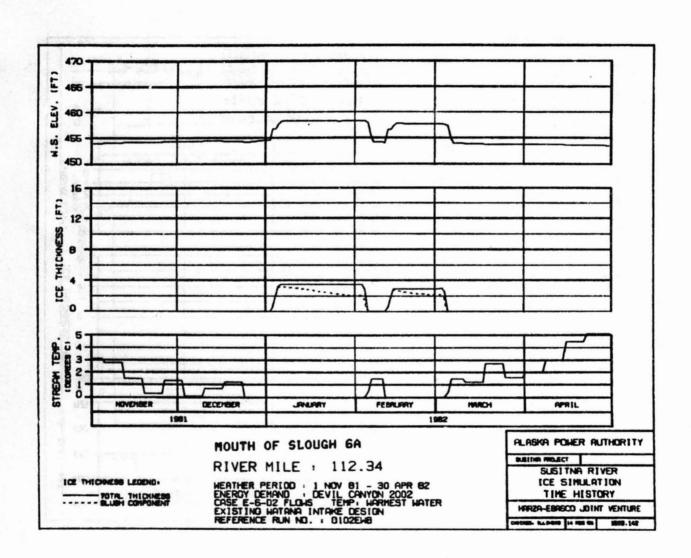


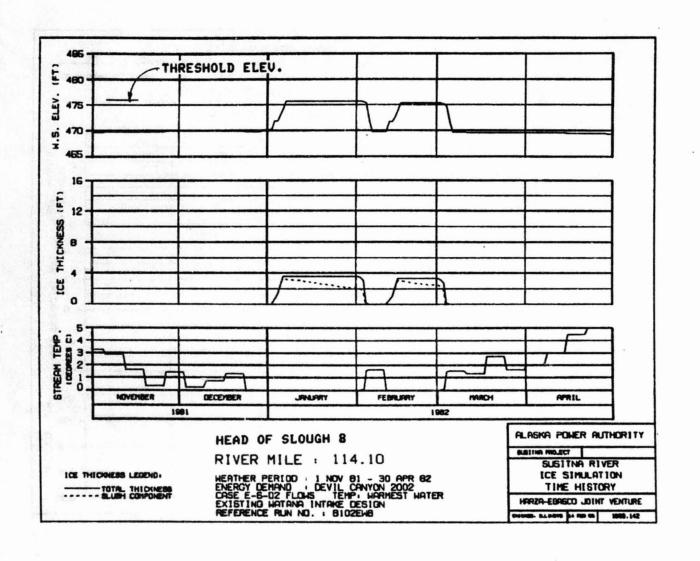


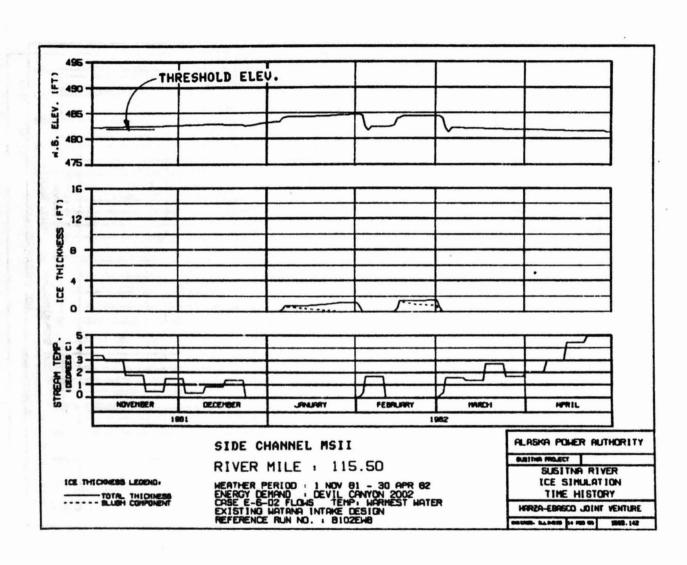


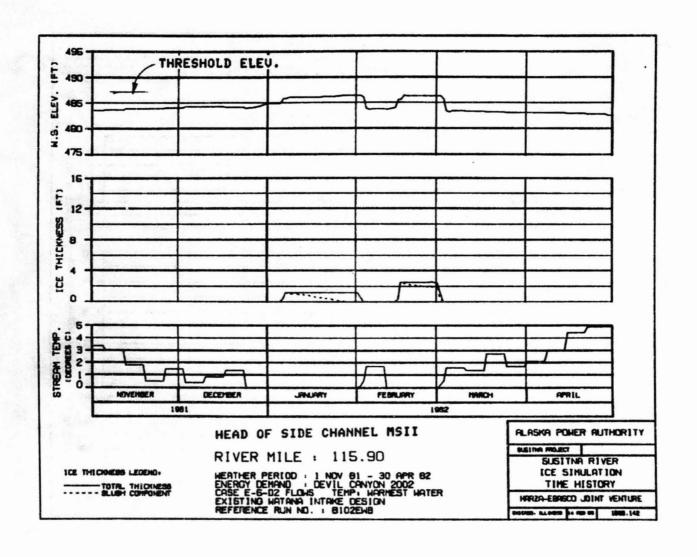


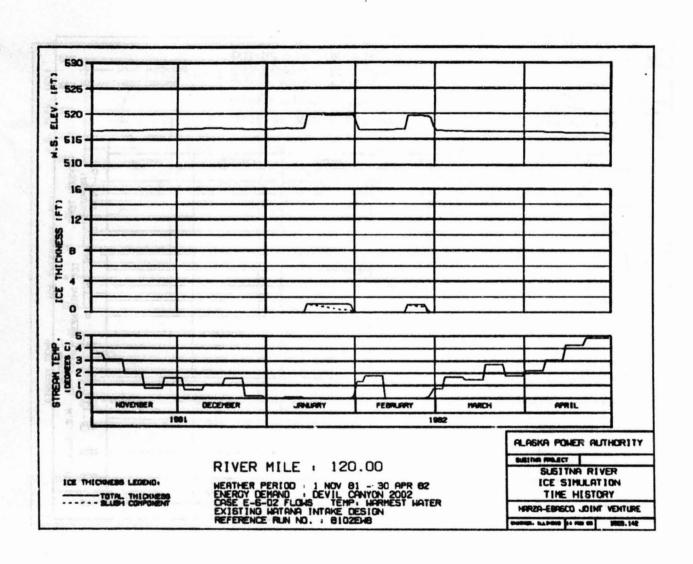


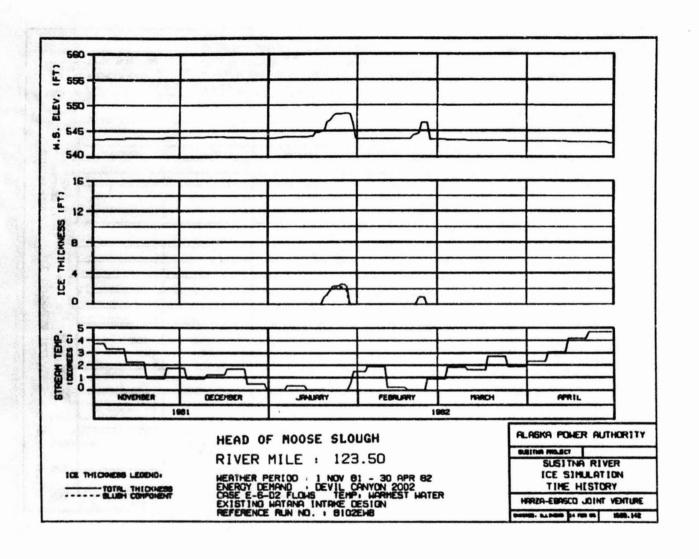


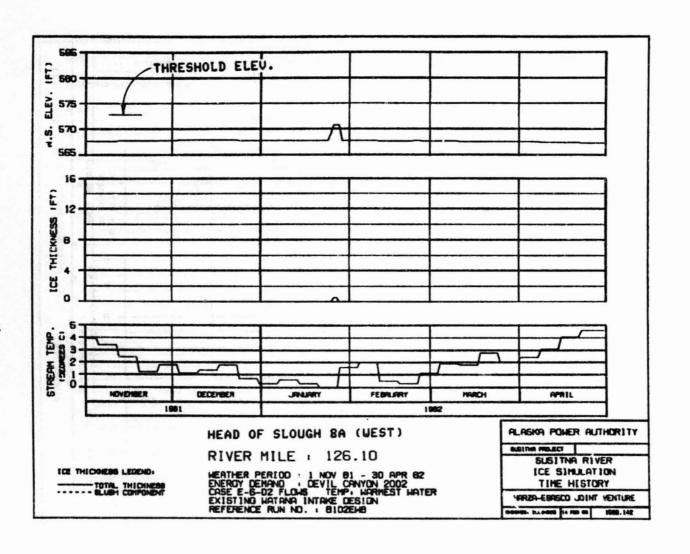


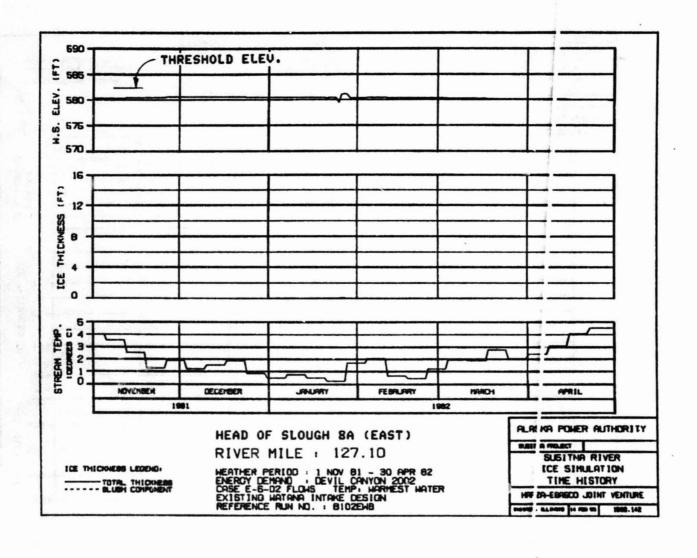


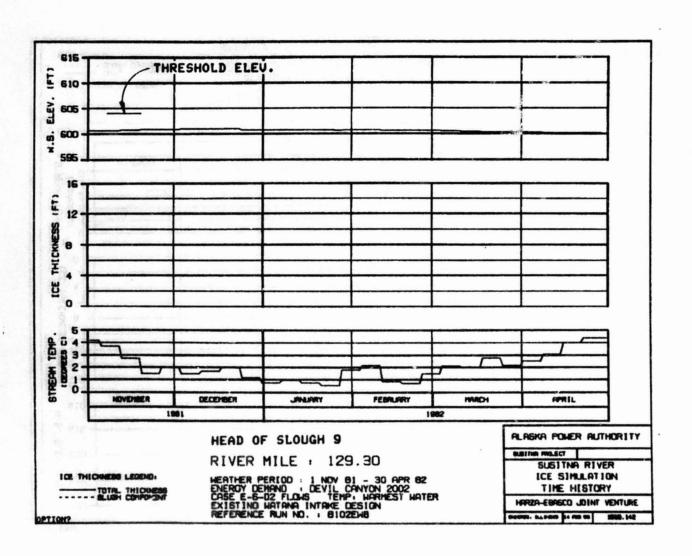


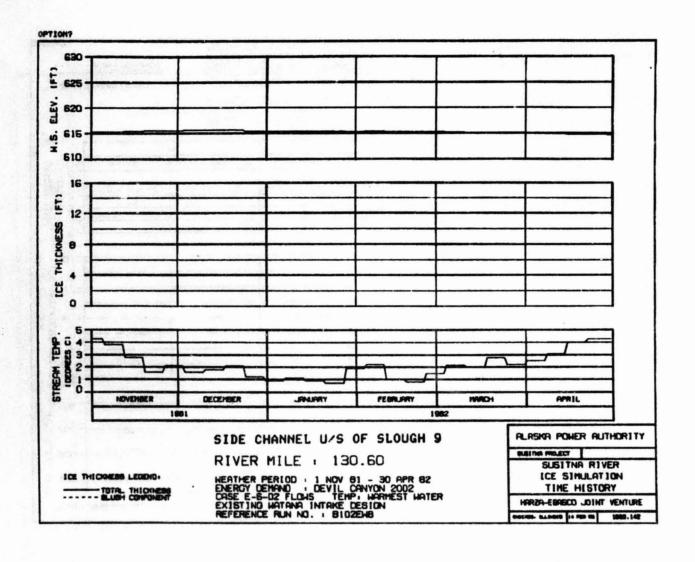


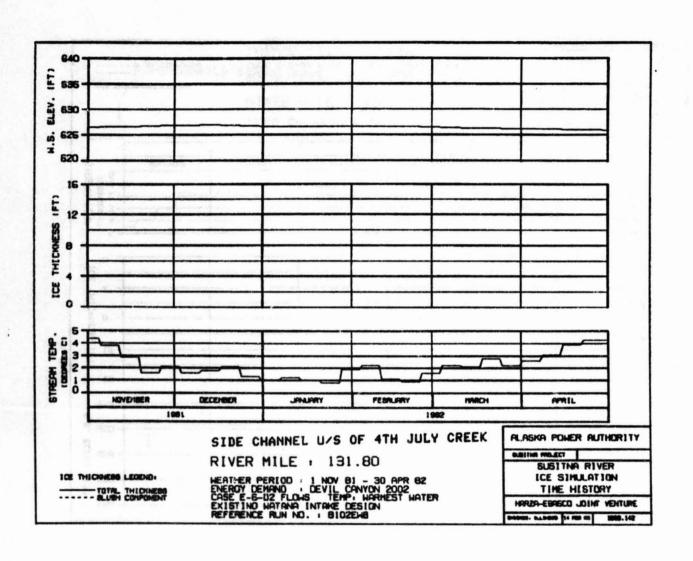


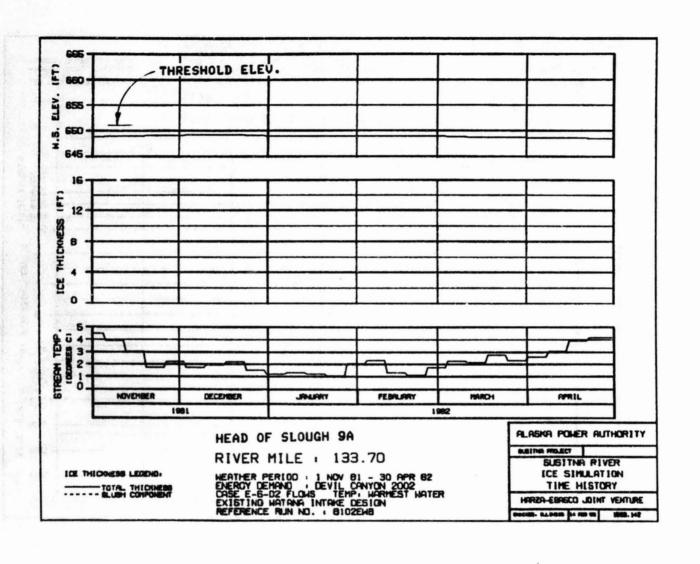




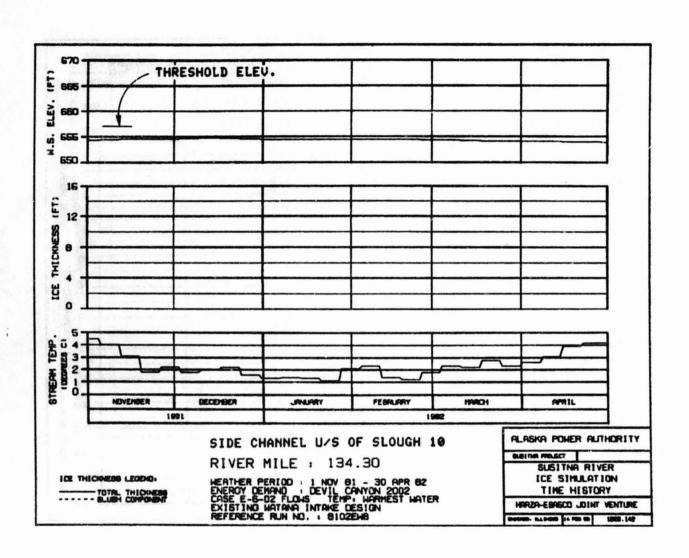


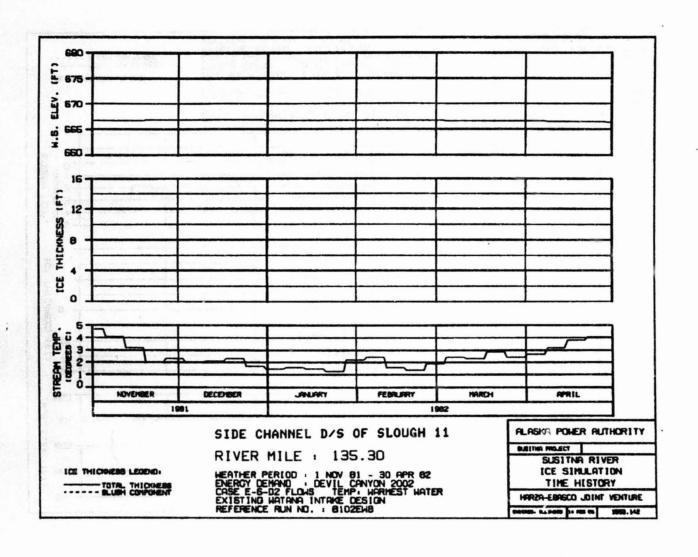


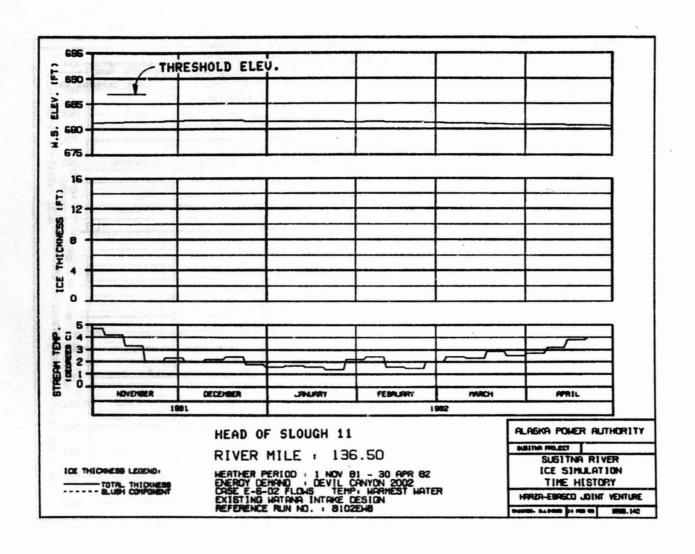


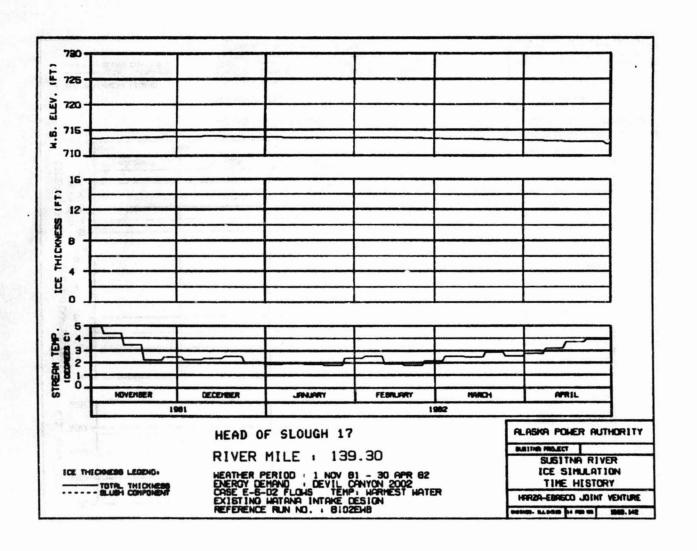


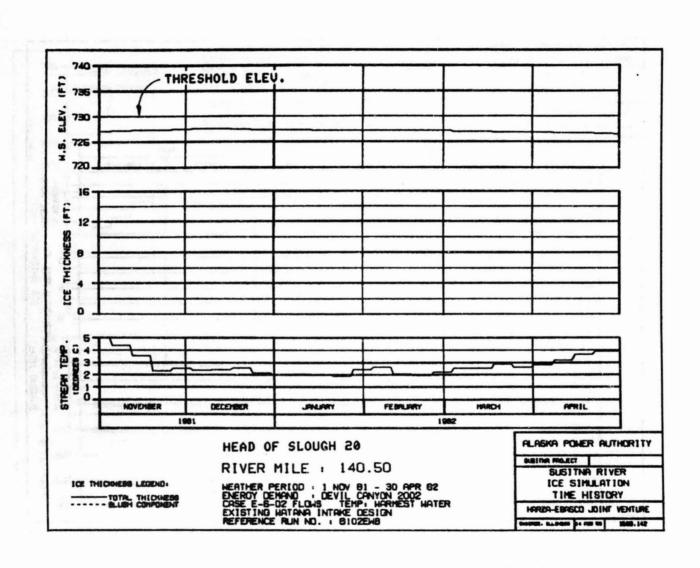
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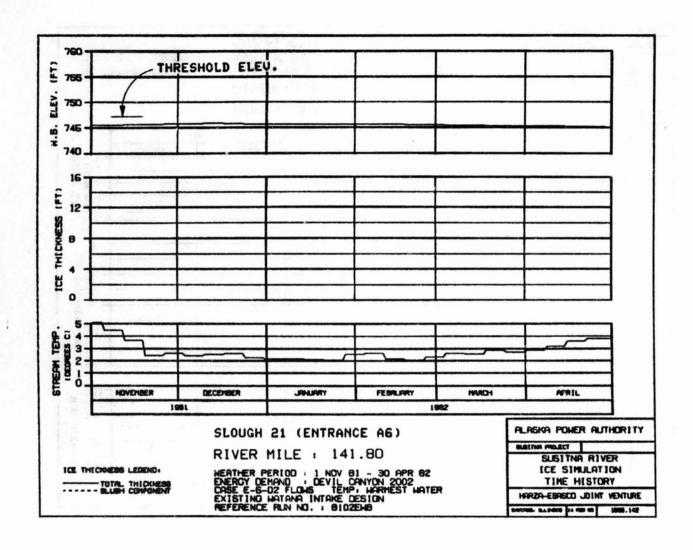


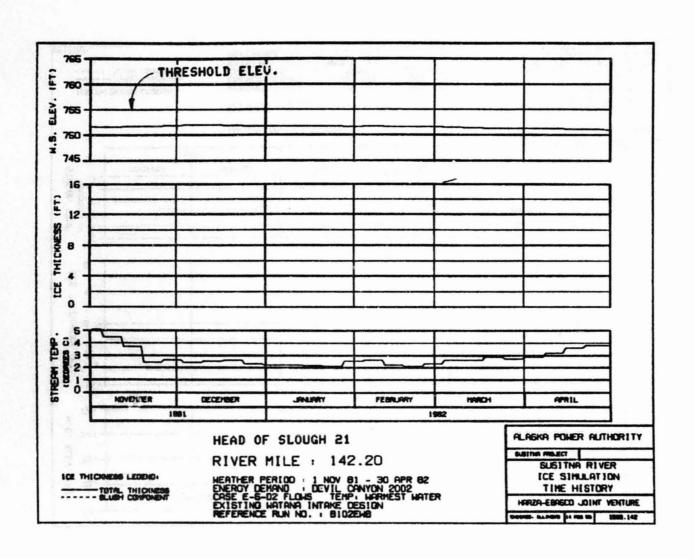


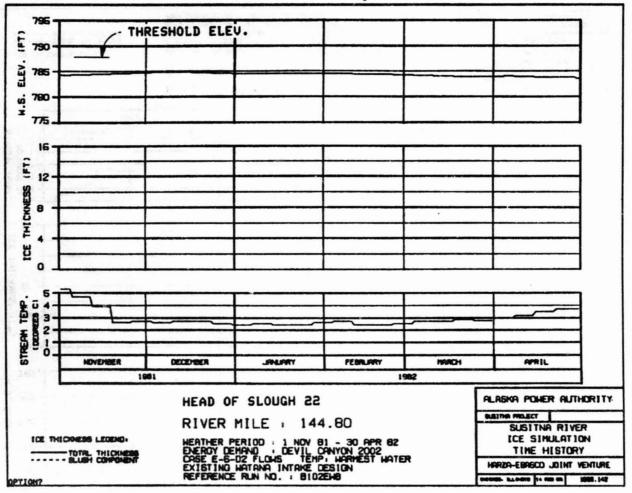






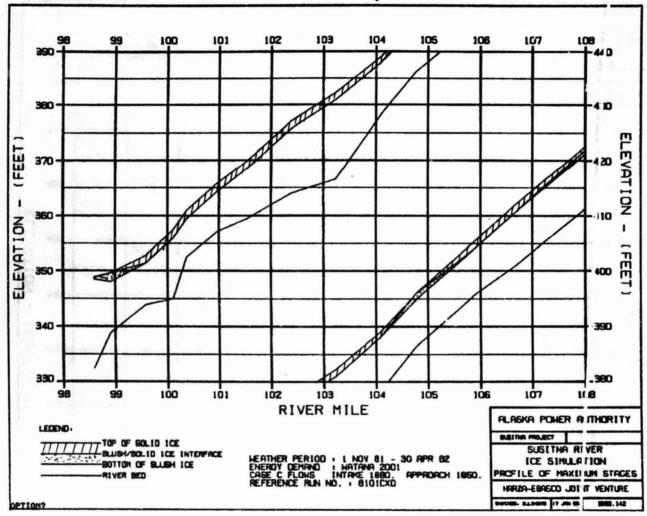


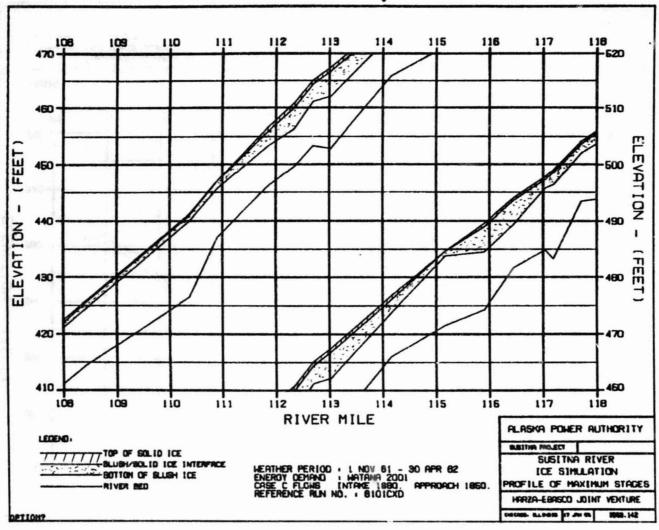




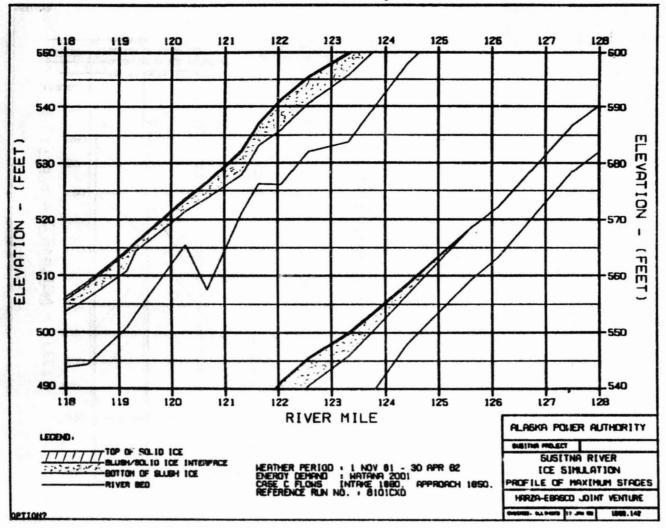
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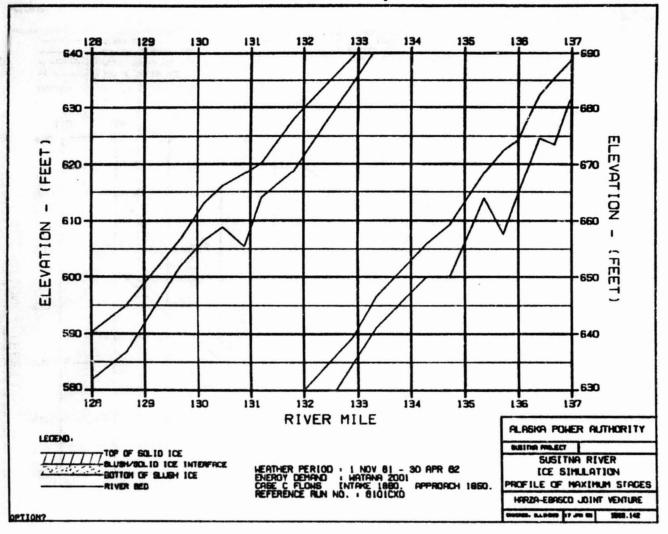




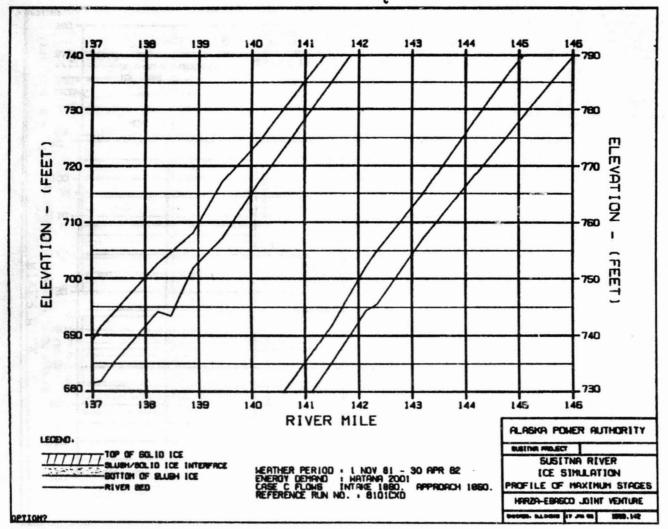


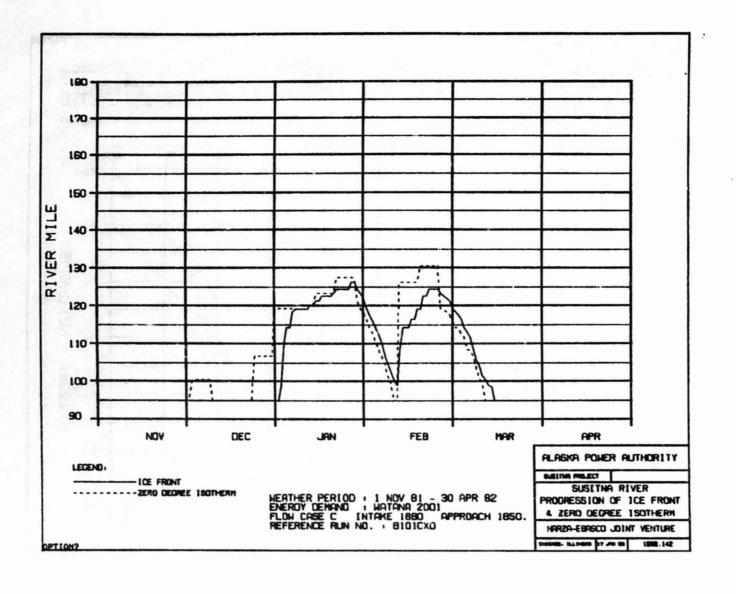


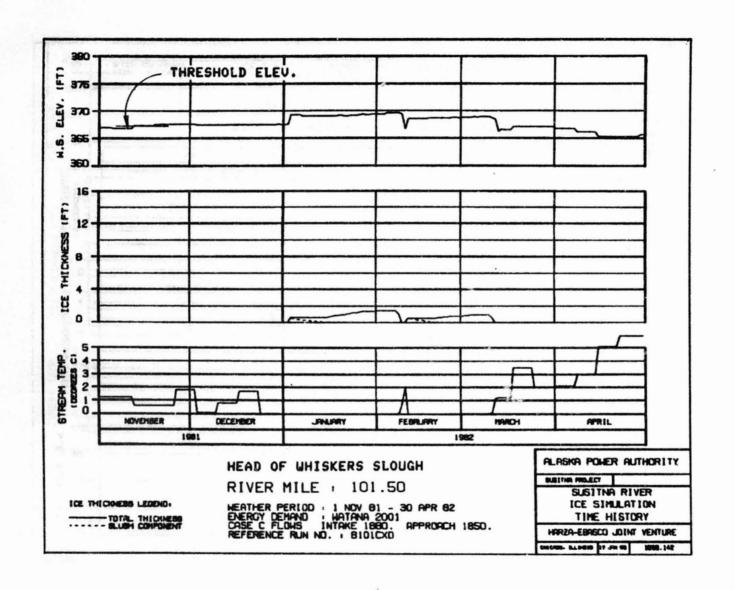


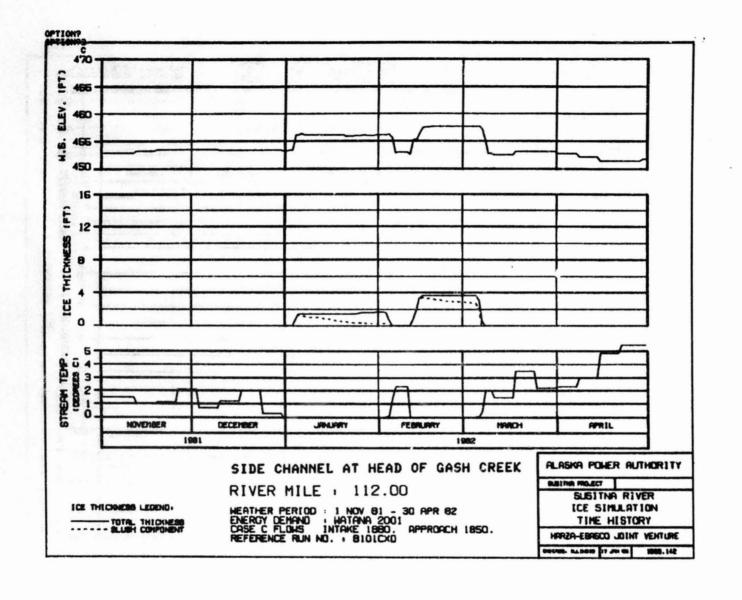


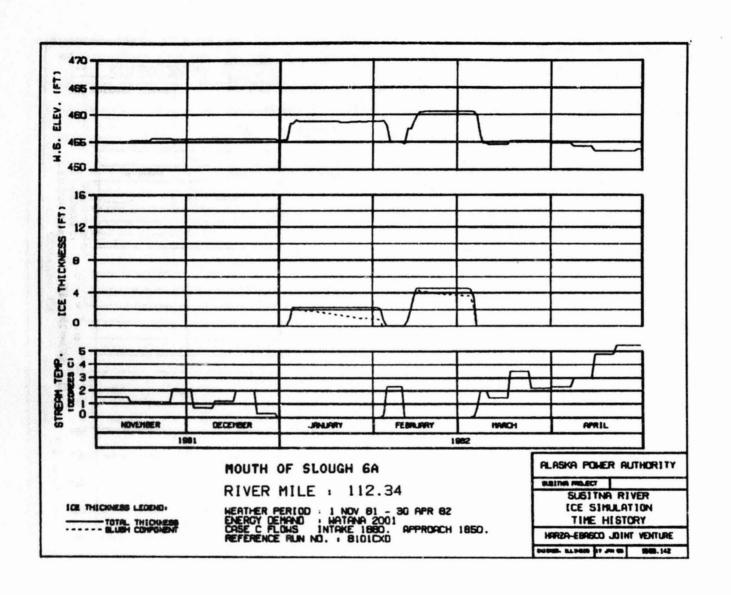


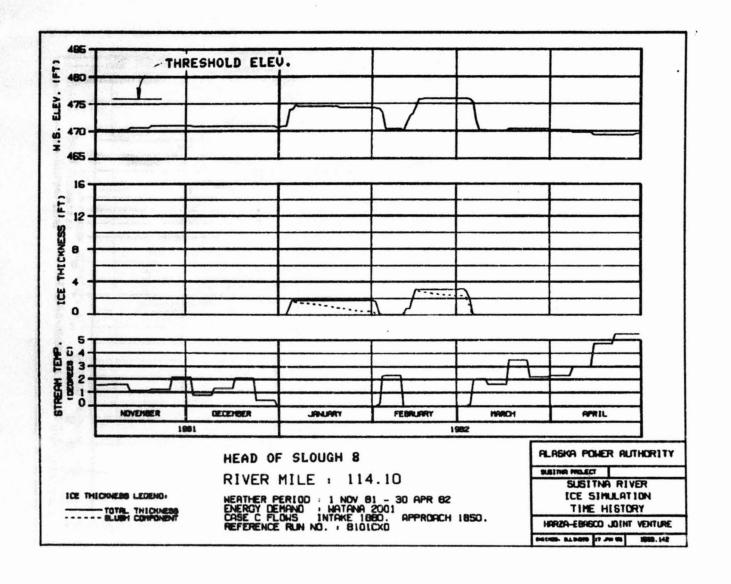


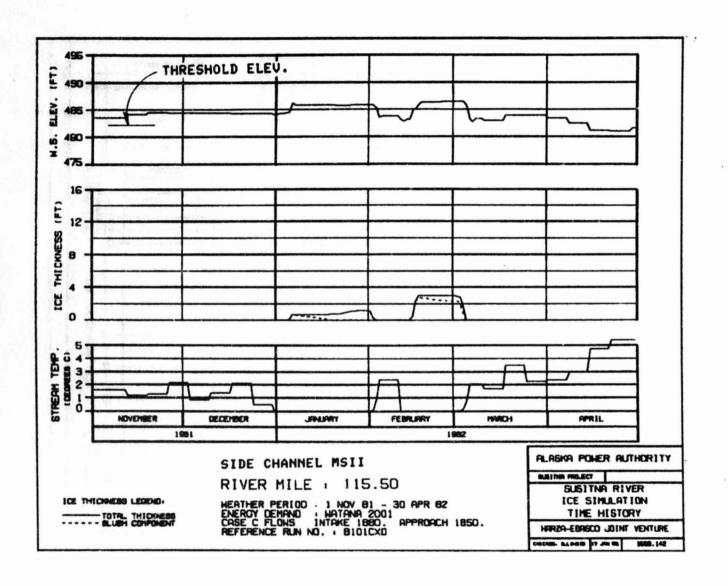


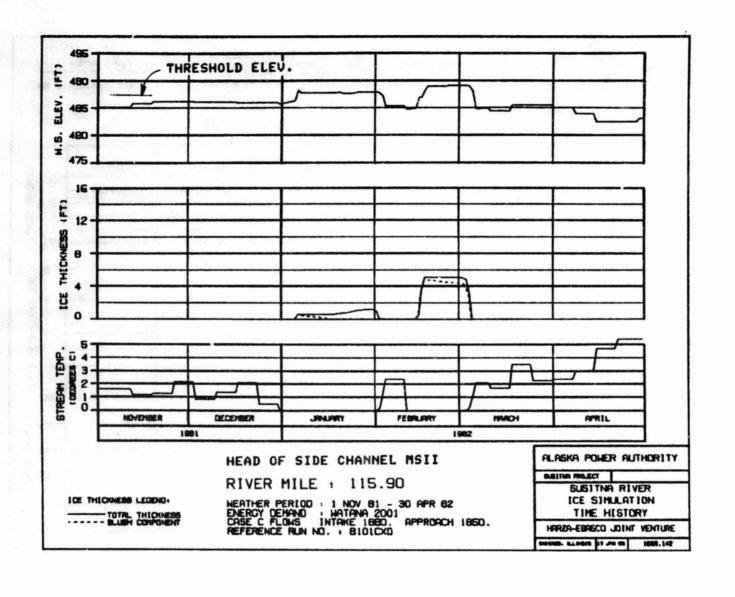


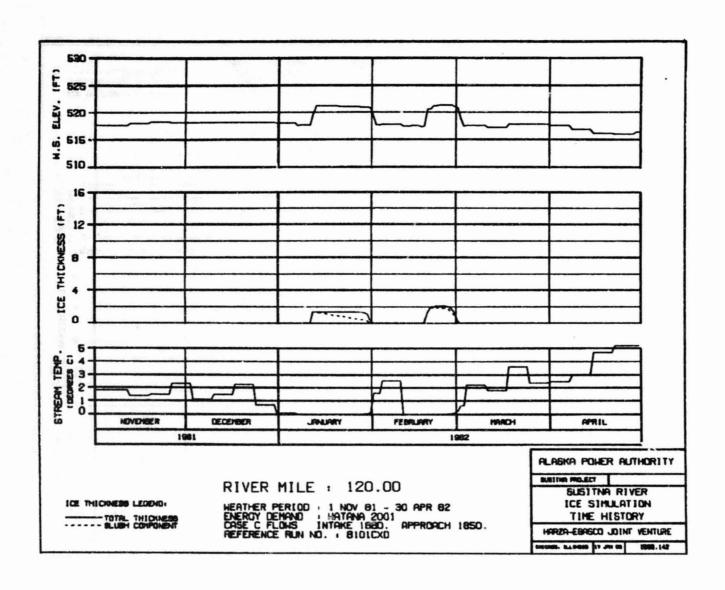


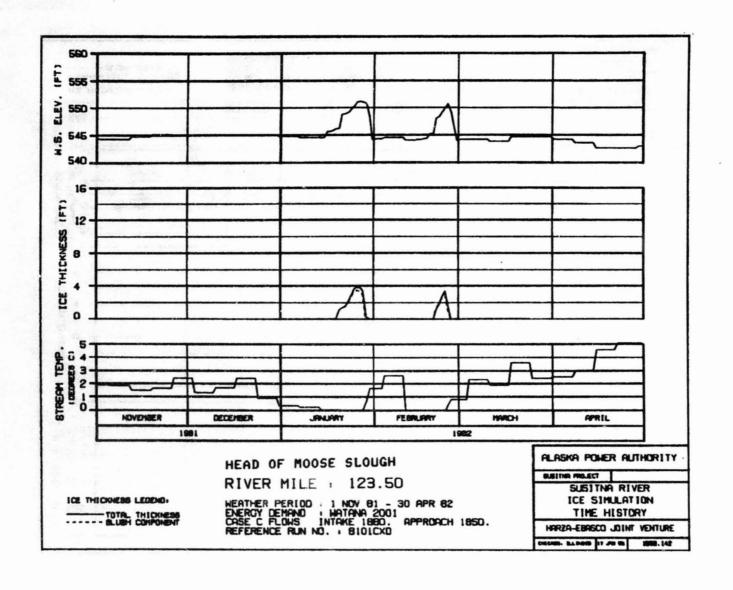


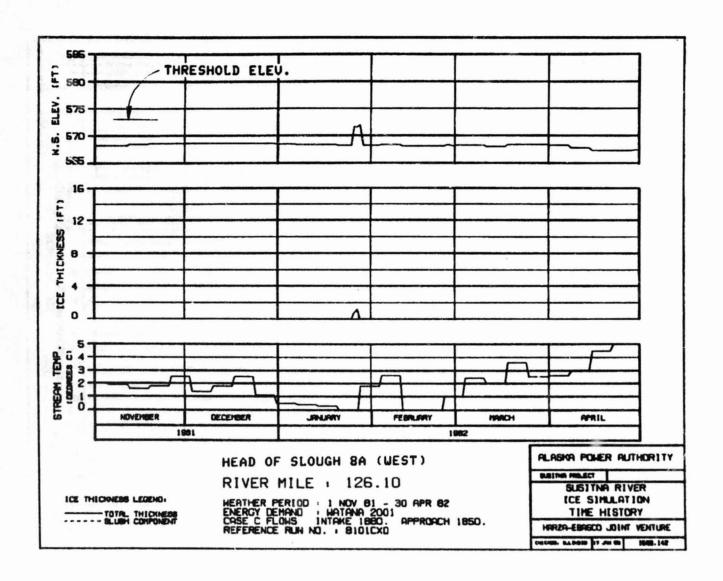


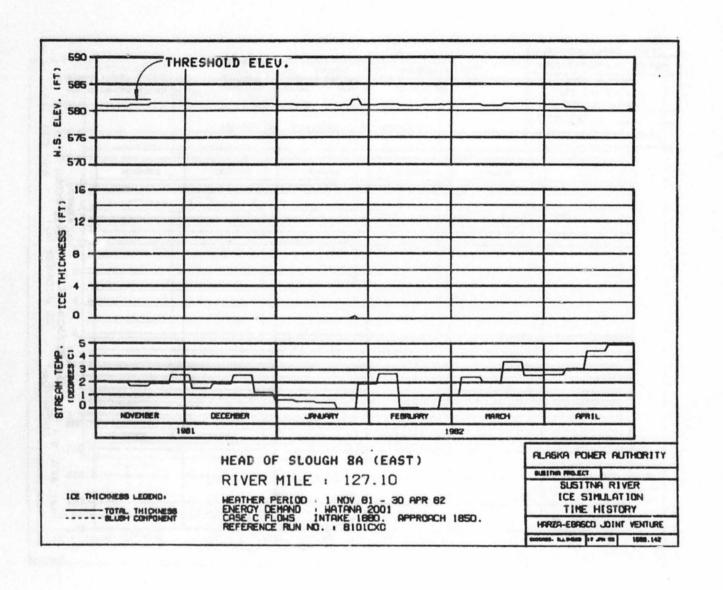


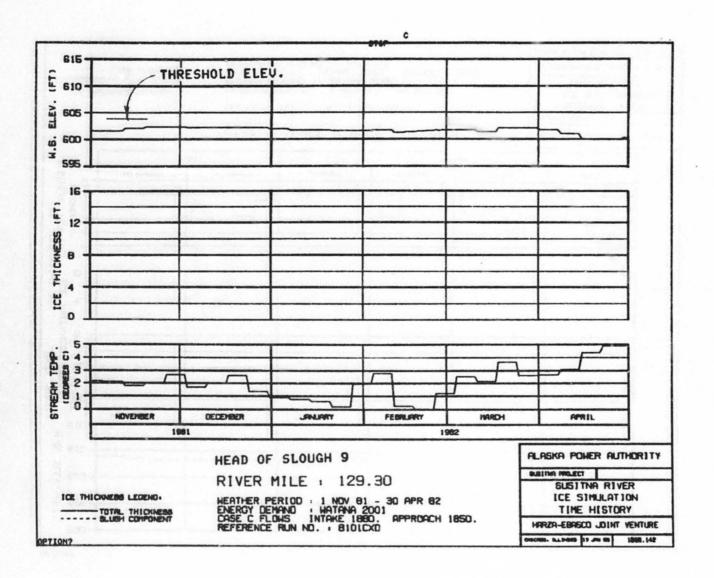


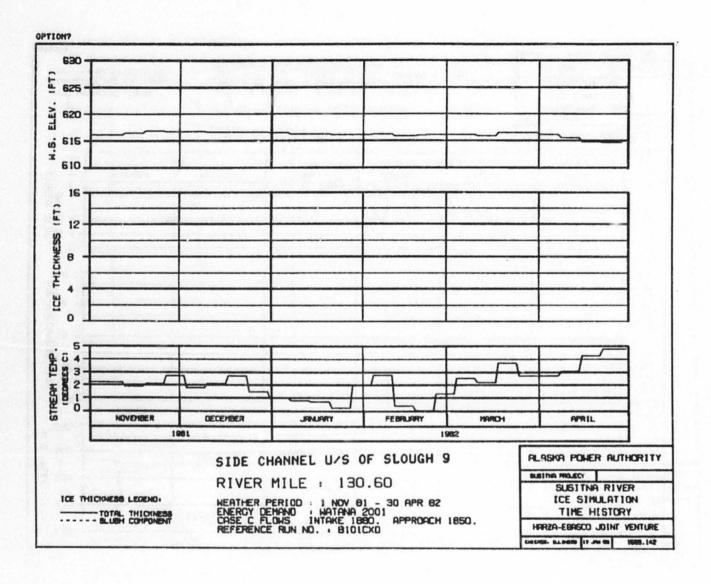


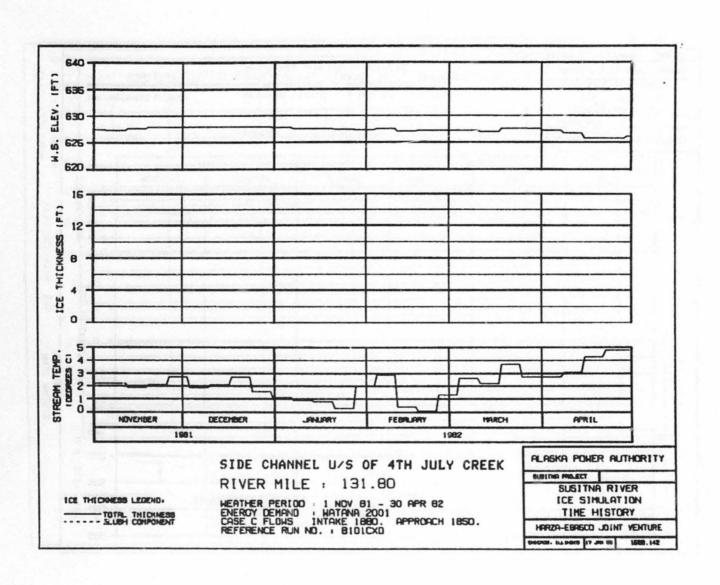


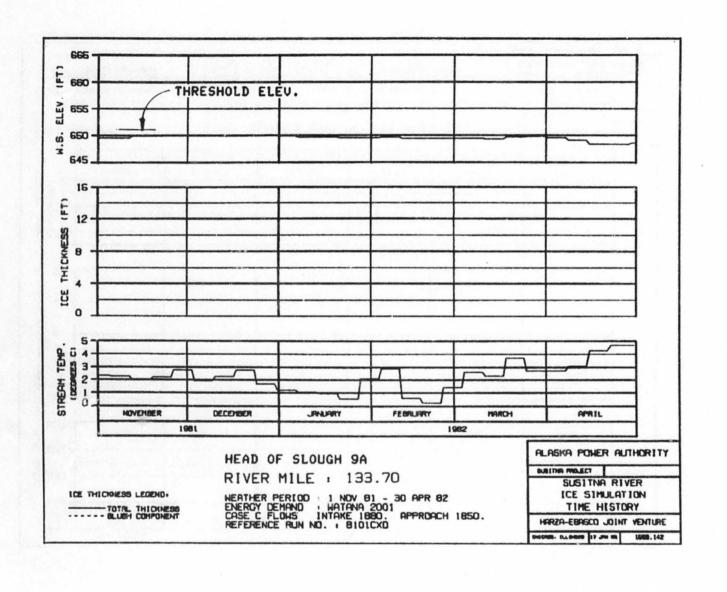


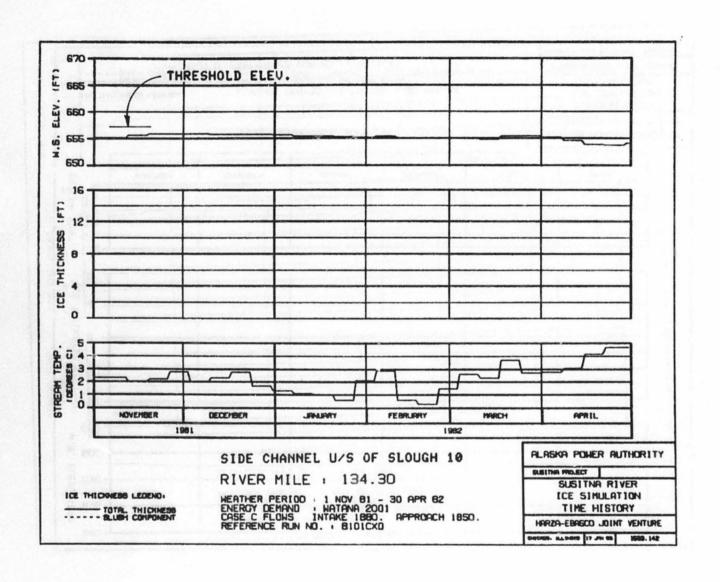


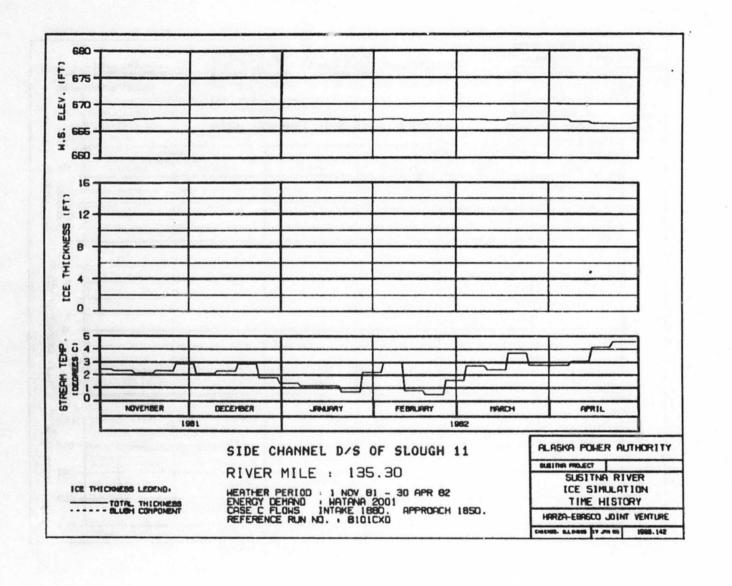


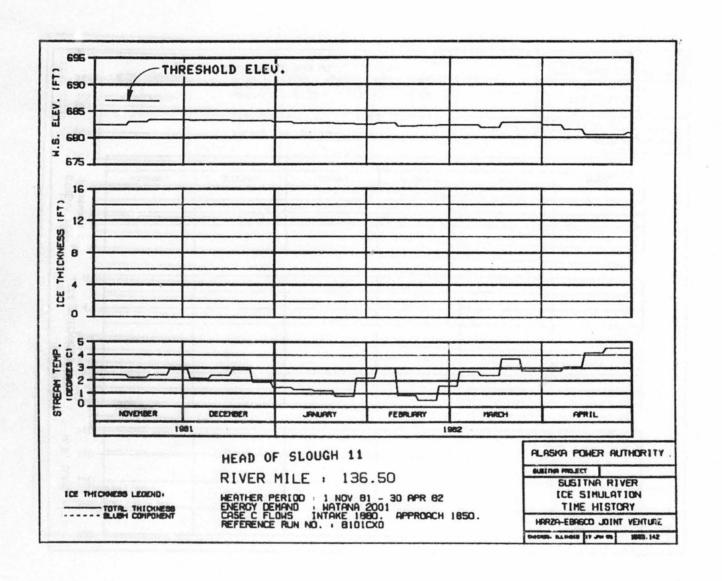


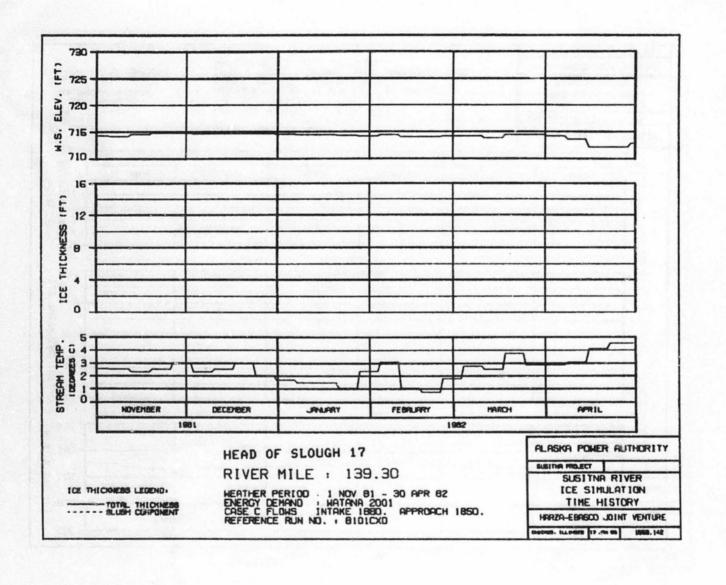




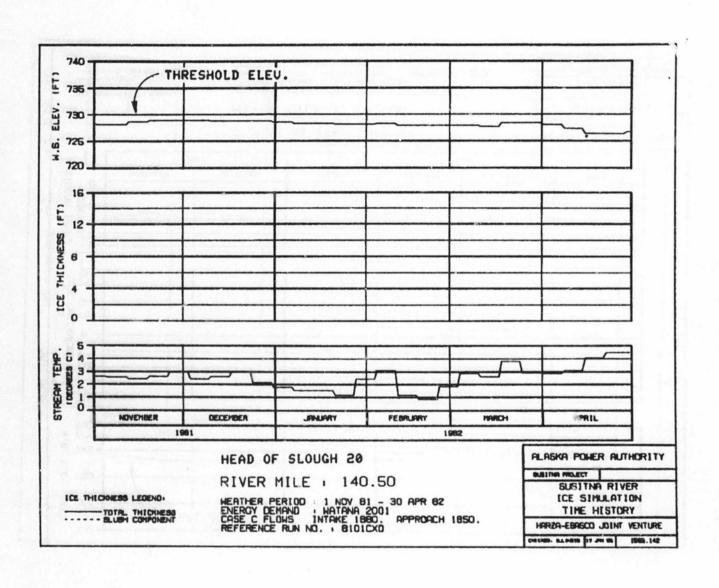


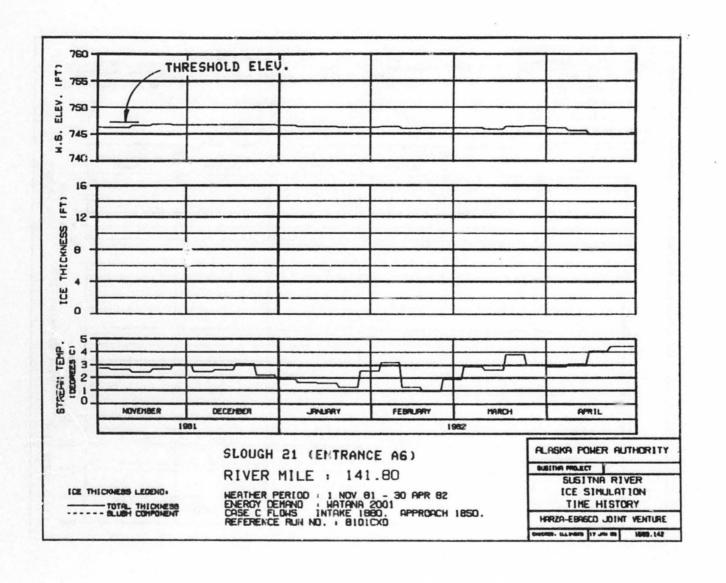




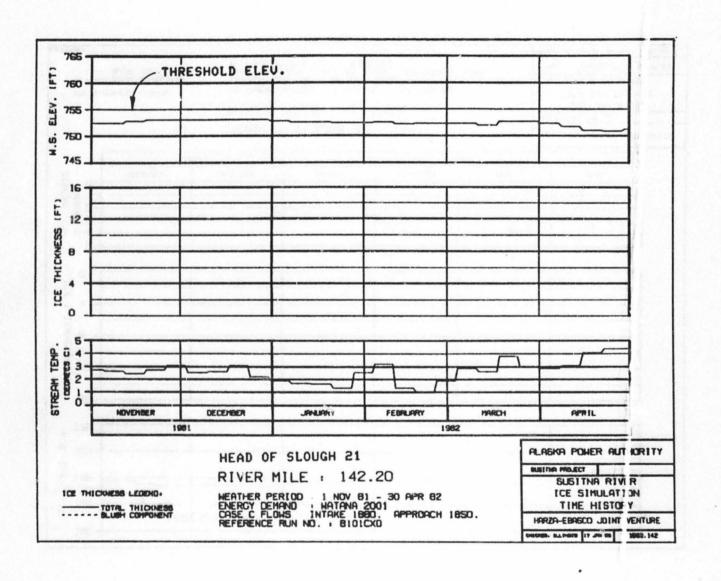


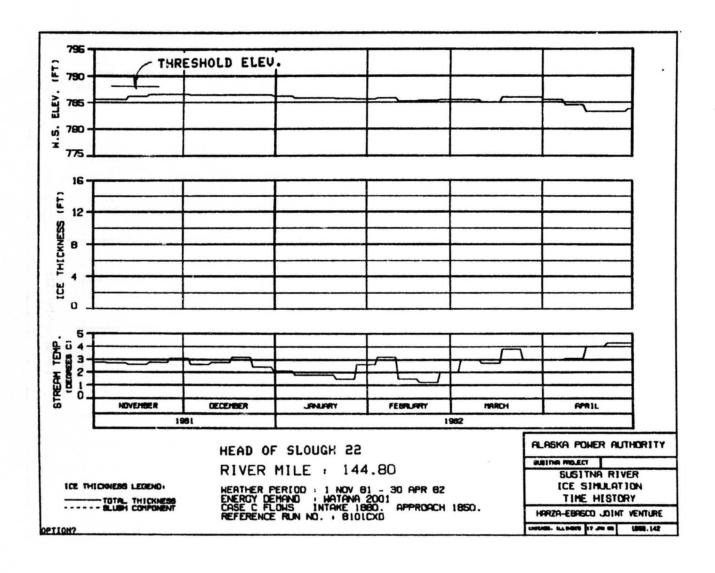
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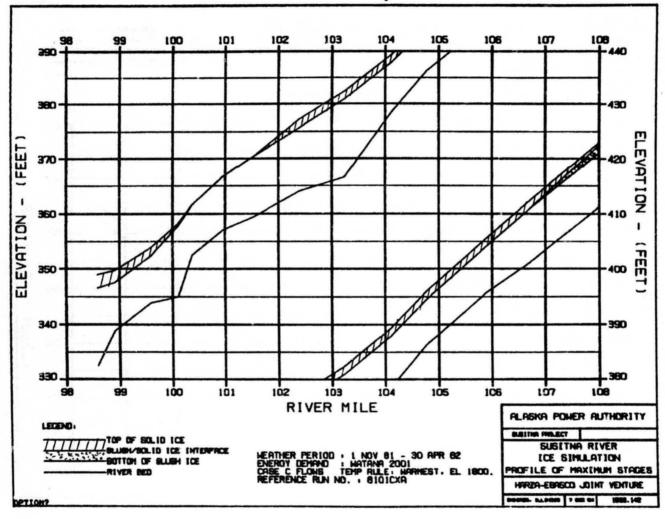


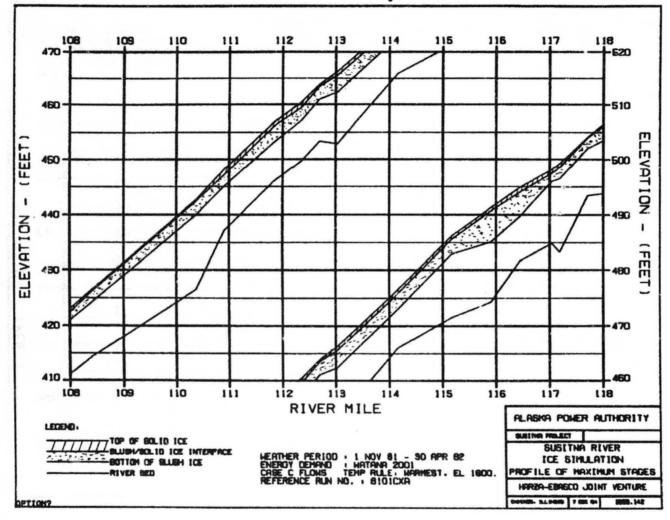


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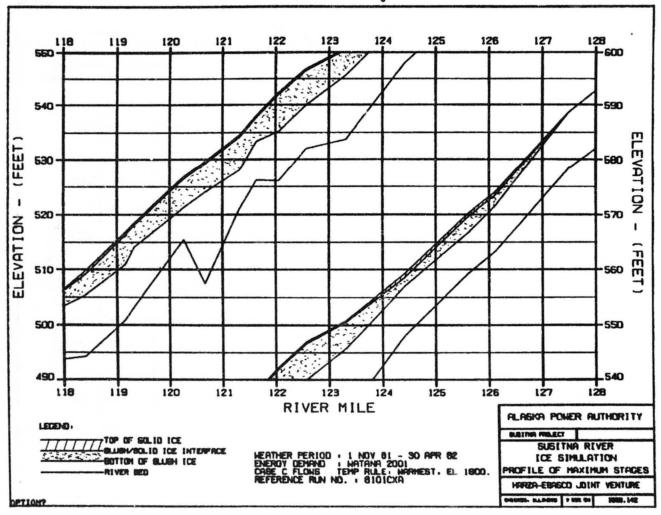
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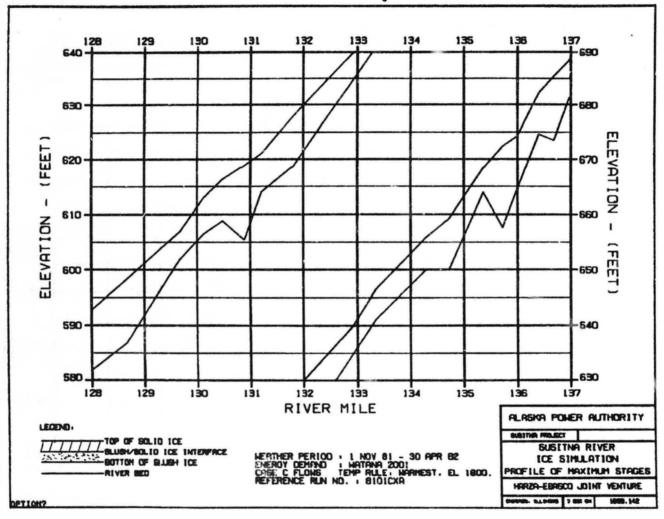


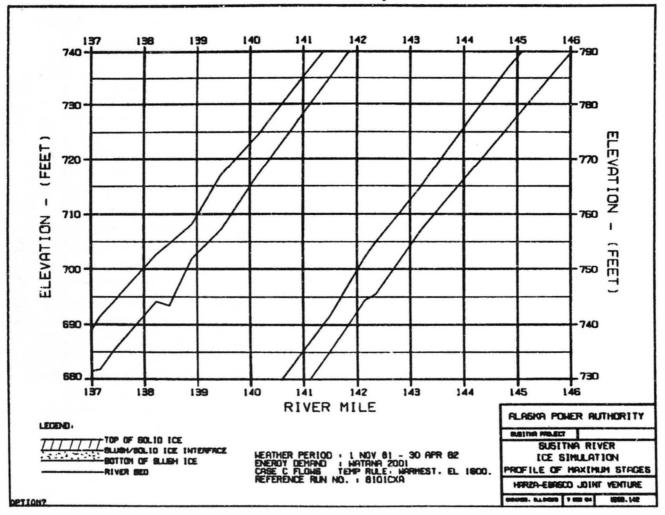


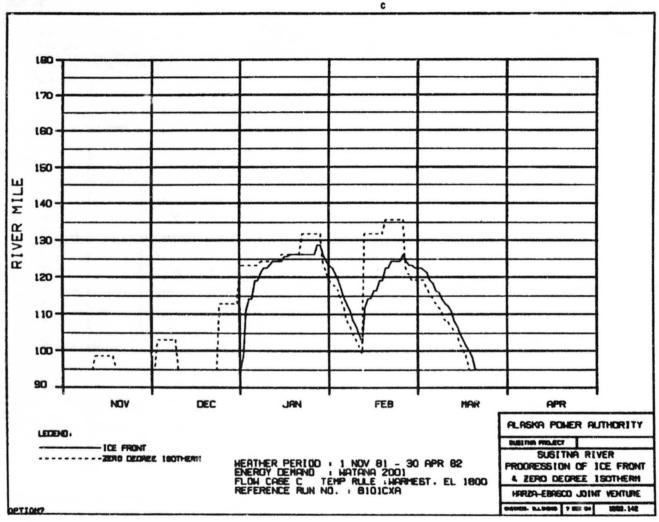


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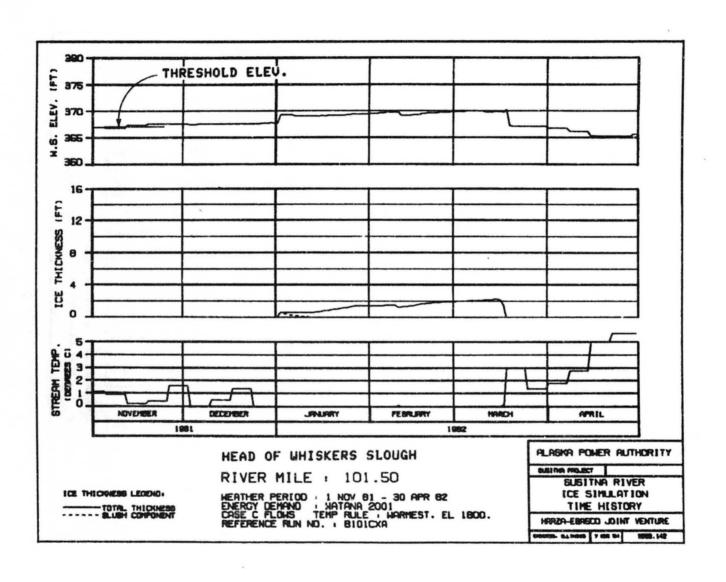


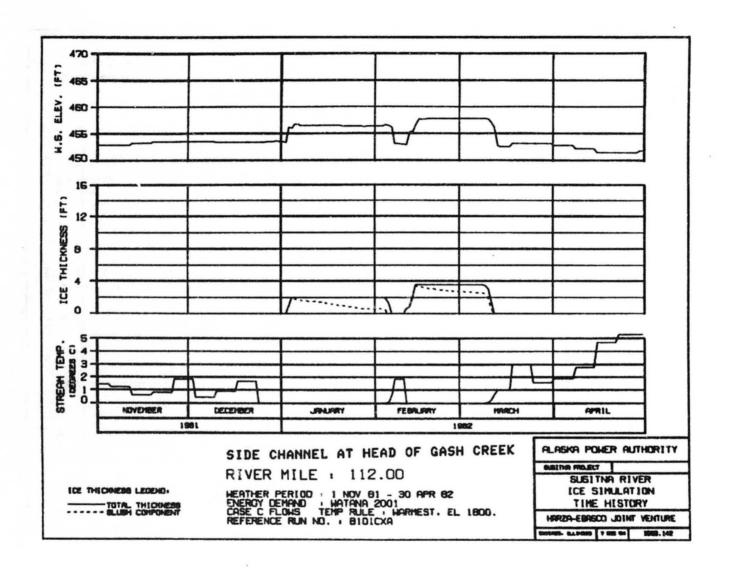


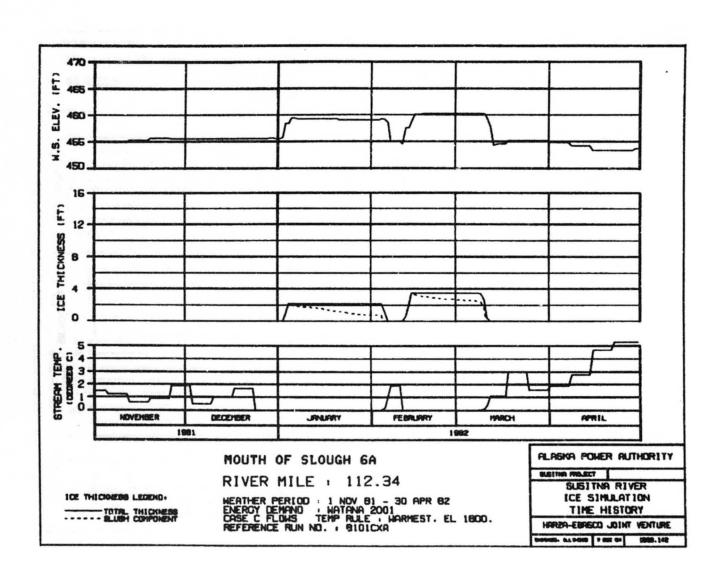


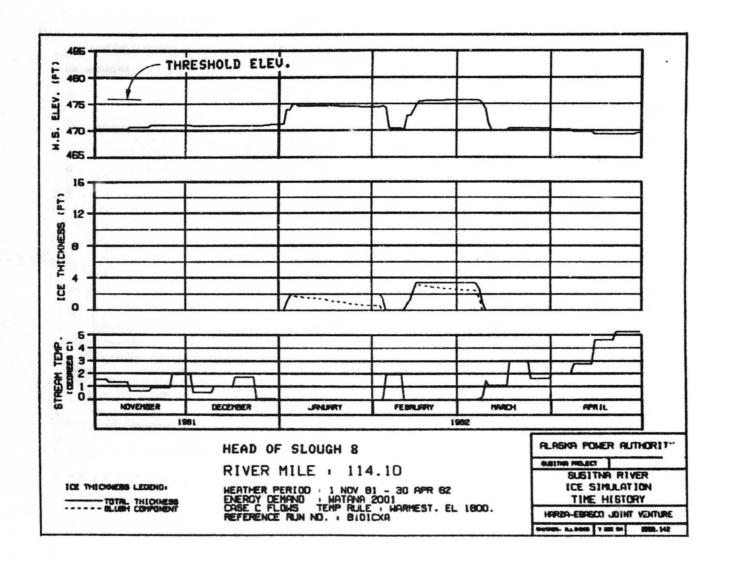


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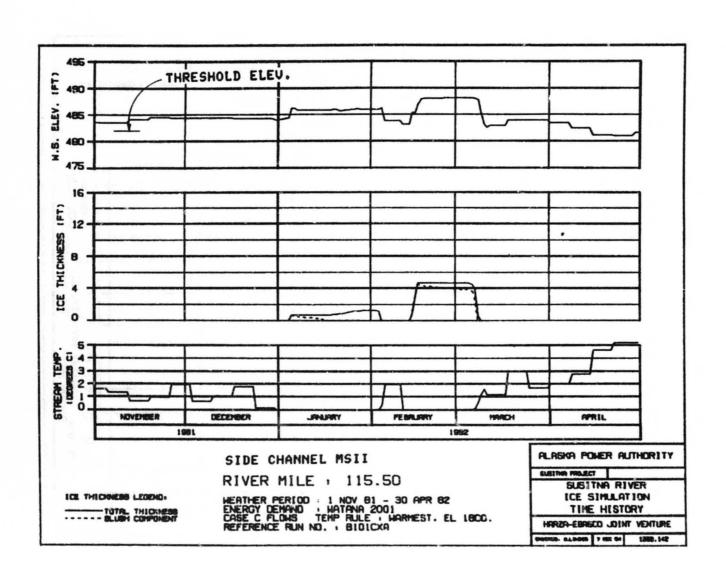


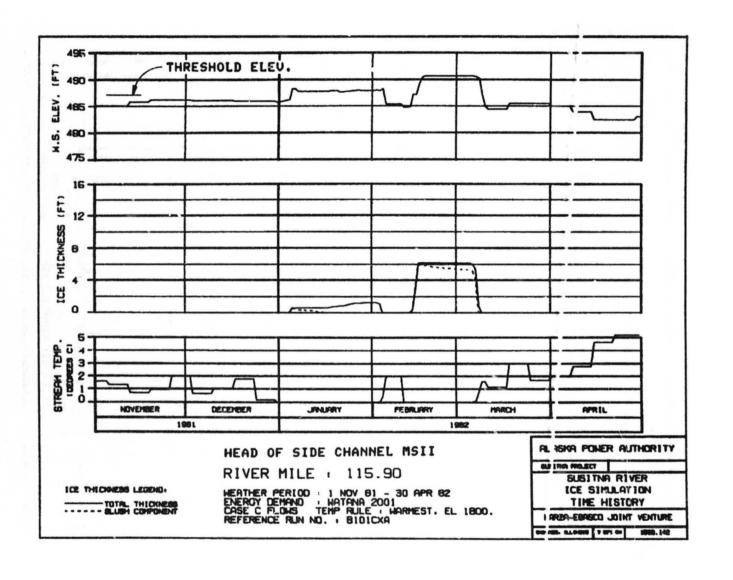


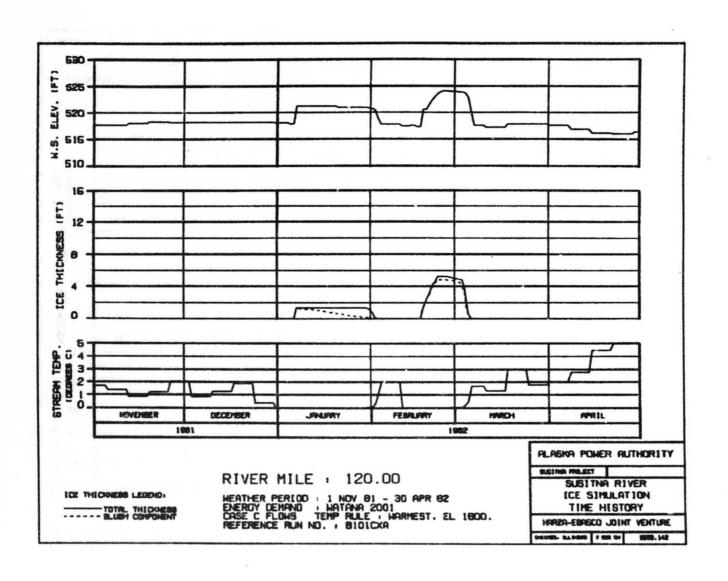


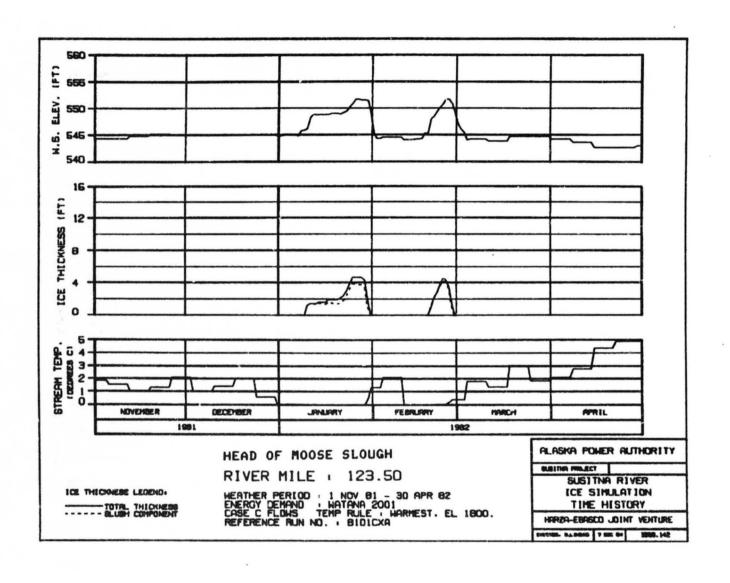


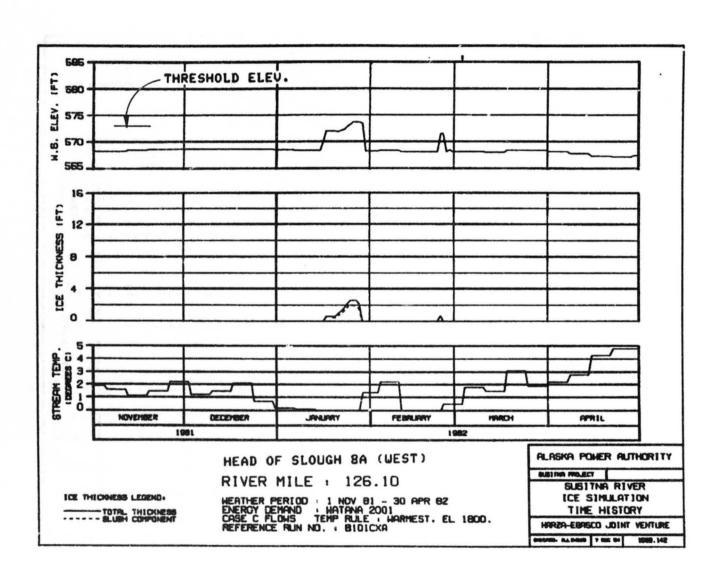
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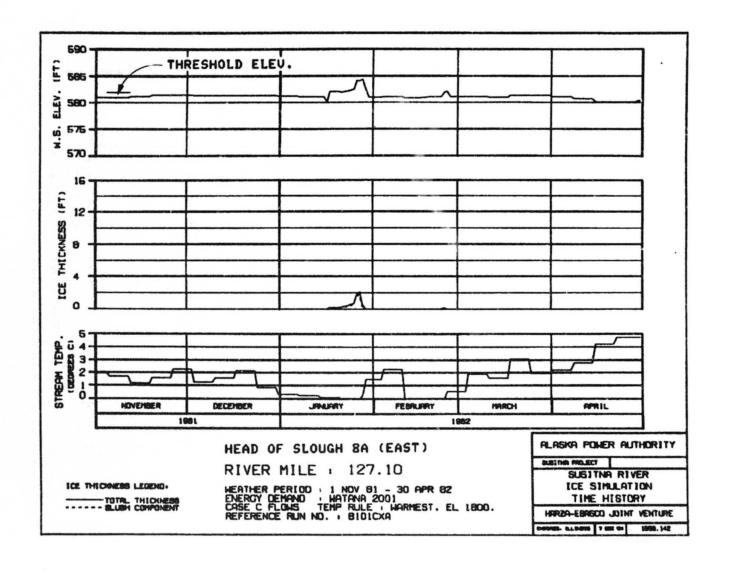




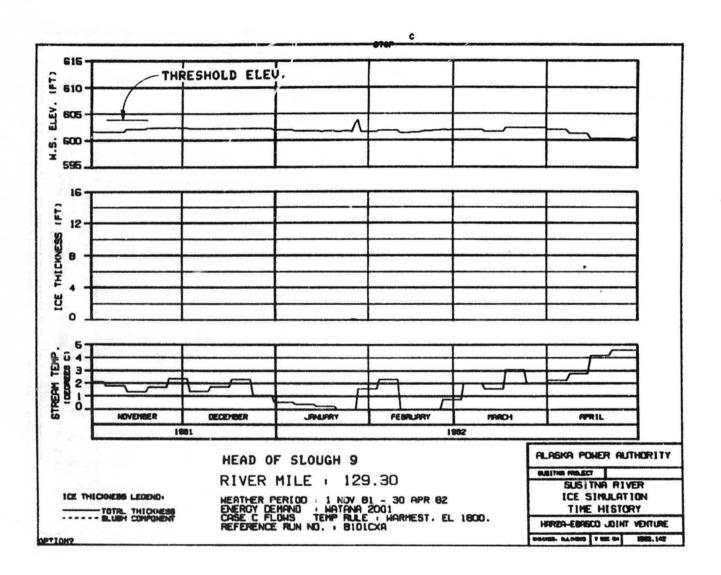


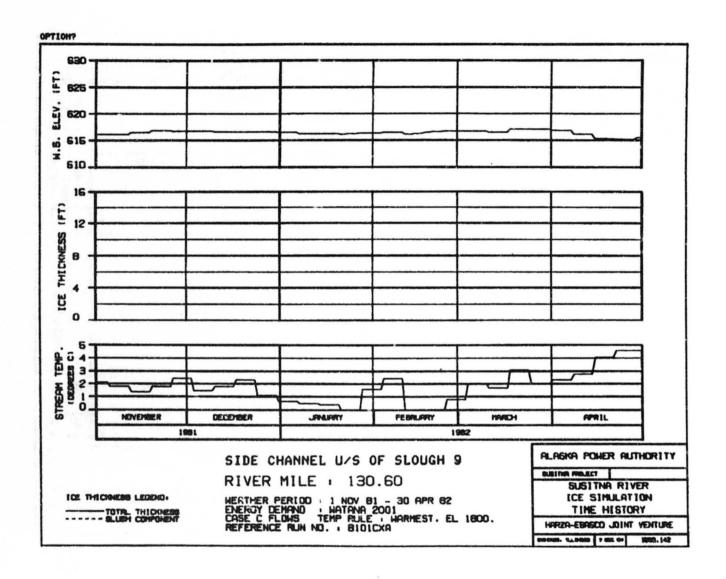


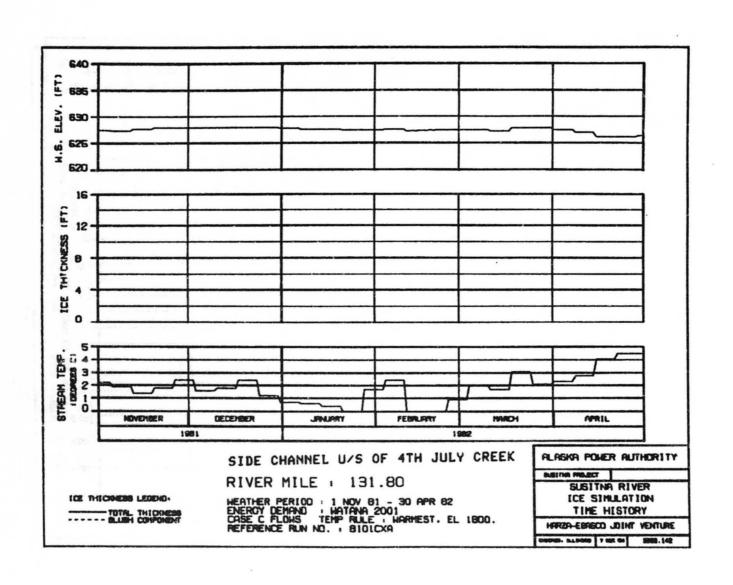


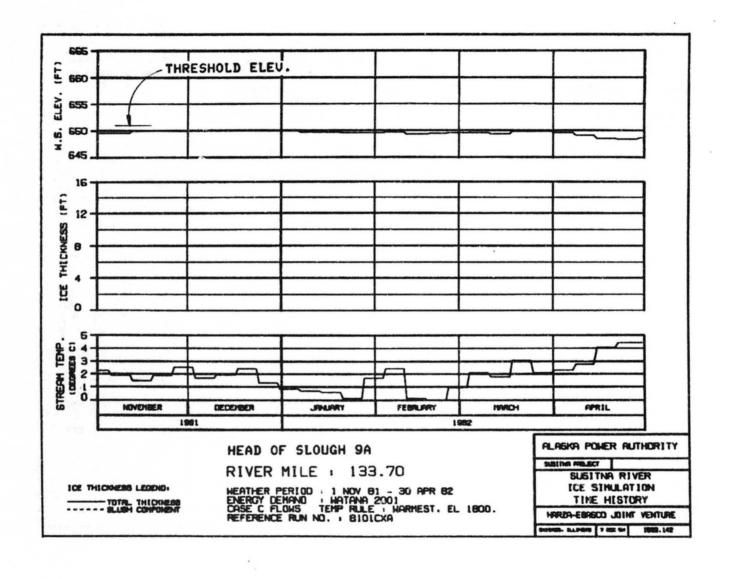


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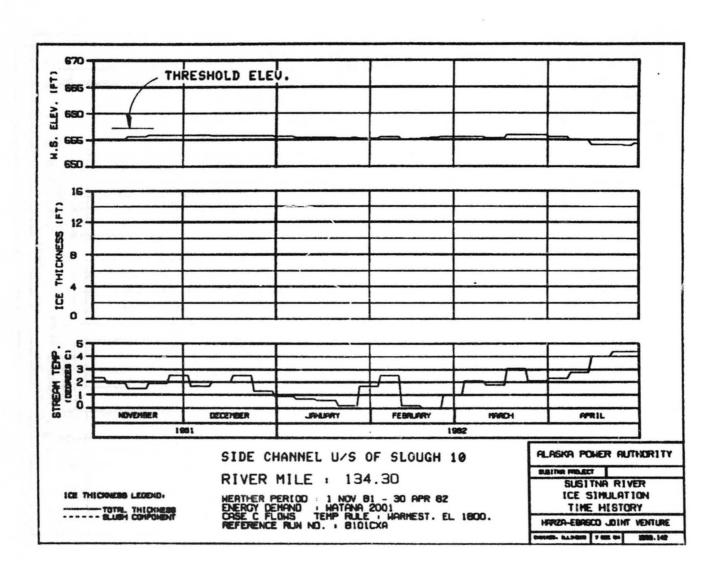


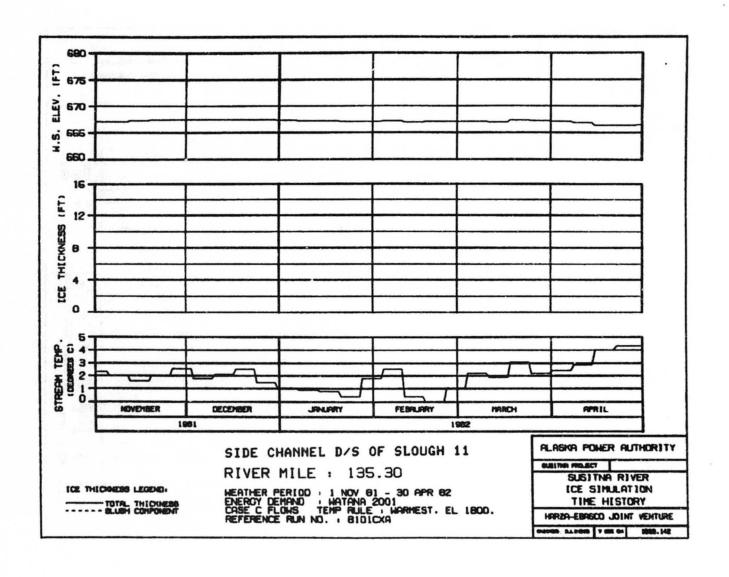


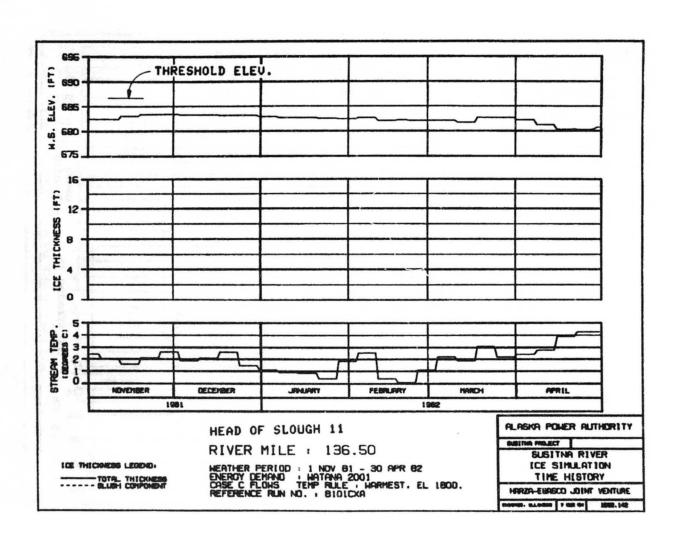


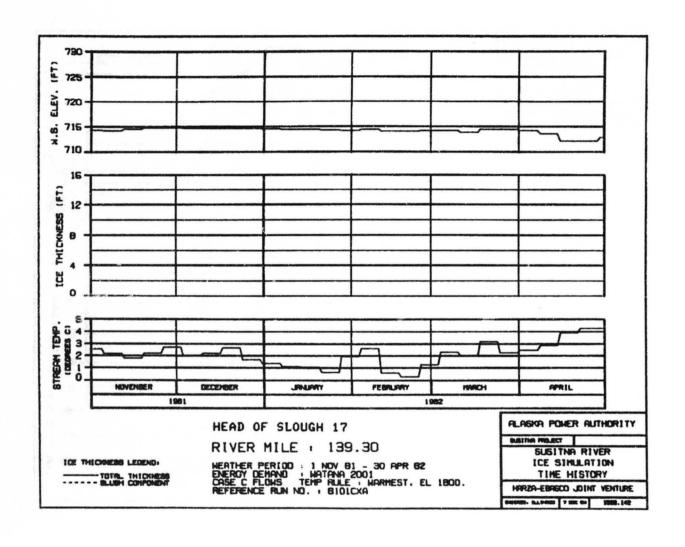


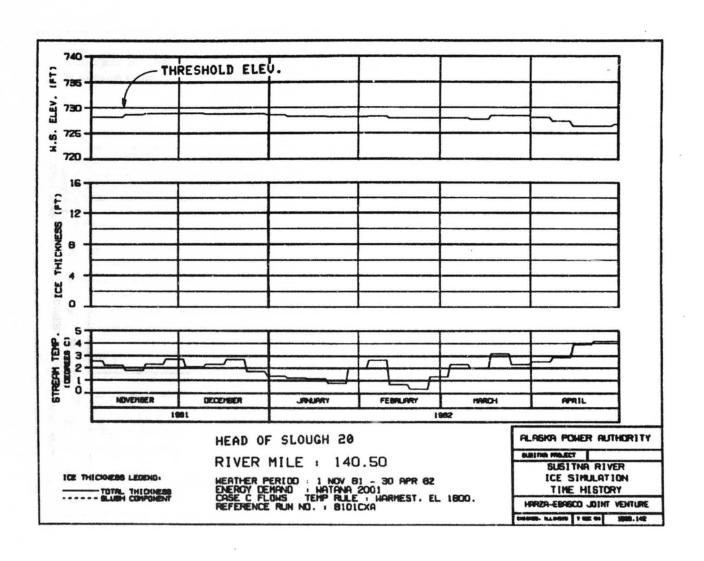
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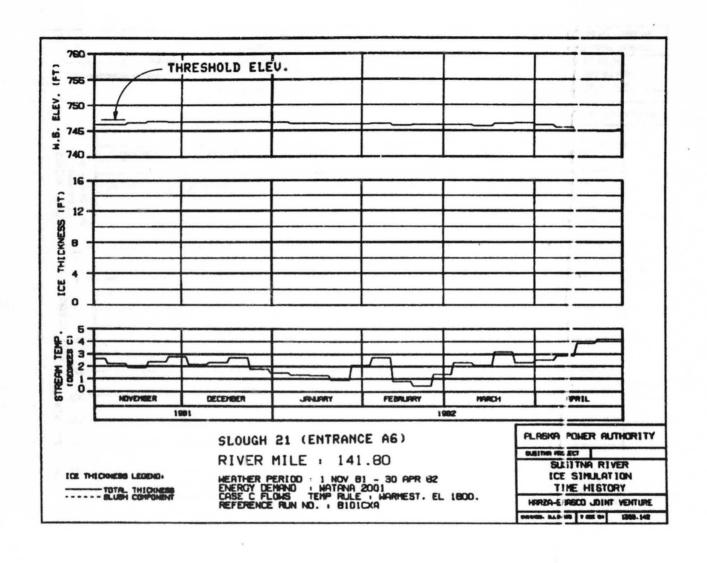




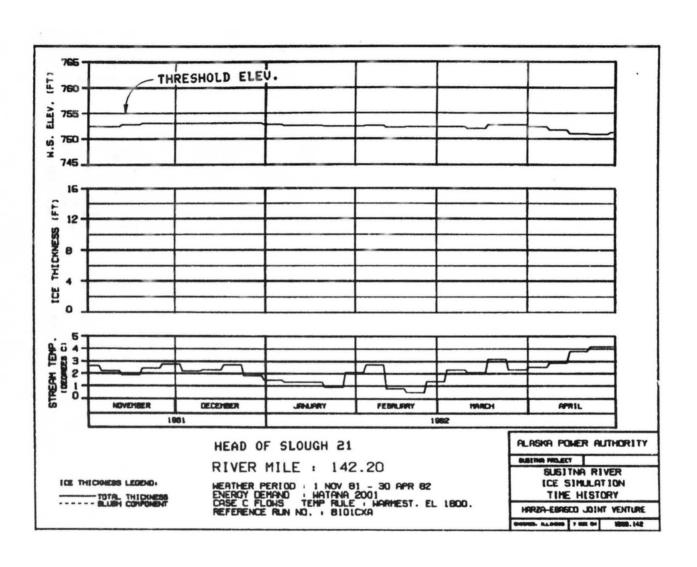


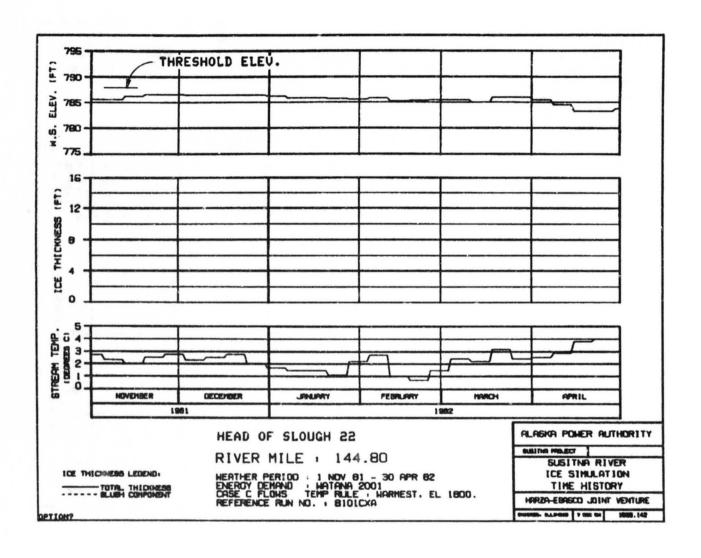




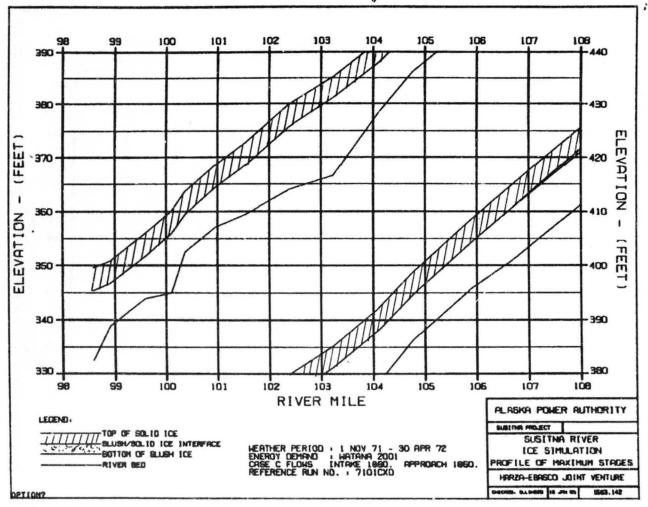


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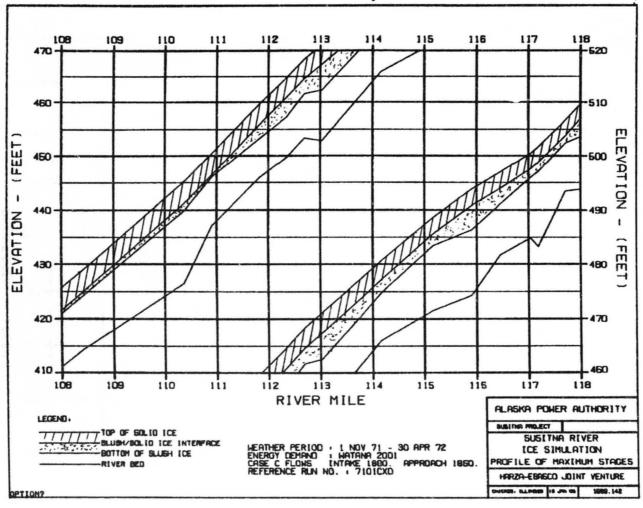


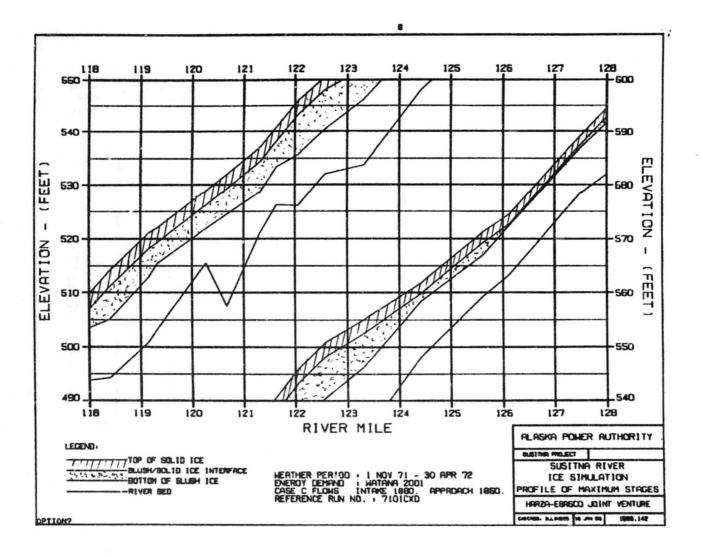


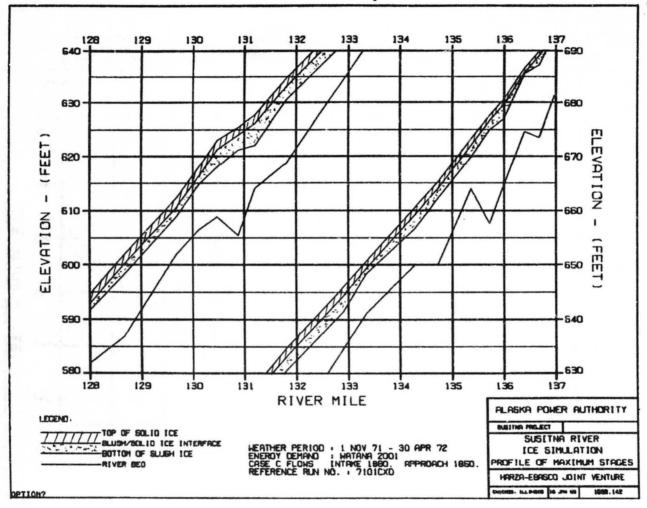




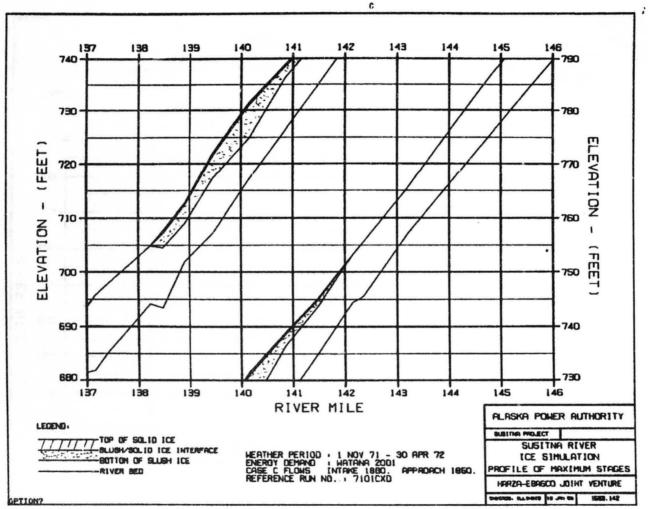


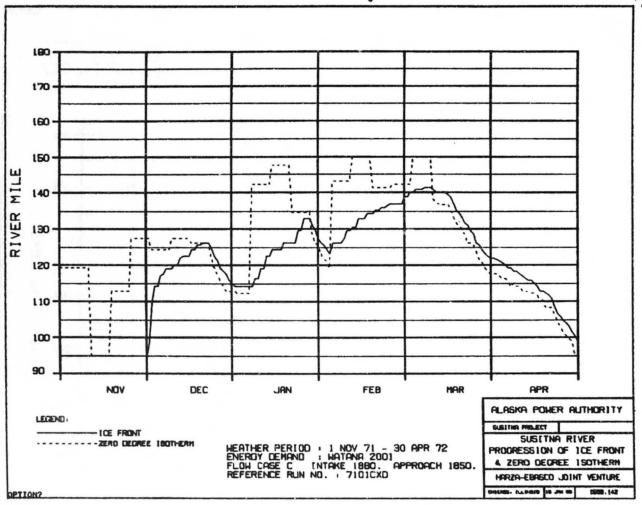




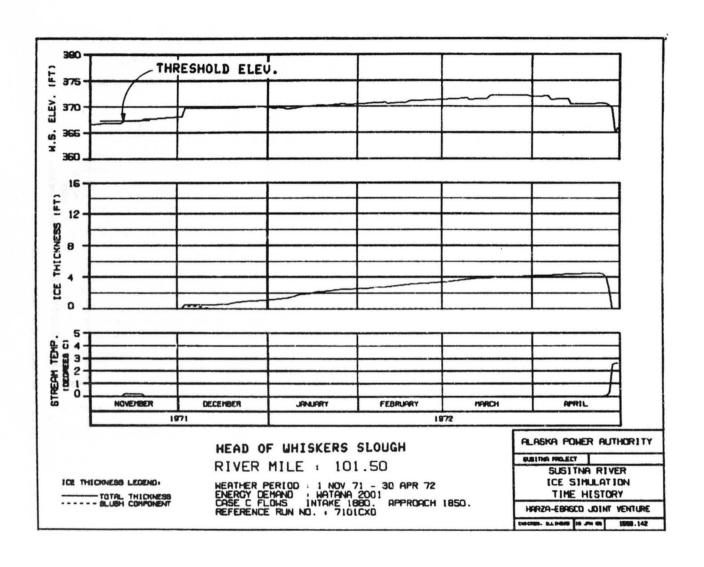


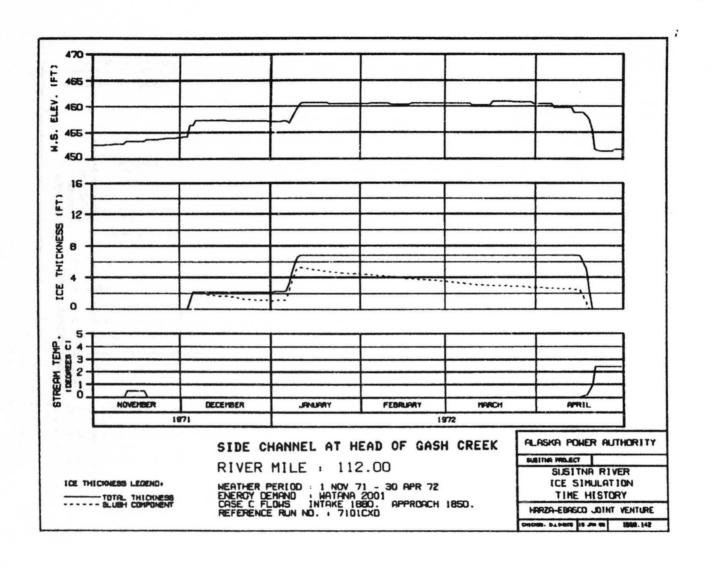
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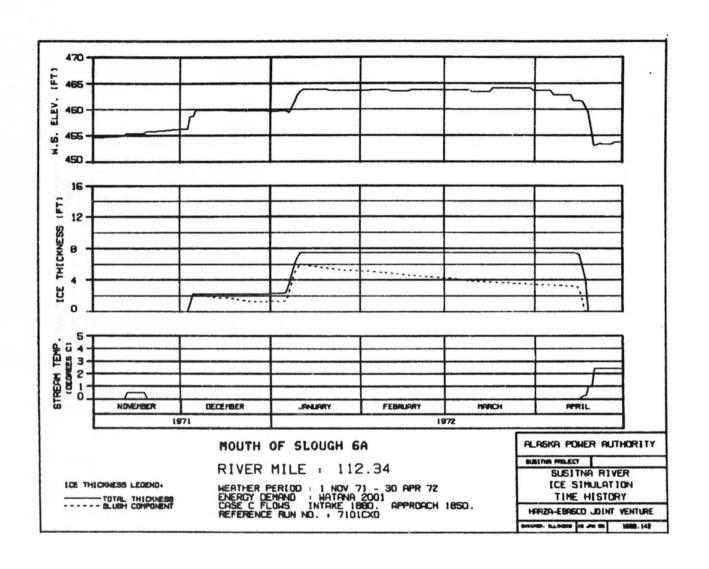


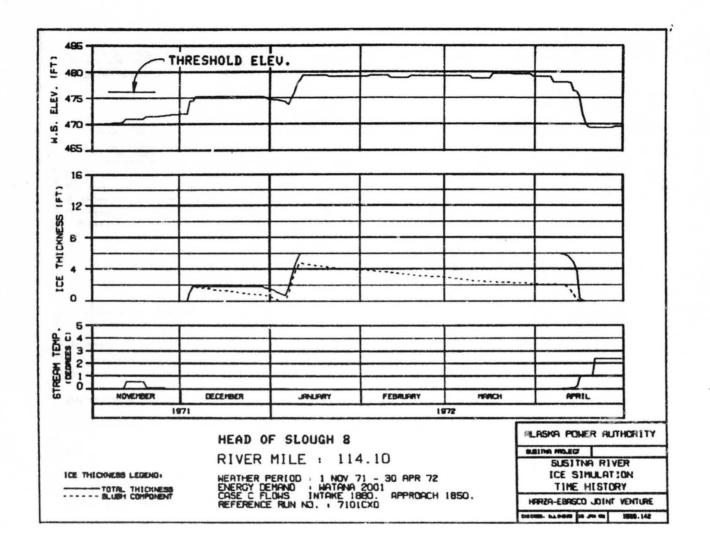


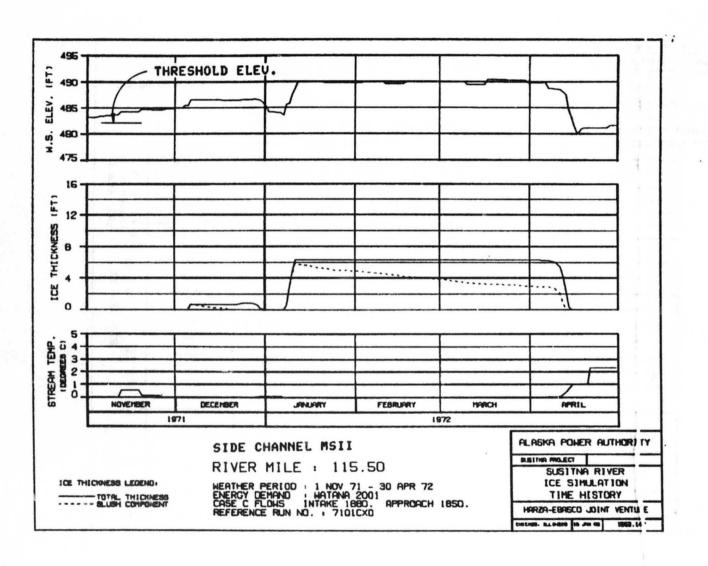
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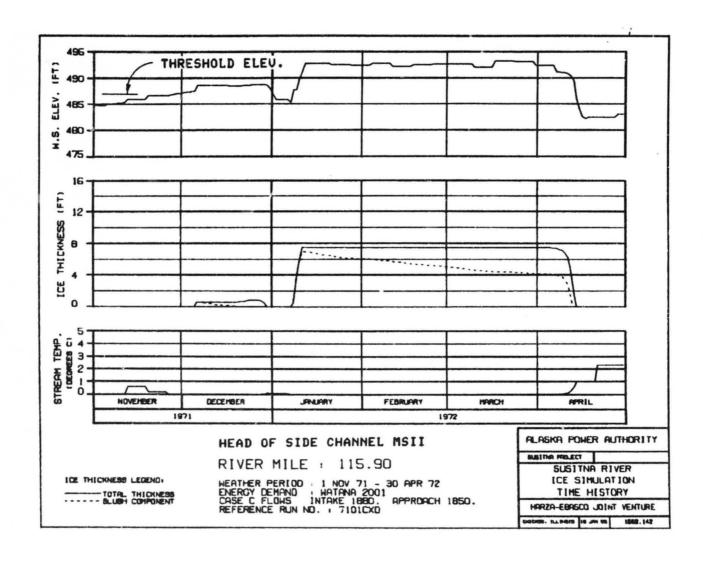


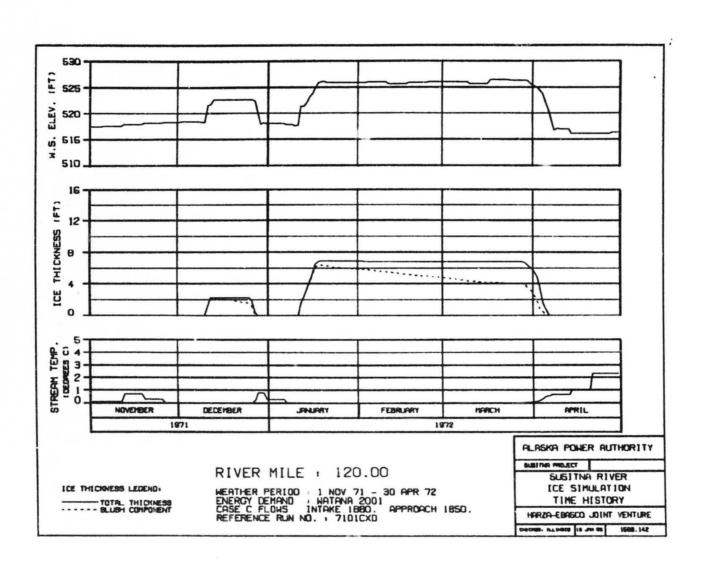


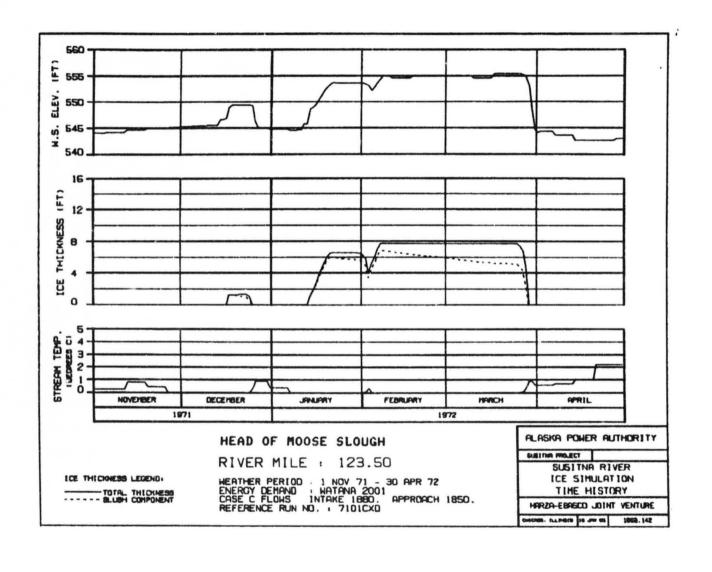




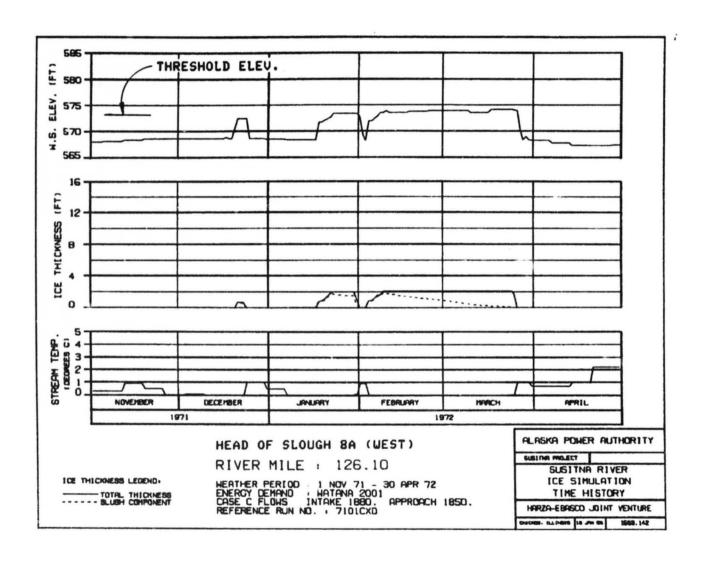




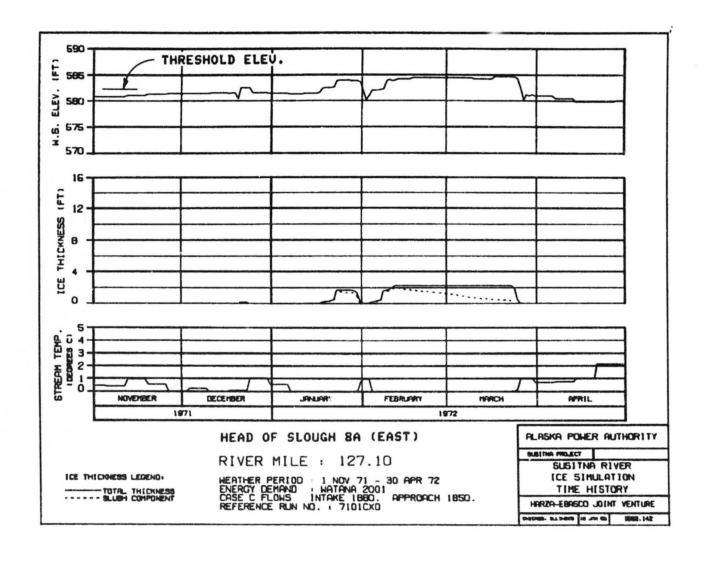




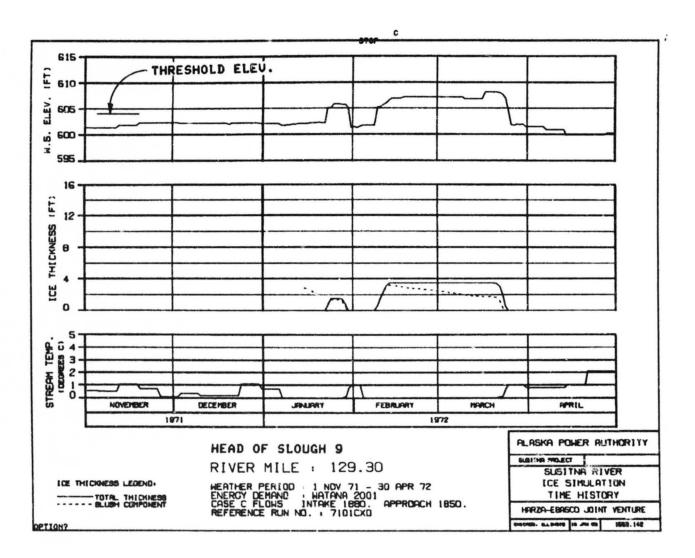
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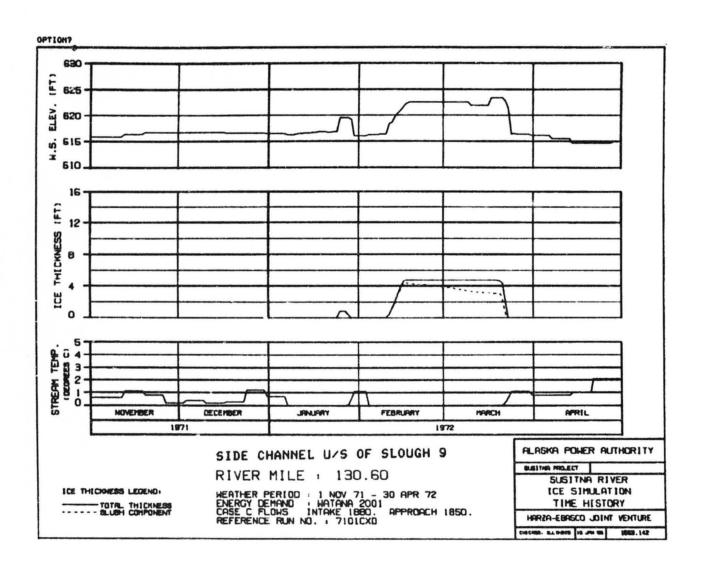


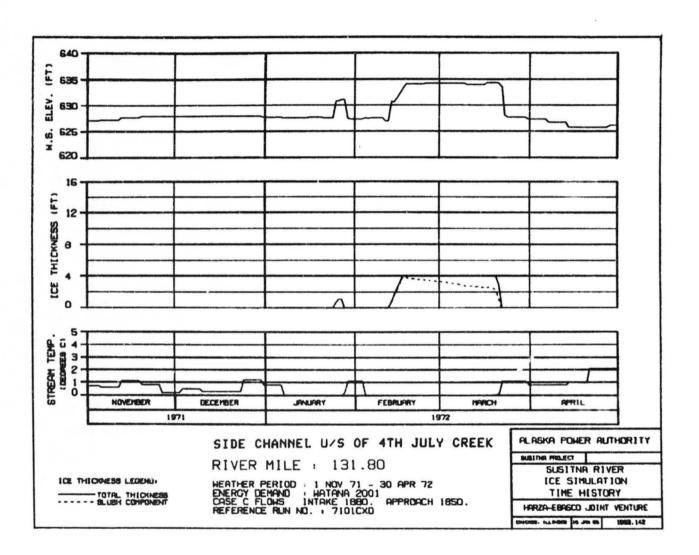
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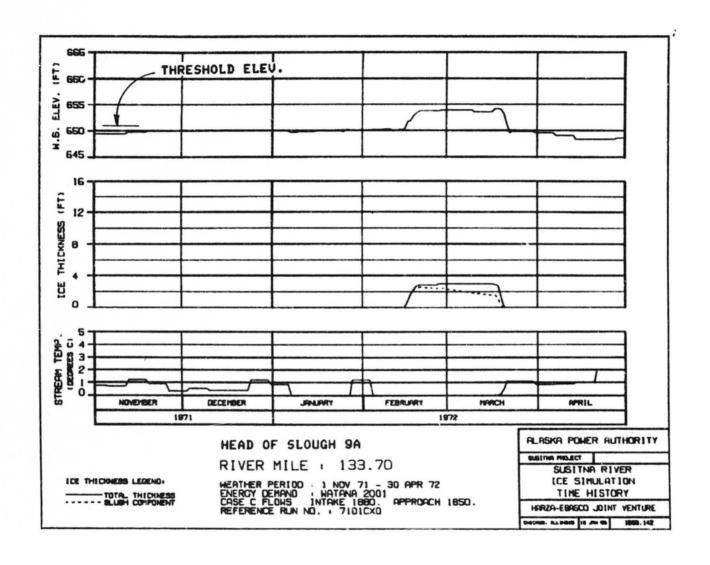


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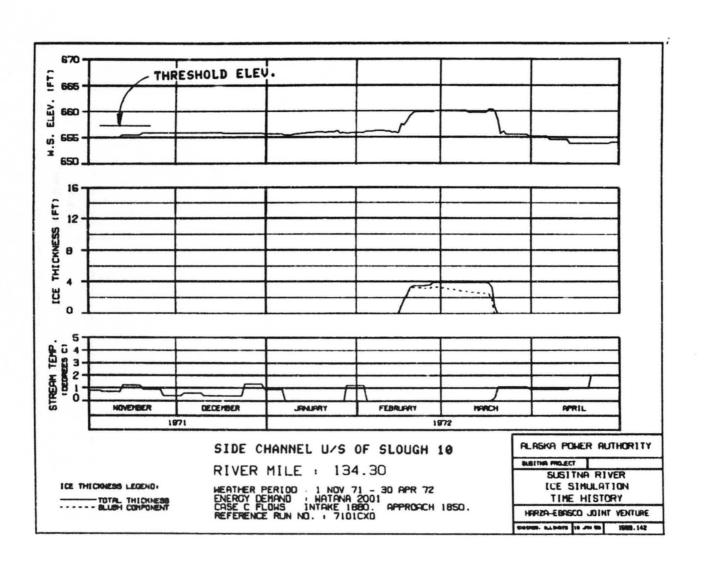


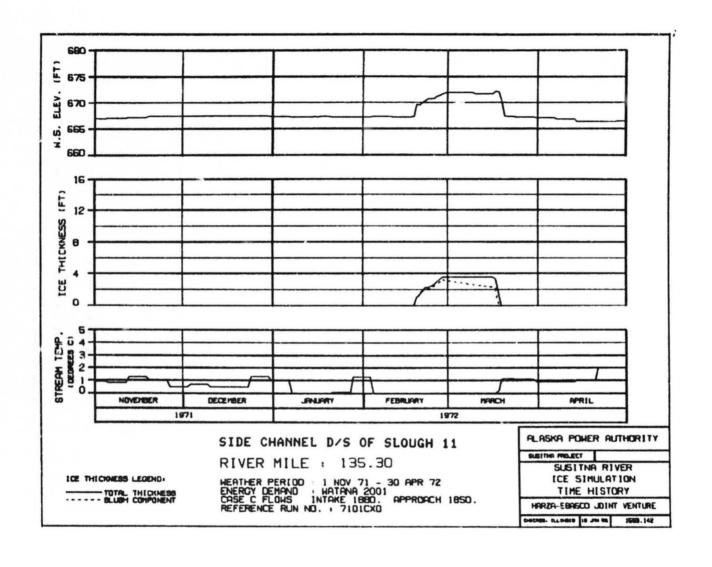




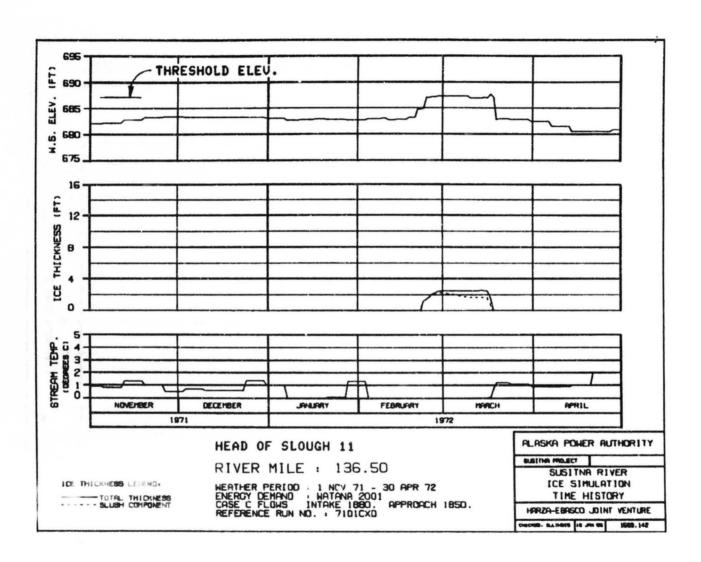


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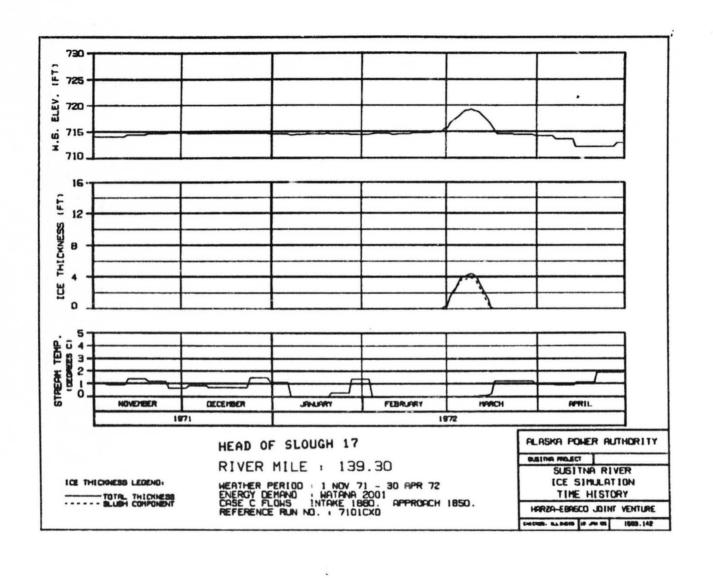


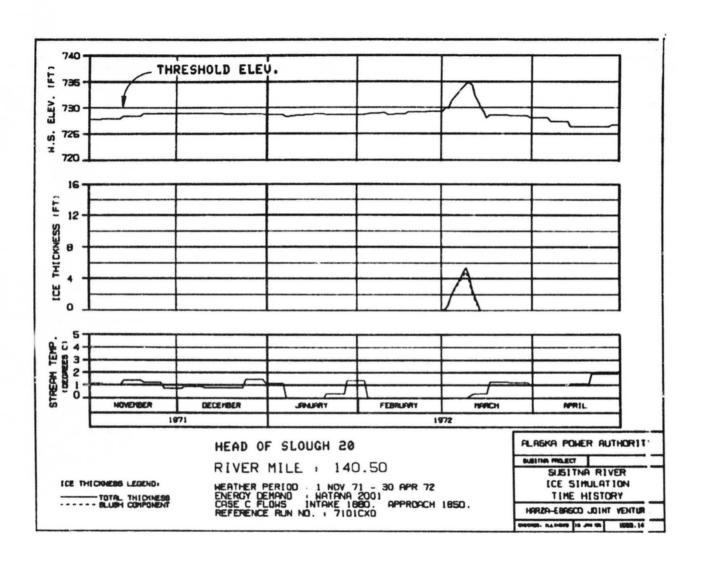


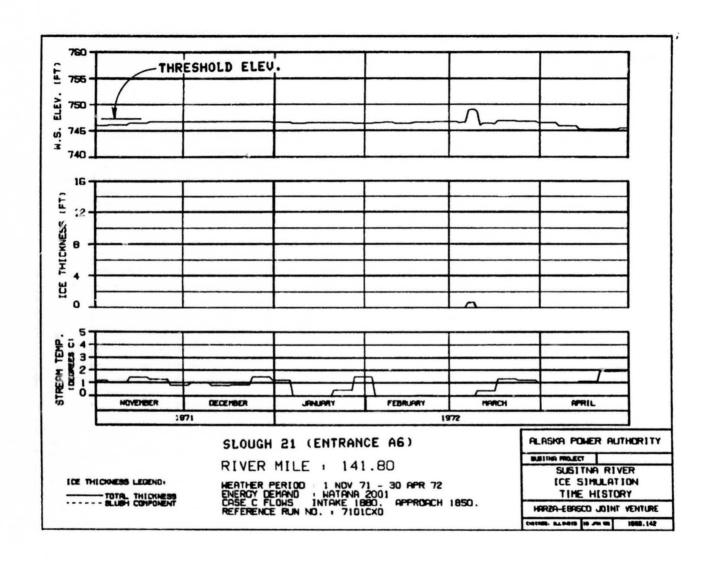
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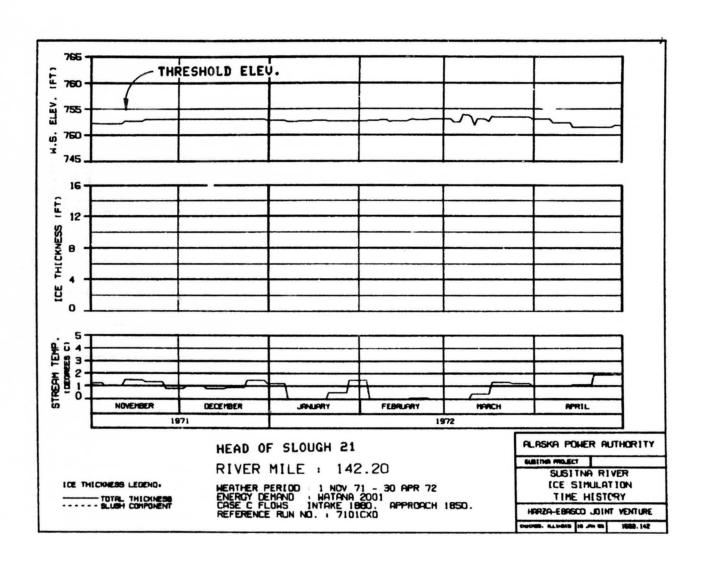
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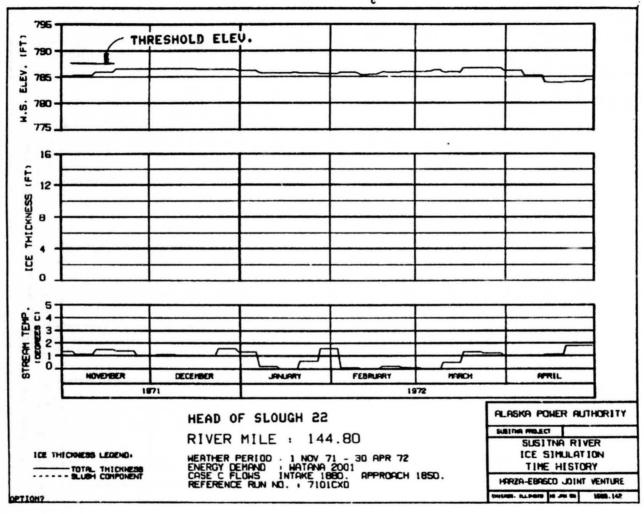


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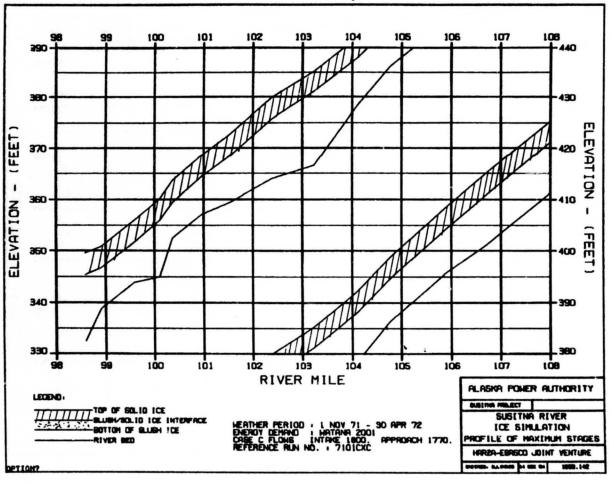


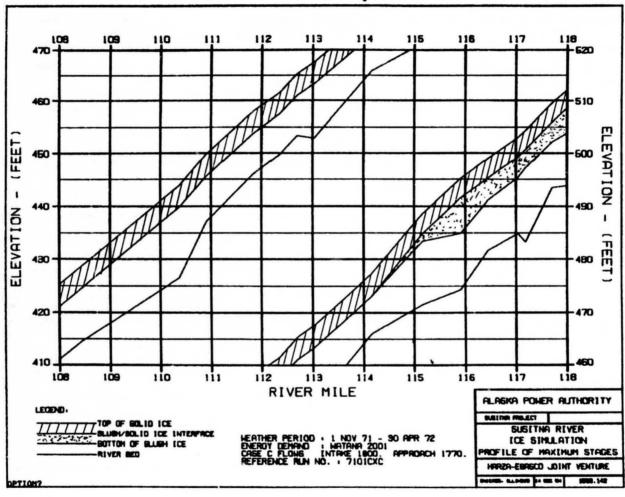
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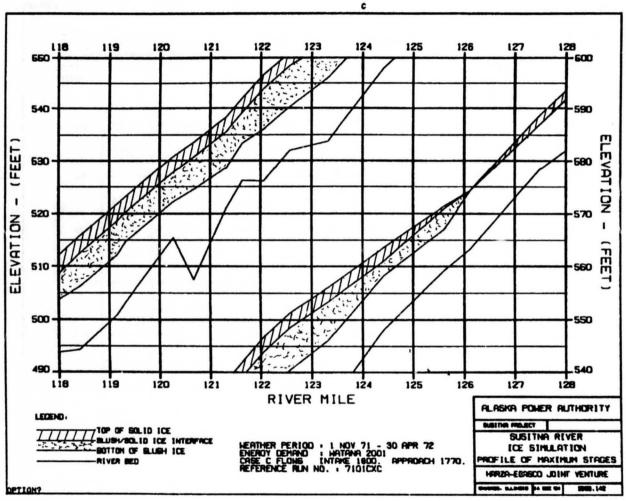


## EXHIBIT S

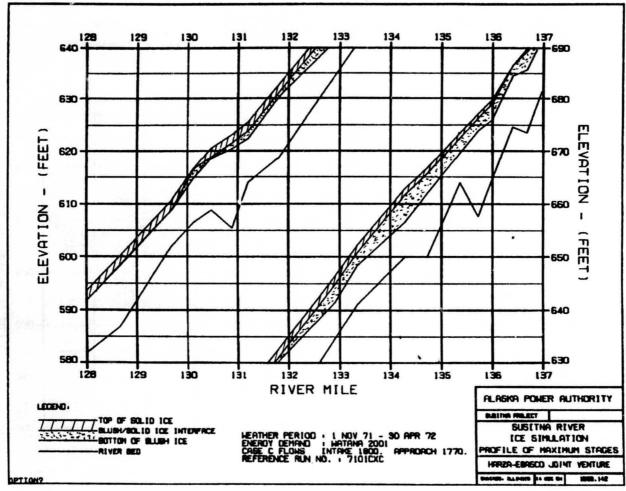




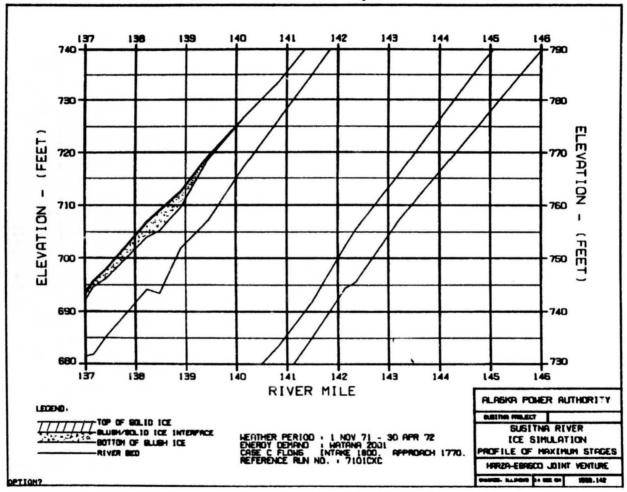
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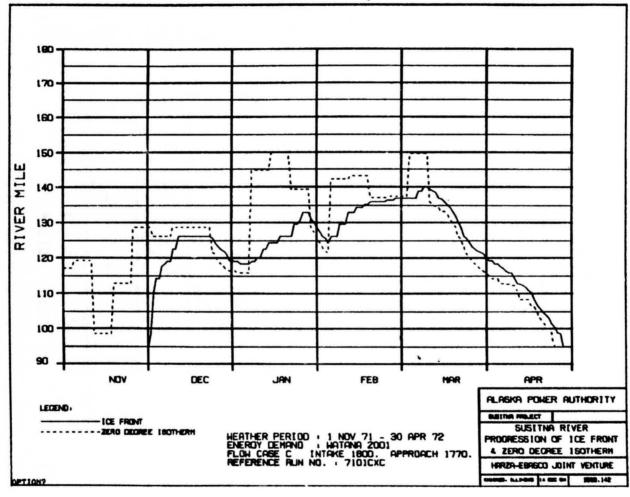


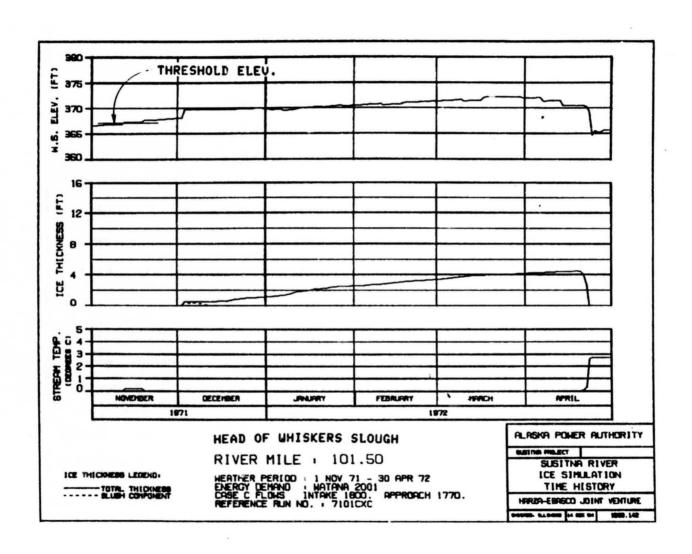


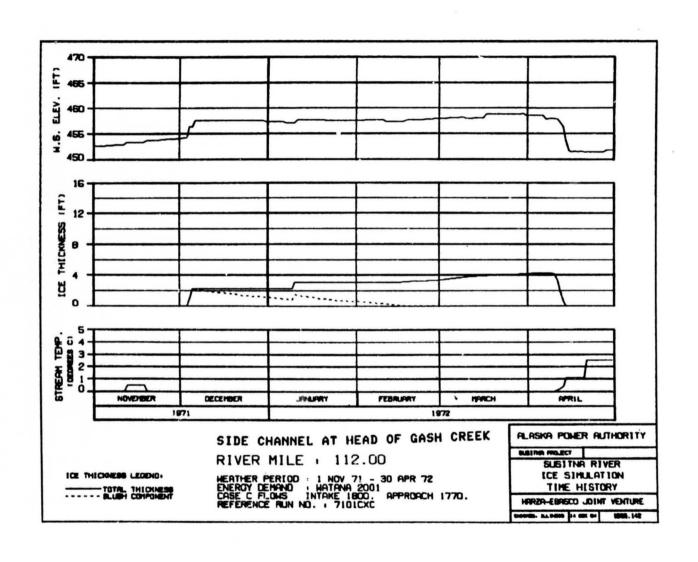


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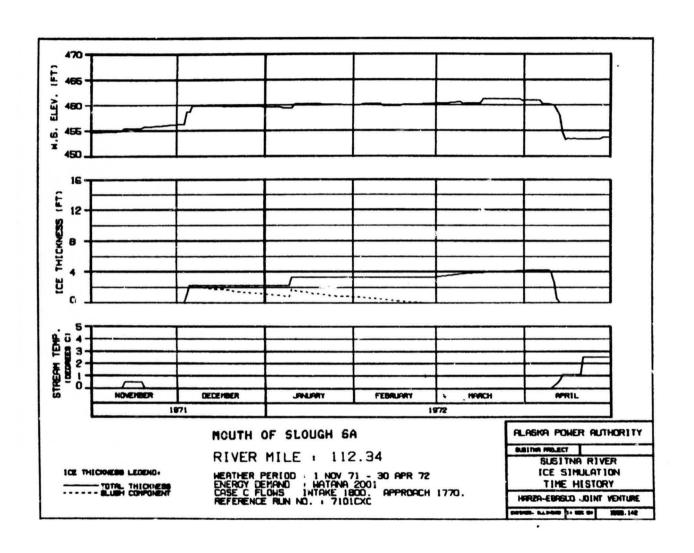


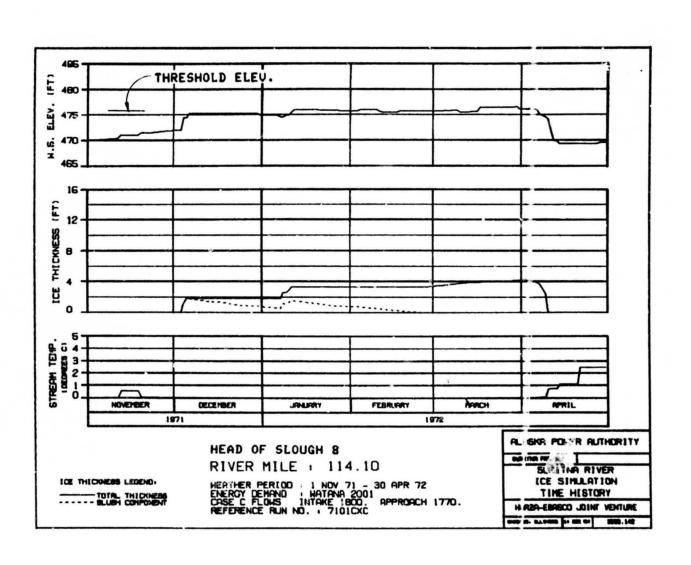


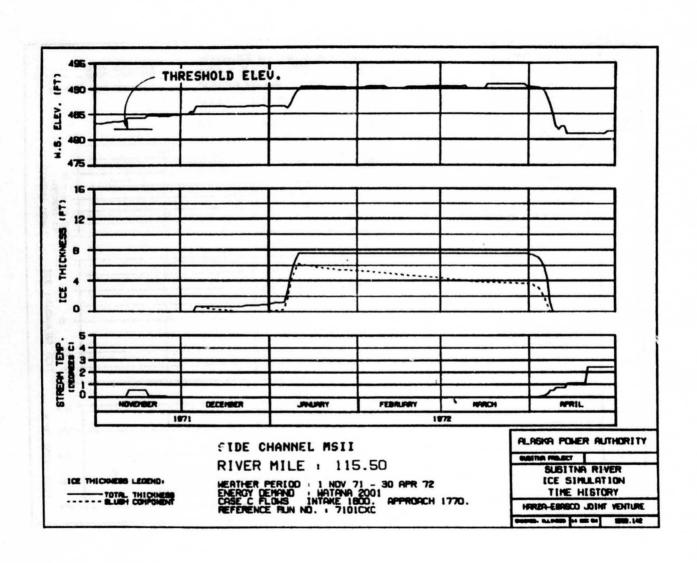


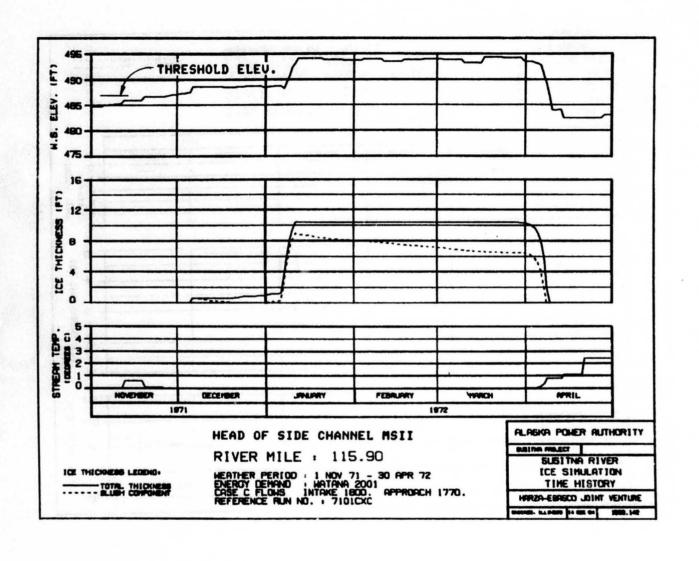


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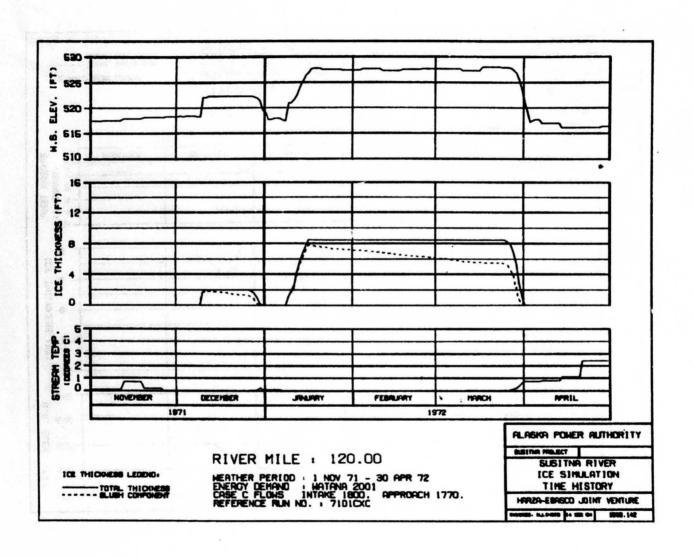


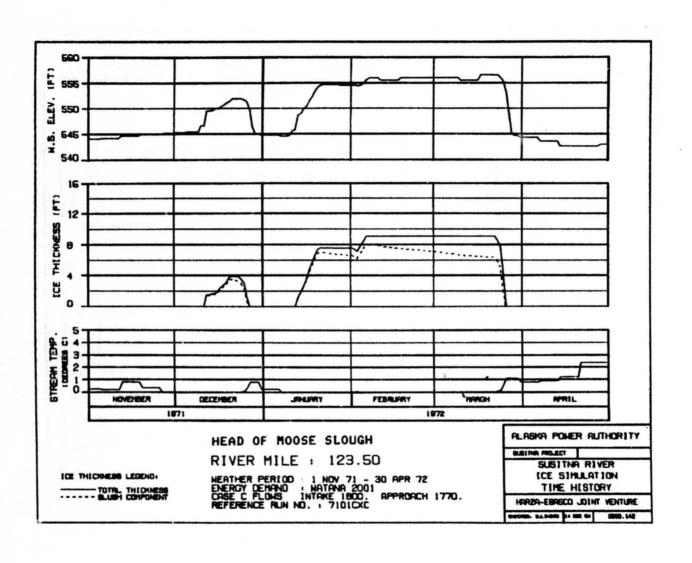


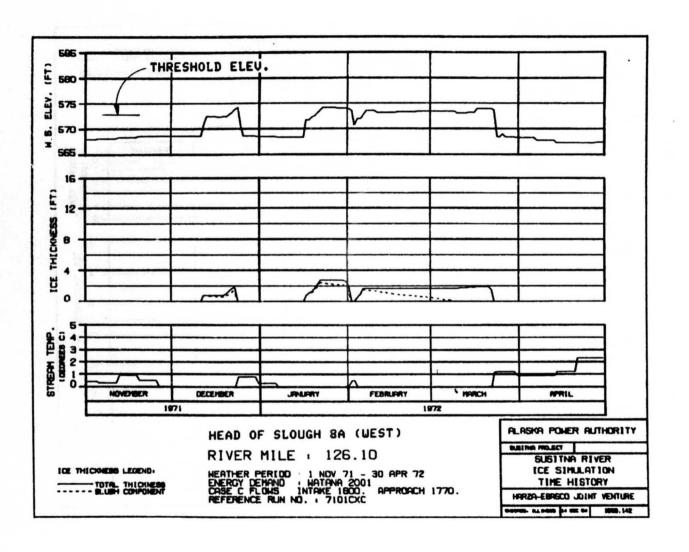


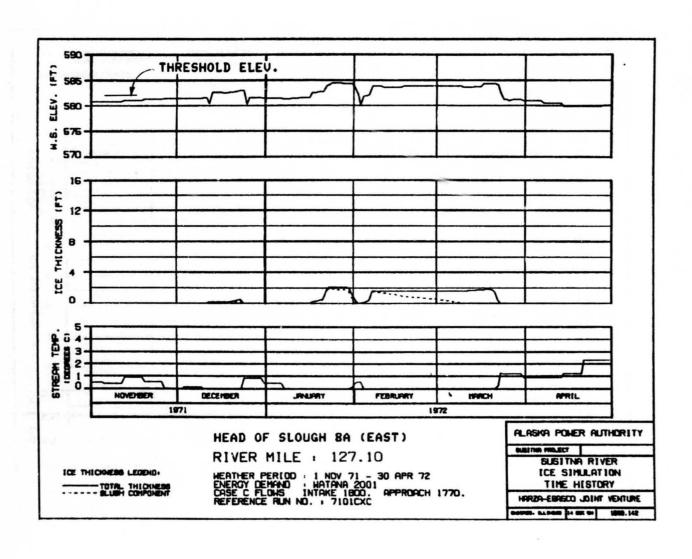


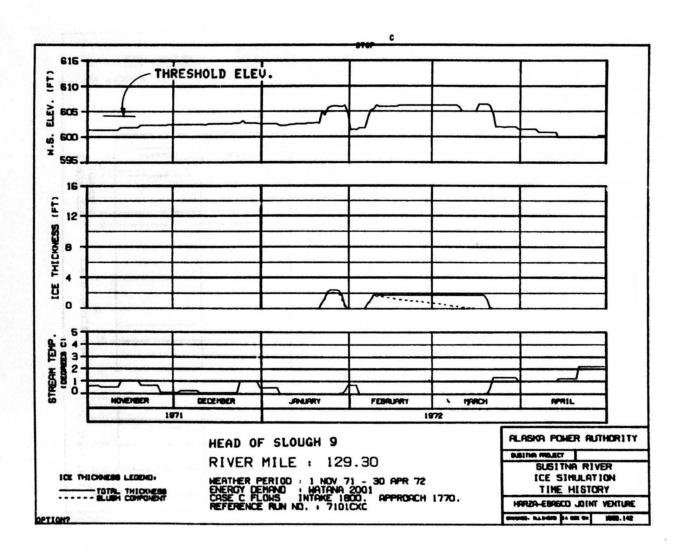
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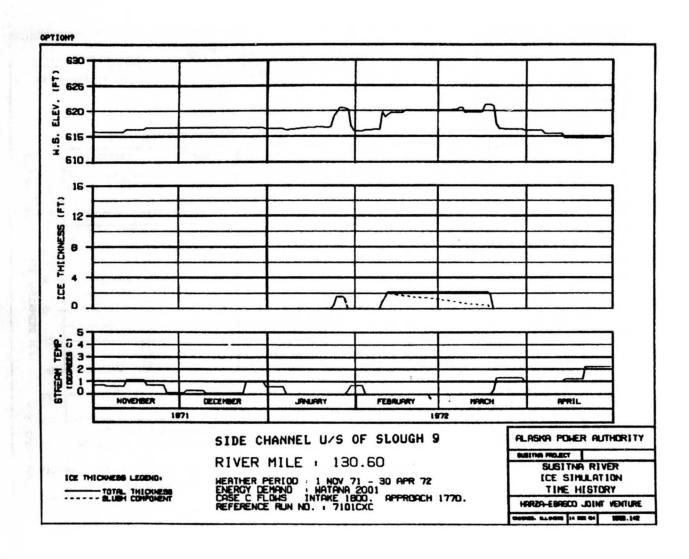


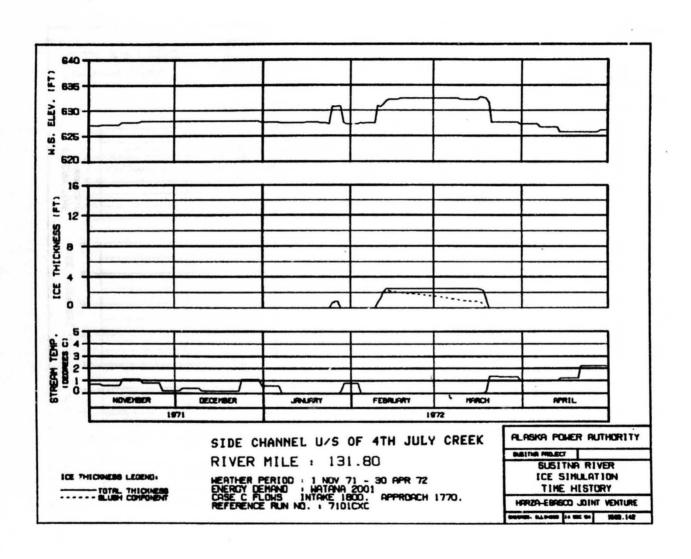


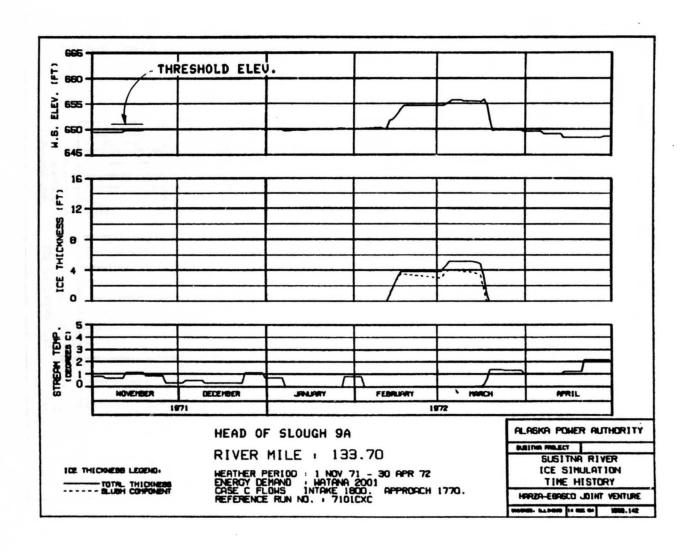


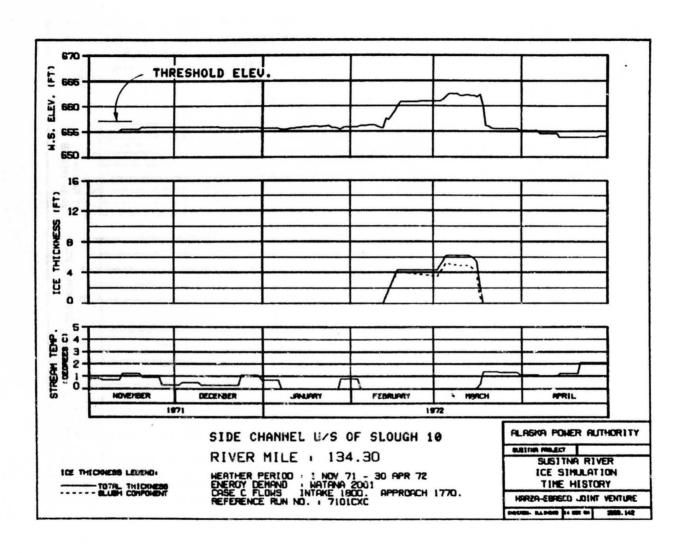


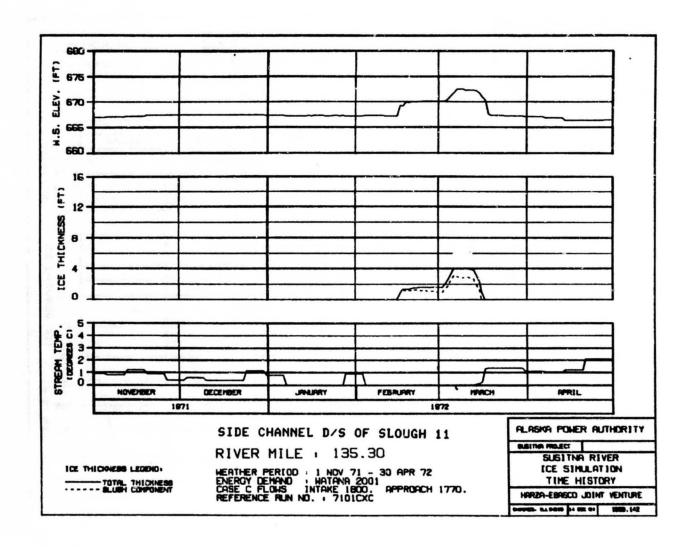


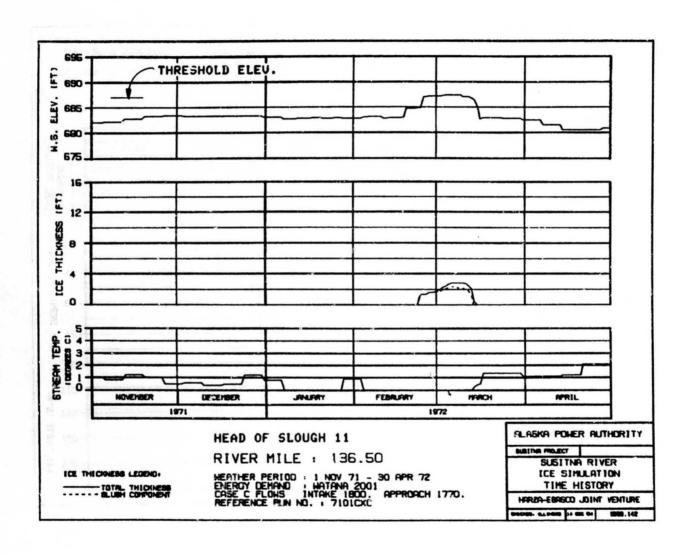


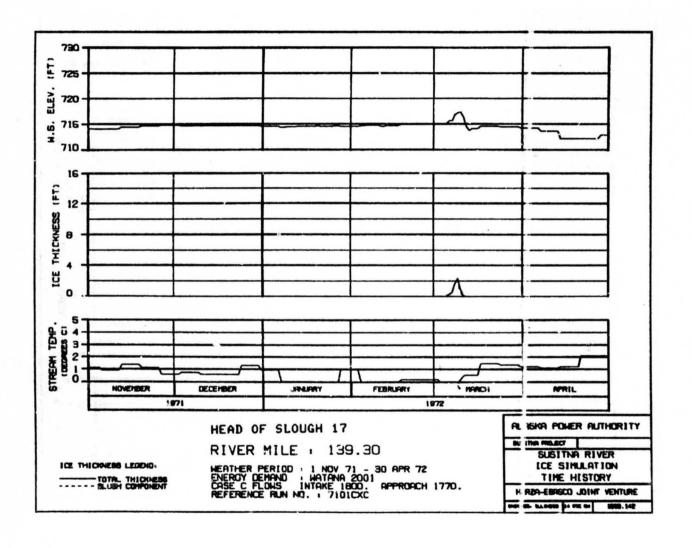


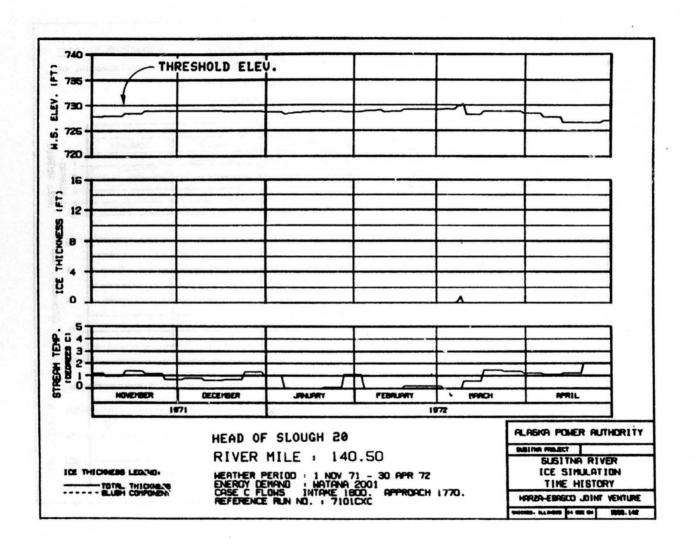


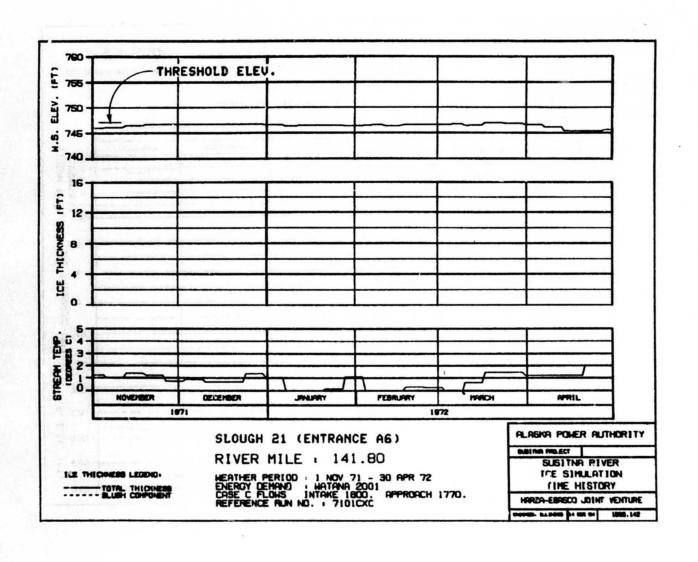


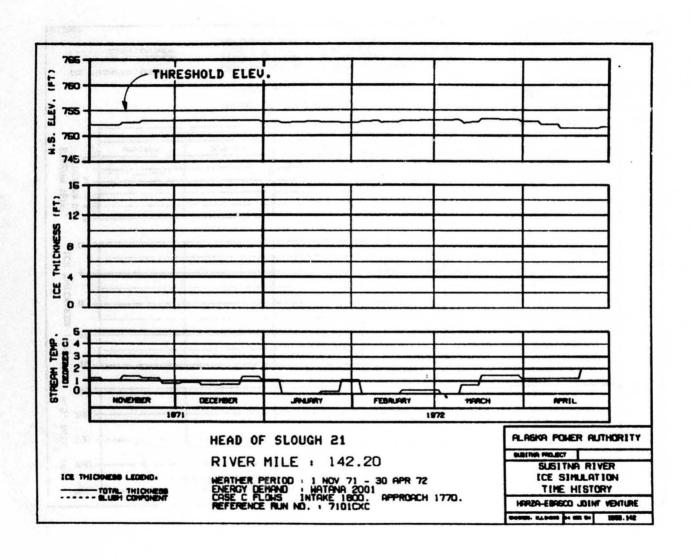


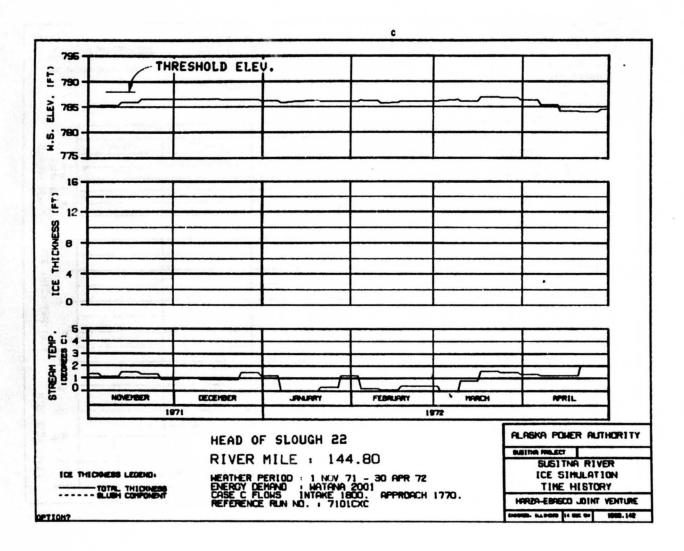


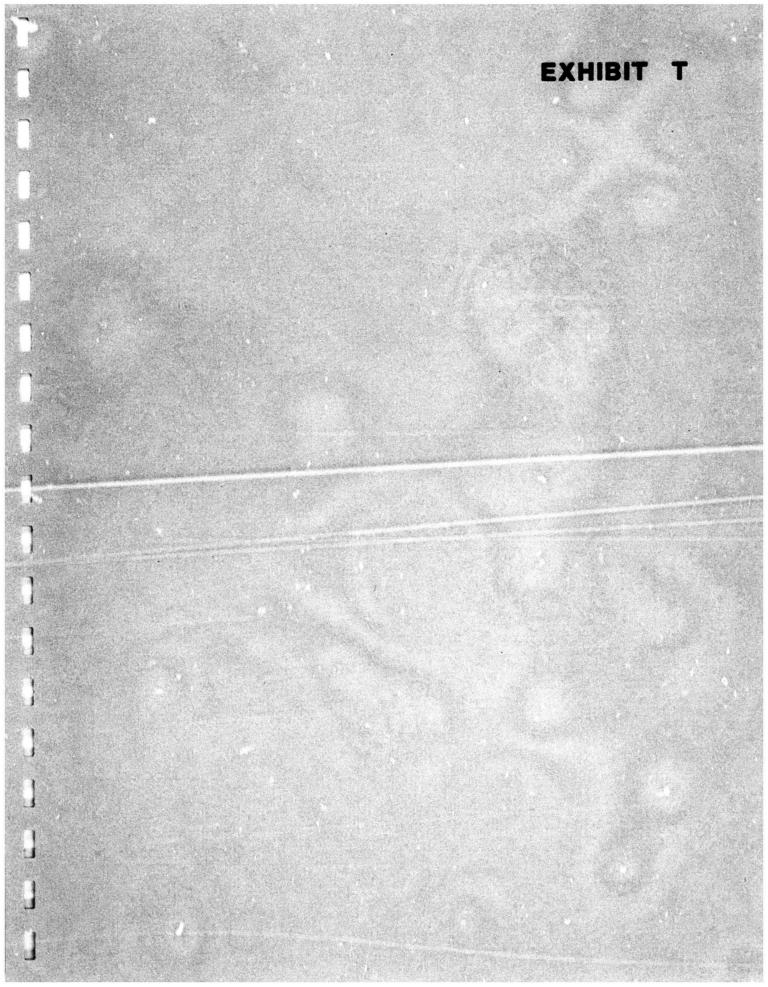


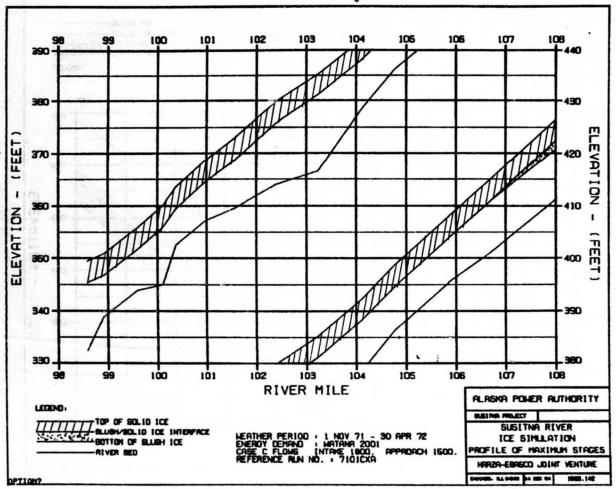


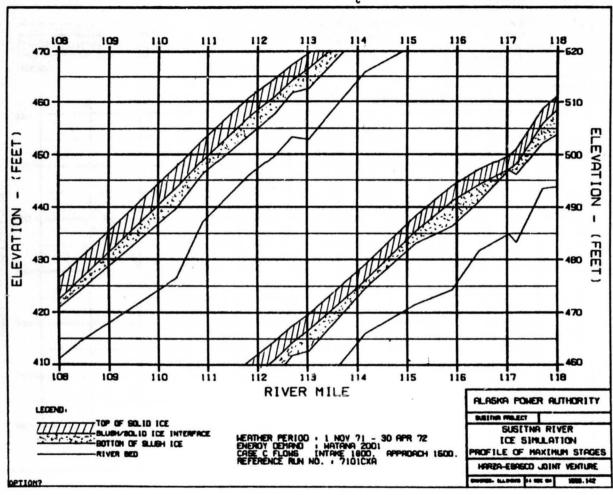


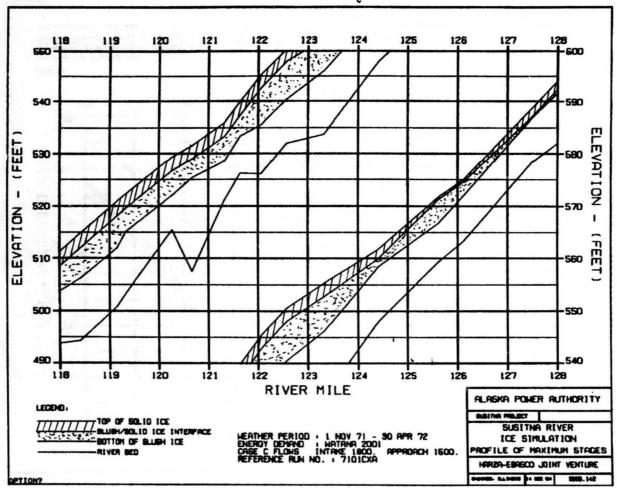


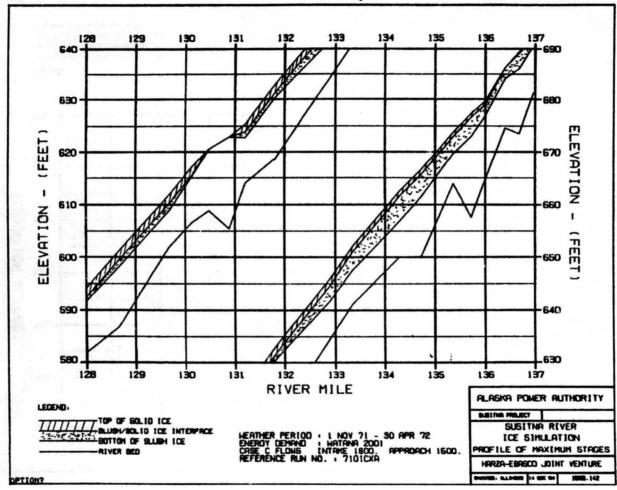




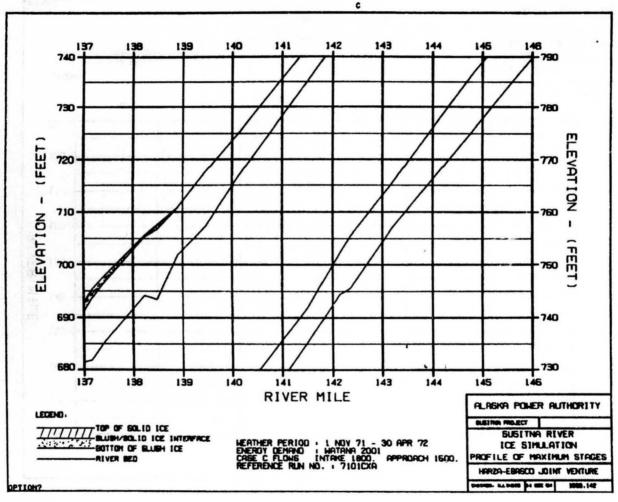




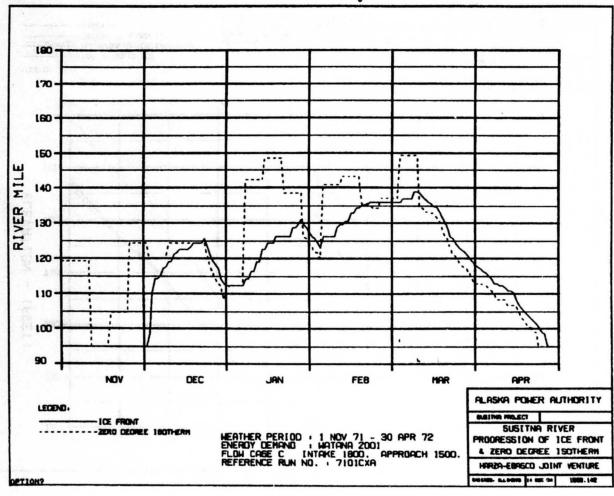


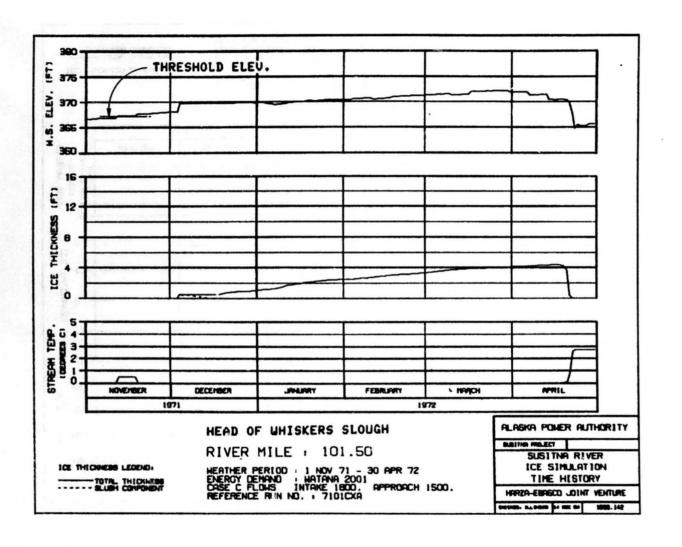


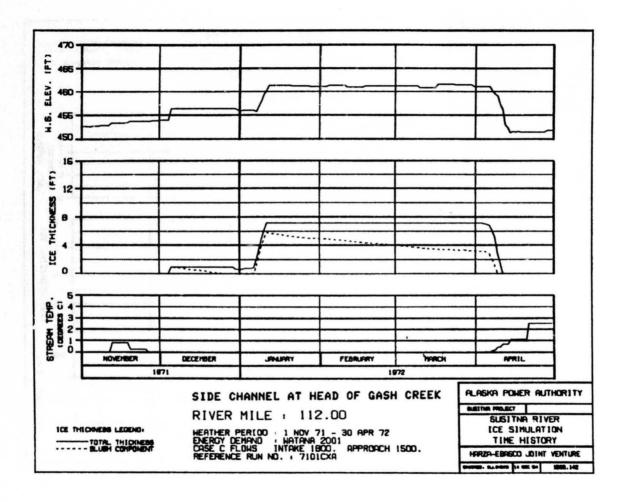


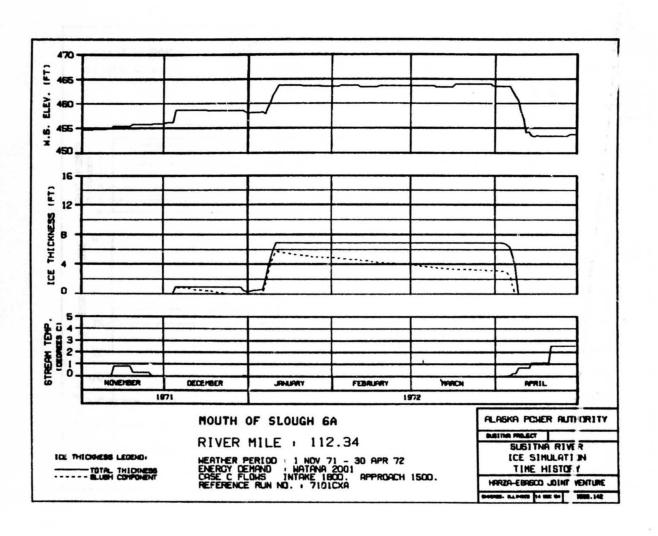


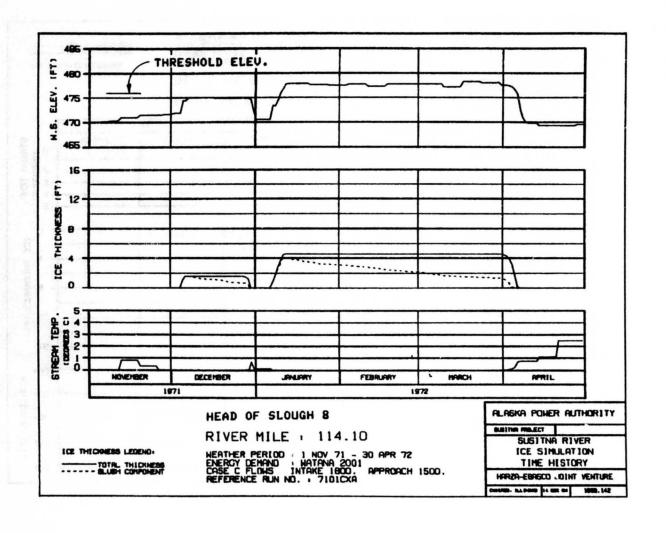


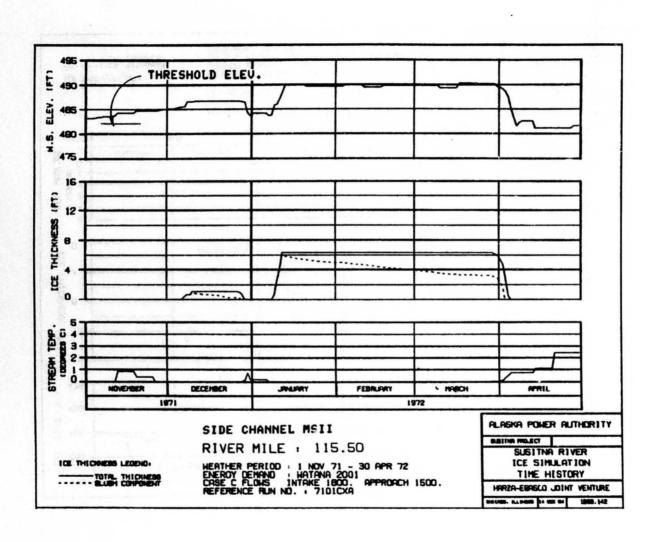


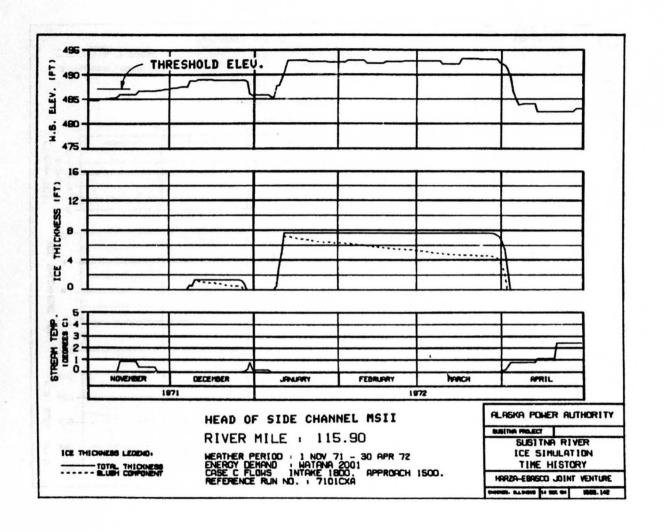


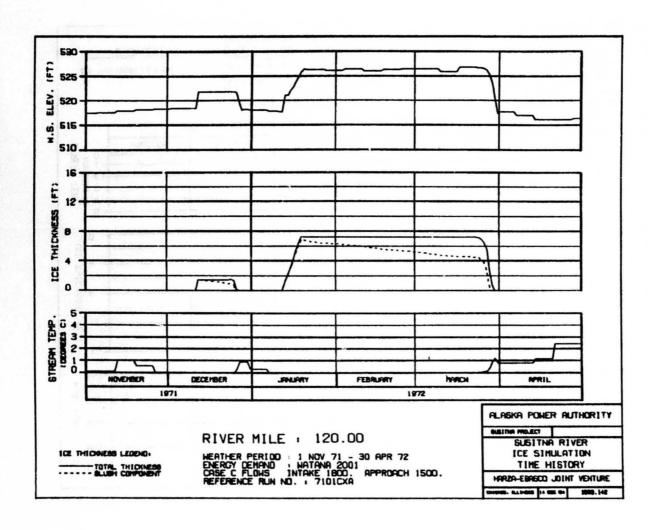


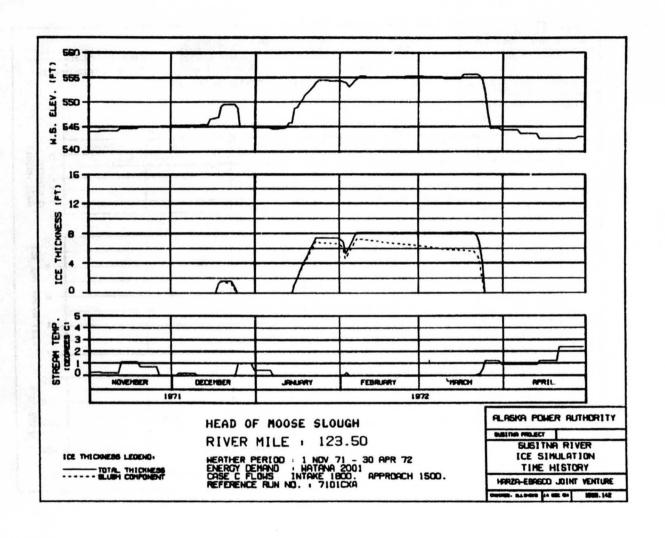




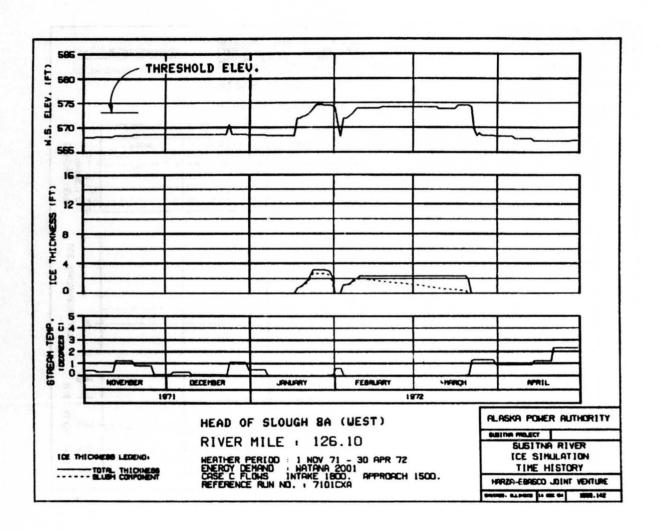


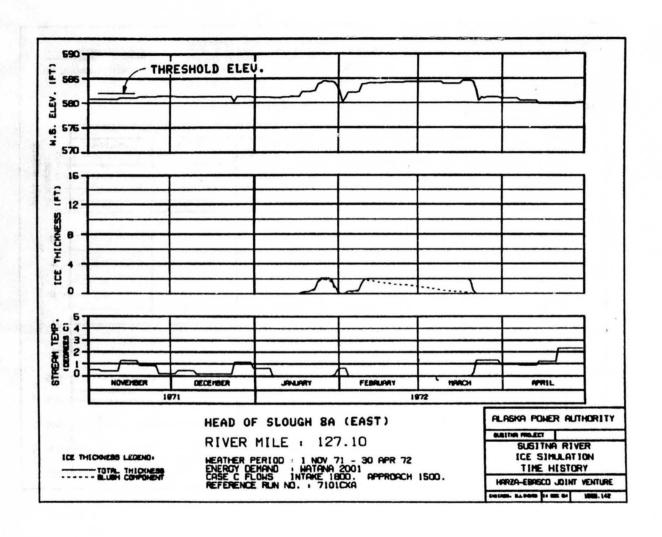




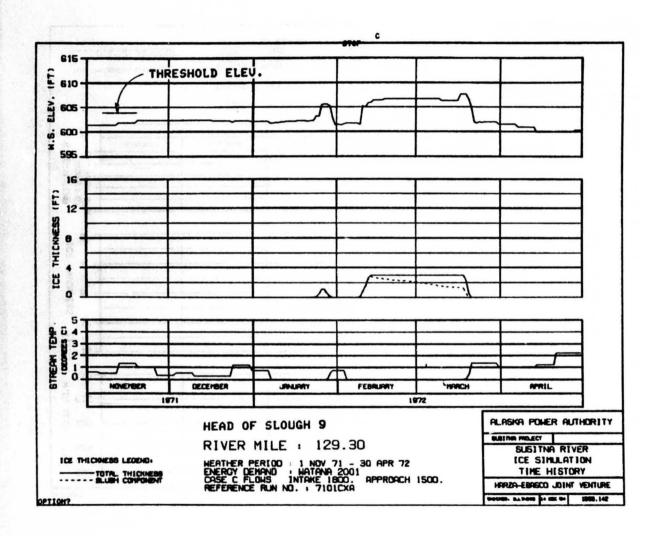


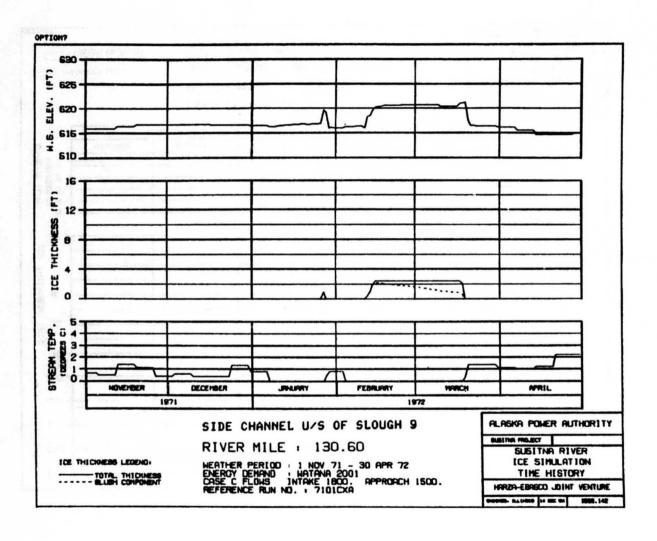
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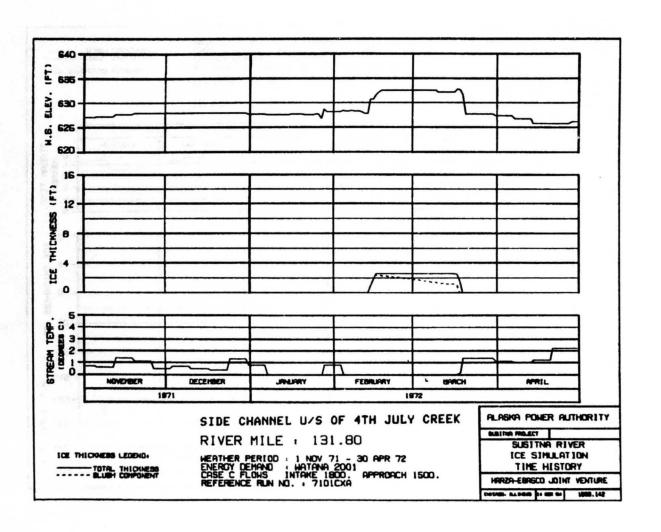


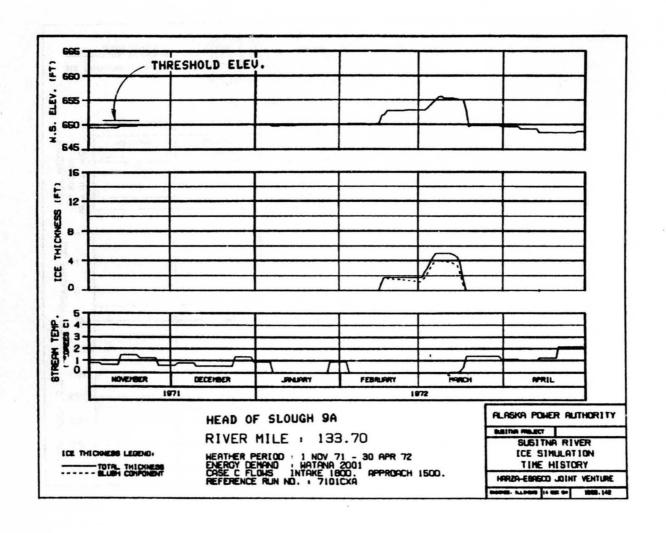


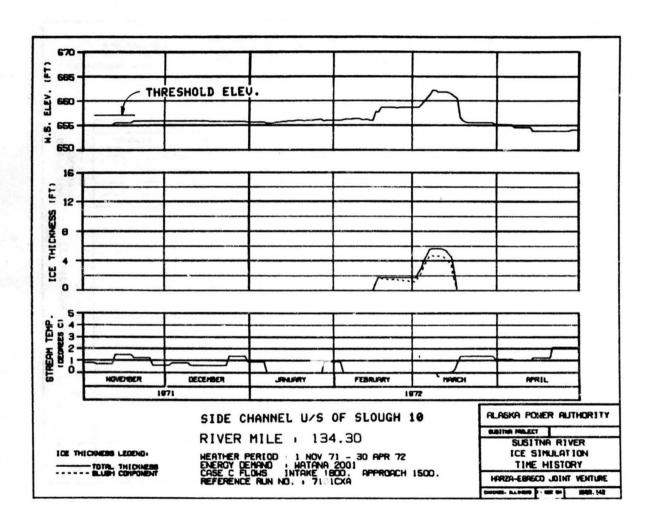
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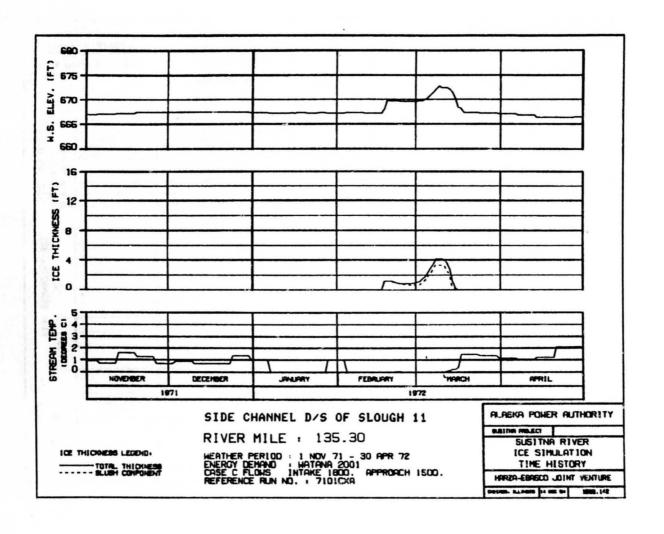




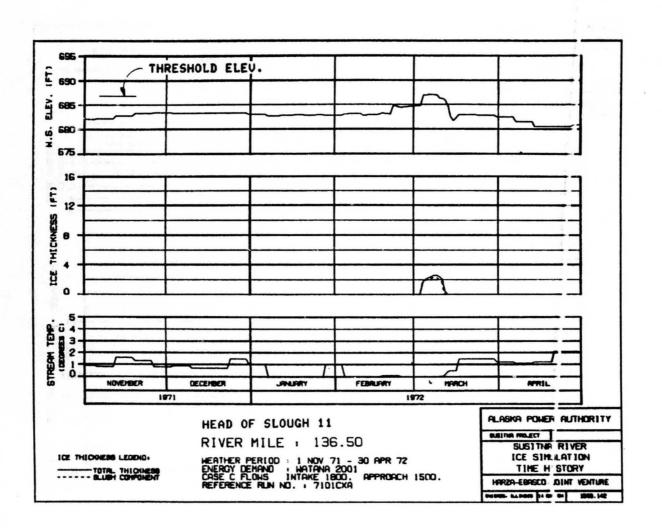


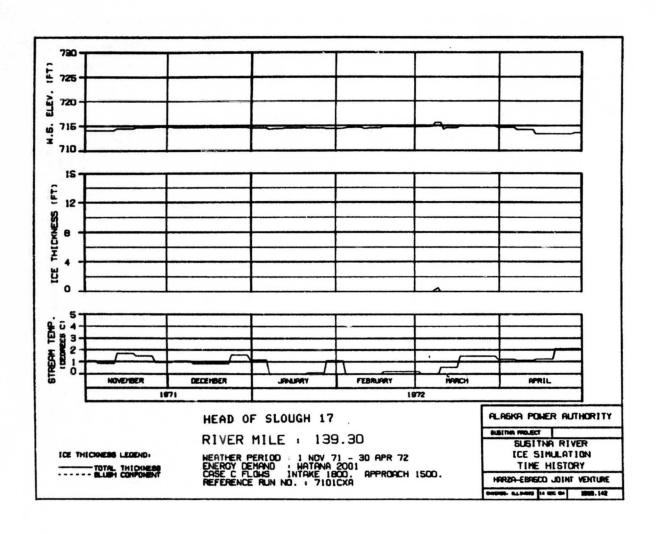


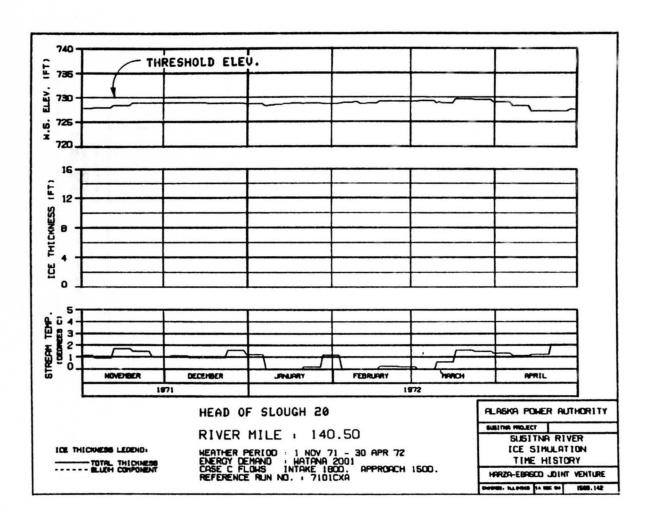


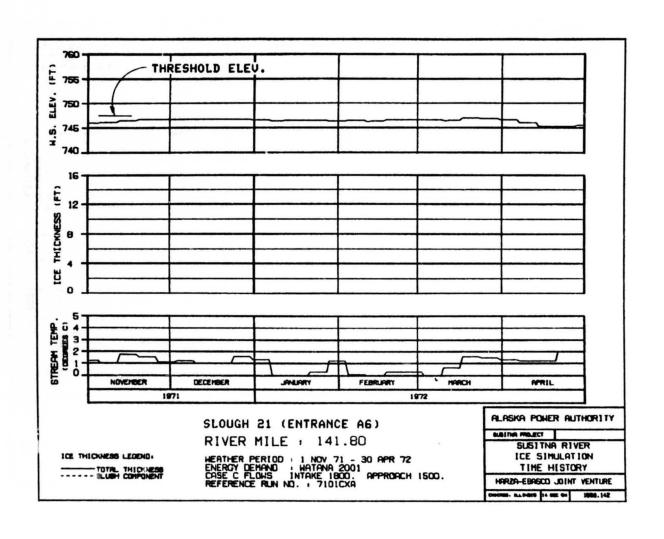


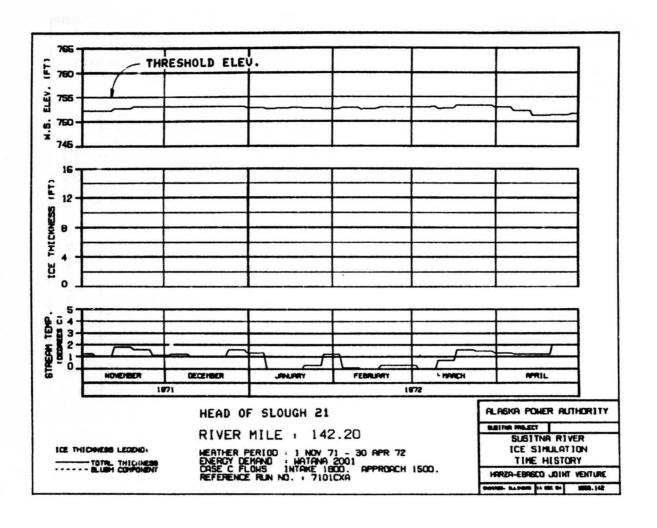
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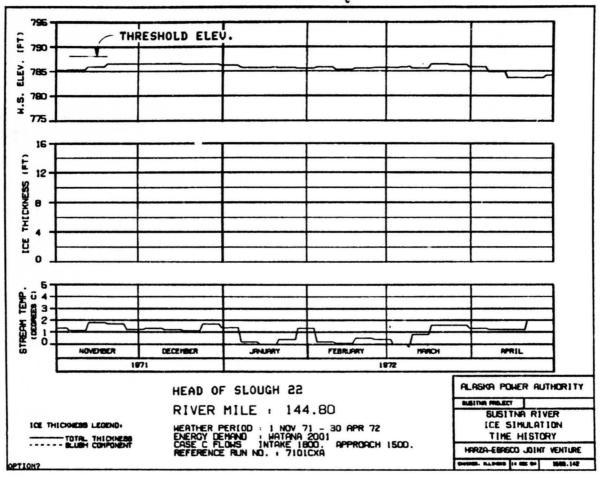
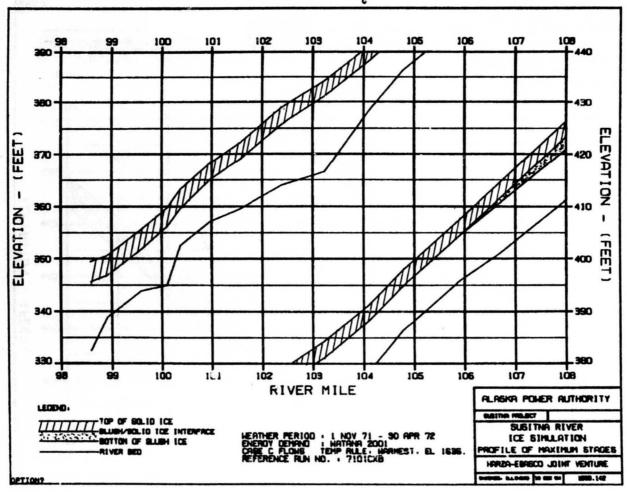
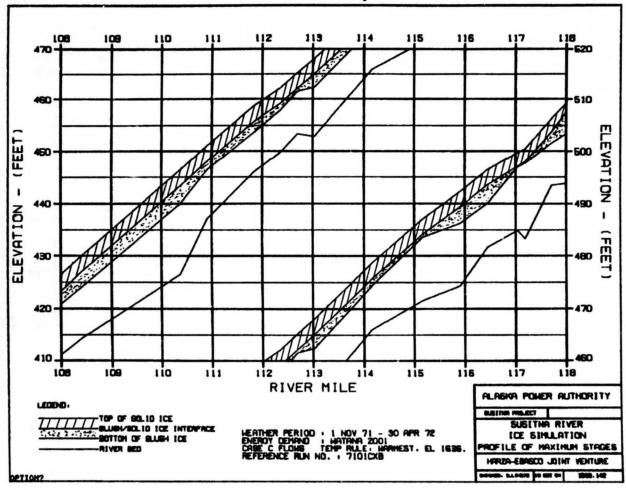
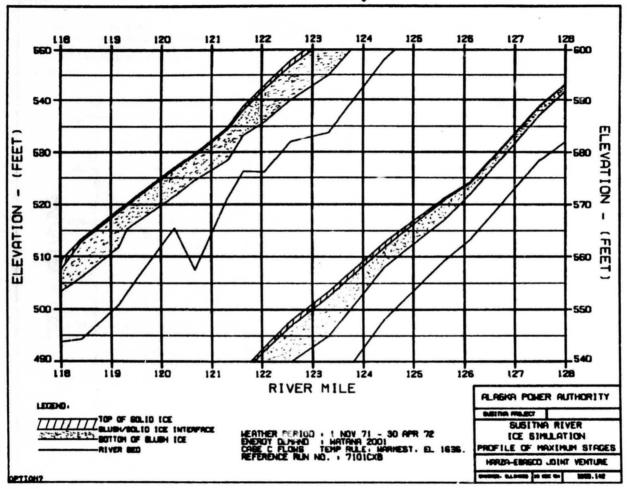
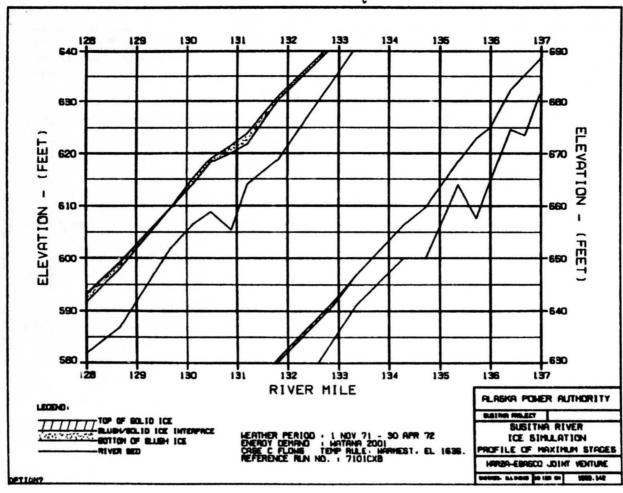


EXHIBIT U



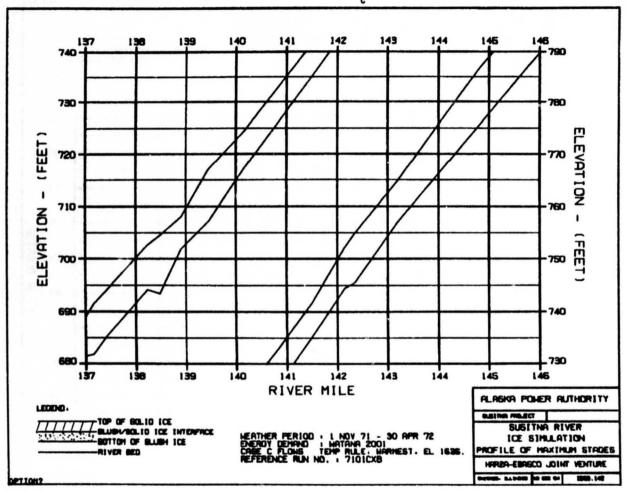


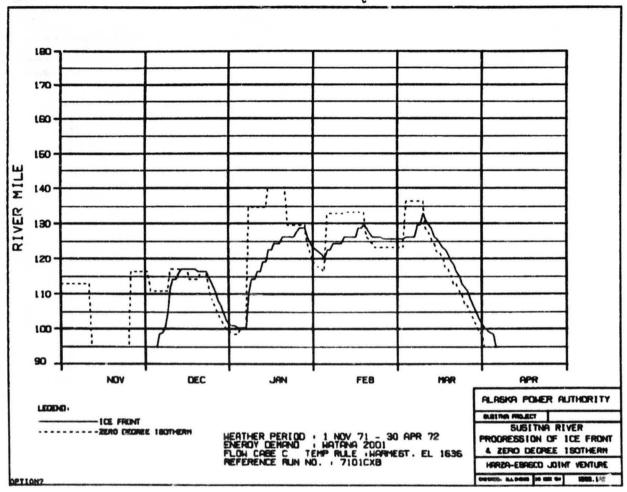


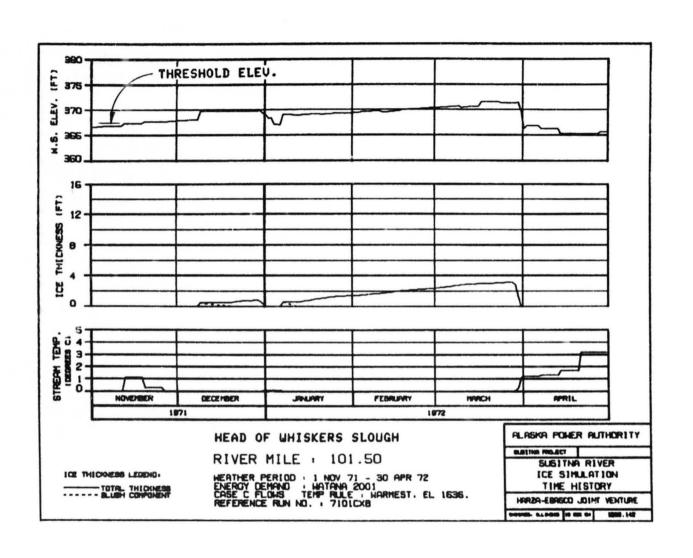


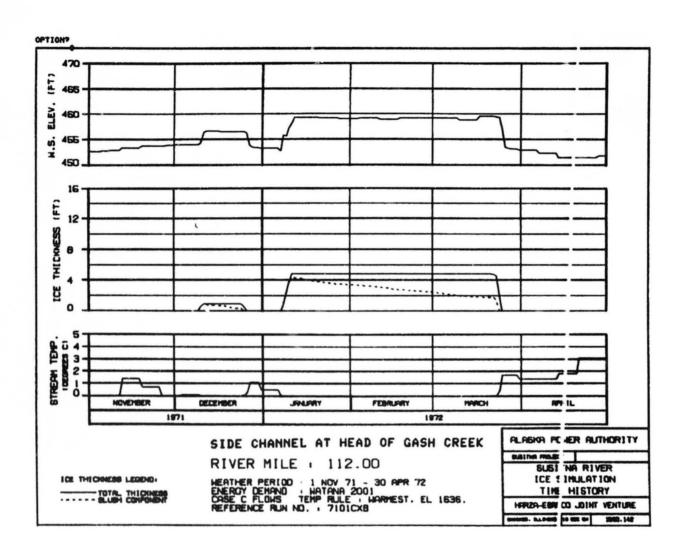
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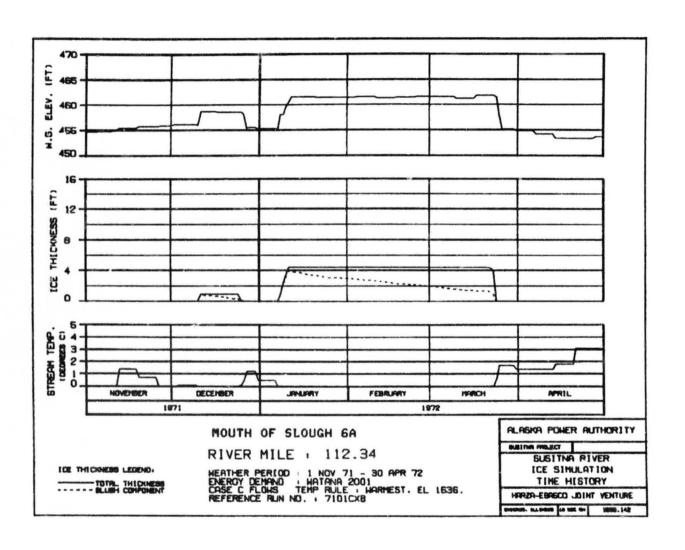
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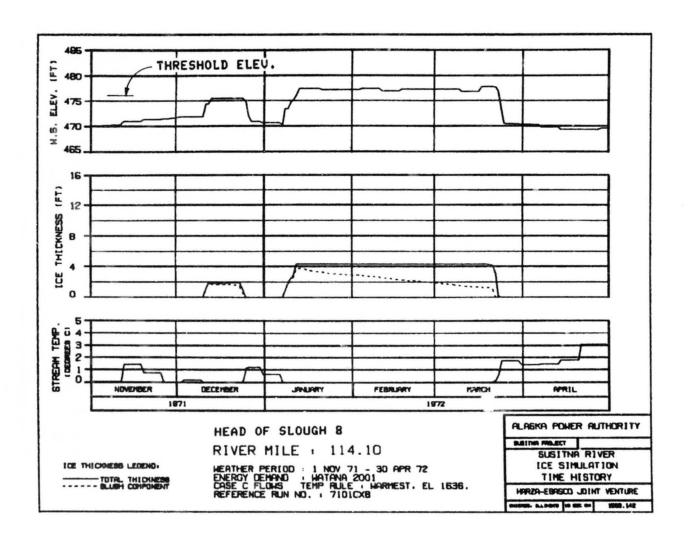




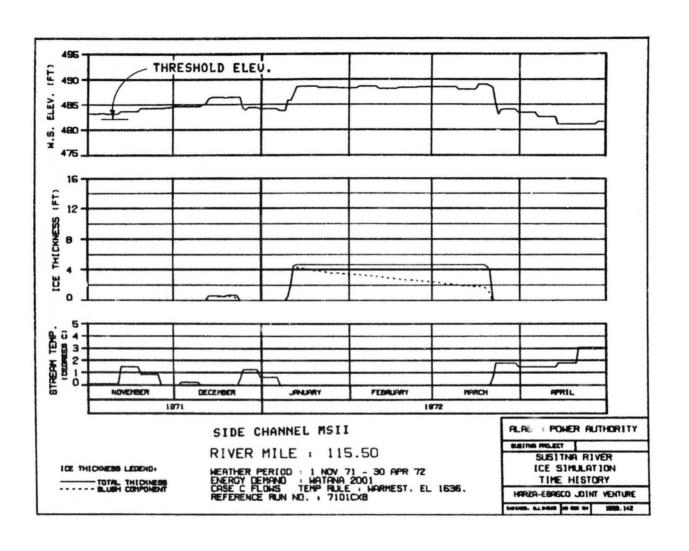






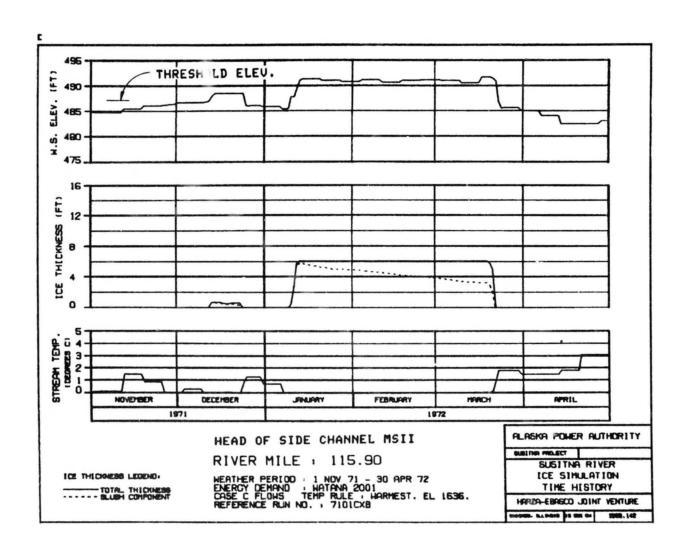


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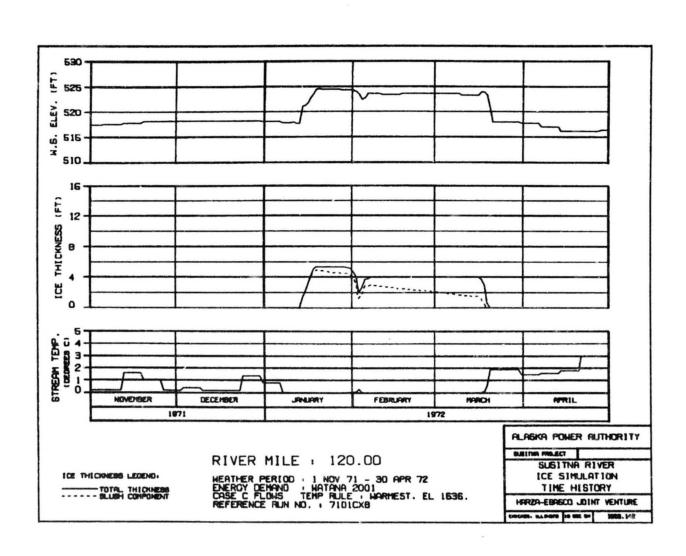


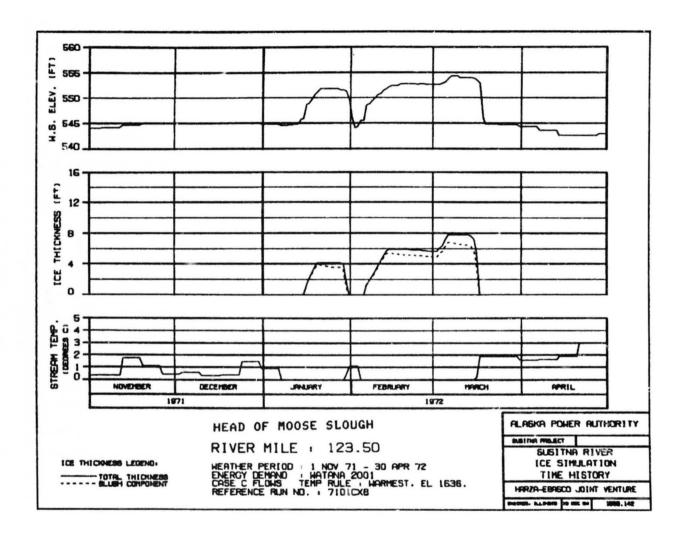
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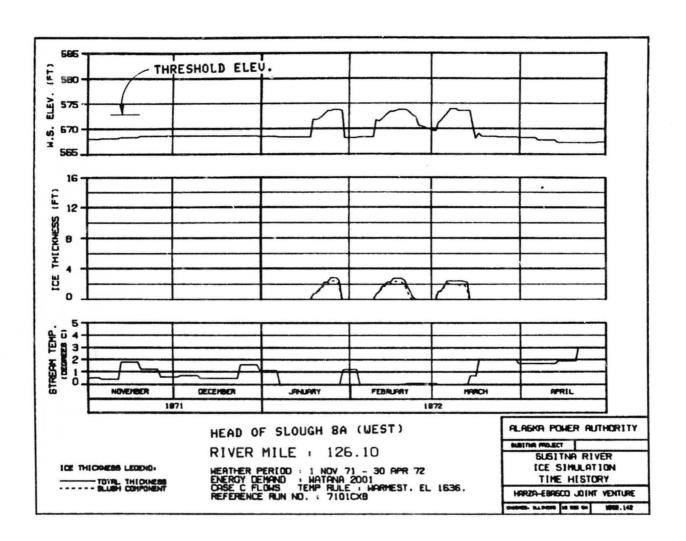


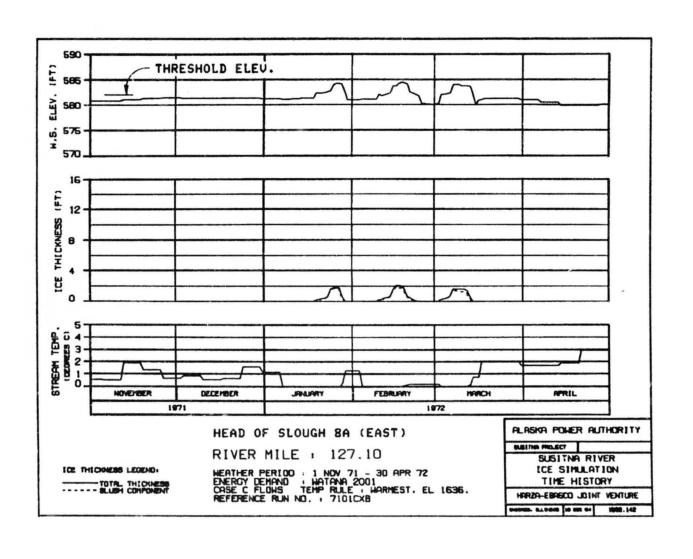
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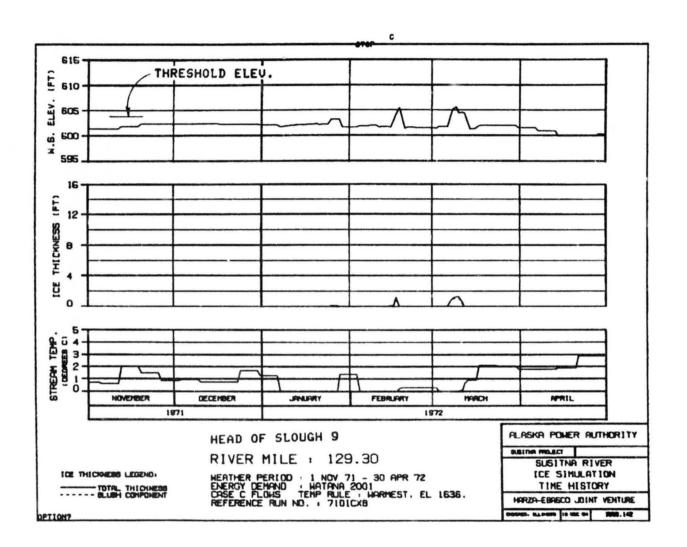


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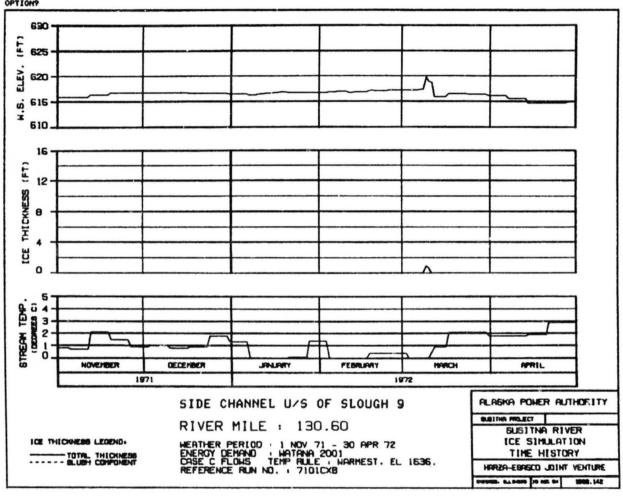


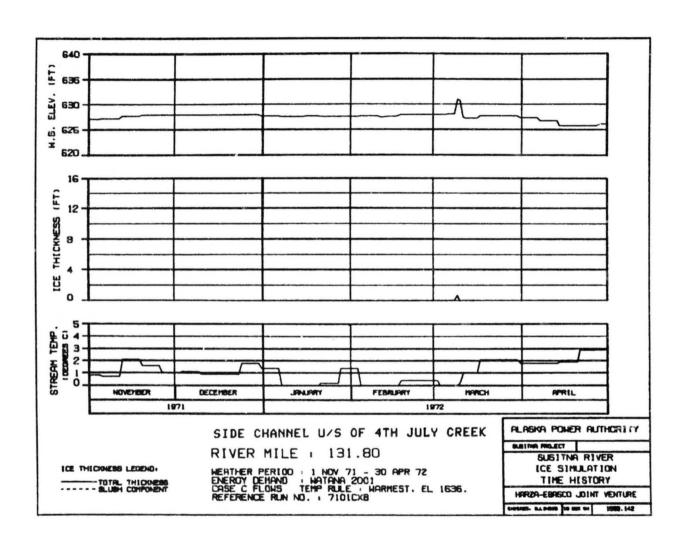
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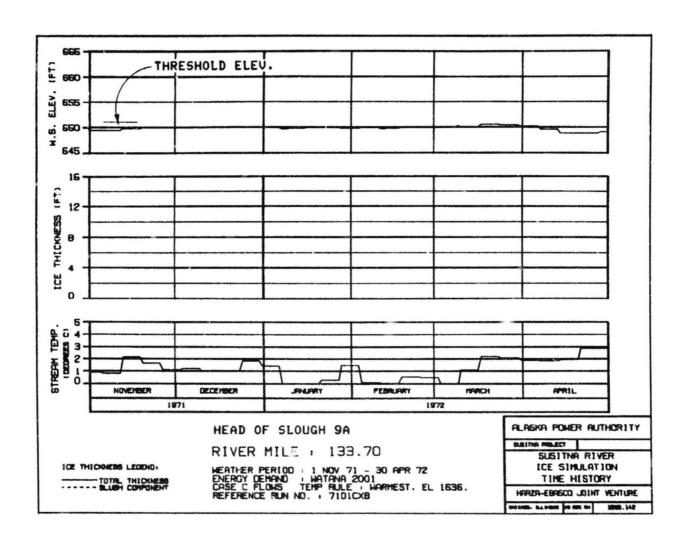
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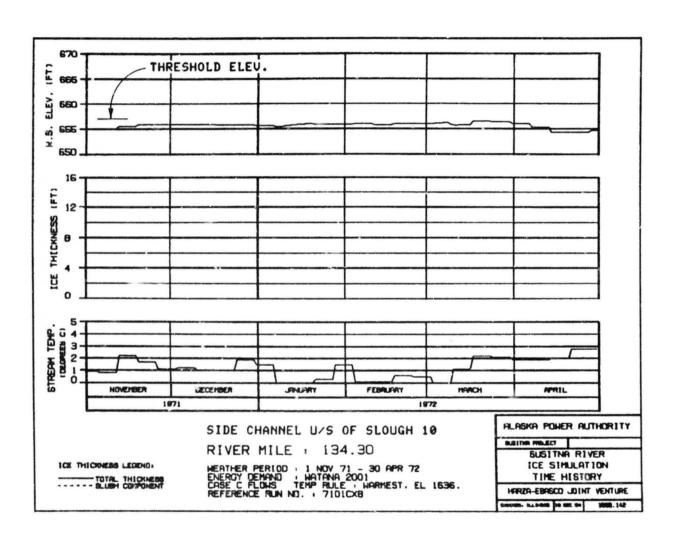




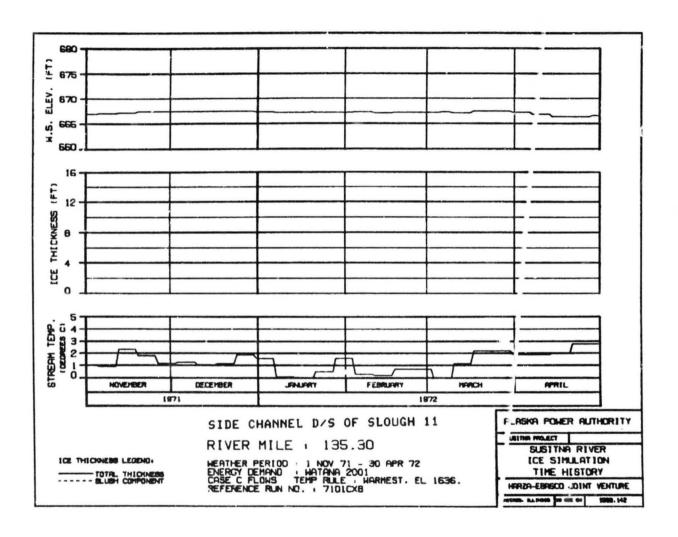


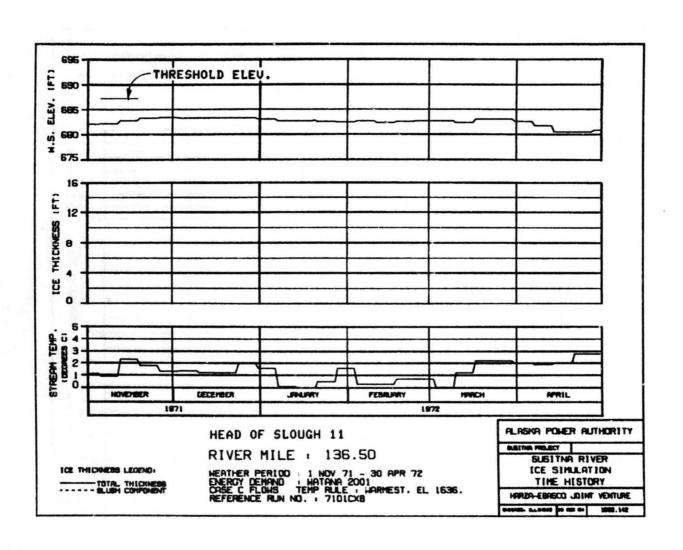
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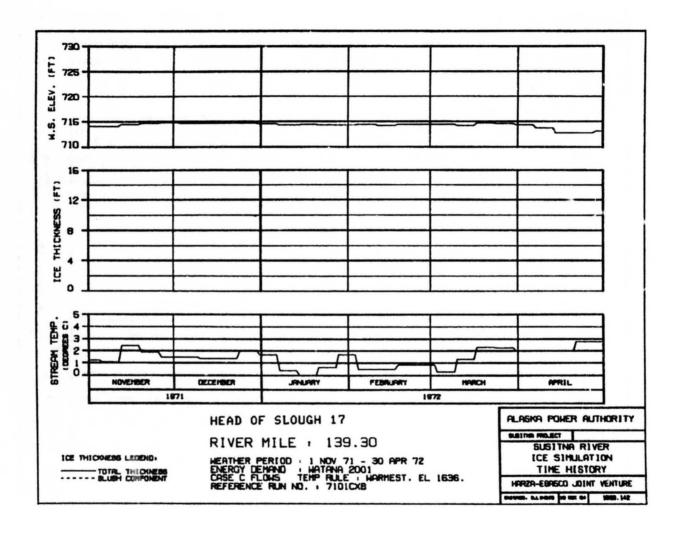


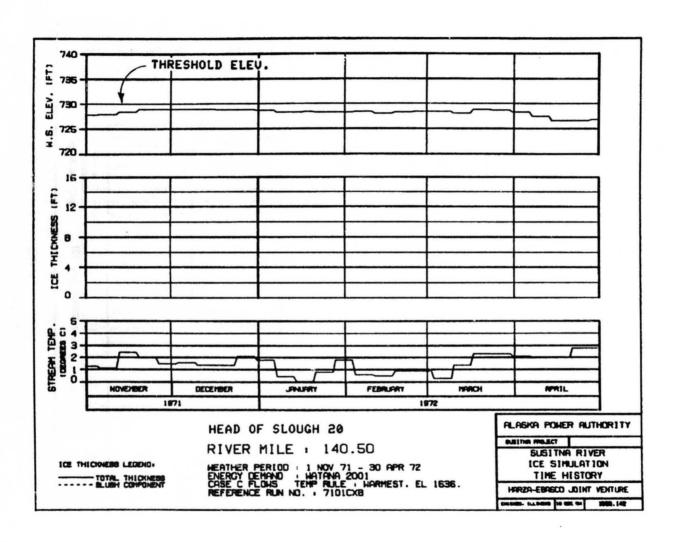


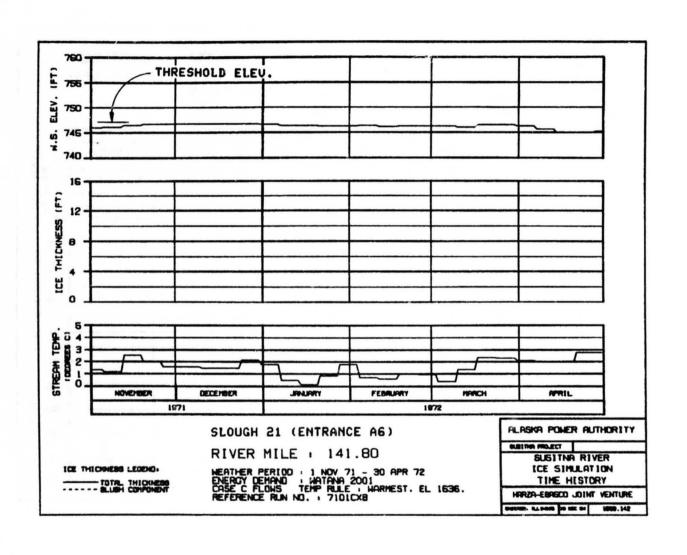
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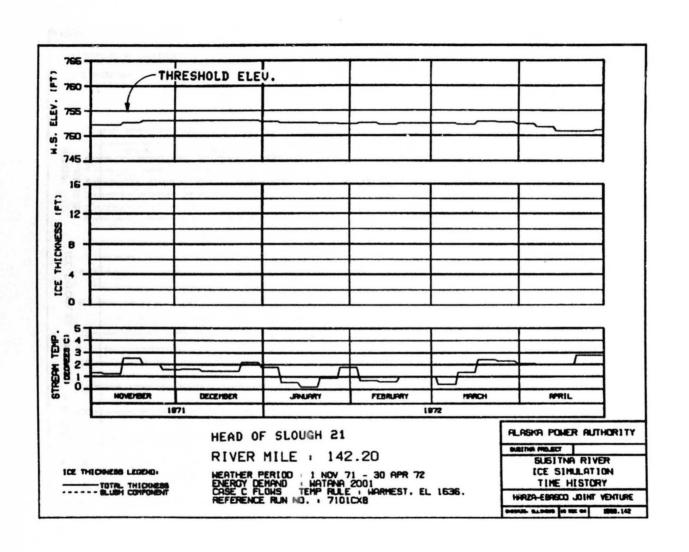


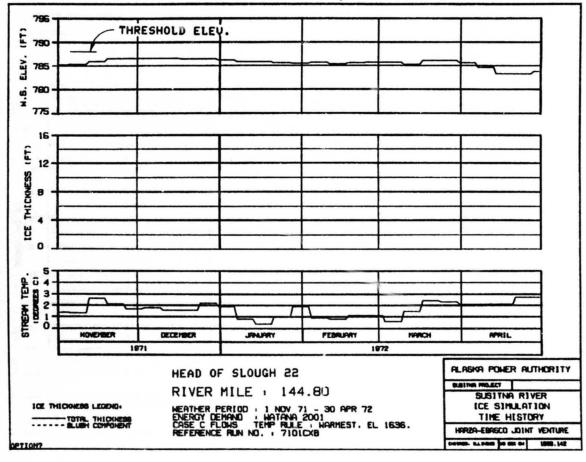






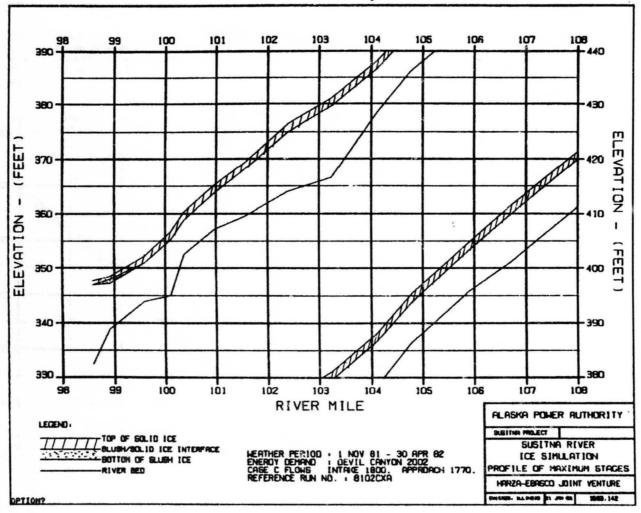


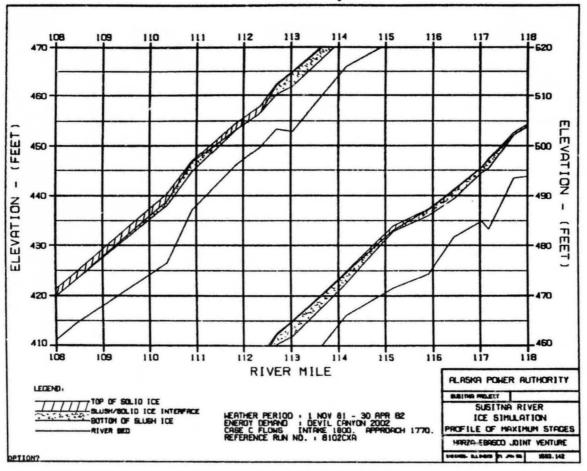


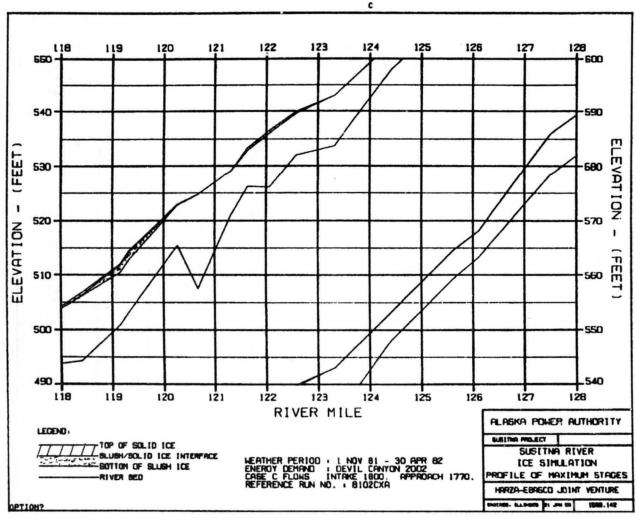


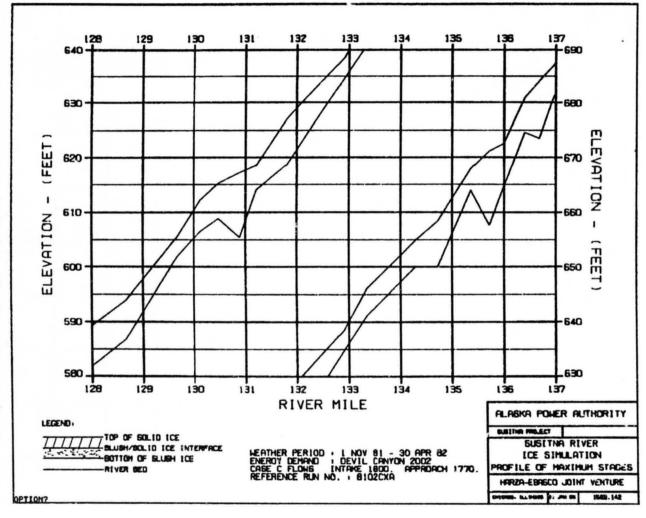




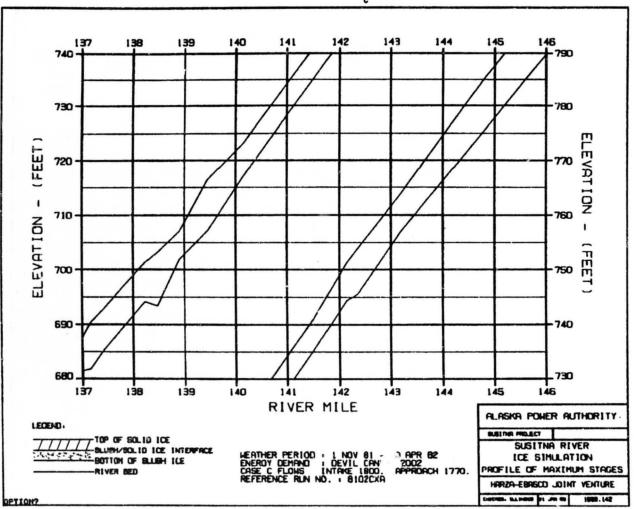




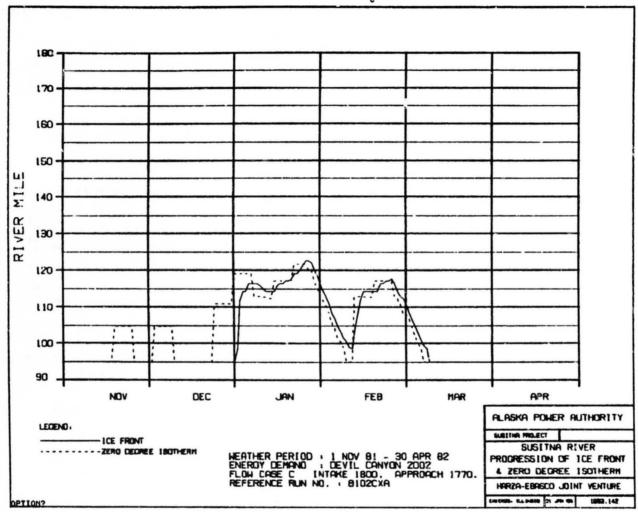


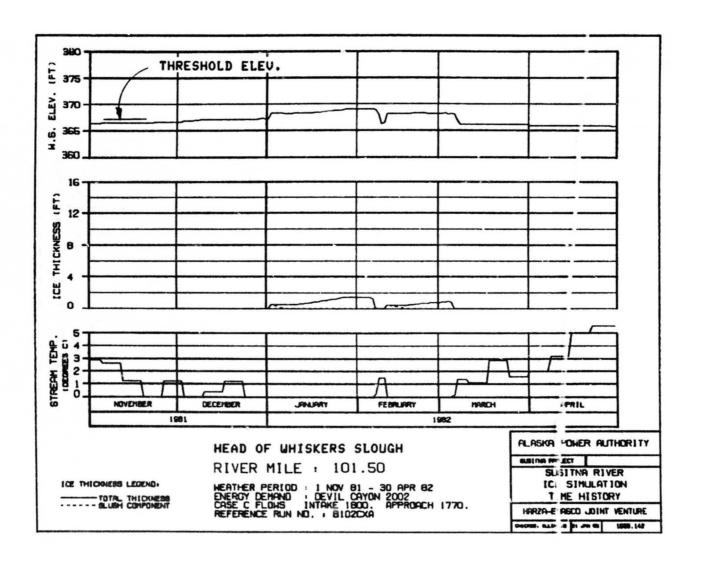




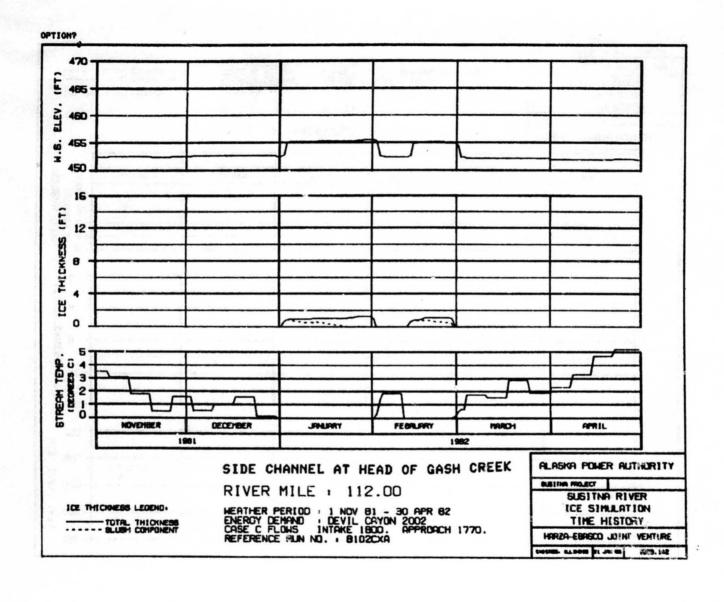




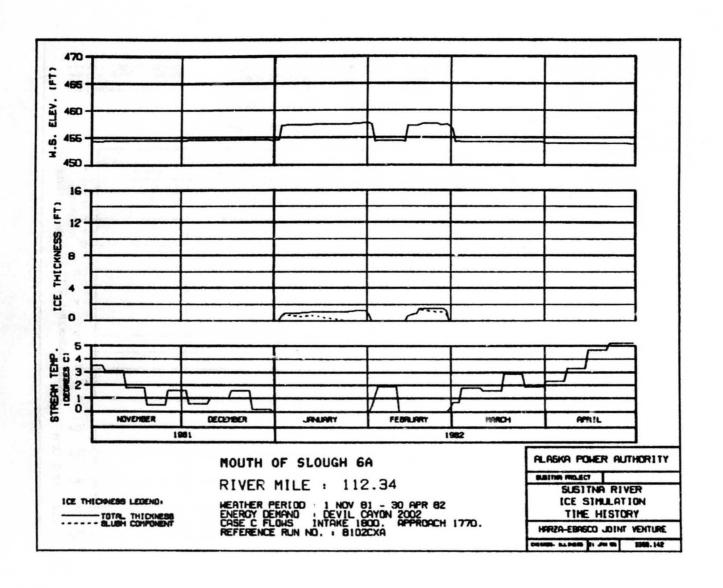


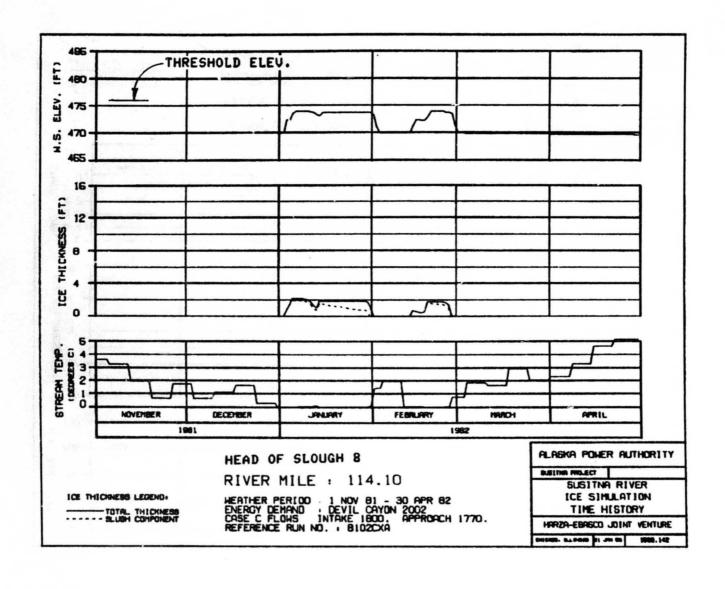


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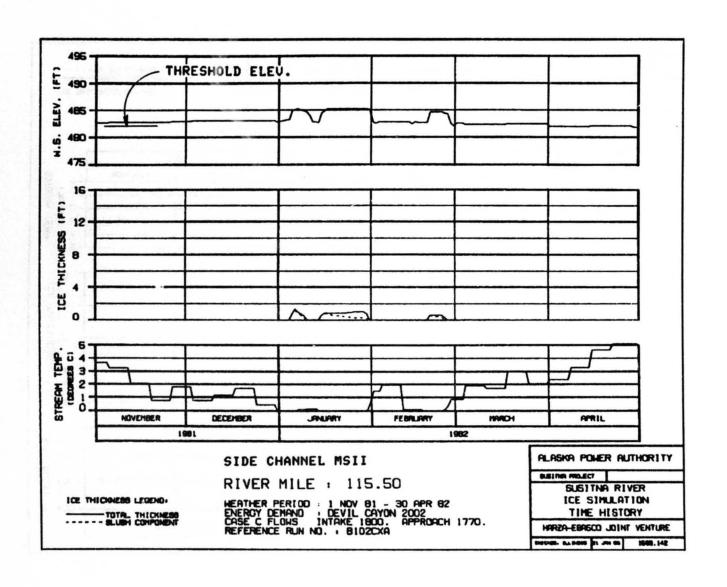
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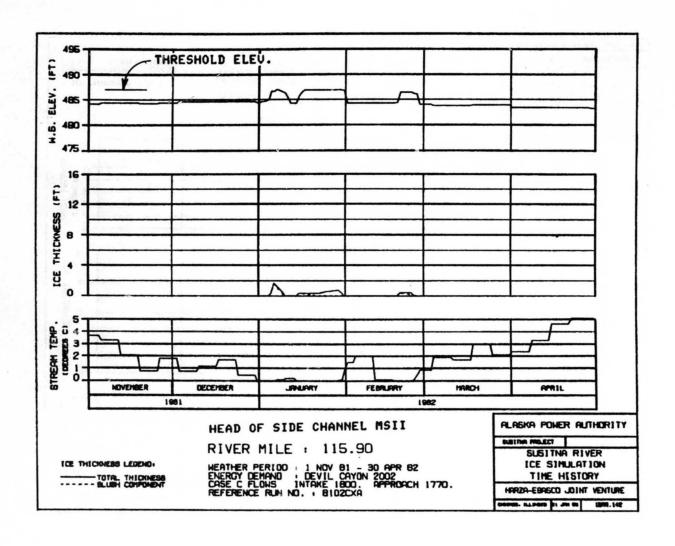




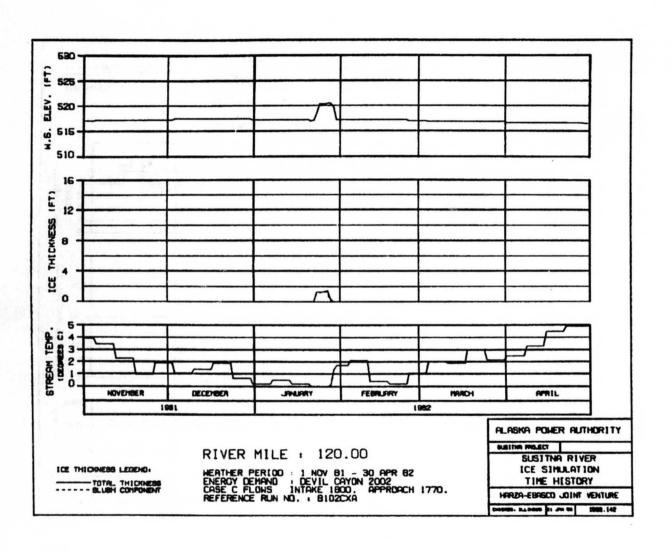
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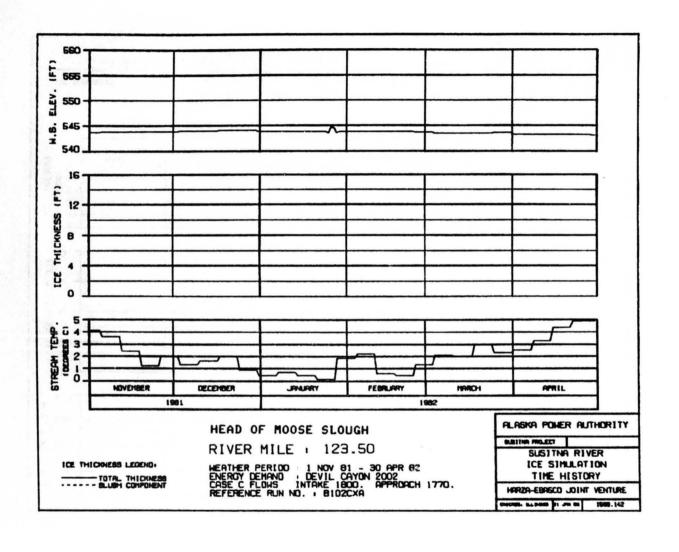
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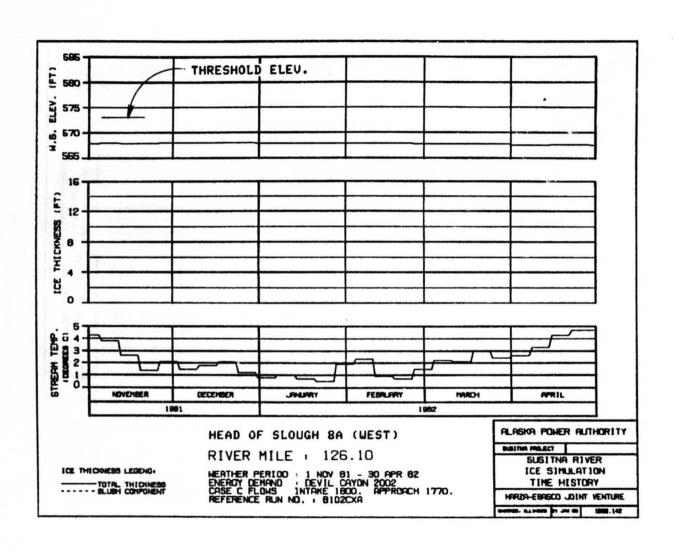


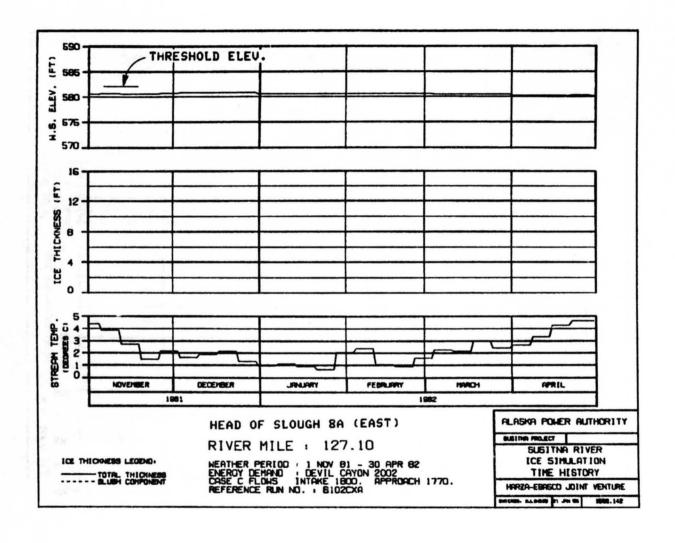


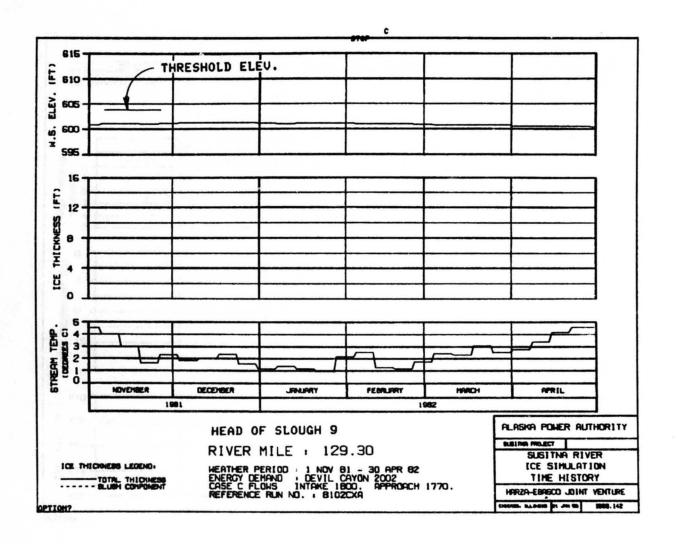
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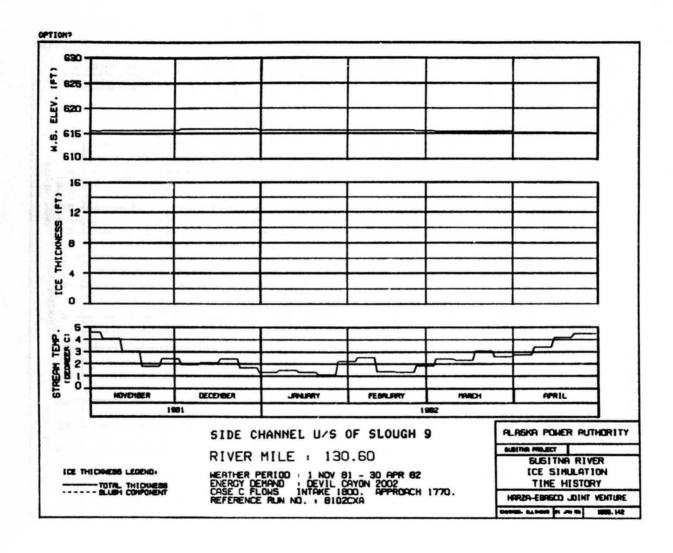




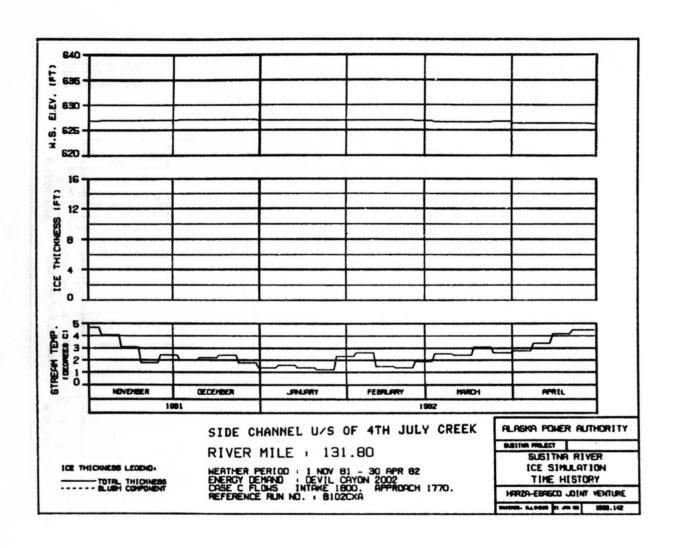


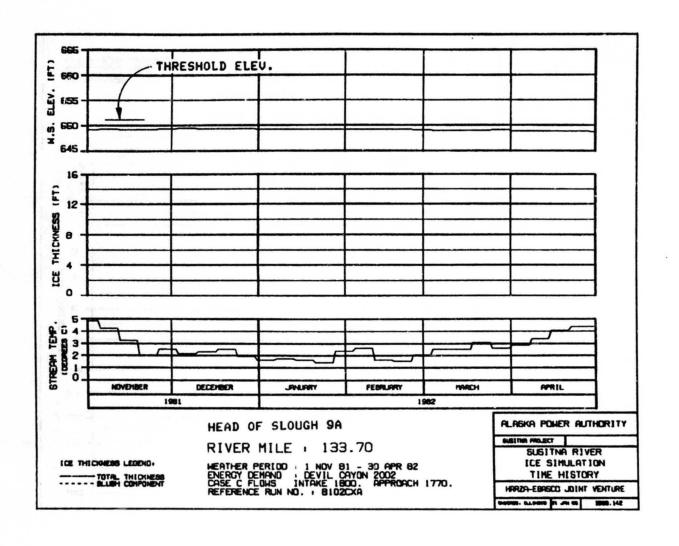


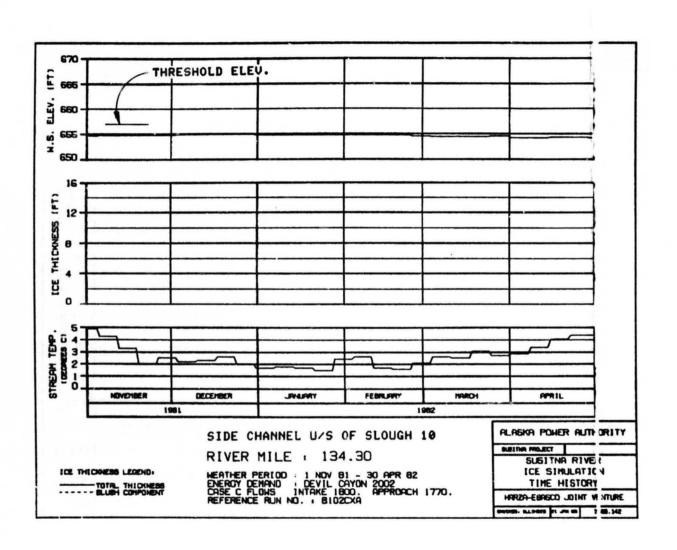


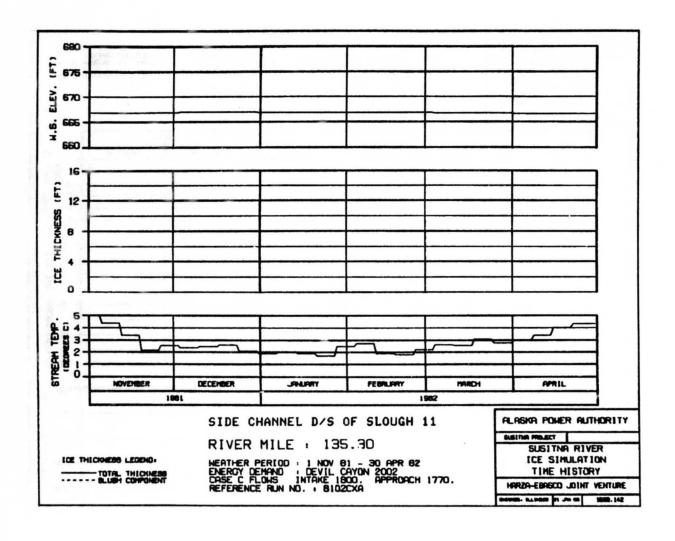


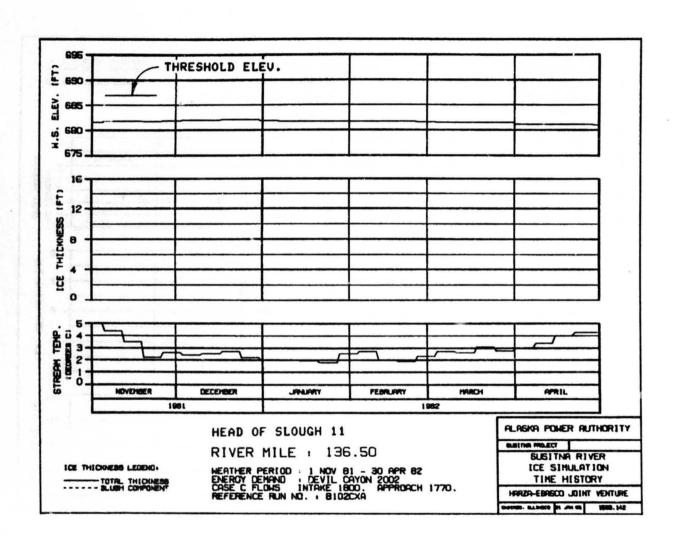
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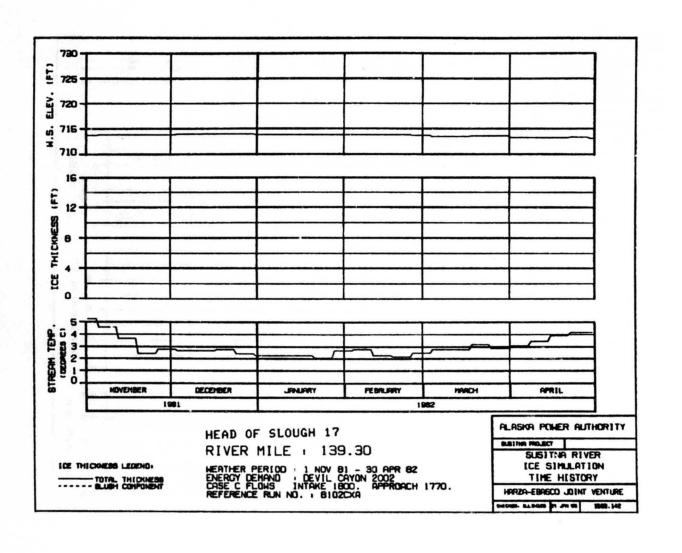




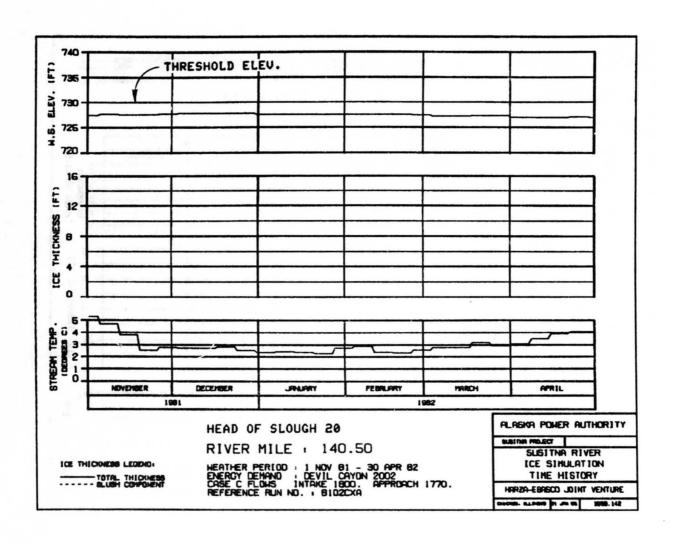


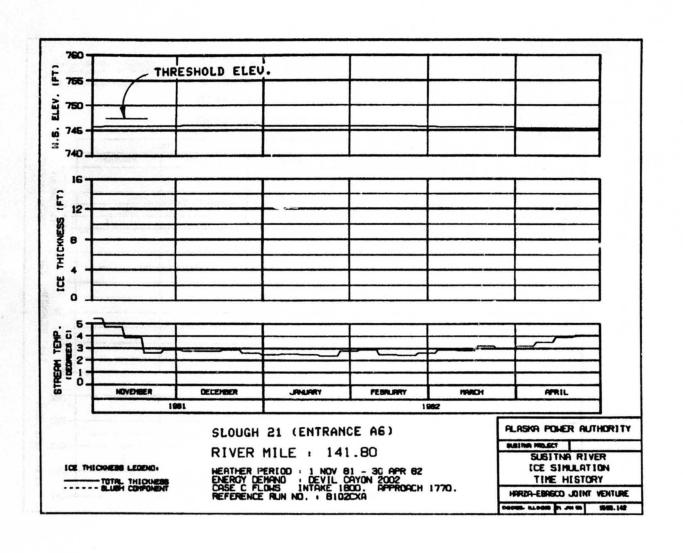


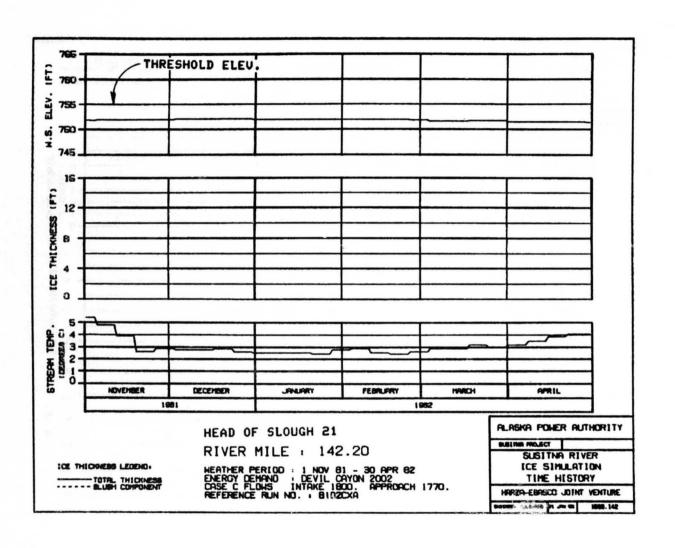


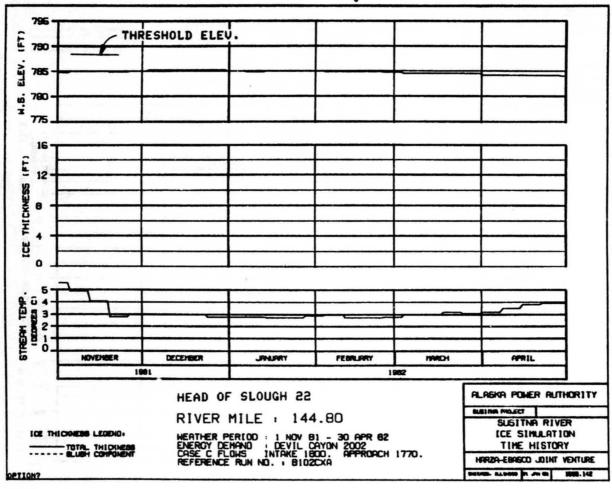


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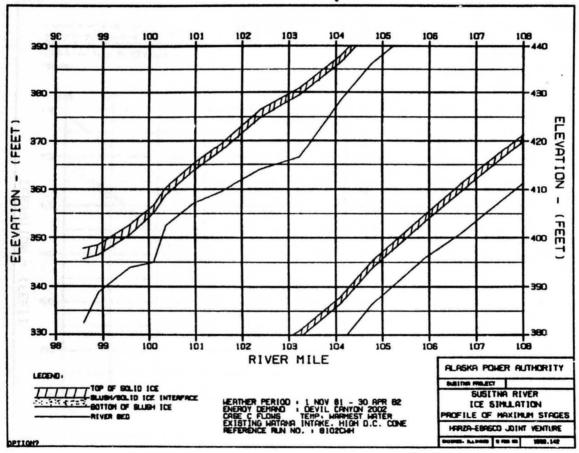




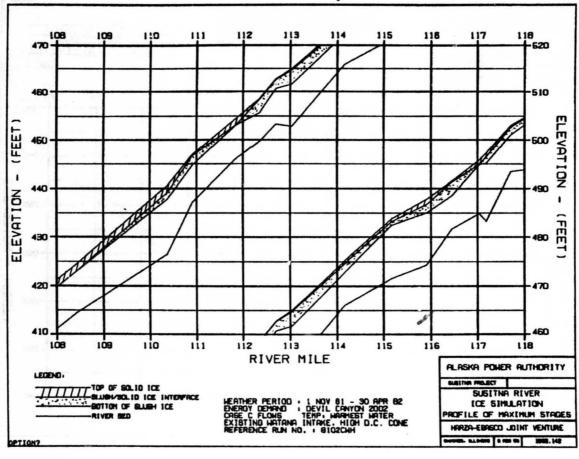




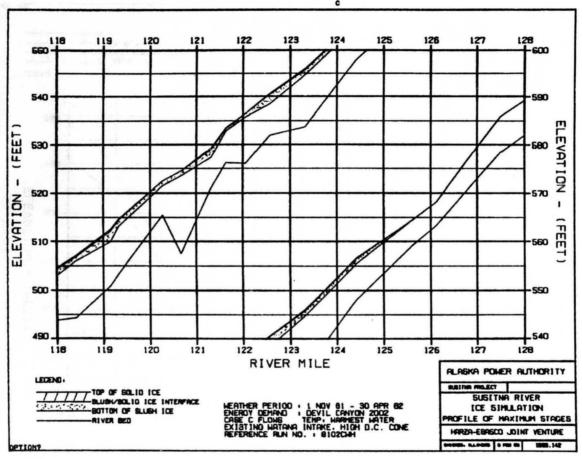




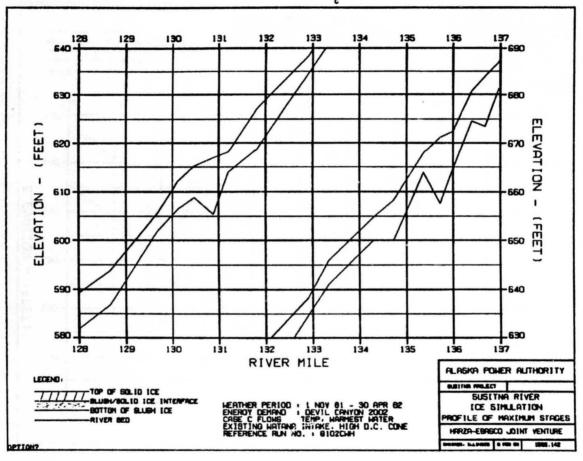


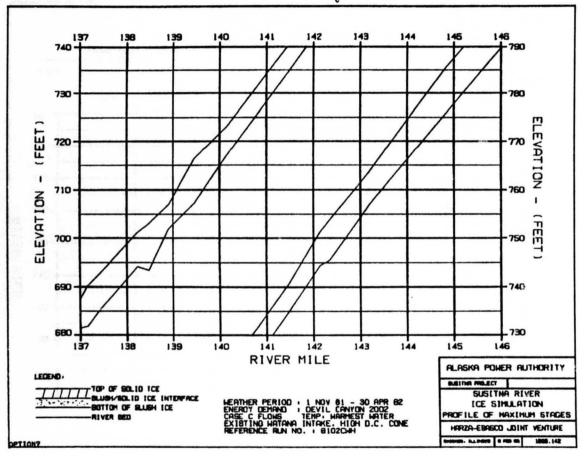


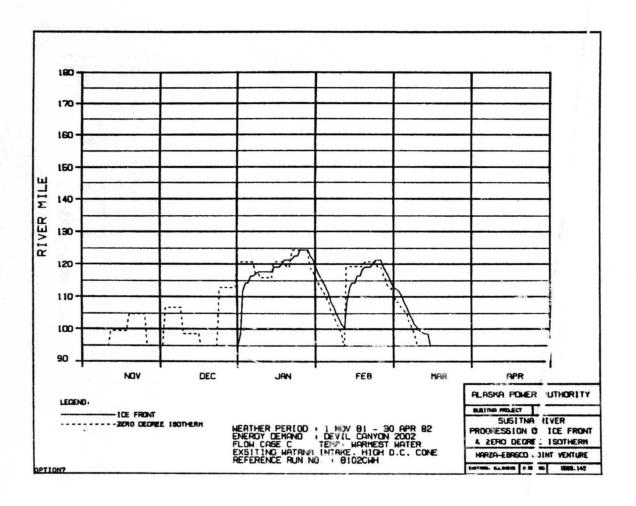


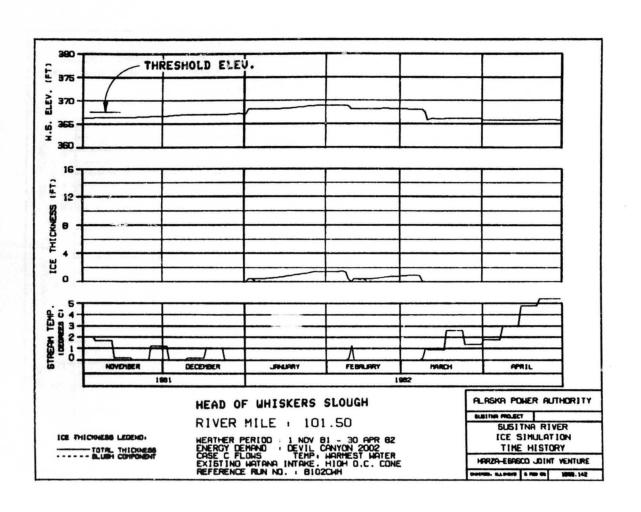


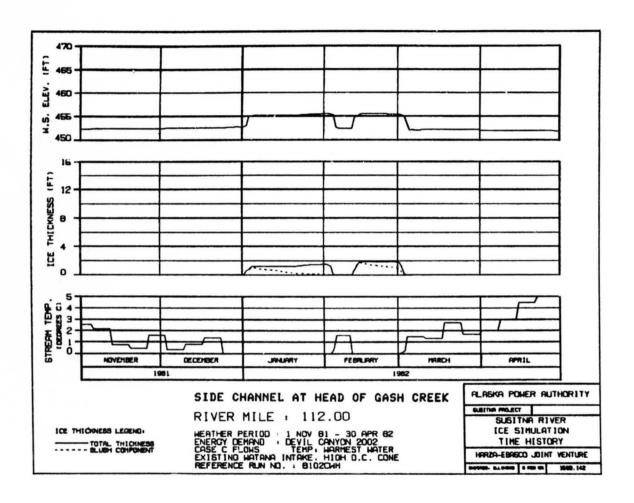


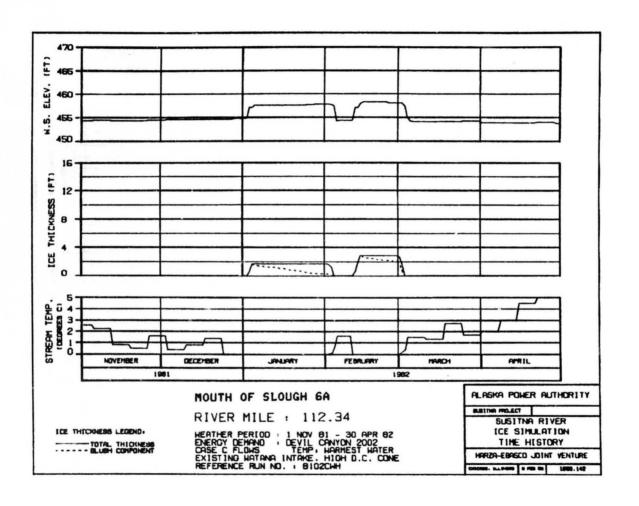




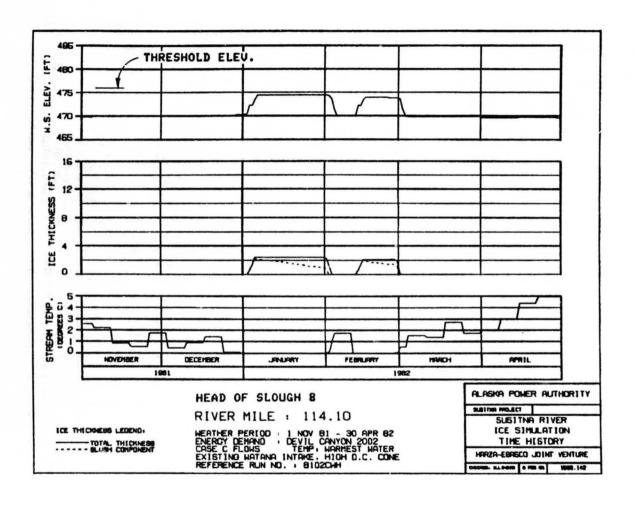




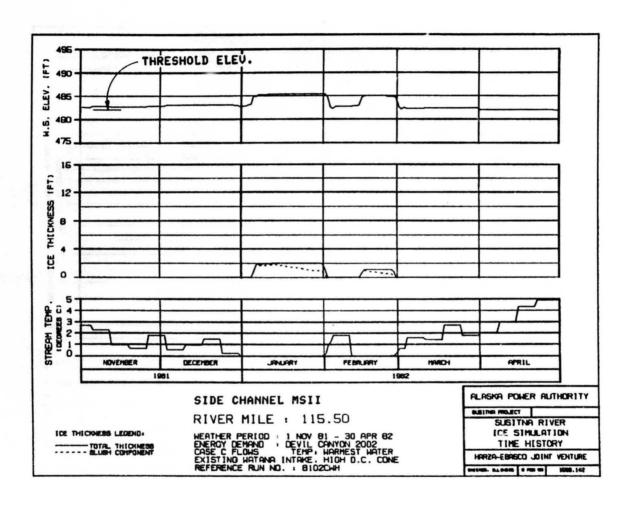


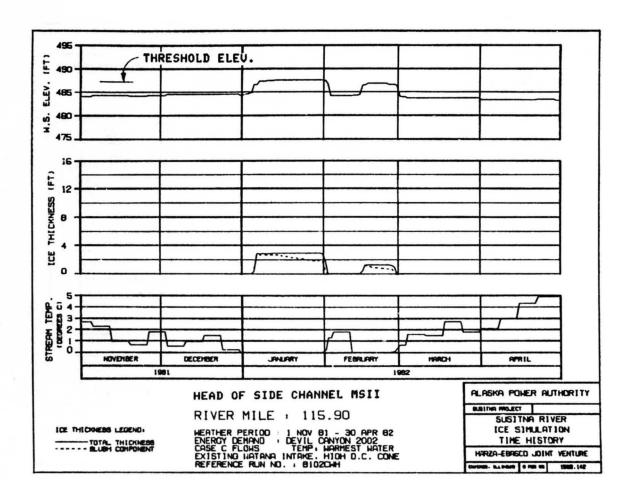


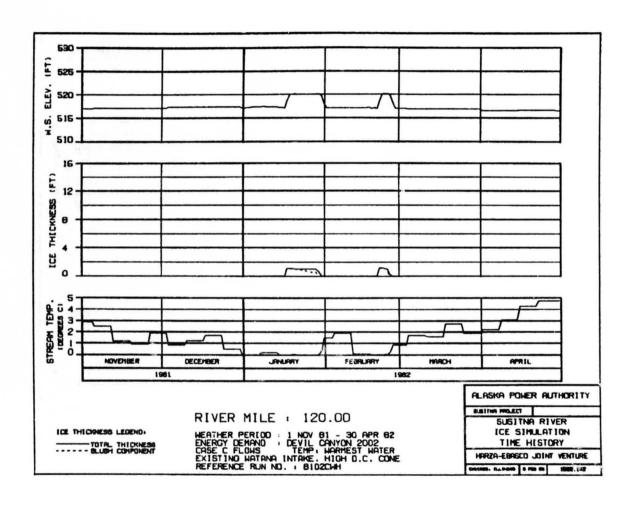
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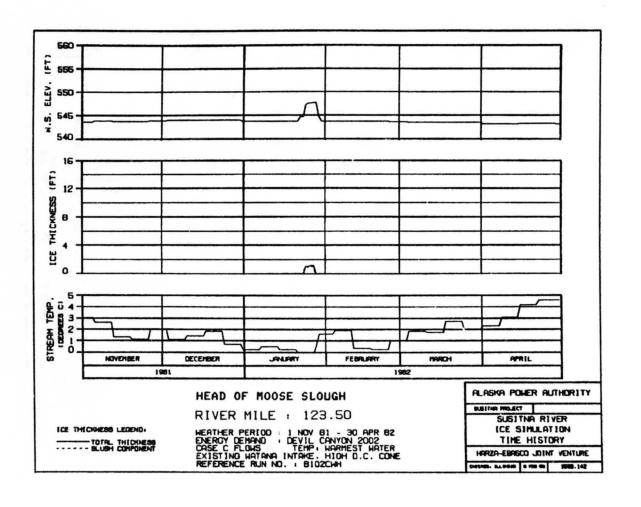


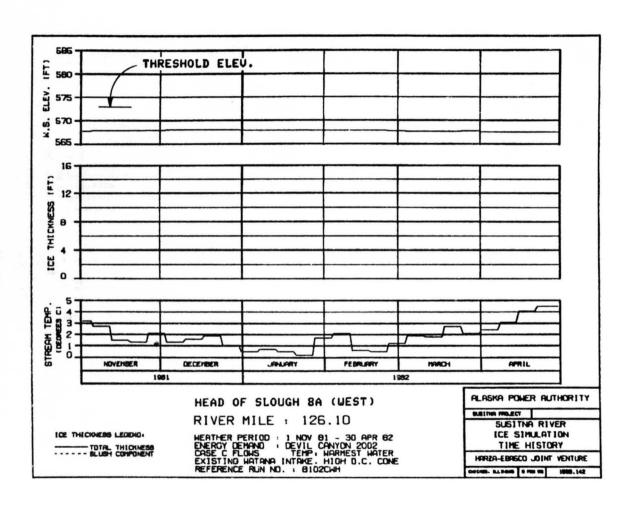
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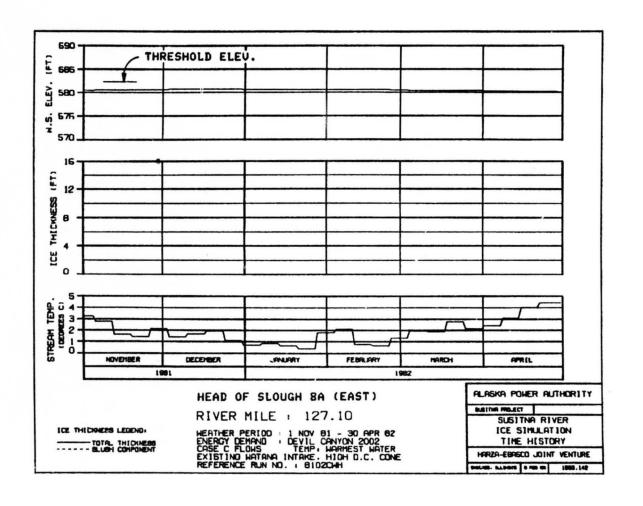




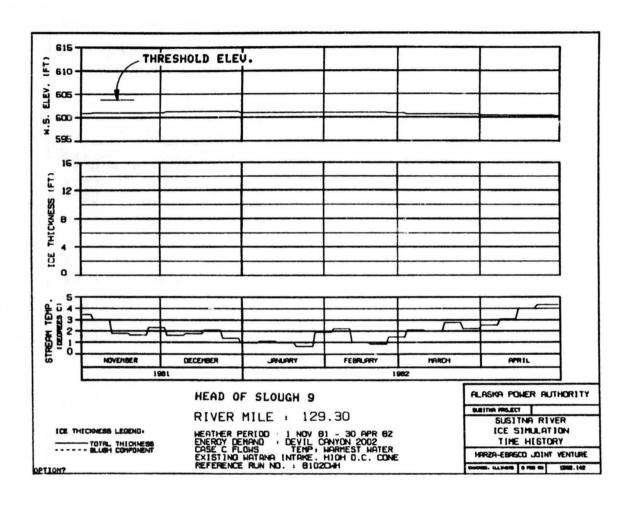


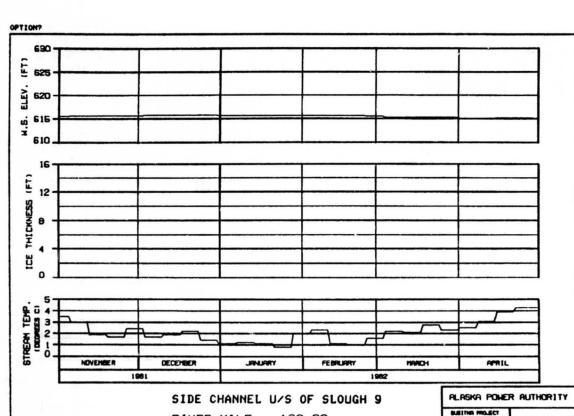




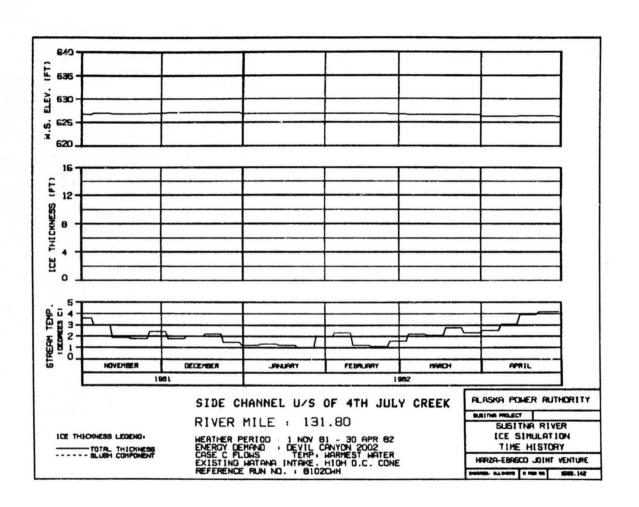


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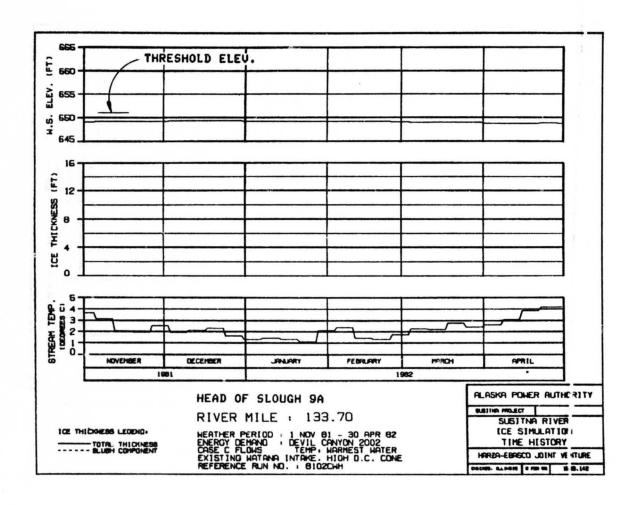


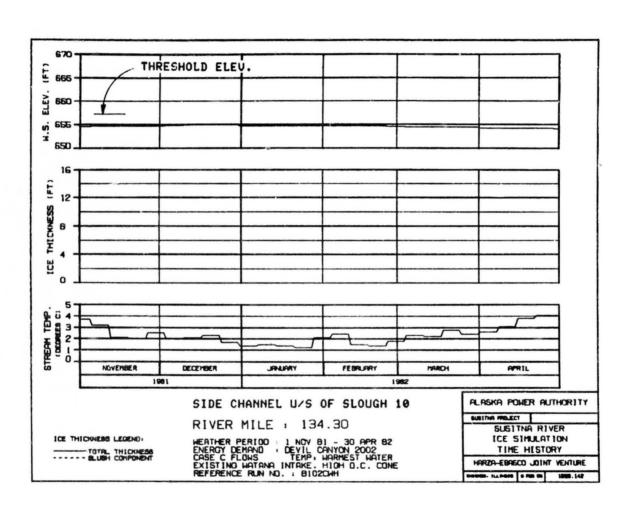
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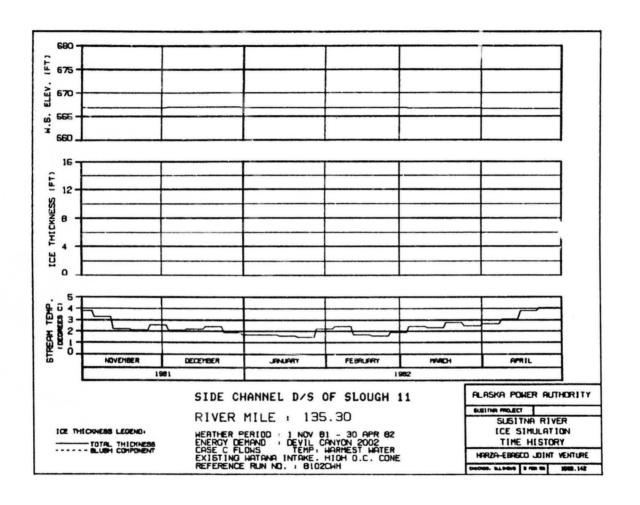


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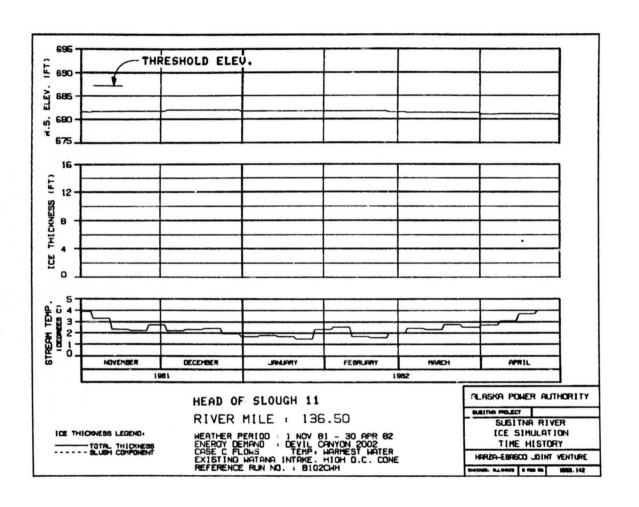
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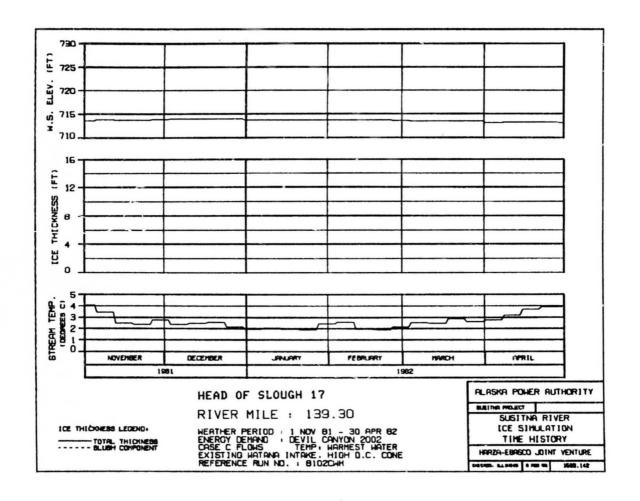




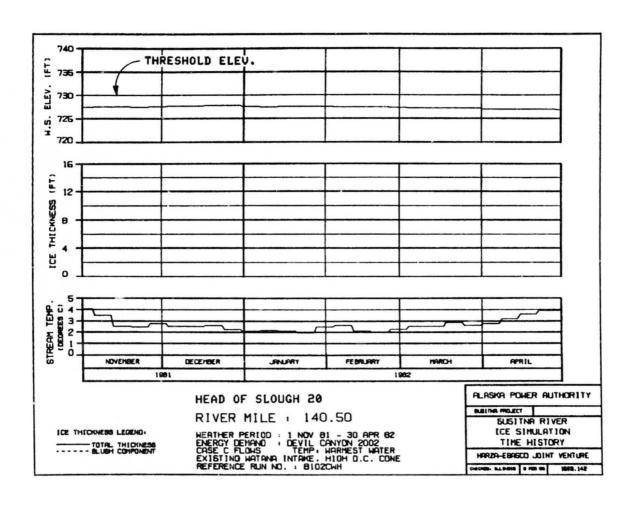
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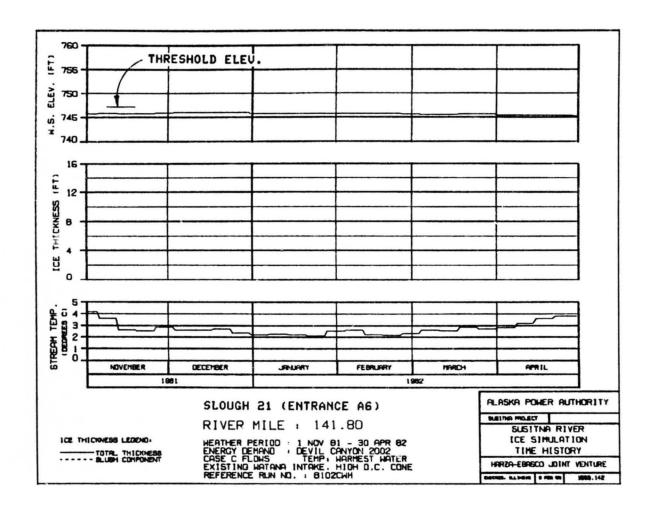
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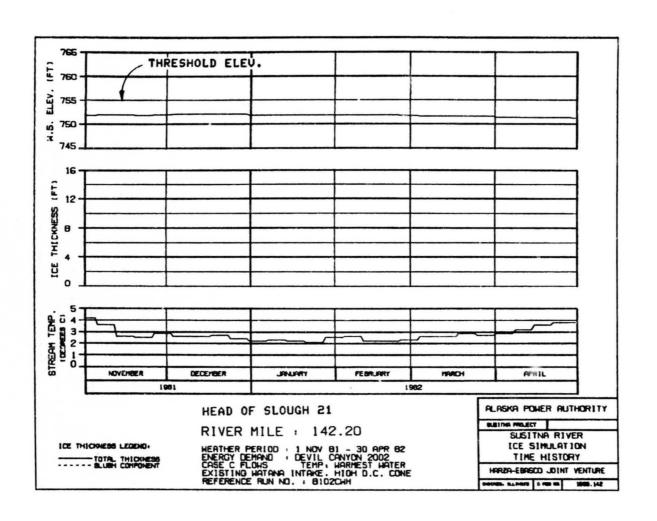
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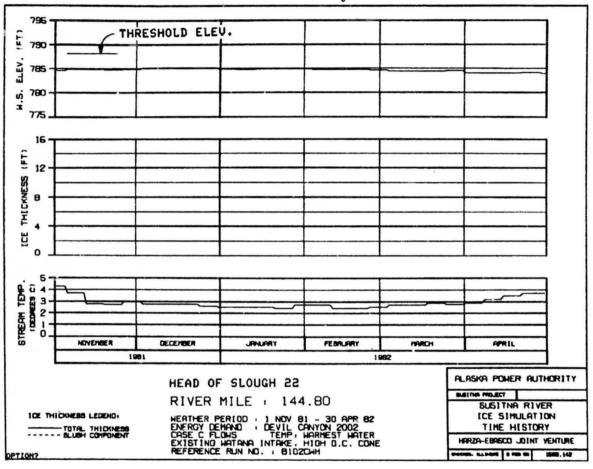
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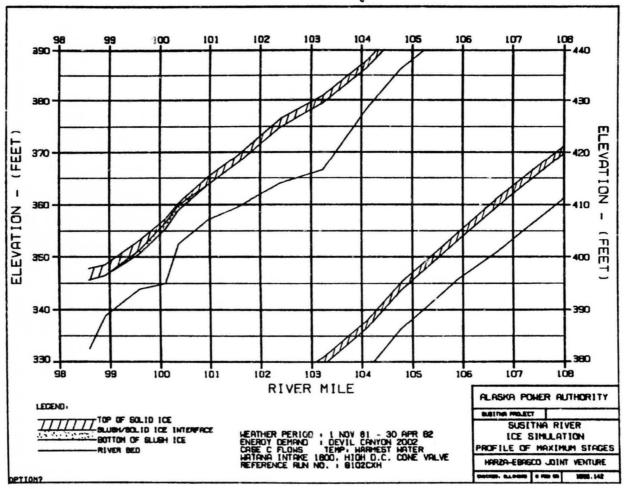




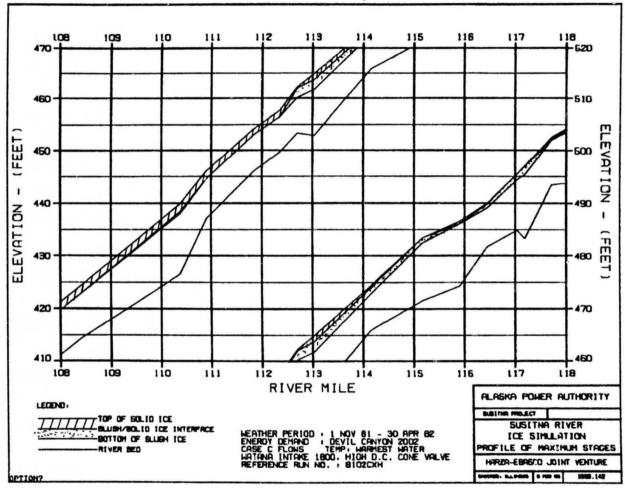


## EXHIBIT X

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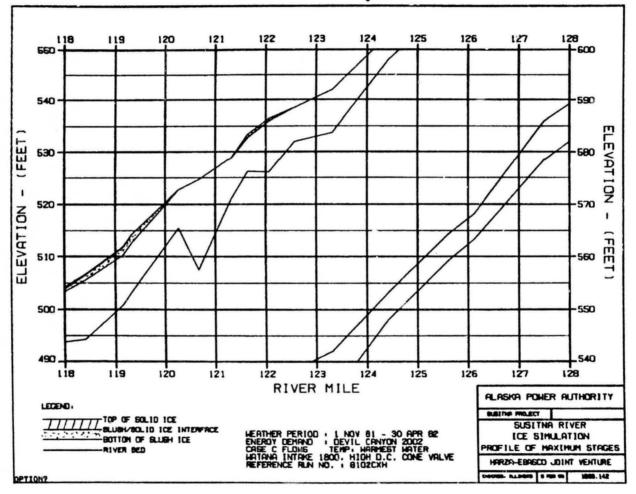




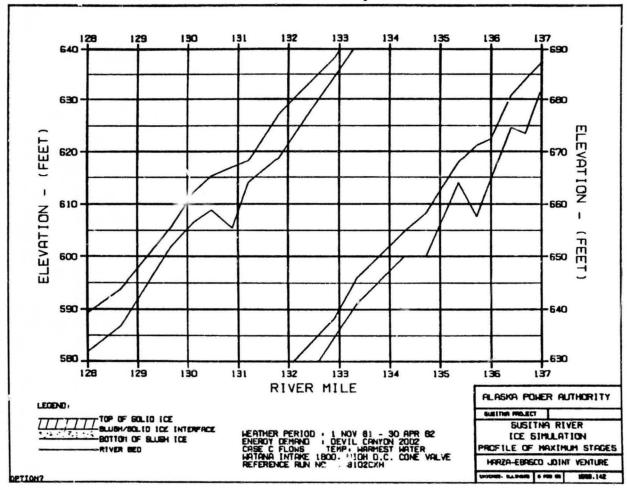


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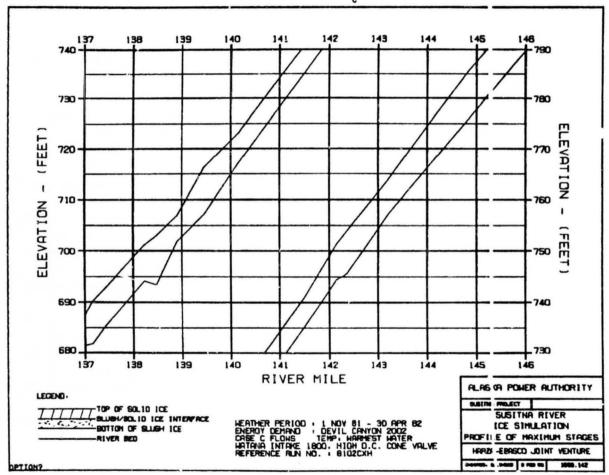


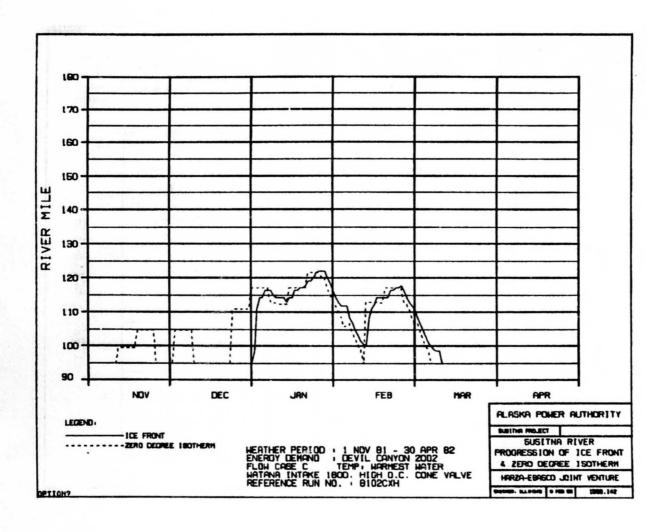


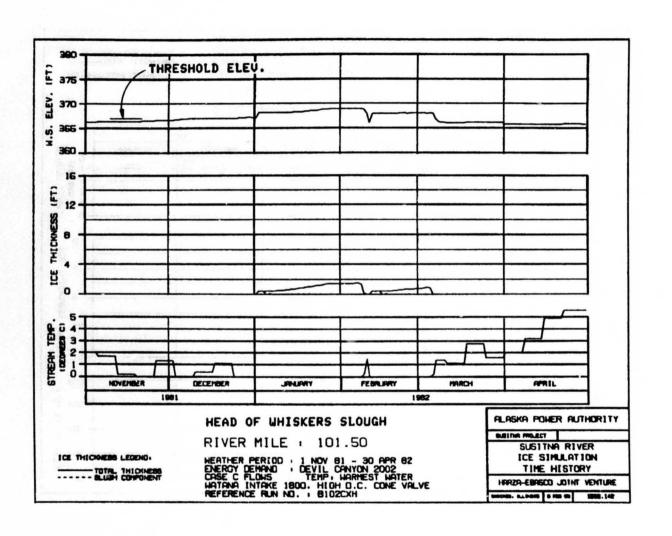


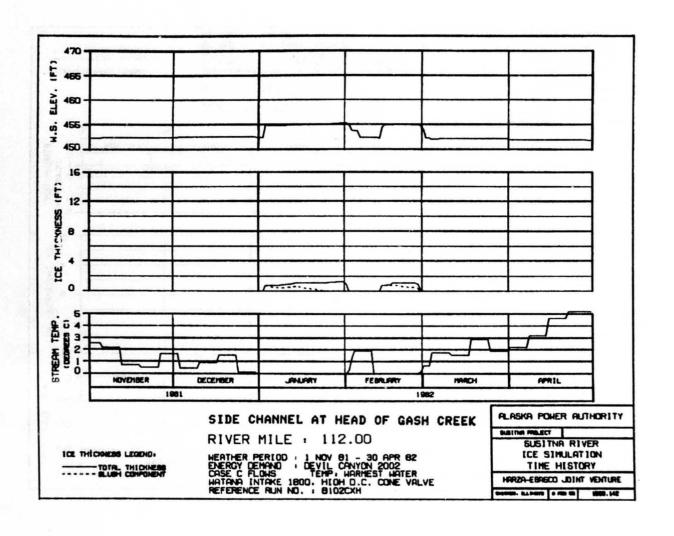


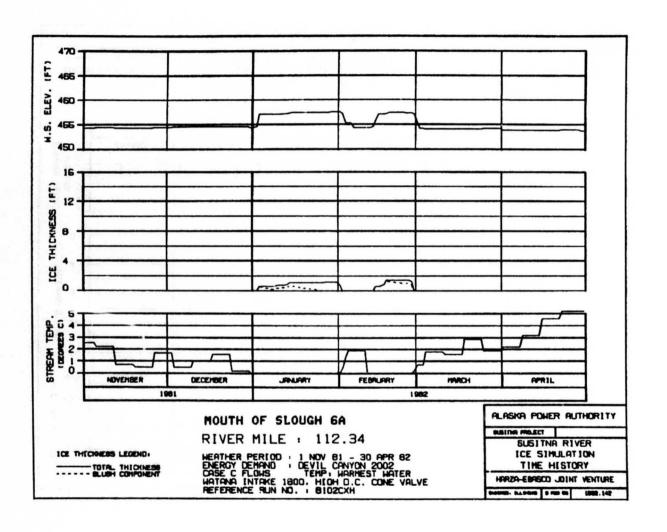
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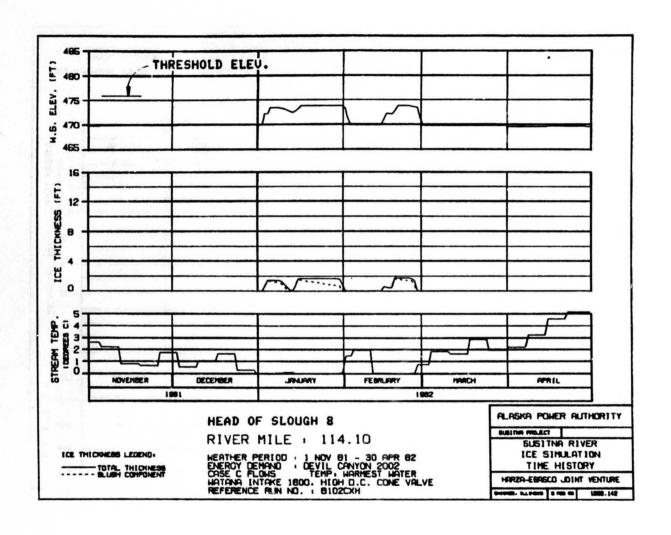


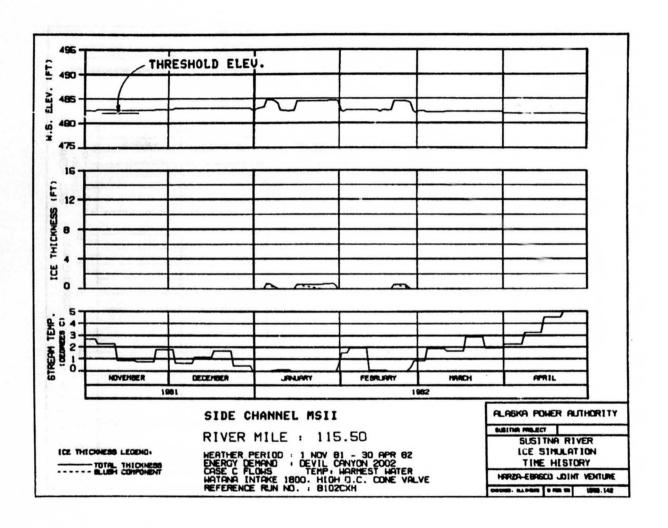


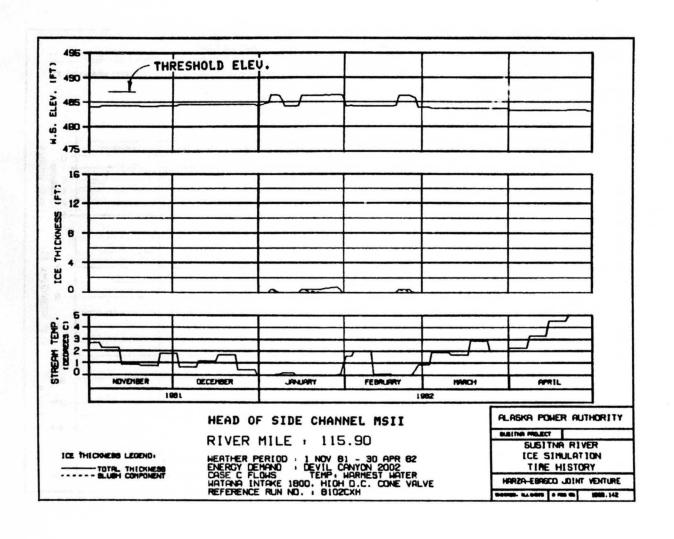




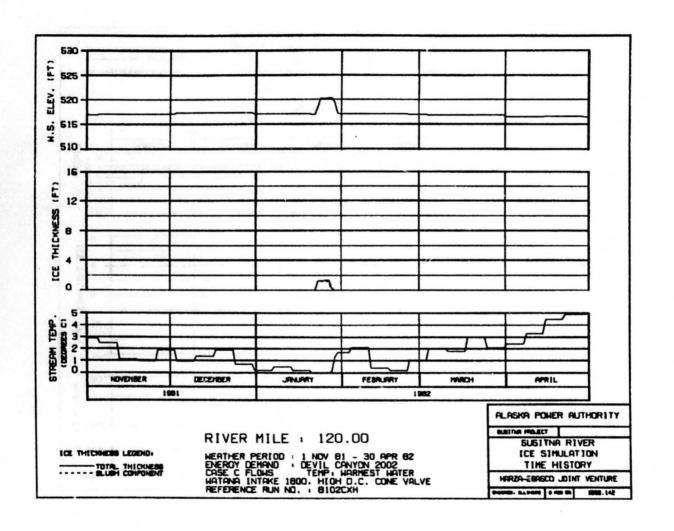


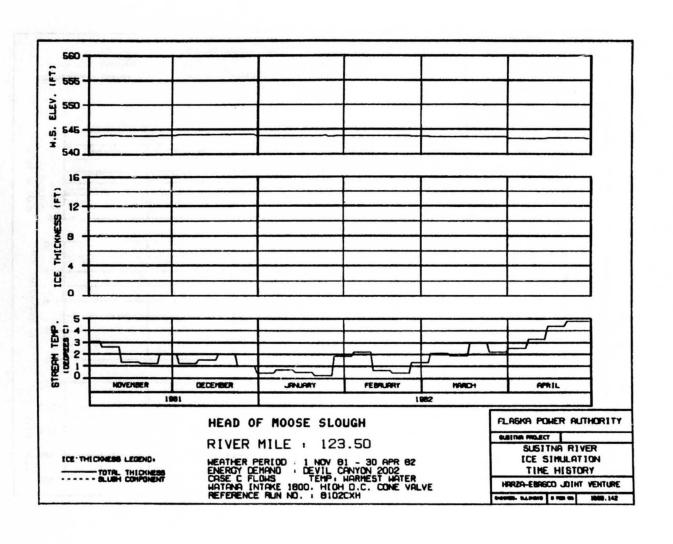


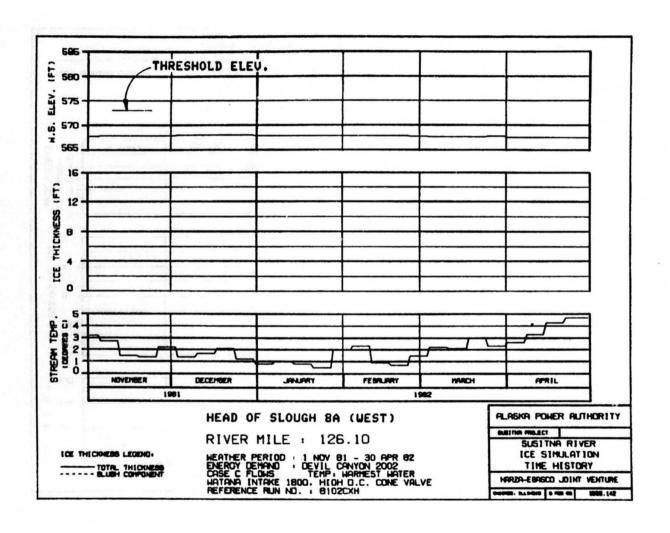


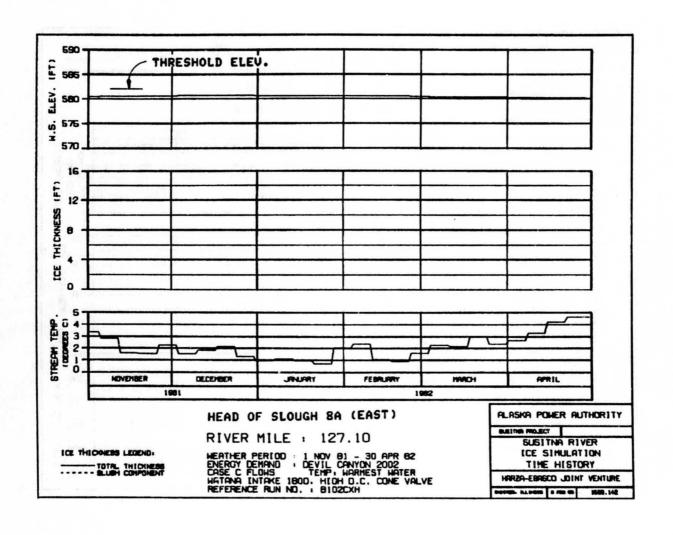


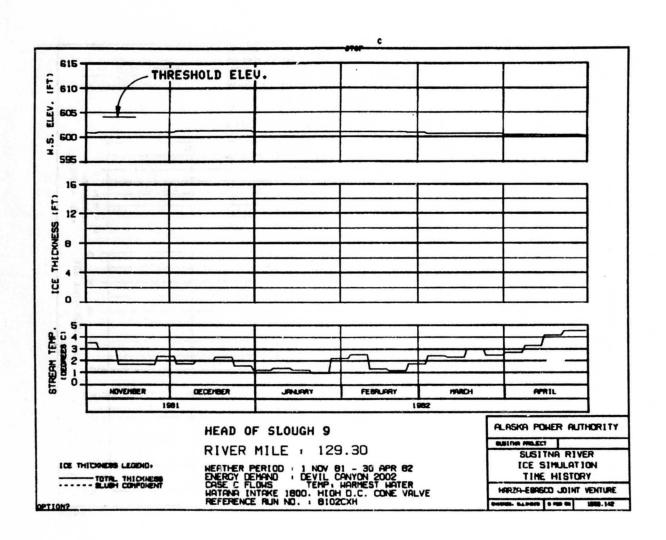
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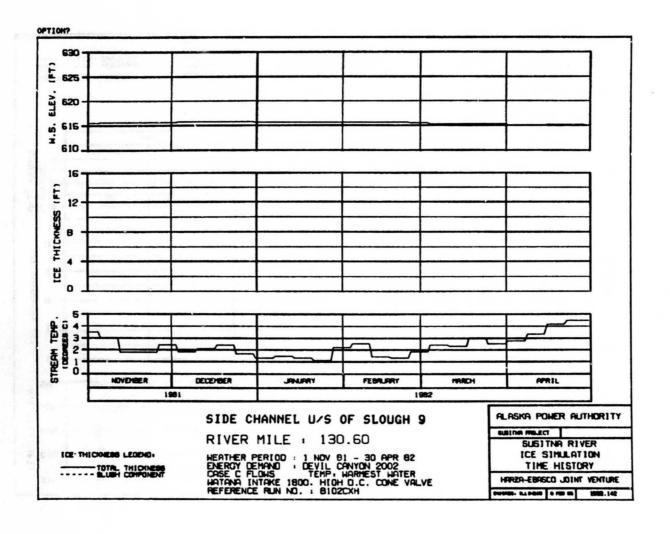


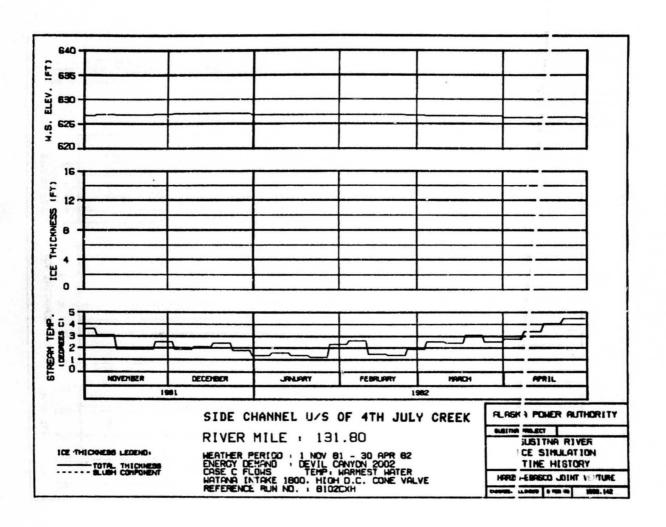


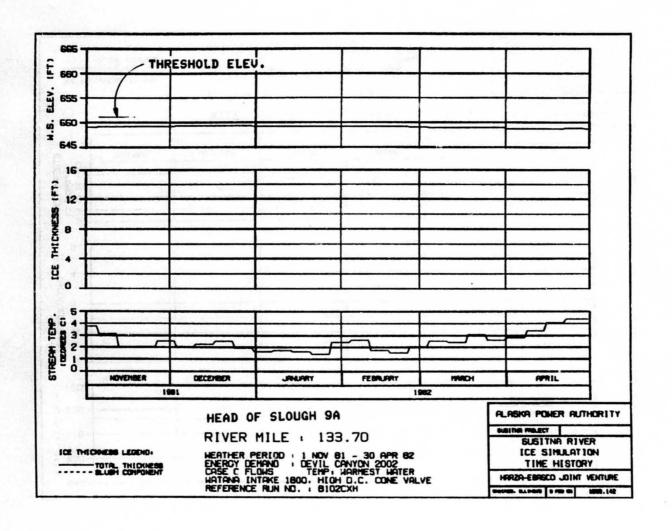




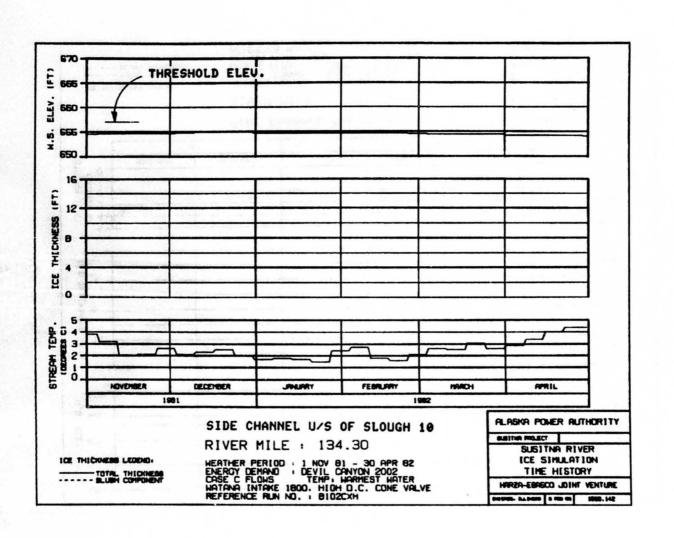


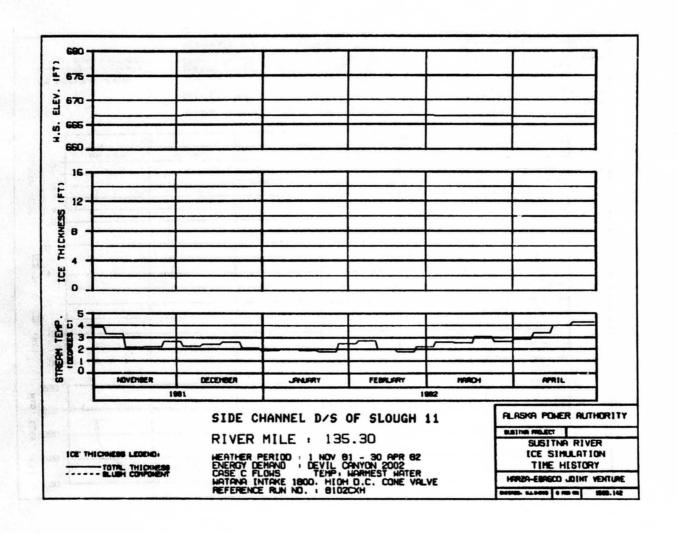




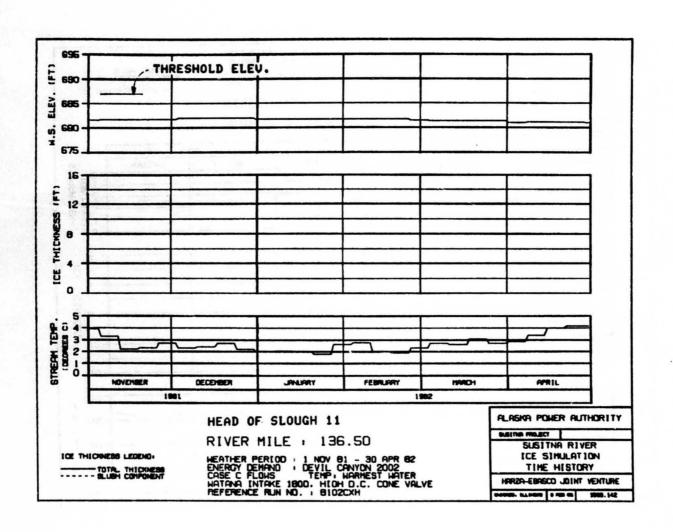


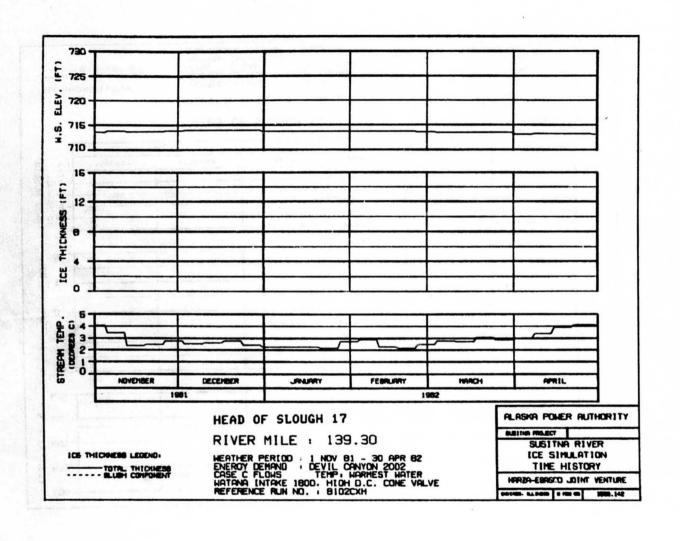
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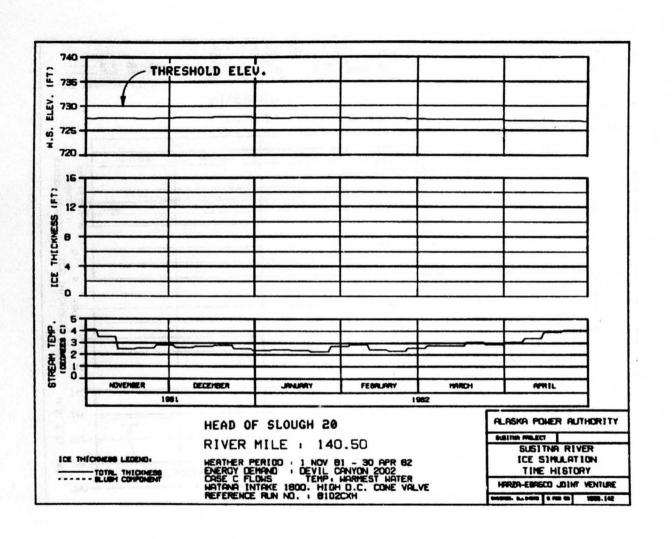


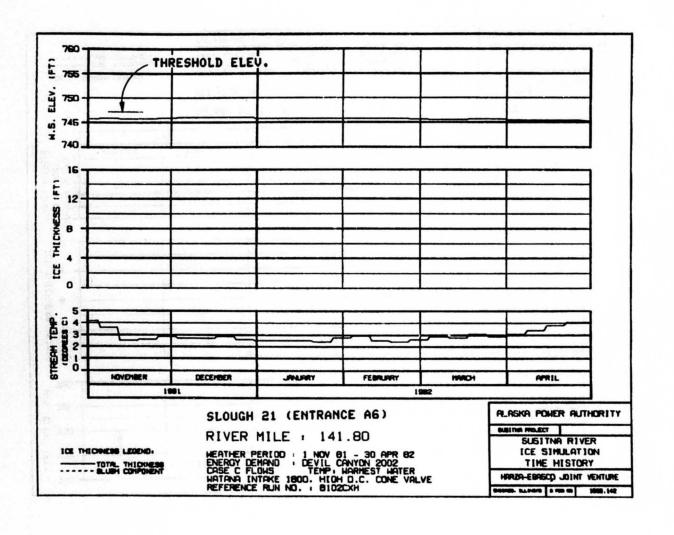


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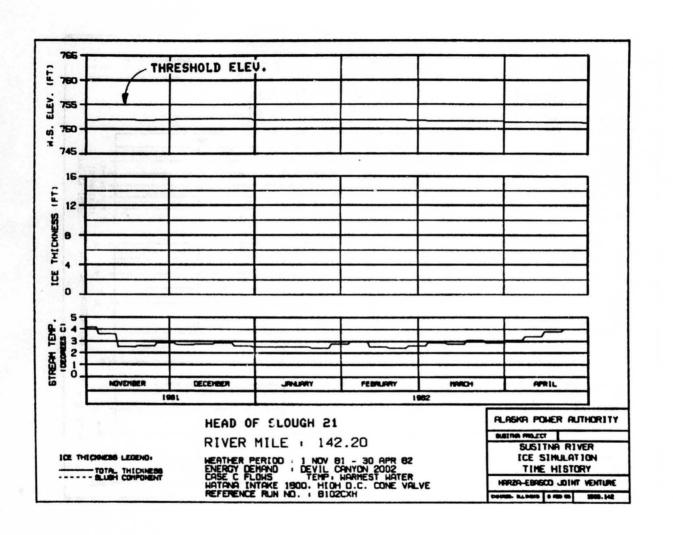




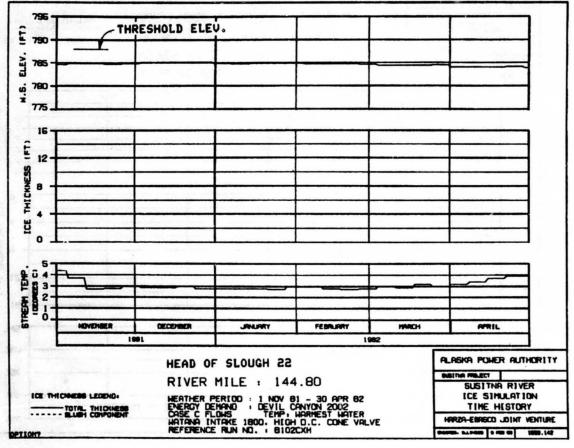




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