

SUSITNA HYDROELECTRIC PROJECT

FEDERAL ENERGY REGULATORY COMMISSION PROJECT No. 7114

INSTREAM ICE SIMULATION STUDY

FINAL REPORT

HARZA-EBASCO SUSITNA JOINT VENTURE OCTOBER 1984 DOCUMENT NO. 1986

ALASKA POWER AUTHORITY

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no. 1986

INSTREAM ICE SIMULATION STUDY

Report by Harza-Ebasco Susitna Joint Venture

> Prepared for Alaska Power Authority

> > Final Report October 1984

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A	1971-72	Cold	Natural Conditions		
В	1976-77	Very Warm	Natural Conditions		
C	1981-82	Average	Natural Conditions		
D	1982-83	Warm	Natural Conditions		
E	1983-84		Natural Conditions		
F	1971-72	Cold	Watana Operating	1996	Inflow-Matching
G	1976-77	Very Warm	Watana Operating	1996	Inflow-Matching
H	1981-82	Average	Watana Operating	1996	Inflow-Matching
I	1982-83	Warm	Watana Operating	1996	Inflow-Matching
J	1971-72	Cold	Watana Operating	1996	4°C
K	1971-72	Cold	Watana Operating	2001	Inflow-Matching
L	1982-83	Warm	Watana Operating	2001	Inflow-Matching
М	1971-72	Cold	Watana and D.C. Operating	2002	Inflow-Matching
N	1976-77	Very Warm	Watana and D.C. Operating	2002	Inflow-Matching
0	1981-82	Average	Watana and D.C. Operating	2002	Inflow-Matching
P	1982-83	Warm	Watana and D.C. Operating	2002	Inflow-Matching
Q	1971-72	Cold	Watana and D.C. Operating	2020	Inflow-Matching
R	1982-83	Warm	Watana and D.C. Operating	2020	Inflow-Matching
S	1982-83	Warm	Watana Filling (lst Winter)		
T	1981-82	Average	Watana Filling (2nd Winter)		

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INTERPRETIVE SKETCHES OF ICECAL RESULTS:

	Weather	Winter Air	•	Energy	Reservoir Release
<u>Exhibit</u>	Period	<u>Temperatures</u>	Project Status	Demand	Temperature
Ü	1971-72	Cold	Watana Operating	1996	Inflow-Matching
V	1976-77	Very Warm	Watana Operating	1996	Inflow-Matching
W	1982-83	Warm	Watana Operating	1996	Inflow-Matching
X	1971-72	Colđ	Watana Operating	1996	4°C
Y	1971-72	Cold	Watana and D.C. Operating	2002	Inflow-Matching
Z ,	1982-83	Warm	Watana and D.C. Operating	2002	Inflow-Matching
A1	1981-82	Average	Watana Filling (2nd Winter)		

REPORT

1.0 INTRODUCTION

1.1 OBJECTIVE AND SCOPE

This report presents the results to date of the instream ice simulation studies for the Susitna Hydroelectric Project. The objective of these studies is to determine the effect of the proposed Watana and Devil Canyon Dams on river ice processes and the corresponding water surface elevations during the winter season in the Susitna River downstream of the dams. These studies are limited to the Middle Reach of the Susitna River (i.e., upstream of the confluence with the Chulitna River - See Figure 1), wherein the greatest impact of the project is expected.

The information presented in this report will be used in future environmental studies, particularly in assessment of possible project impacts on salmon incubation and spawning. Of special interest in this regard are a number of slough and side channel areas, adjacent to the mainstem of the Susitna River, which are known to be the habitat for salmon spawning. Results of the river ice studies are therefore focused on several of the more important slough and side channel locations along the Middle Susitna River. Results include continuous descriptions of ice thickness, water surface elevation and water temperature at these locations.

This report provides a comparison of simulated pre-project (i.e., "natural") river ice conditions with that expected during operation of the proposed project (i.e., "with-project"). In order to provide a broad range of comparisons, various combinations of winter weather patterns, project energy demands, instream flow requirements and reservoir release temperature policies were considered. The river ice simulations cover the six month period from November 1 through April 30, during which the freeze-up and melt-out of the Middle Susitna River is generally expected to occur with-project.

The river ice simulation studies represent one component of a coordinated environmental study effort. Corresponding simulations of the reservoir operation, reservoir temperature distribution and stream temperature provided boundary conditions on which the river ice studies were based. The results of these related studies were summarized in separate reports provided to the Federal Energy Regulatory Commission in the Alaska Power Authority's comments on the Draft Environmental Impact Statement.

1.2 BACKGROUND INFORMATION

The proposed Susitna Hydroelectric Project is to be located in south-central Alaska approximately 140 miles north-northeast of Anchorage and 110 miles south-southwest of Fairbanks. The proposed project, consisting of Watana and Devil Canyon dams, would generate electrical power for the Railbelt region of Alaska. The Watana and Devil Canyon dam sites are 184 and 152 river miles, respectively, upstream from the mouth of the Susitna River at Cook Inlet. Construction of the Watana dam, an 885 ft high earthfill structure, is planned to be completed in 1994 with power generation beginning in 1996. The 645 ft high Devil Canyon concrete arch dam is planned to be completed in 2002.

Observations of natural ice processes on the Middle Susitna River have been documented for the past four winters; 1980-81, 1981-82, 1982-83 and 1983-84 (R&M Consultants 1981, 1982a, 1983, 1984). An additional study of natural hydraulic and ice conditions has also been presented (R&M Consultants 1982b). The reader may find it useful to review these materials in order to become familiar with Susitna river ice processes and general ice terminology used in this report.

The present river ice simulation studies are based upon application of the computer model "ICECAL." ICECAL computes hydraulic and ice conditions within the river on a daily basis and its capabilities are briefly outlined in Section 2.1. A detailed documentation of ICECAL and its calibration to the Middle Susitna River has been presented previously (Harza-Ebasco, 1984).

Each ICECAL simulation of with-project conditions is based upon corresponding simulations of the flow rates and water temperatures released from the Watana or Devil Canyon reservoir and the subsequent cooling (or warming) of this water as it travels in the river downstream of the reservoir. Flow rates and water temperatures released from the proposed reservoirs are simulated with the Dynamic Reservoir Simulation Model, i.e. "DYRESM" (Alaska Power Authority 1984). Results of the DYRESM simulations are input to a stream temperature simulation model, "SNTEMP" (Arctic Environmental Information and Data Center 1984, Alaska Power Authority 1984), which computes longitudinal stream temperature profiles in the Susitna River on a weekly basis. Results of the DYRESM and SNTEMP simulations are then input to the ICECAL model for simulation of the instream hydraulic and ice conditions.

2.0 METHODOLOGY

2.1 MODEL

The computer model, ICECAL, was used to generate the river ice simulations presented in this report. The model provides a daily summary of hydraulic, temperature and ice conditions throughout the study reach. A brief outline of ICECAL operations is presented in this section. A detailed documentation of ICECAL and its calibration to the Middle Susitna River for the winters of 1982-83 and 1983-84 has been presented previously in a calibration report (Harza-Ebasco 1984).

Two improvements have been incorporated into ICECAL since the preparation of the calibration report. Computation of solid ice growth (See Item 6 below) has been refined to include the effects of snow cover which tends to insulate the ice cover from the ambient air temperature. Also, computation of lateral ice growth (See Item 4 below) has been improved to more accurately reflect observations on the Susitna River. The effects of these ICECAL improvements were checked by repeating the calibration simulations for the 1982-83 and 1983-84 winters. It was found that the improved ICECAL version gave equivalent or better calibration results compared to the previous version, in terms of agreement with the observed ice conditions. The improved ICECAL calibration runs for the 1982-83 and 1983-84 winters are presented in this report as Exhibits D and E respectively. All river ice simulations presented in this study are based on the improved version of ICECAL.

The particular hydraulic and ice operations performed by the ICECAL model include the following:

Hydraulic profiles are computed daily for the study reach.
 Computations are based upon the Bernoulli and Manning equations and include the effects of existing ice in the river.

- 2. Water temperature profiles required for with-project simulations are provided by the SNTEMP stream temperature studies (AEIDC 1984). The SNTEMP stream temperatures are based upon open water conditions and are therefore not applicable to that portion of the river which is ice covered. For ice covered reaches, therefore, stream temperatures are computed by ICECAL based on a heat transfer coefficient approach (Harza-Ebasco 1984).
- 3. Generation of small ice crystals, know as frazil ice (Ashton 1978), is computed for reaches of turbulent, open water in which the water temperature has dropped to 0°C. Frazil ice flow rates are tabulated as the ice is carried downstream with the flow.
- 4. Lateral or border ice growth proceeding from the river banks (See Figure 2) is computed based on Susitna River observations. This lateral ice growth tends to reduce the open water surface area available for frazil ice generation.
- 5. Frazil ice particles tend to coalesce into floating pans or larger rafts of slush ice which may accumulate downstream at the front of a developing ice cover (See Figure 2). Hydraulic conditions at the ice cover are analyzed to determine if the incoming ice pans will accumulate at the upstream edge of the cover, thereby advancing the "ice front". Alternately, the incoming ice may be swept beneath the ice front and deposited downstream on the underside of the ice cover, thereby thickening the ice cover.
- 6. Slush and solid ice component thicknesses of the river ice cover are computed. Initial ice cover accumulations consist of slush ice as discussed in (5) above. The initial slush ice cover then gradually freezes into solid ice, beginning at the upper surface (exposed to the cold air) and proceeding down. ICECAL computes this daily growth of solid ice within the initial accumulations of slush ice. If the solid ice grows thru the slush, the model computes the additional thickness below the slush.

7. Melting of the ice cover and retreat of its ice front are computed when warm water (i.e., above 0°C) reaches the ice cover. In this manner, a spring "melt-out" is simulated. Mechanical "break-up" of the ice cover is not considered, being beyond the state-of-the-art in river ice modeling. Although severe springtime break-up activity and resulting ice jams have been observed for certain years under natural conditions, it is expected that a gradual spring melt-out, as considered in the model, will be more characteristic of the with-project condition. Severe springtime break-up activity is largely associated with rapid natural flow increases which lift and fracture the ice cover (R&M 1982a). The proposed project reservoirs will regulate such seasonal flow events, yielding a more stable flow regime for the Middle Susitna River and thereby allowing an existing ice cover to melt in place.

Required input data for the ICECAL model includes the following:

- 1. River cross-sectional geometry and bed roughness for study reach
- Weather conditions (daily air temperature and wind velocity)
 within the study reach
- 3. Water inflow hydrograph at upstream boundary of study reach
- 4. Daily frazil ice discharges at upstream boundary of study reach
- 5. Water temperature profiles in the study reach upstream of the ice front.

Further discussion of the input data used for natural and with-project simulations is presented in Sections 2.3 and 2.4, respectively.

2.2 RANGE OF SIMULATED CONDITIONS

The particular river ice simulations included in this report are tabulated in Table I. As shown, the simulations include four winters of historical weather and flow data; 1971-72, 1976-77, 1981-82 and 1982-83. Air temperatures for these four winters are plotted in Figure 3. Figure 4 shows the corresponding natural river flows during the winter season. The four particular winters were selected to include possible extremes in expected withproject river ice conditions. Based on Talkeetna air temperatures averaged over the 5 month period from November through March, as shown in Figure 5, the winters of 1971-72 and 1976-77 respectively represent the coldest and warmest winters recorded during the past 40 years. The winter of 1981-82 is considered average in air temperature and the winter of 1982-83 is considered warmer than average.

Talkeetna air temperatures averaged over the 3 month period from December through February (See Figure 6) show similar historical trends as the 5 month period from November through March.

The range of simulated conditions also includes various stages during development of the project; natural conditions, filling of Watana Reservoir (first and second winters), Watana operating alone (1996 and 2001 energy demands), and Watana and Devil Canyon operating together (2002 and 2020 energy demands). The year 1996 represents the expected first year of Watana power generation. Start-up of the Devil Canyon power generation is planned for the year 2002.

Reservoir releases for the with-project simulations satisfy the Case C operating guide (Alaska Power Authority, 1983). Flow rates for the with-project simulations are adjusted on a weekly basis and are shown in Figure 7.

Temperature of the reservoir releases is controlled by operation of a multilevel intake structure. The policy of operation used in the simulations is based on an attempted match of the release temperature with that of the natural flow entering the reservoir. In effect, this "inflow matching" policy results in release of the coldest available water during the winter months. As a sensitivity investigation, one river ice simulation considers the effect of an assumed release of warm, 4°C water throughout the period of simulation. Release of 4°C water is a hypothetical situation only, since the warmest water available to the proposed intake structure (using the lowest level intake ports) will be somewhat colder than 4°C during the winter months.

The range of simulated conditions in this study is intended to provide a broad base for comparisons between the natural and with-project river ice environments. Of necessity, all combinations of meteorology, hydrology, energy demands and reservoir operations could not be considered herein. However, the range of simulations included is believed adequate to allow significant conclusions regarding river ice behavior.

2.3 SIMULATIONS OF NATURAL ICE CONDITIONS

As shown in Table I, this report includes natural ice simulations for the winters of 1971-72, 1976-77, 1981-82 and 1982-83. These simulations were based on the following conditions and assumptions:

1. Study Reach

The study reach extends from River Mile 98.6 (Chulitna confluence) to River Mile 139.4 (slightly upstream of Gold Creek). Progression of a defineable ice front has been observed in this reach under natural conditions. Upstream of Gold Creek, however, localized unstable ice bridging processes have been observed to close the river prior to arrival of the ice front. Since the ICECAL model does not attempt to simulate such processes, and since observations of frazil ice quantities are available only at Gold Creek, the model does not extend upstream of this vicinity for the simulations of natural ice conditions. The central questions regarding project-induced changes in natural ice conditions

pertain principally to civil structures or environmental concerns within the 40 mile river segment included in the ICECAL natural simulations. Project effects on natural ice processes upstream of RM 139 can be forecast on the basis of the stream temperature modeling and the experience gained from winter ice observations and modeling the lower 40 miles of the Middle Susitna River with ICECAL.

2. Period of Simulation

Simulations cover the 6 month period from November 1 through April 30. Ice front progression up the Middle Susitna River has not occurred prior to November 1 during the four years of ice observations. Simulation of spring break-up or melt-out is not attempted for natural conditions.

3. Starting Date for Ice Front Progression into the Middle Susitna River

When available, actual observations are used for the starting date of the ice front progression at the Susitna-Chulitna confluence. Observed starting dates have ranged from November 5 through December 8 and are shown in Table II. For years when observations are not available, an assumed date is selected within the observed range based on the severity of the particular winter.

4. Water Flow Rates

Historical flow data at Gold Creek (River Mile 137) were used as recorded by the USGS and/or R&M Consultants, Inc. (See Figure 4). Daily flow rates were interpolated for periods when data are not available. Flow rate adjustment factors were applied along the study reach to account for tributary inflows (R&M 1982b).

5. Weather Data

Daily air temperatures and wind speeds recorded at Talkeetna and Watana weather stations were interpolated linearly along the river length. Talkeetna data are available for all years simulated. Watana data, when not available, were estimated from a correlation with available Talkeetna data.

6. Frazil Ice Discharge at Gold Creek

This quantity was computed from actual ice observations at Gold Creek (River Mile 137), when available. These ice discharges were found to be well correlated with Talkeetna air temperature data. This correlation provided an estimate of frazil ice discharge at Gold Creek for years in which observations were not available.

7. Stream Temperatures

Stream temperatures were assumed to be 0°C throughout the natural simulations.

2.4 SIMULATIONS OF WITH-PROJECT ICE CONDITIONS

The various with-project ice simulations were based on the following conditions and assumptions:

1. Study Reach

The study reach extends from the Susitna-Chulitna confluence (River Mile 98.6) to the Watana (River Mile 184.4) or Devil Canyon (River Mile 152) damsite.

2. Period of Simulation

Simulations cover the 6 month period from November 1 through April 30. The freeze-up and melt-out of the Middle Susitna River are generally expected to occur during this period.

3. Starting Date for Ice Front Progression into the Middle Susitna River

Progression of the ice front upstream of the Susitna-Chulitna confluence begins when the Lower Susitna River (downstream of the Chulitna confluence) has frozen over. The Lower Susitna freeze-up is characterized by an initial ice bridge formation near River Mile 9 and the subsequent advance of an ice cover up to the Chulitna confluence.

The Lower Susitna ice cover during with-project conditions is supplied by frazil ice generated in the Yentna, Talkeetna, Chulitna, Lower Susitna (upstream of the ice cover) and Middle Susitna Rivers. The ICECAL model considers the total volume of ice required to fill the Lower Susitna River from the Yentna confluence (River Mile 30) to the Chulitna confluence (River Mile 98.6) and computes the time needed to generate the necessary frazil ice. Frazil ice generation in the Middle Susitna River is computed directly by the model. The frazil ice contributions of the Talkeetna, Chulitna and Lower Susitna Rivers are computed by correlation with cumulative freezing degree days at the Talkeetna weather station.

Lower Susitna River ice observations suggest that the ice front typically reaches the Yentna confluence (River Mile 30) in late October or early November under natural conditions (See Table II). It is expected that this event will not be significantly delayed under with-project conditions. Although the frazil ice contribution from the Middle Susitna River is greatly reduced under with-project conditions, the Yentna River, which produces more than 50%

of the total ice downstream of River Mile 30 (R&M, 1984), remains unchanged. Also unchanged are the frazil ice contributions of the Chulitna and Talkeetna Rivers which represent about 20% of the natural Susitna frazil ice discharge at Talkeetna (R&M 1983).

Based on the above, November 1 was selected as a representative date on which the Lower Susitna ice front reaches the Yentna confluence during with-project conditions. The ICECAL model and related computations of tributary frazil ice production therefore begin on November 1 for the with-project river ice simulations. Daily tabulations of cumulative ice production are performed until the ice storage capacity of the Lower Susitna is reached. At this point, the model begins progression of the ice cover at the Chulitna confluence (River Mile 98.6).

4. Water Flow Rates

Water flow rates at the upstream boundary of the ICECAL simulation are determined by releases from the Watana or Devil Canyon reservoirs. This information is read directly from the output of the corresponding DYRESM simulation and is summarized in Figure 7. The flow rates are provided on a weekly basis and are adjusted along the study reach to account for tributary inflows (R&M 1982b). Fluctuations of flow within a particular day or week are not considered.

5. Weather Data

Daily air temperature and wind speed data are interpolated along the river length between Talkeetna, Devil Canyon and Watana weather stations. Watana and Devil Canyon data, when unavailable, are estimated from a correlation with Talkeetna data.

6. Frazil Ice Discharge at Upstream Boundary of Model

Water released from the Watana and Devil Canyon reservoirs remains above 0°C throughout the year. Therefore, no frazil ice exists at the upstream boundary of the with-project simulations.

7. Stream Temperatures

Reservoir release temperatures are computed in daily time steps by the DYRESM simulations. Corresponding SNTEMP simulations provide stream temperature profiles on a weekly basis throughout the study reach. This information is read directly into the ICECAL model. The SNTEMP stream temperature profiles are based upon open water conditions and are therefore not applicable to that portion of the river which is ice covered. The SNTEMP results are therefore superseded by ICECAL temperature computations for that portion of the river where an ice cover exists.

2.5 SLOUGH AND SIDE CHANNEL AREAS

Various slough and side channel areas adjacent to the mainstem Susitna River are of special importance as salmon spawning habitat. A typical slough, illustrated in Figure 8, is an overflow channel separated from the mainstem by a well-vegetated bar or island (Alaska Power Authority 1983). Sloughs are generally fed by a small stream and/or upwelling of groundwater. Side channels are similar to sloughs, but are not fed by such a stream or groundwater upwelling. An alluvial berm generally extends across the upstream end of the slough or side channel, shielding it from the river. High natural river flows or ice activity will periodically overtop this upstream berm and flood the slough or side channel with water or ice. The water level at a given mainstem river mile which results in overtopping of a nearby slough or side channel berm is referred to in this study as the "threshold elevation." Since slough and side channel systems may include a network of multiple channels, overtopping of a particular berm may be controlled by the water level in the mainstem at a different river mile

location. For this reason, the "threshold elevation" in the mainstem is not necessarily equal to the corresponding berm crest elevation.

The important sloughs and side channels have been identified and are tabulated in Table III. For the purpose of the river ice simulations, it is assumed that particular sloughs have been isolated from the river channel. That is, the model assumes that the cross-sectional area of these particular sloughs (See Table III) is not available to pass flow or store ice. This assumption has no influence on the model results for those simulations in which the river stages remain below the natural threshold elevations. For those simulations which show slough overtoppings, the slough isolation assumption yields river stages which may be slightly higher than those expected had these slough areas been included in the cross sections. The slough isolation assumption therefore yields conservative results, reflecting levels to which slough berms would have to be constructed if that slough were to be protected from overtopping.

2.6 INTERPRETATIONS OF COMPUTER SIMULATIONS

River ice mechanics and modeling is a relatively primitive field of study. Ice processes are complicated, unsteady and non-uniform, and many aspects are not yet fully understood. Although the ICECAL model is considered state-of-the-art, certain simplifications and limitations are necessarily involved. Three dimensional concepts are presented in a one-dimensional format, and the model therefore computes an average or characteristic velocity and ice thickness to represent a particular cross-section. The actual spatial distribution of velocity and ice thickness may be highly non-uniform and is beyond the scope of the model. Figure 9 contrasts actual and computed ice distribution at a hypothetical cross-section.

For these reasons, selected ICECAL computer simulations have been interpretted by R&M Consultants, Inc., based on their experience with Su itna River ice over the past four years. These interpretations are identified in Table I and are presented in Exhibits U-Al. The resulting interpretive sketches combine the quantitative ICECAL results with observed river ice

distribution trends to yield the best estimate of the actual river appearance at selected cross-sections.

3.0 RESULTS

3.1 GENERAL

Results of the river ice simulations are presented in Exhibits A through T. Each exhibit includes the following information:

- 1. Profile of the maximum river stages which occurred during the simulation period and the corresponding ice cover thickness which existed on the date of maximum stage. (Since river stage is influenced by both flow rate and ice thickness, the ice thicknesses shown do not necessarily represent the maximum thickness.)
- 2. Location of the ice front and 0°C water isotherm throughout the simulation.
- 3. Time history plots of water surface elevation, ice thickness and water temperature at selected slough and side channel areas.

Table IV is a summary of the maximum water surface elevations which occurred at selected slough and side channel areas for all the river ice simulations. Table V summarizes the number of occurrences where with-project simulations resulted in higher maximum stages than the corresponding natural conditions for the same weather period. Table VI shows those slough and side channel areas where the known threshold elevation was simulated to be overtopped with-project but not under natural conditions, and vice versa. Table VII summarizes the starting date, maximum extent and melt-out date of the ice front for each simulation. Tables VIII and IX present the maximum total and solid ice thicknesses, respectively, which occurred during the simulations.

Interpretive sketches for selected ICECAL simulations are presented in Exhibits U-Al. Each sketch shows natural river conditions observed in 1983-84, a selected ICECAL simulation result and an interpreted version of the

ICECAL result for a particular river cross section. This interpreted version is based on detailed observation of Susitna River ice processes and represents the best estimate of the actual appearance of the particular river cross section at the time of its maximum winter stage. Relative to the ICECAL results, the interpretive sketches show that the thickest deposits of slush ice will generally accumulate in the low velocity zones near the river banks. Correspondingly thinner ice and occasional open water is shown in the high velocity zones of the channel.

3.2 SIMULATIONS OF NATURAL CONDITIONS

Of the four years simulated, the cold winter of 1971-72 (Exhibit A) typically results in the greatest ice thicknesses and highest river stages within the study reach. For this winter, maximum total ice thicknesses (solid + slush component) within the study reach range from 5 ft. to 11 ft., including up to 5 ft. of solid ice. The winter of 1981-82 (Exhibit C), an average winter in terms of air temperatures, shows maximum total ice thicknesses of 4 ft. to 10 ft., of which 3 ft. to 4 ft. is typically solid ice. Maximum river stages for 1981-82 are often 1 ft. to 3 ft. lower than those for 1971-72.

The winter of 1982-83, a relatively warm winter, was used for model calibration purposes (Harza-Ebasco 1984). Actual ice observations are shown along with simulated results in Exhibit D. Maximum total ice thicknesses for 1982-83 range from 3 ft. to 8 ft., of which 3 ft. is typically solid ice. Maximum river stages are generally 0 ft. to 4 ft. lower than those of 1971-72.

The very warm winter of 1976-77 results in the smallest ice thicknesses and lowest river stages of the four winters simulated. Maximum total ice thicknesses range from 1 ft. to 7 ft., of which 1 ft. to 2 ft. is solid ice. Maximum river stages for 1976-77 are generally 2 ft. to 6 ft. lower than those of 1971-72.

For the winters of 1971-72, 1981-82 and 1982-83, ice front progression at the Chulitna confluence (River Mile 98.6) begins in early or mid-November and reaches Gold Creek in late December or early January. The winter of 1976-77 however, shows the ice front beginning in early December and reaching Gold Creek in early March. All four simulations are characterized by a rapid initial ice front progression rate in the lower portion of the study reach with a gradual slowing as it approaches Gold Creek.

3.3 WATANA OPERATING WITH 1996 ENERGY DEMAND

Simulation results are presented in Exhibits F-J. As shown, the start of the ice front progression at the Chulitna confluence ranges from late November (1971-72 winter) to late December (1981-82 winter). This represents a delay of 2 to 5 weeks relative to natural conditions for the corresponding winters. The maximum upstream extent of the ice front is between River Miles 137 and 140 for the winters of 1971-72, 1976-77 and 1981-82, and at River Mile 127 for the winter of 1982-83. Completion of the spring melt-out in the Middle Susitna (i.e., down to River Mile 98.6) ranges from mid March (1982-83 winter) to mid May (1971-72 winter). The spring melt-out occurs 5 to 7 weeks earlier than natural river break-up based on observation of 1981-82 and 1982-83.

The most severe ice conditions for Watana operation and 1996 energy demand occur for the winter of 1971-72 (Exhibit F). For this simulation, maximum total ice thicknesses range from 2 ft. to 11 ft., including up to 5 ft. of solid ice. These ice thicknesses are generally similar to those of natural conditions in the reach downstream of Gold Creek (River Mile 137). Maximum river stages, however, are 3 ft. to 7 ft. higher than natural conditions due to the significantly higher winter flow rates with the project.

The mildest simulated river ice conditions for the 1996 energy demand occur for the winter of 1982-83 (Exhibit I). Maximum total ice thicknesses for this simulation range from 2 ft. to 8 ft., including up to 2 ft. of solid ice. These thicknesses are generally similar to natural 1982-83 conditions, but maximum with-project river stages are 2 ft. to 5 ft. higher than natural

conditions due to the higher with-project winter flows. Maximum river stages for the 1982-83 with-project simulation are 0 ft. to 7 ft. lower than those of the 1971-72 severe conditions.

The effect of a hypothetical warm (4°C) water release from the Watana reservoir throughout the 1971-72 winter was considered as shown in Exhibit J. With these "warm" reservoir releases, the ice cover progression at the Chulitna confluence begins 3 weeks later and melt-out occurs approximately 7 weeks earlier than with the "inflow matching" temperature release policy of Exhibit F (See Section 2.2). Maximum ice thicknesses with the warm releases range from 2 ft. to 7 ft., and maximum river stages are typically 1 ft. to 7 ft. lower than those with the "inflow-matching" releases. Maximum extent of the ice cover with the warm releases is River Mile 127, versus River Mile 140 under inflow matching release temperatures. It therefore appears that control of the reservoir release temperatures may have a significant impact on river ice development.

3.4 WATANA OPERATING WITH 2001 ENERGY DEMAND

Simulations of Watana operating with the 2001 energy demand were made for the winters of 1971-72 and 1982-83 (See Exhibits K and L). Results show that the ice front starting date, melt-out date and maximum upstream extent are similar to those of the 1996 energy demand for the corresponding winters. However, some redistribution of the frazil ice depositions along the river length is apparent. Such differences in ice distribution can be caused by different patterns of reservoir release temperatures occuring at different times within a given winter season. In particular, for the 1971-72 winter, the 2001 energy demand shows colder December reservoir releases than the 1996 demand, thereby causing a faster ice front progression. The subsequent heavy frazil production in January is accumulated at a further upstream location for the 2001 demand. As a result, maximum river stages in the vicinity of river miles 137-142 for the 1971-72 winter with 2001 energy demand are 2 ft. to 10 ft. higher than those with the 1996 demand.

Maximum total ice thicknesses for the 1971-72 winter with 2001 energy demand range from 4 ft. to 14 ft. of which 4 ft. to 5 ft. is solid ice. Maximum river stages are 2 ft. to 6 ft. higher than for natural 1971-72 conditions.

Maximum total ice thicknesses for the 1982-83 winter with 2001 energy demand range from 2 ft. to 7 ft. including up to 2 ft. of solid ice. Maximum river stages are 1 ft. to 6 ft. higher than natural conditions in the reach downstream of River Mile 124 where the with-project ice cover exists. Upstream of the with-project ice cover, however, maximum river stages are 1 ft. to 4 ft. lower than natural conditions. Although the with-project flow rates are higher, the displacement and frictional resistance of the natural ice cover in this reach result in higher river stages for natural conditions than with-project.

3.5 WATANA AND DEVIL CANYON OPERATING WITH 2002 ENERGY DEMAND

Simulation results for Watana and Devil Canyon operating with 2002 energy demand are presented in Exhibits M-P. Results show that the beginning of the ice front progression at the Chulitna confluence ranges from early December to mid-January, approximately 0-2 weeks later than the corresponding Watana-only simulations, and 4-6 weeks later than natural conditions for the same winters. Maximum upstream extent of the ice front ranges from River Mile 123 to 137, and is 3-13 miles downstream of that with Watana only and 1996 energy demand. Simulated melt-out with both dams operating and 2002 energy demand ranges from mid-March to mid-May, being 0-3 weeks earlier than Watana-only simulations for the corresponding winters, and 7-8 weeks earlier than the natural break-up observed for the 1981-82 and 1982-83 winters.

For both dams operating with 2002 energy demand, the most severe ice conditions occur with the 1971-72 winter (Exhibit M). Maximum ice thicknesses for this case range from 3 ft. to 7 ft., of which 3 ft. to 5 ft. is solid ice. Maximum river stages are 1 ft. to 5 ft. lower than the corresponding Watana-only simulation with 1996 energy demand. Maximum river stages downstream of River Mile 130 are 0 ft. to 4 ft. higher than natural

conditions. Upstream of this location, however, the ice cover is much thinner with-project and maximum river stages are 0 ft. to 3 ft. lower than natural conditions.

The winters of 1976-77, 1981-82 and 1982-83 (Exhibits N, O and P) all show relatively mild ice conditions for both dams operating with the 2002 energy demand. Maximum ice thicknesses for these cases range from 1 ft. to 6 ft., including 1 ft. to 2 ft. of solid ice. Maximum river stages are 0 ft. to 7 ft. lower than the corresponding Watana-only simulations with 1996 energy demand. Maximum river stages, where an ice cover exists, are 1 ft. to 4 ft. higher than corresponding natural conditions. Upstream of the with-project ice cover, maximum river stages are 0 ft. to 5 ft. lower than natural conditions. Again, the higher natural stages in this reach are due to the displacement and frictional resistance of the natural ice cover.

3.6 WATANA AND DEVIL CANYON OPERATING WITH 2020 ENERGY DEMAND

Simulations of Watana and Devil Canyon operating with the 2020 energy demand were performed for the winters of 1971-72 and 1982-83 (Exhibits Q and R). Results show that the ice front starting date and maximum upstream extent are generally similar to those of the 2002 energy demand for the corresponding winters. The spring melt-out with the 2020 energy demand, however, occurs 1 to 3 weeks earlier than with the 2002 energy demand. This is apparently caused by somewhat warmer reservoir release temperatures resulting from the 2020 reservoir simulation.

Simulation of the 1971-72 winter with 2020 energy demand shows maximum ice thicknesses which range from 2 ft. to 7 ft. including 1 ft. to 4 ft. of solid ice. Maximum river stages in the ice-covered reach (downstream of River Mile 130) are 1 ft. to 7 ft. higher than corresponding natural conditions. Upstream of the with-project ice cover, maximum river stages are 1 ft. to 5 ft. lower than those of natural conditions, due to the displacement and frictional resistance of the natural ice cover.

Simulation of the 1982-83 winter with 2020 energy demand shows maximum ice thicknesses ranging from 1 ft. to 3 ft., including up to 1 ft. of solid ice. Maximum river stages in the ice-covered reach are 0 ft. to 4 ft. higher than natural conditions. Upstream of the with-project ice cover, maximum stages are 0 ft. to 4 ft. lower than corresponding ice-covered natural conditions.

3.7 WATANA FILLING

River ice simulations for the first and second years of filling the Watana reservoir are shown in Exhibits S and T. The first winter of filling, which involves relatively warm reservoir releases from the low level outlet works, was simulated with the relatively warm 1982-83 weather conditions. The second winter of filling includes release of colder water from the reservoir surface and was simulated with the colder 1981-82 weather conditions. The two simulations were selected to provide a typical range of ice conditions during the filling of the Watana reservoir.

Results for Watana filling show that the ice front progression at the Chulitna confluence begins in mid-December, 5-7 weeks later than corresponding natural conditions. The simulated melt-out for the first winter of filling occurs in early May, similar to the timing of break-up under natural conditions. The second winter of filling shows an estimated melt-out in late May (extrapolated from April conditions), 2 to 3 weeks later than the natural break-up. However, since increasing Watana flow releases during the month of May are not included in the simulation period, a mild spring break-up for the second year of Watana filling may actually occur with similar timing as the natural conditions.

The Watana filling simulations show the ice front progressing up to River Mile 156-162. This ice progression is significantly further upstream than any of the other with-project simulations and is due to the lower river flows and velocities which exist under filling conditions. However, simulation of an ice front progression upstream of River Mile 140 is considered an approximation only, since intermittent bridging of lateral ice has been

observed to be the dominant process in this reach for natural conditions. Such intermittent ice bridging is not modeled by ICECAL.

Simulation of the first year of filling with the 1982-83 winter shows maximum ice thicknesses of 1 ft. to 6 ft., including up to 2 ft. of solid ice. Maximum river stages are 0 ft. to 5 ft. lower than natural conditions for 1982-83.

Simulation of the second year of filling with the 1981-82 winter shows maximum ice thicknesses of 1 ft. to 8 ft., including up to 3 ft. of solid ice. Maximum river stages are generally 0 ft. to 3 ft. lower than natural conditions for 1981-82.

4.0 CONCLUSIONS AND RECOMMENDATIONS

The following conclusions are based upon the river ice simulation results to date and are subject to the various assumptions and conditions described in this report. In particular, the with-project ice results are based on a reservoir release temperature policy which attempts to match the natural stream temperatures incoming to the reservoir (i.e., coldest available water is released from the reservoir during winter season). Conclusions apply only to the Middle Susitna River (i.e, upstream of the confluence with the Chulitna River) wherein the most significant project impacts are expected.

1. Ice Front Progression and Melt-Out

Relative to natural conditions, initial progression of the Middle Susitna ice front at the Chulitna confluence (River Mile 98.6) is expected to be delayed by 2 to 5 weeks with Watana operating alone, and 4 to 6 weeks with Watana and Devil Canyon operating together. Completion of a gradual spring melt-out in the Middle Susitna River with Watana operating alone is expected 5 to 7 weeks earlier than the natural, mechanical break-up. With both dams operating, completion of the spring melt-out is expected 7 to 8 weeks earlier than the natural break-up.

Maximum upstream extent of the river ice cover during the selected warm, average and cold winters is expected to range from River Mile 124 to 142 with Watana operating alone. With the addition of the Devil Canyon dam, this maximum upstream extent will be somewhat reduced, with an expected range of River Mile 123 to 137.

2. Ice Thicknesses

In those reaches where an ice cover exists, the maximum total and solid ice thicknesses with Watana operating alone are expected to be generally similar to those of natural conditions. With both dams operating, the maximum total and solid ice thicknesses are expected to be typically 1 ft. to 2 ft. less than those of natural conditions.

3. River Stages and Slough Overtopping

In those reaches where an ice cover exists, the maximum river stages with Watana operating alone are expected to be generally higher than those of the natural conditions, typically by 2 ft. to 7 ft. Corresponding maximum river stages in ice covered reaches with both dams operating are expected to be typically 1 ft. to 6 ft. higher than those of natural conditions.

Upstream of the with-project ice front, however, the maximum river stages with Watana operating alone are expected to be typically 1 ft. to 3 ft. lower than the corresponding natural conditions. With both dams operating, these maximum river stages are expected to be typically 1 ft. to 5 ft. lower than natural conditions.

As a result of the above, overtopping of the natural threshold elevations in various slough and side channel areas in the lower reaches of the Middle Susitna (downstream of River Mile 127) is expected to be more frequent with the project than under natural conditions (See Table VI). However, various slough and side channel areas in the upper reaches of the Middle Susitna (upstream of River Mile 127) are expected to be overtopped less frequently with the project than under natural conditions.

4. Further Considerations

It is expected that the policy which governs reservoir release temperatures may have a major impact on the river ice development (See Exhibit F vs. Exhibit J). Additional simulations including possible alternate temperature release policies may therefore be useful for future aquatic assessments.

5.0 REFERENCES

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TABLES

TABLE I
SUSITNA HYDROELECTRIC PROJECT
SCOPE OF RIVER ICE SIMULATIONS

Project Status Operating Guide Energy Demand		Natural Conditions	Watana Operat Case 1996	ing C 2001	Watana a Canyon O Case C 2002	2020	Filling		
<u>Re</u> Historica	lease Temperature 1 Period:		N W	N_	N	N	lst Winter	2nd Winter	
1971-72 1976-77	(Cold winter) (Very Warm winter)	x x	® ®	X	⊗ x	X			
1981-82 1982-83	(Average winter) (Warm winter)	x x	x Ø	x	x ®	x	х .	⊗	

Notes: 1. N represents natural "inflow matching" policy for reservoir release temperatures.

2. W represents assumed warm, 4°C temperature release.

Legend: X ICECAL simulation

X ICECAL simulation and interpretive sketch

TABLE II

SUSITNA HYDROELECTRIC PROJECT OBSERVED ICE FRONT PROGRESSION ON THE SUSITNA RIVER

Location of Loc Front	River Mile	1980	1981	1982	1983
River Mile 9	9	Unknown	Early Nov.	Oct. 22	Oct. 26
Chulitna Confluence	98.6	Nov. 29	Nov. 18	Nov. 5	Dec. 8
Near Gold Creek	136	Dec. 12	Dec. 31	Dec. 27	Jan. 5

TABLE III

SUSITNA HYDROELECTRIC PROJECT SLOUGH AND SIDE CHANNEL AREAS IN MIDDLE SUSITNA RIVER

Area	River Mile Location	Threshold Elevation (feet)
*Whiskers Slough Side Channel at Head of Gash Creek *Slough 6A *Slough 8 Side Channel MSII Side Channel MSII Curry Slough *Moose Slough *Slough 8A - West Channel *Slough 8A - East Channel *Slough 9 Side Channel Upstream of Slough 9 Side Channel Upstream of 4th July Creek Slough 9A Side Channel Upstream of Slough 10 Side Channel Downstream of Slough 11 *Slough 11 *Slough 17 Slough 20	133.7 ⁿ 134.3 135.3 136.5 ^H 139.3 ^H 140.5 ^H	367 Unknown U 476 482 487 Unknown Unknown 573 582 604 Unknown Unknown 651 657 Unknown 687 Unknown
*Slough 21 - Entrance A6 *Slough 21 Slough 22	141.8 ^H 142.2 ^H 144.8	747 755 788

Legend:

- * For purposes of simulation, these sloughs are assumed to be isolated from the cross-section.
- H Indicated location represents the head of the slough or channel
- M Indicated location represents the mouth of the slough or channel
- U "Upland" slough with no upstream head or berm.

SUSITNA HYDROELECTRIC PROJECT MAXIMUM SIMULATED WINTER RIVER STAGES

TABLE IV

				MAZAMA CAMAZA TO TOTAL CAMAZA													<u> </u>					
			NATURAL				<u> </u>	WATANA ONLY						WATANA AND DEVIL CANYON					WATANA FILLING			
				COND	HTION:		1 996 DEMAND					DEN	MAND	2002 DEMAND					20 IAND	YR.1	YR. 2	
Slough or Side Channel	River Mile	Threshold Elevation	1971-72	1976-77	1981-82	1982-83		1971-72	1976-77	1961-62	1982-83	1971.72 ^W	1971-72	1962-83	1971-72	1976-77	1981-82	1982-83	1971.72	1962-83	1982-83	188142
Whiskers	101.5	367	369	366	368	367	lι	372	370	371	370	371	372	370	371	368	369	360	372	370	367	367
Gash Creek	112.0	Unknown	456	455	455	466		459	457	460	459	460	459	461	458	455	456	457	459	457	455	465
64	112.3	(Upland)	459	457	457	459		462	460	462	462	463	461	463	460	458	458	460	461	459	457	467
	114.1	476	474	472	472	474	6	478	475	477	476	477	476	478	475	474	475	475	476	475	473	473
MS II	116.6	482	484	480	484	484	[490	487	468	488	488	489	489	487	485	485	487	490	488	481	463
MS II	115.9	487	485	482	486	486	[492	489	401	491	490	491	492	489	488	488	490	492	400	495	465
Curry	120.0	Unknown	522	520	523	520	} ;	526	52 5	52 7	525	523	525	521	522	521	520	520	625	523	520	521
Moose	123.5	Unknown	552	546	549	548	,	556	554	55 5	550	552	555	550	553	550	548	546	555	550	546	546
SA West	126.1	573	572	569	571	570	0	576	57 5	574	572	572	575	568	574	_571	568	568	575	572	568	570
8A East	127.1	582	584	581	583	582	j 6	587	585	545	682	582	586	581	584	582	580	581	585	582	580	542
9	129.3	604	605	603	606	605	[609	607	077	603	603	610	603	606	602	601	602	608	603	602	603
9 u/s	130.6	Unknown	622	616	620	621		624	622	620	617	617	625	617	620	616	616	616	621	617	616	618
4th July	131.8	Unknown	632	626	629	630		635	633	631	628	628	636	628	633	627	627	627	631	628	625	628
9 A	133.7	861	655	649	651	651	[657	655	63	650	650	659	650	652	650	650	650	651	660	650	650
10 u/s	134.3	867	662	654	657	658	[[663	661	459	656	656	665	656	659	655	655	655	657	656	658	655
11 d/s	135.3	Unknown	673	667	670	672	1 4	675	672	67 0	668	668	676	668	670	667	667	667	668	668	670	668
11	136.5	687	684	681	683	684	[688	686	6 87	683	683	690	683	685	6B2	682	682	684	684	682	682
17	139.3	Unknown	i -	-	_	- 1	;	717	715	715	715	715	727	715	714	714	714	714	715	715	712	713
20	140.5	730	-	-	_	-		732	730	729	729	729	741	729	728	728	728	728	729	729	727	729
21 (A6)	141.8	747	-	_		-		746	746	746	746	745	751	746	746	746	745	746	747	747	746	746
21	142.2	756	-	-	_	-		753	753	763	753	753	755	753	752	752	752	752	763	754	751	750
22	144.8	788			_	- \	1	787	787	787	786	787	787	786	785	786	785	785	787	787	782	782

NOTES:

Upstream Boundary of Natural Simulations

Upstreem Extent of Ice Cover Progression

1971-72 cold

1976-77 very warm 1981-82 average

1982-83 warm

Indicates locations where maximum river stage equals or exceeds a known slough threshold elevation. See Exhibits A-T for duration of overtoppings.

^{2. &}quot;Case C" operating guide is assumed for with-project simulations.

 ^{1971-72&}lt;sup>W</sup> simulation assumes warm, 4°C reservoir raleases. All other withproject simulations assume an "inflow-matching" temperatura policy.

Upstream extent of simulated ica cover progression for Watana filling occurs upstream of River Mile 146.8.

^{5.} All river stages in feet.

^{6.} Winter air temperatures:

TABLE V

SUSITNA HYDROELECTRIC PROJECT OCCURRENCES WHERE WITH-PROJECT MAXIMUM RIVER STAGES ARE HIGHER THAN NATURAL CONDITIONS

Slough or Side Channel	River <u>Mile</u>	Watana Only Operating	Watana and Devil Canyon Operating	Watana Filling
Whiskers	101.5	6/6	6/6	0/2
Gash Creek	112.0	6/6	5/6	0/2
6A	112.3	6/6	5/6	0/2
8	114.1	6/6	6/6	1/2
MSII	115.5	6/6	6/6	0/2
MSII	115.9	6/6	6/6	0/2
Curry	120.0	6/6	3/6	0/2
Moose	123.5	6/6	4/6	0/2
8A West	126.1	5/6	4/6	0/2
8A East	127.1	4/6	2/6	0/2
9	129.3	4/6	2/6	0/2
9 u/s	130.6	3/6	0/6	0/2
4th July	131.8	3/6	2/6	0/2
9A	133.7	3/6	1/6	0/2
10 u/s	134.3 ⁻	4/6	1/6	0/2
11 d/s	135.3	3/6	0/6	0/2
11	136.5	4/6	2/6	0/2

Notes:

- 1. For example, 4/6 means that 4 of the 6 with-project simulations resulted in a higher maximum river stage than the natural conditions for corresponding winters.
- 2. "Case C" operating guide and "inflow-matching" reservoir release temperatures are assumed for with-project simulations.

TABLE VI

SUSITNA HYDROELECTRIC PROJECT EXPECTED PROJECT EFFECTS ON WINTER SLOUGH OVERTOPPING

WATANA ONLY									WATANA AND DEVIL CANYON					N	WATANA FILLING	
			C	1996 DEMAN	D		2001 DEMAND		2002 DEMAND				20 DEM	20 AND	!	YR. 2
						>										
Slough or Side Channel	River Mile	1971-72	1976-77	1981-82	1982-83	1971-72W	1971-72	1982-83	1971-72	1976-77	1981-82	1982-83	1971-72	1982-83	1982-83	1981-82
Whiskers	101.5		X							×					0	0
8	114.1	×		x	X	×	×	×					х	İ		
MSII	115.5		x							x					0	
MS II	115.9	×	x	X	x	х	х	×	x	x	X	X	x	X		
8A West	126.1	×	x	X			x		x				х			
8A East	127.1		x					o		X	0	0		:	0	
9	129.3		X		0	o		o			0	0		0	0	0
9A	133.7		x		0	0		0			0	0		0	0	0
10 u/s	134.3		x		0	O		o			0	0		0		0
11	136.5	×		×			×									

LEGEND:

- X Slough is overtopped with project, but not under simulated natural conditions for the corresponding winter.
- Slough is overtopped with simulated natural conditions, but not over*opped with project.

NOTES:

- 1. "Case C" operating guide is assumed for with-project simulations.
- 2. 1971-72^W simulation assumes warm, 4° C reservoir releases. All other with-project simulations assume an "inflow-matching" temperature policy.
- 3. Winter air Temperatures:

1971-72 cold 1976-77 very warm 1981-82 average 1982-92 warm

TABLE VII

SUSITNA HYDROELECTRIC PROJECT SIMULATED ICE FRONT PROGRESSION

	Starting Date at Chulitna Confluence	Melt-Out 	Maximum Upstream Extent (River Mile)
Natural Conditions			N
1971-72	Nov. 5	. 	137 ^N
1976-77	Dec. 8	R	137 ^N _N
1981-82	Nov. 18	May 10 _₹ 15 ^B	137 ^N
1982-83	Nov. 5	May 10 ^B	137 ^N
Watana Only - 1996 Demand		Tr	
1971–72	Nov. 28	May 15 ^E	140
1976-77	Dec. 25	May 3 ^E	137
1981-82	Dec. 28	April 3	137
1982–83 1971–72 ^W	Dec. 12	Mar. 20	127
1971-72 ^w	Dec. 17	Mar. 27	127
Watana Only - 2001 Demand		ĸ	
1971–72	Nov. 28	May 15 ^E	142
1982-83	Dec. 19	March 16	124
Both Dams - 2002 Demand		ĸ	
1971–72	Dec. 2	May 3^{E}	137
1976–77	Jan. 10	April 20	126
1981-82	Dec. 30	Mar. 12	124
1982-83	Dec. 22	Mar. 20	123
Both Dams - 2020 Demand			
1971-72	Dec. 3	April 15	133
1982-83	Dec. 14	Mar. 12	127
Watana Filling		. F.	т
1982-83 (YR.1)	Dec. 23	May 2 E	156_{T}^{I}
1981-82 (YR.2)	Dec. 23	May 30°	162

Legend:

- B Observed natural break-up.
- E Melt-out date is extrapolated from results when occurring beyond April 30.
- N Ice cover for natural conditions extends upstream of Gold Creek (River Mile 137) by means of lateral ice bridging.
- I Computed ice front progression upstream of Gold Creek (River Mile 137) is approximation only. Observations indicate closure of river by lateral ice in this reach for natural conditions.

Notes:

- 1. "Case C" operating guide is assumed for with-project simulations.
- 2. 1971-72 simulation assumes 4°C reservoir releases. All other with-project simulations assume an "inflow-matching" temperature policy.
- 3. Weather conditions:

1971-72: Cold winter 1981-82: Average winter 1976-77: Very warm winter 1982-83: Warm winter

SUSITNA HYDROELECTRIC PROJECT TOTAL ICE THICKNESS MAXIMUM SIMULATED VALUES

			NATI	IRA		WATANA ONLY				′		WA	TANA	ANI	DEVI	L CAN	YON	WATANA	FILLING	
		•	OND		_		1996 DEMAND				01 AND			XO2 IAND		2020 DEMAND		YR. 1	YR. 2	
Slough or Side Channel	River Mile	1971-72	1976-77	1981-82	1982-83	1971-72	1976-77	1981-82	1982-83	1971-72w	1971-72	1982-83	1971-72	1976-77	1981-82	1982-83	1971-72	1982-83	1982-83	1961-82
Whiskers	101.5	5	2	4	3	5	2	3	2	3	5	2	5	1	2	2	4	1	2	3
Gash Creek	112.0	5	4	4	4	5	3	5	5	6	5	7	5	2	2	3	4	1	3	4
6A	112.3	6	5	4	5	5	3	5	4	6	5	7	5	2	3	4	4	1	5	5
8	114.1	5	2	4	4	5	2	4	3	4	5	5	4	2	3	3	4	1	3	3
MSII	115.5	5	2	5	5	6	2	5	5	4	6	6.	4	3	3	4	4	2	3	5
MSII	115.9	5	3	7	6	7	3	7	6	6	5	8	4	6	4	6	5	3	5	8
Curry	120.0	6	5	7	4	7	5	8	5	3	5	1	4	3	1	_1_	4	2	4	6
Moose	123.6	10	4	7	5	0	6	8	2	4	6	2	7	4	1_	j	7	2	5	6
8A West	126.1	5	2	3	3	5	3	3	1	1	5		3	,_1_			3	1	1	2
8A Enst	127.1	5	2	3	3	1 4	3	2	0	0	4		3				3	0	1	2
9	129.3	6	4	7	6	5	3	3			6		. 3	ļ			3	1	2	4
9 u/s	130.6	8	3	6	7	5	4	2	ĺ		6		3				2) 1	3	6
4th July	131.8	7	1	3	5	5	3	2			7		3	1			_2_	1	1	3
9A	133.7	7	1	3	3	6	4	2	!		8		3						. 3	2
10 u/s	134.3	11	1	3	4	7	5	2			9	 	4						6	2
11 d/s	135.3	6	1	3	5	6	4	2			8		3						3	3
11	136 .5	_ 5	1	3	4	3	2	2	j		5			ا					3	4
17	139.3	(4	٠.		2					13						ŀ		1	4
20	140.5		0	f	ndary	2]				12					:			1	4
21 (A6)	141.8	Net	urat S	erru H	tions	/	Upsti	ream l	Exten	t of	3								1	2
21	142.2					l '	los Co	over P	ragre	sion	_1						Ì		1	1
22	144.8												_						1	1

NOTES:

- 1. "Case C" operating guide is assumed for with-project simulations.
- 1971-72W simulation assumes warm, 4°C reservoir releases.
 All other with-project simulations assume an "inflow-matching" temperature policy.
- 3. Upstream extent of simulated ice cover progression for Watana filling occurs upstream of River Mile 144.8.
- 4. All ice thickness in feet.
- 5. Winter air temperatures: 1971-72 cold 1976-77 very warm 1981-82 average

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SUSITNA HYDROELECTRIC PROJECT SOLID ICE THICKNESS MAXIMUM SIMULATED VALUES

		NATURAL	WATANA ONLY	,	WATANA AND DEVI	L CANYON	WATANA FILLING	
		CONDITIONS	1996 DEMAND	2001 DEMAND	2002 DEMAND	2020 DEMAND	YR. 1 YR. 2	
Slough or Side Channel	River Mile	1971-72 1976-77 1981-82 1982-83	1971-72 1976-77 1981-82 1962-83 1971-72**	1971-72	1971-72 1976-77 1981-82 1982-83	1971-72	1982-83	
Whiskers	101.5	5 2 4 3	5 2 3 2 3	5 2	5 1 2 2	4 1	2 3	
Gash Creek	112.0	5 2 4 3	5 2 3 2 2	5 1	5 1 2 1	4 1	2 3	
6A	112.3	5 2 4 3	5 2 3 2 2	5 1	5 1 2 1	4 1	2 3	
8	114.1	5 2 4 3	5 2 3 2 2	5 1	5 1 2 1	4 1	2 3	
MSII	115.5	5 2 4 3	5 2 3 2 1	5 1	4 1 1 1	4 1	2 3	
MSII	115.9	5 2 4 3	5 2 3 1 1	5 0	4 1 1 1	4 1	2 3	
Curry	120.0	5 2 4 3	5 2 2 0 1	5 0	4 1 1 0_	3 0	2 3	
Moose	123.5	5 2 4 3	4 1 2 0 0	4 0	4 0 0	2 0	2 2	
8A West	126.1	5 2 3 3	4 1 1 0 0	4	3 0	1 0	1 2	
8A East	127.1	5 2 3 3	3 1 1 0 0	4	3	1 0_	1 2	
9	129.3	5 2 3 3	3 1 1	4	3	1	1 2	
9 u/s	130.6	5 2 3 3	3 1 1	4	2	0	1 2	
4th July	131.8	5 1 3 3	2 1 1	4	2	0	1 2	
9A	133.7	5 1 3 2	2 1 0	4	1		1 2	
10 u/s	134.3	5 1 3 2	2 0 0	3	1		1 2	
11 d/s	135.3	4 1 3 2	2 0 0	3	0		1 2	
11	136.5	4 1 3 2	1 0 0	3	0		1 2	
17	139.3	[(0	2			0 2	
20	140.5	Upstreem Boundar of	1 0 1	2			0 2	
21 (A6)	141.8	Natural Simulation	Upstream Extent of	1			0 2	
21	142.2		Ice Cover Progression	_0			0 1	
22	144.8	i .		11			0 1	
		[1		1	1	<u> </u>	

NOTES:

- 1. "Case C" operating guide is assumed for with-project simulations.
- 1971-72^W simulation assumes warm, 4°C reservoir releases.
 All other with project simulations assume an "inflow-matching" temperature policy.
- Upstream extent of simulated ice cover progression for Watana filling occurs upstream of River Mile 144.8.
- 4. All ice thickness in feet.
- 5. Winter air temperatures: 1971-72 cold

1971-72 cold 1976-77 very warm 1981-82 average 1982-83 warm

FIGURES

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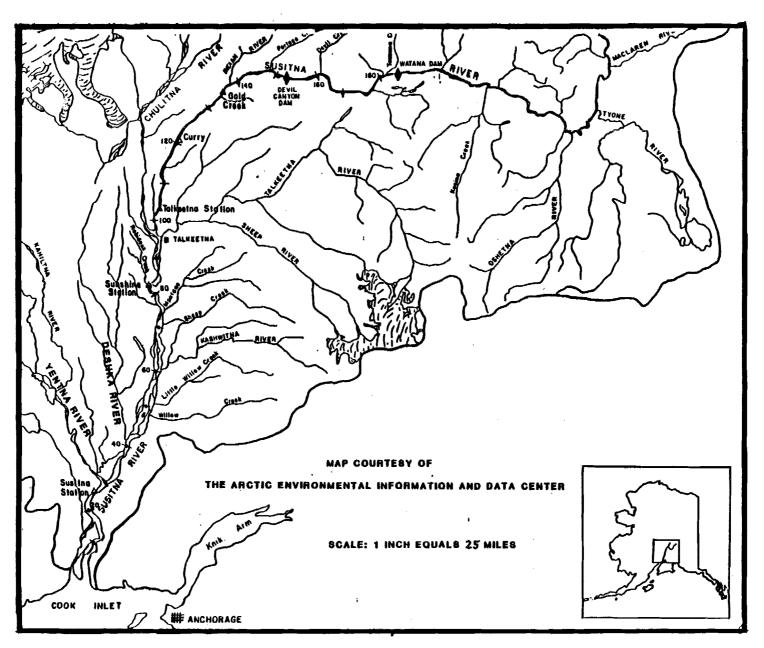
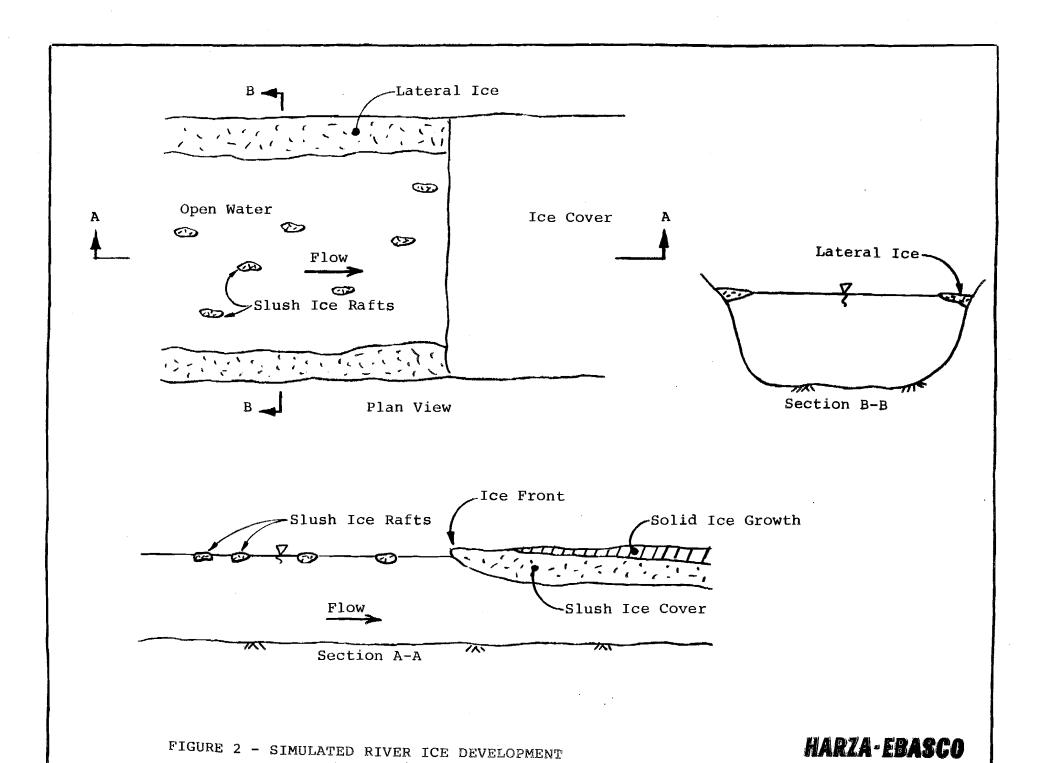


FIGURE 1 - SUSITNA RIVER



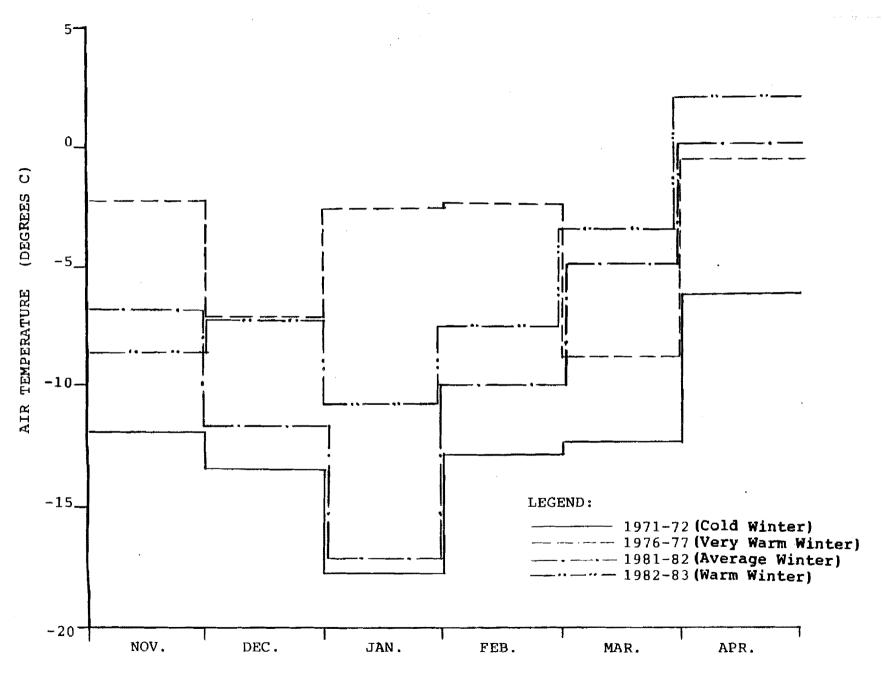


FIGURE 3 - AVERAGE MONTHLY AIR TEMPERATURES AT TALKEETNA

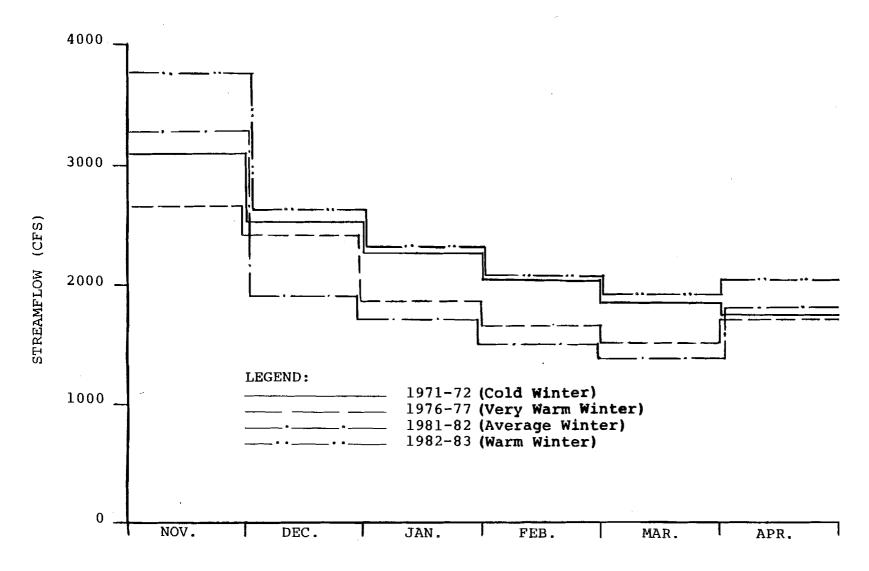


FIGURE 4 - SUSITNA RIVER NATURAL STREAMFLOWS AT GOLD CREEK - AVERAGE MONTHLY VALUES

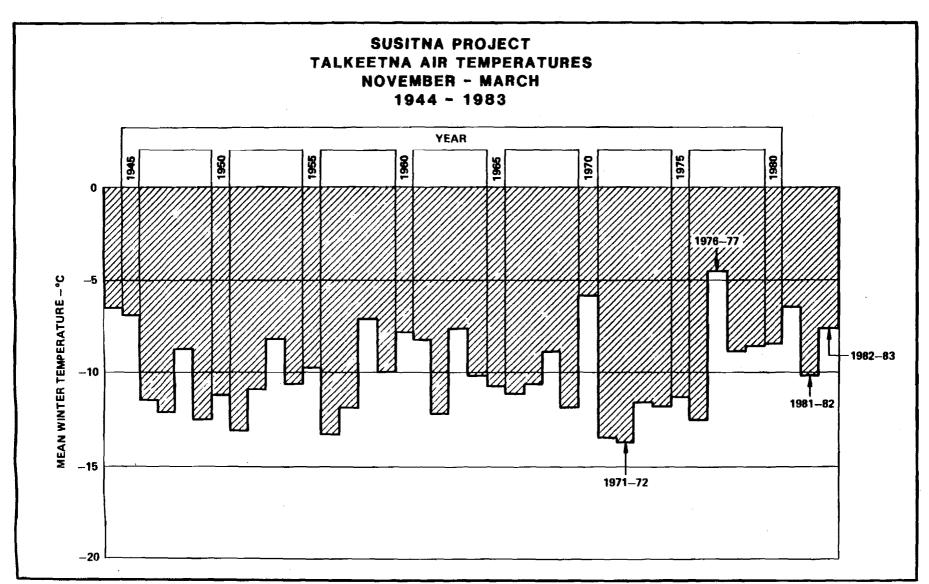


FIGURE 5

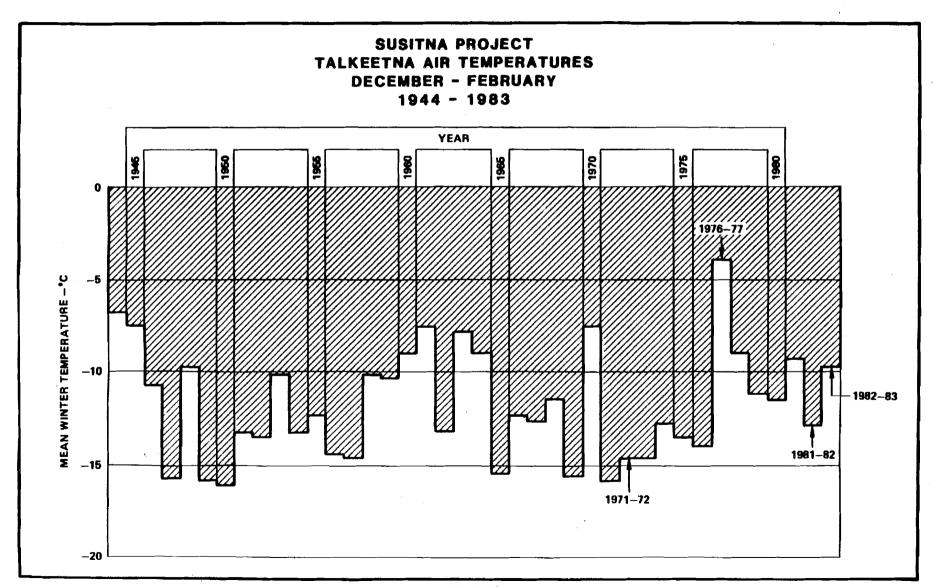


FIGURE 6 ·

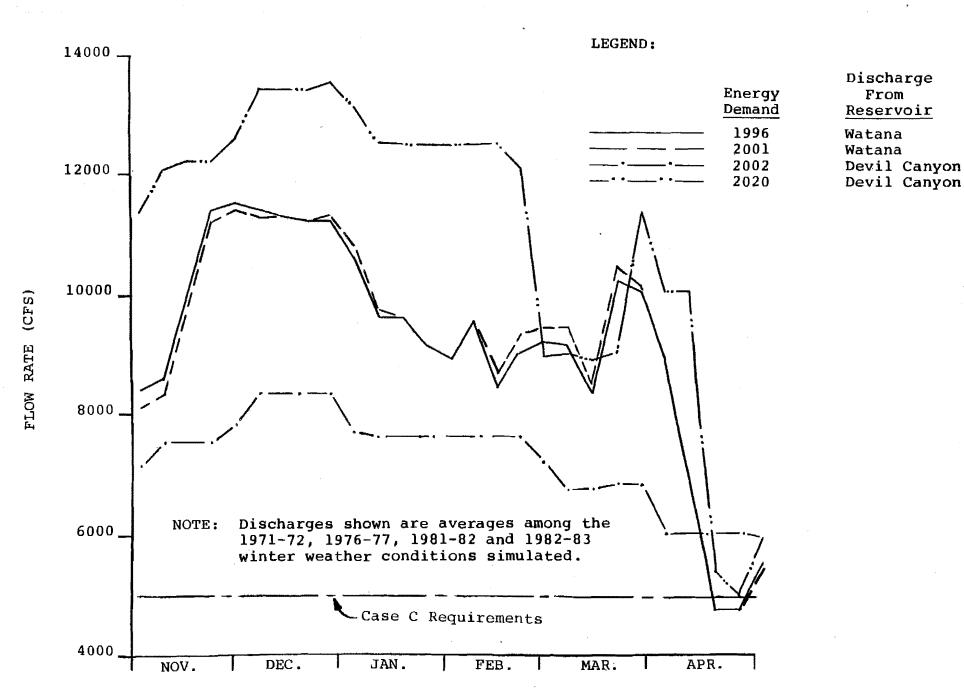
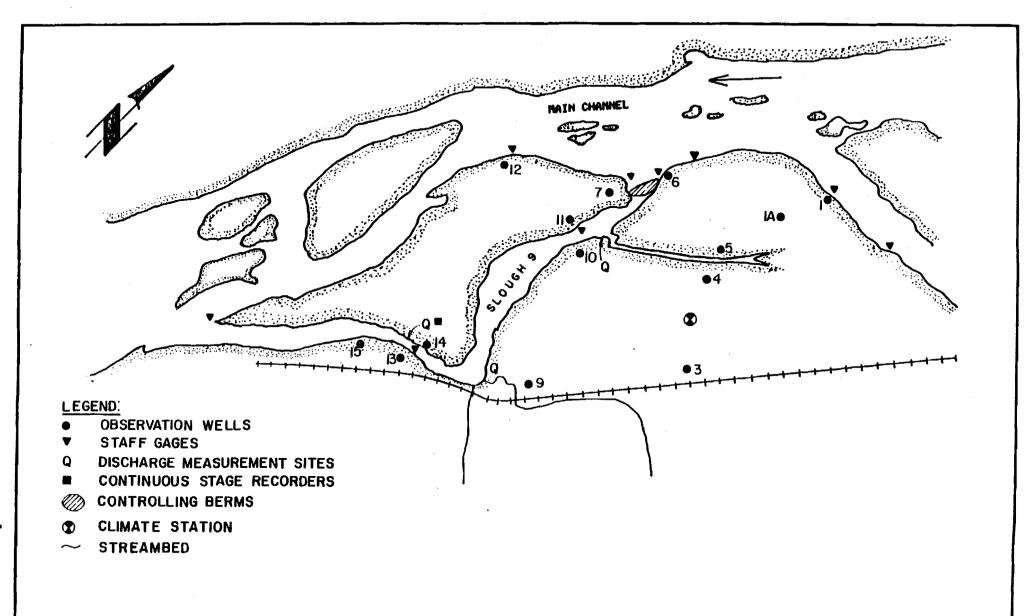


FIGURE 7 - DISCHARGE FROM PROJECT RESERVOIRS

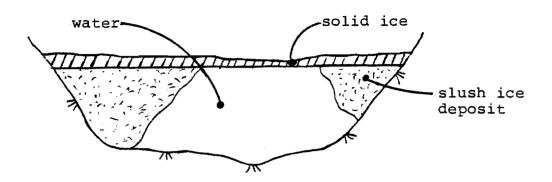


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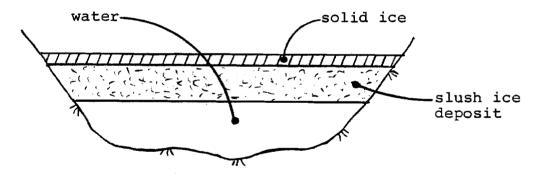


FIGURE 8 - TYPICAL SLOUGH

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a. Actual River Cross-Section

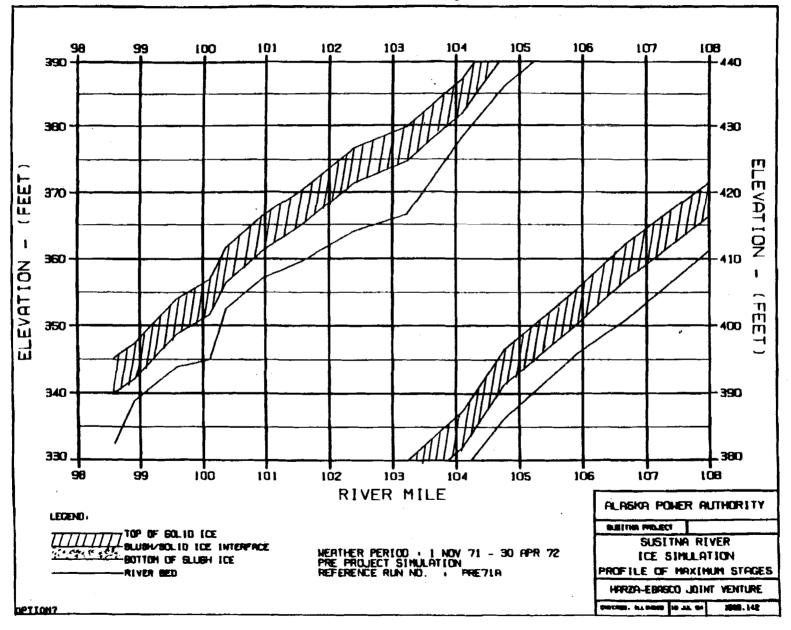


b. Simulated River Cross-Section

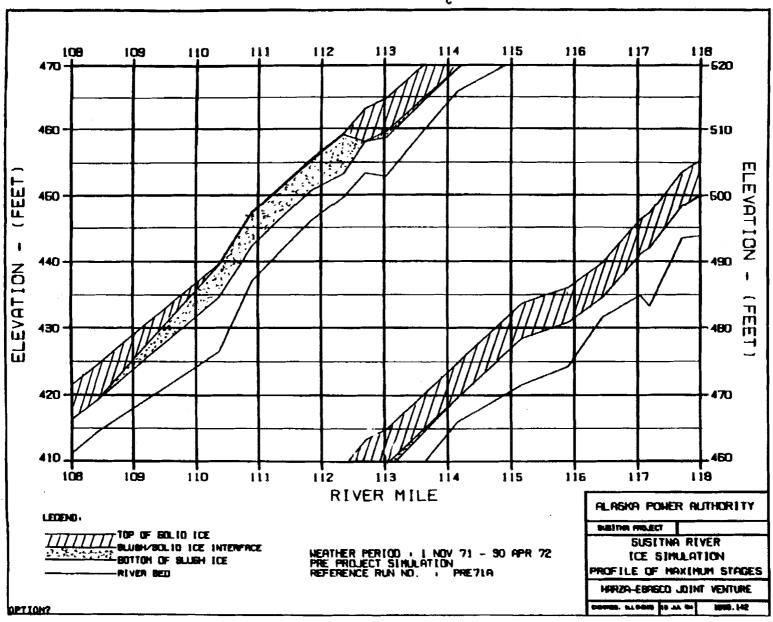
FIGURE 9 - ICE DISTRIBUTION - ACTUAL VS. SIMULATED

EXHIBIT A

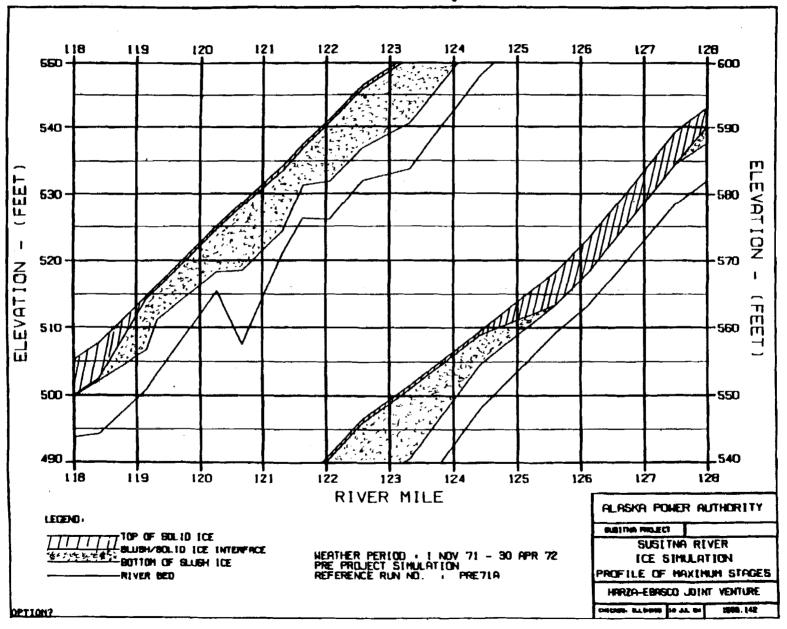


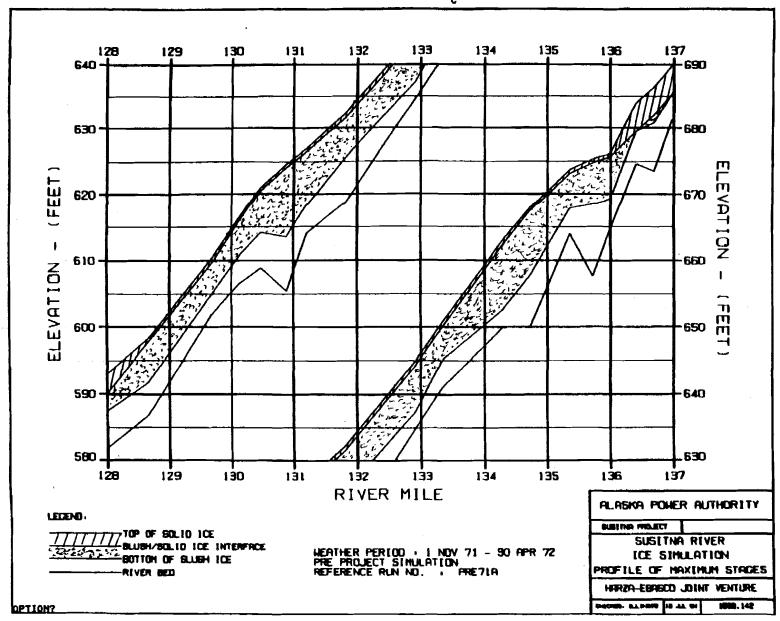




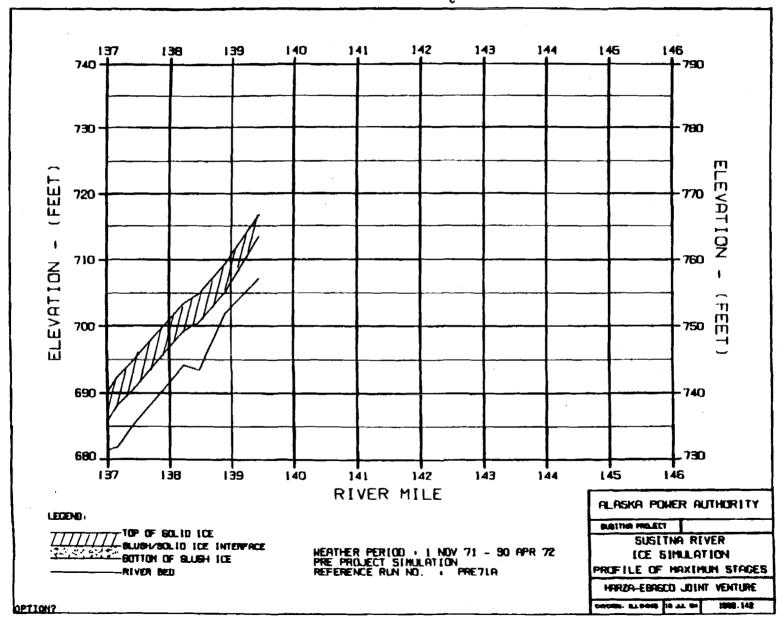


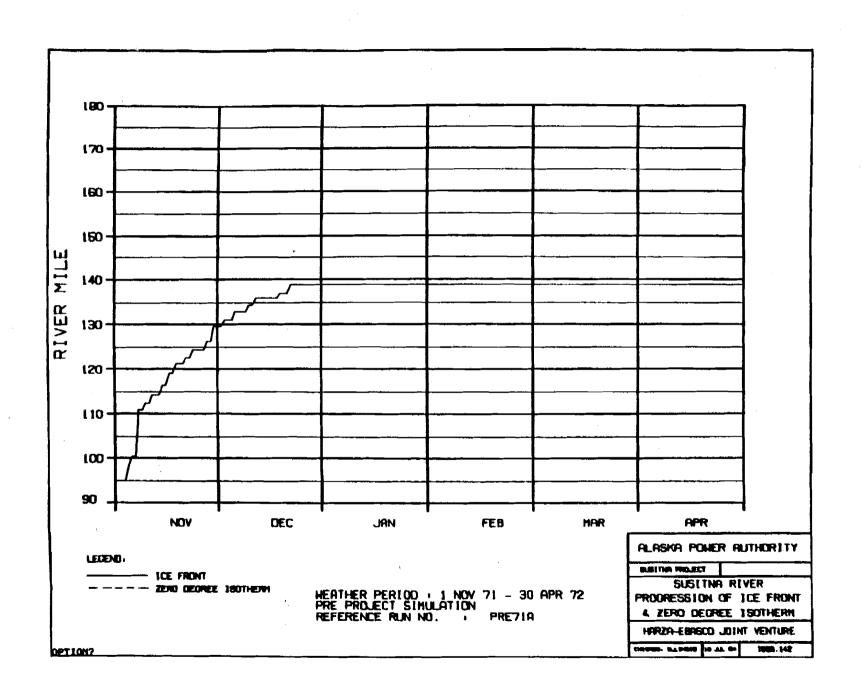


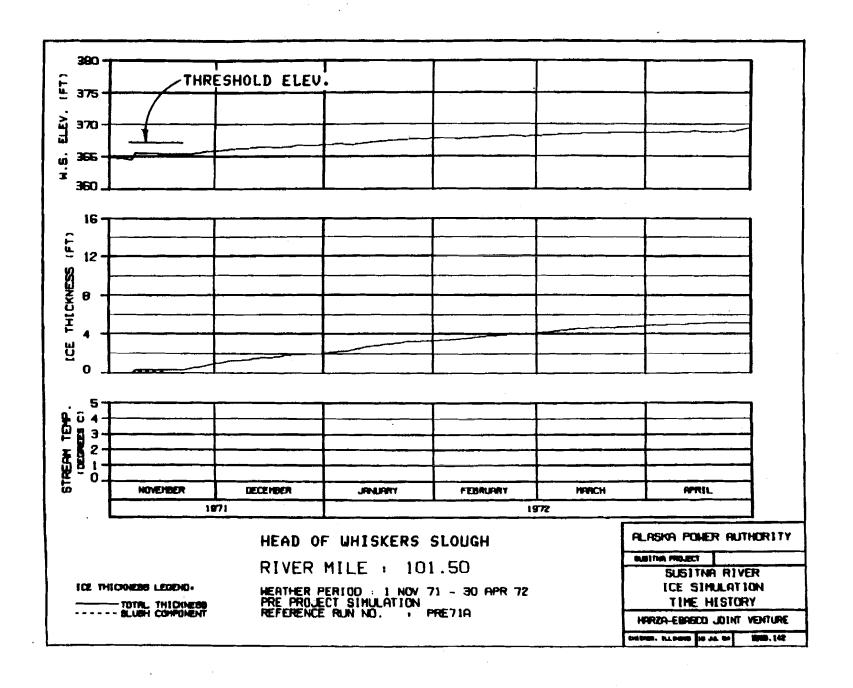


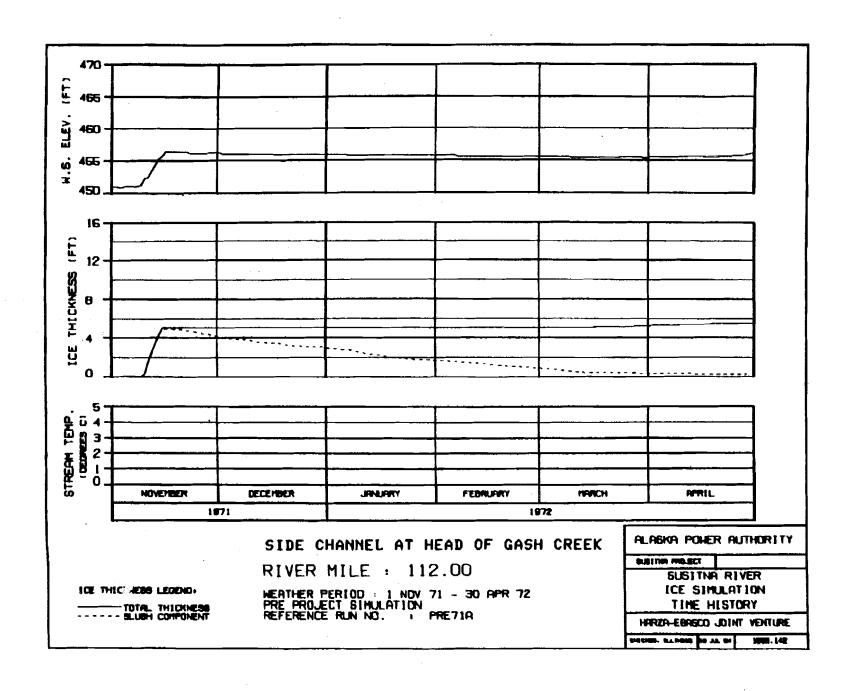


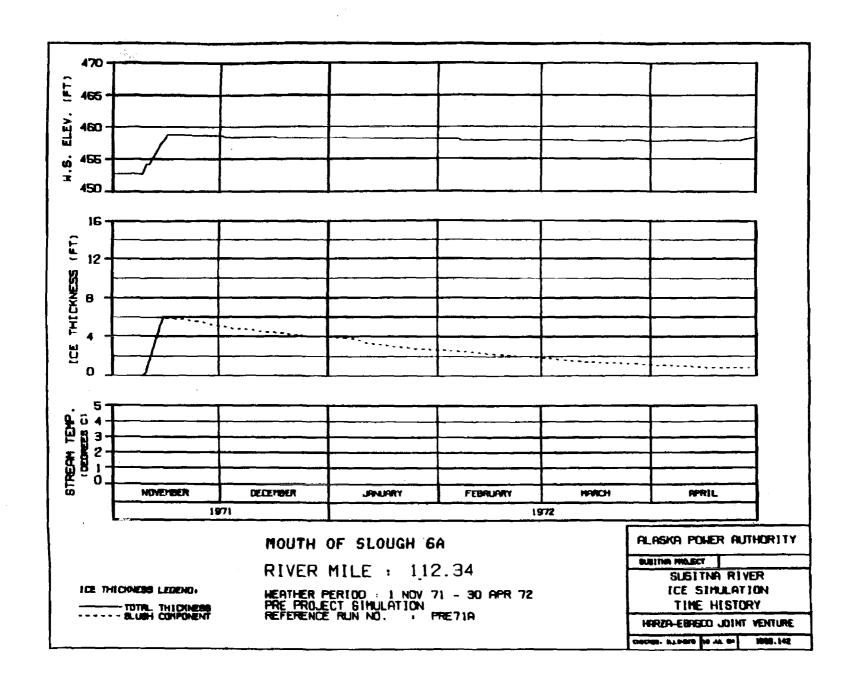
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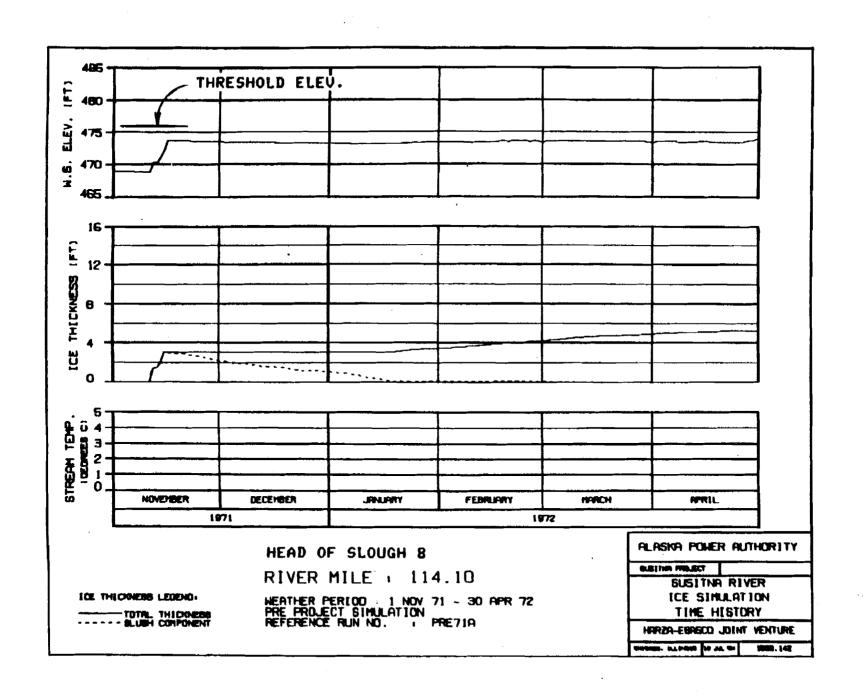



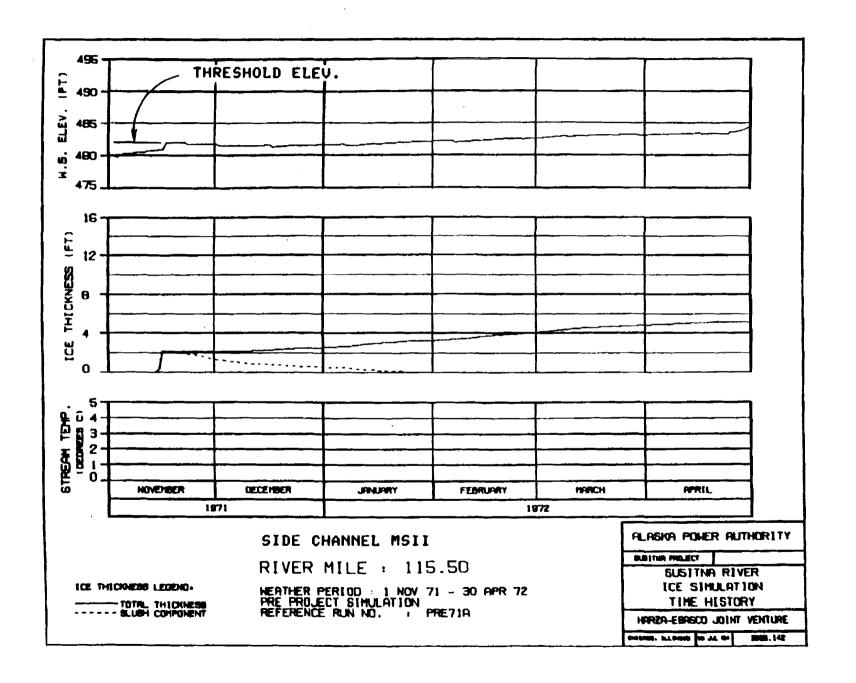


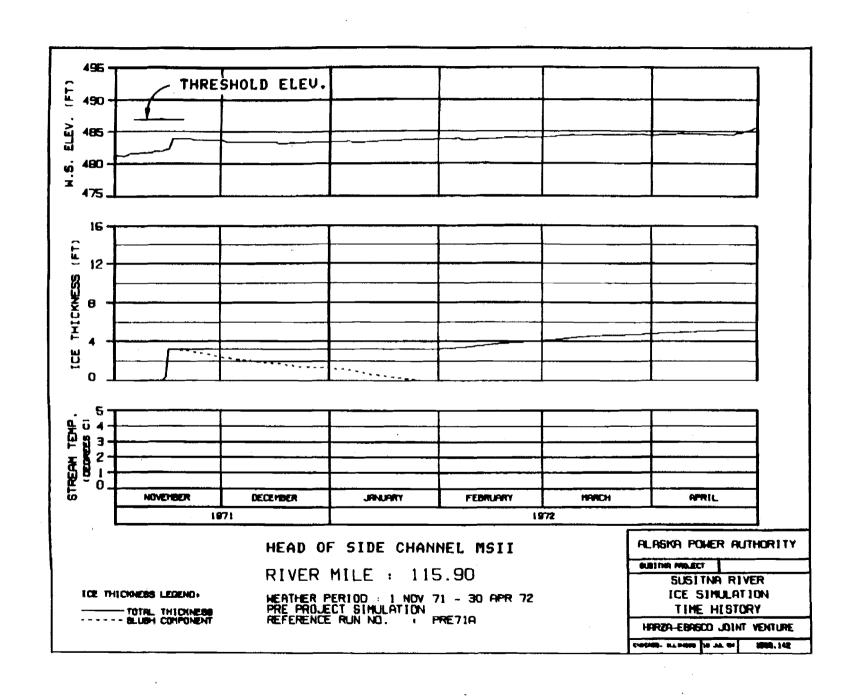




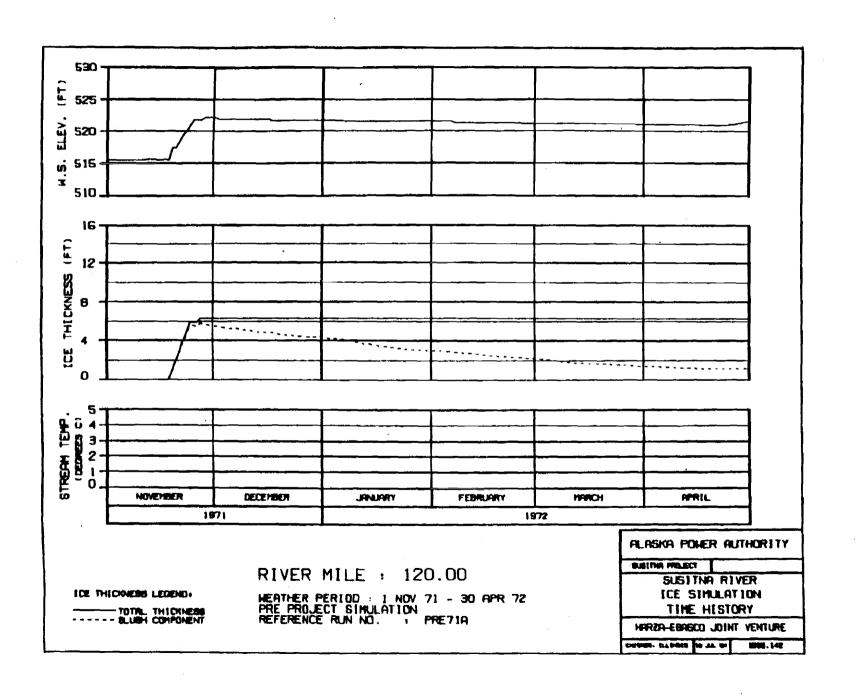


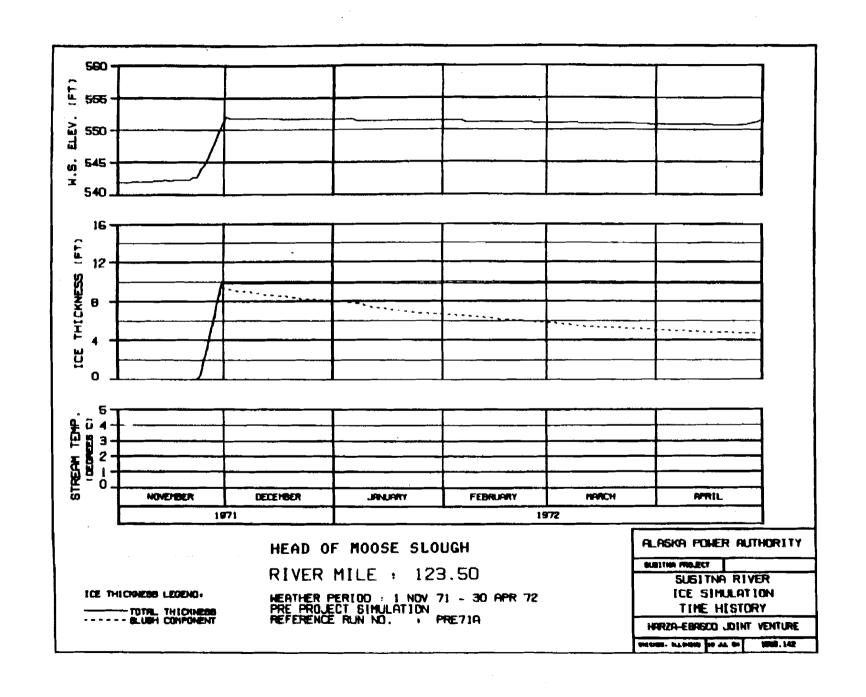


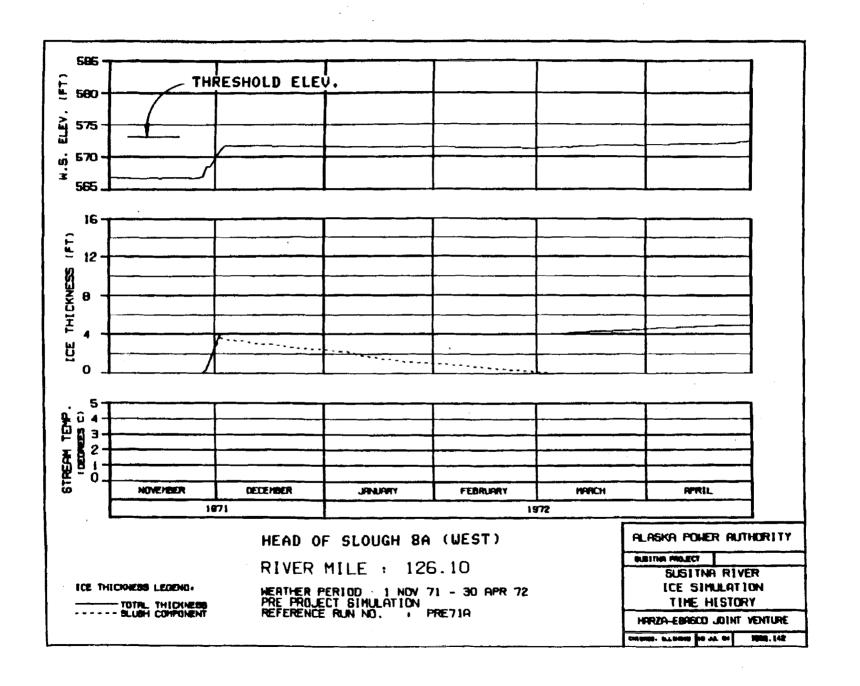


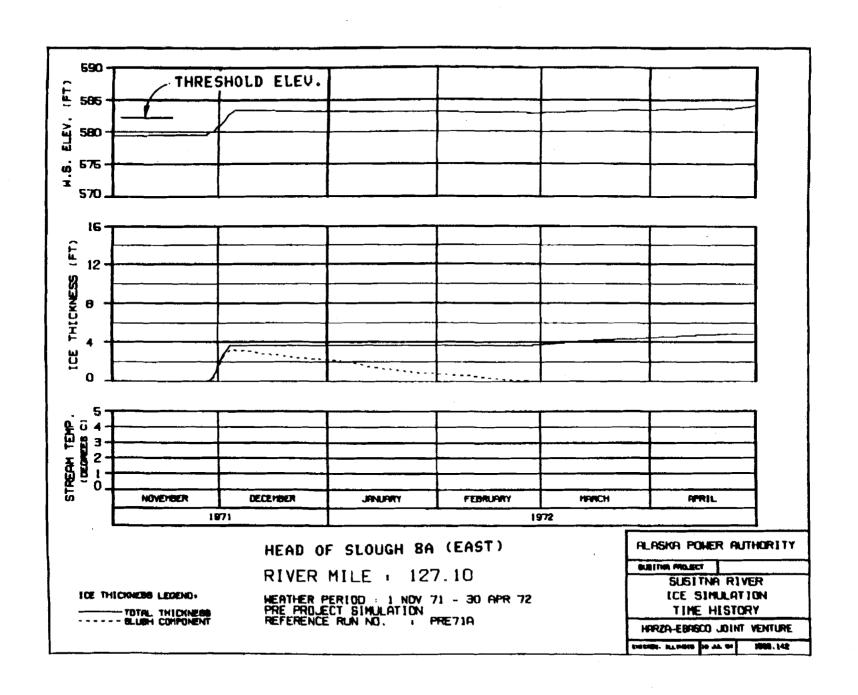


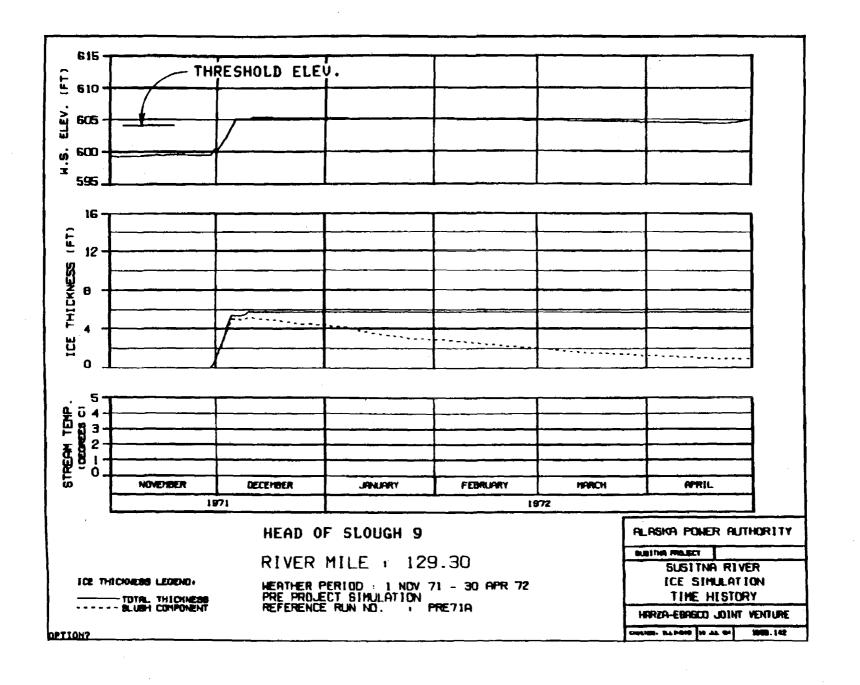
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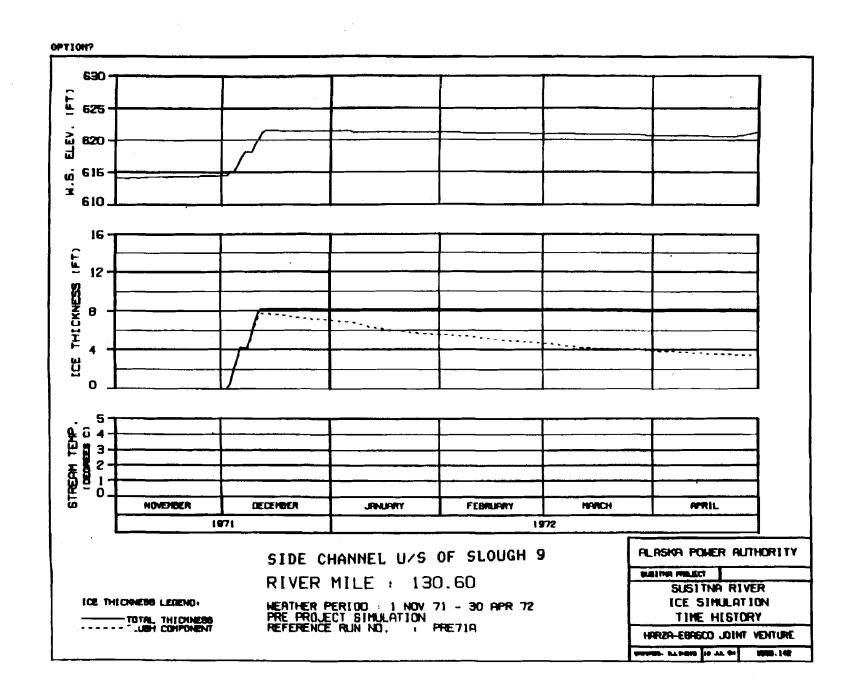


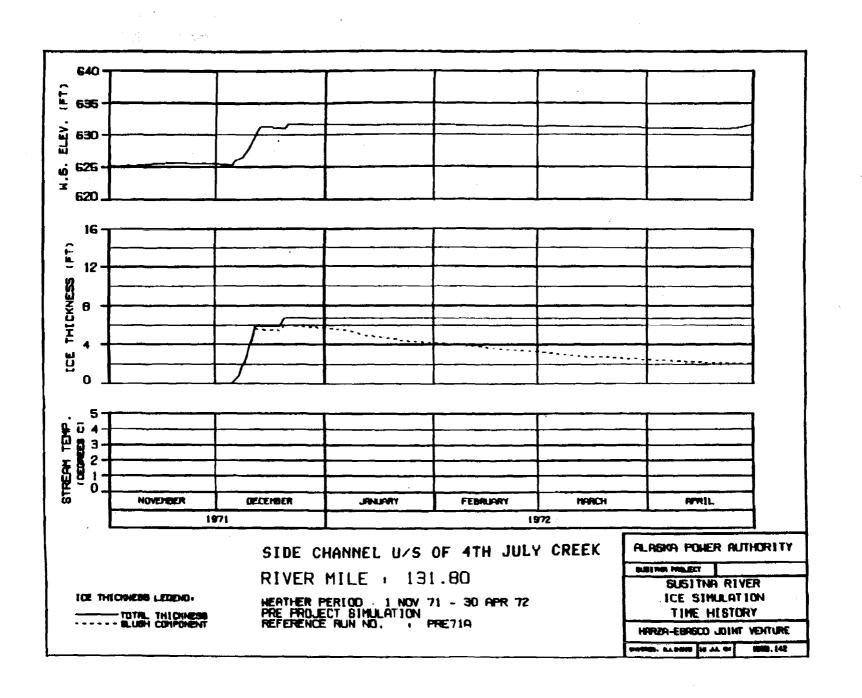


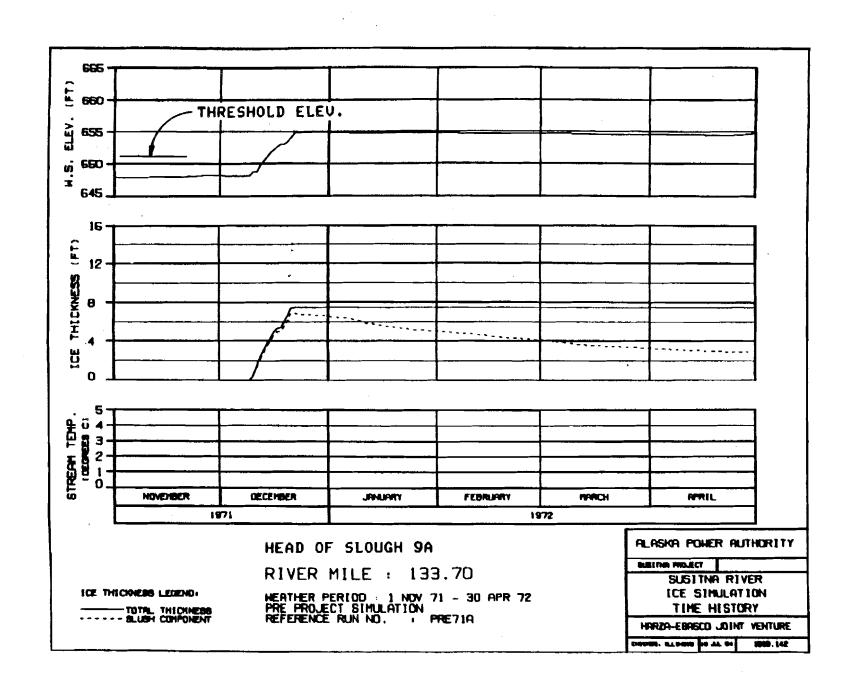


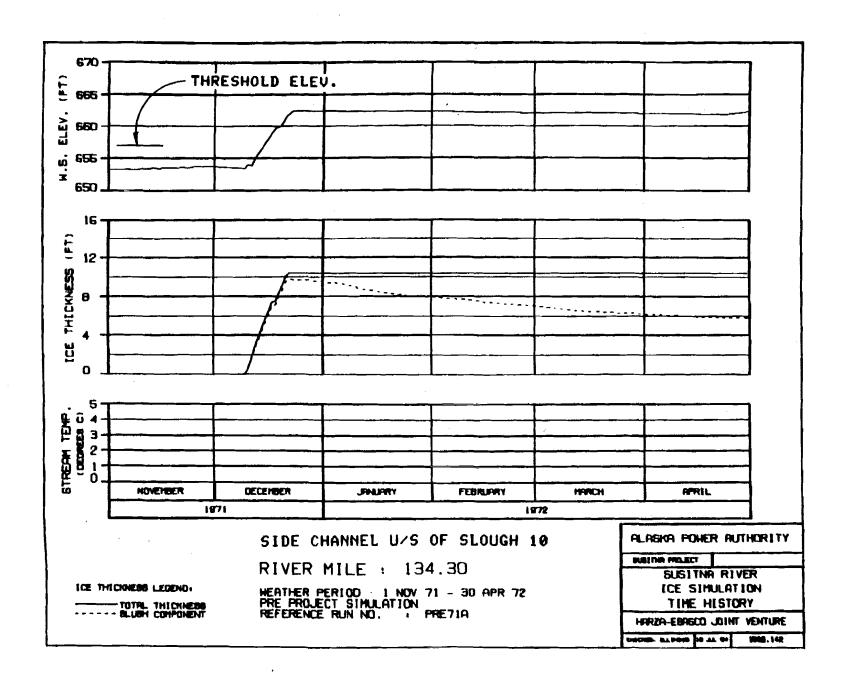


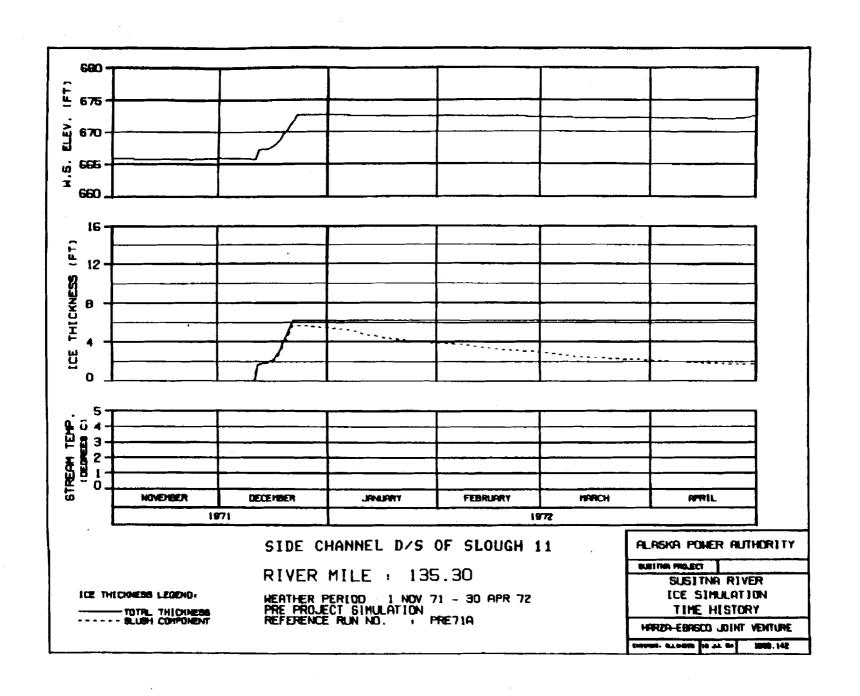












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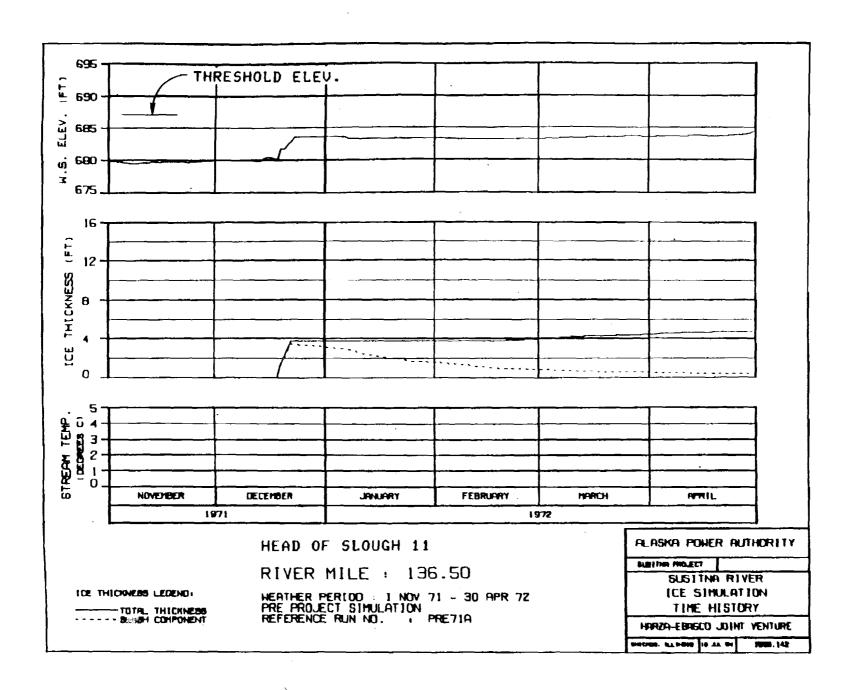
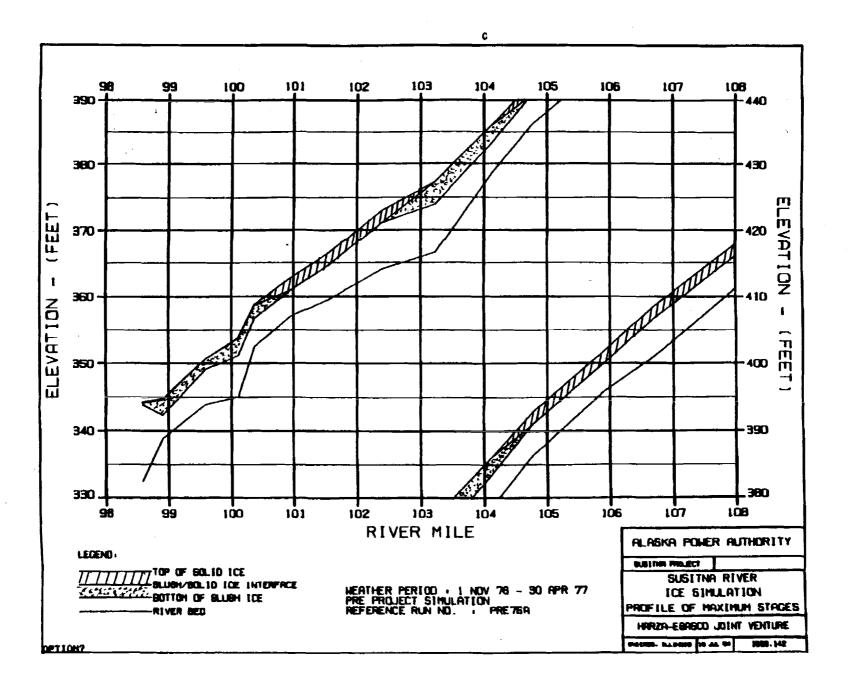
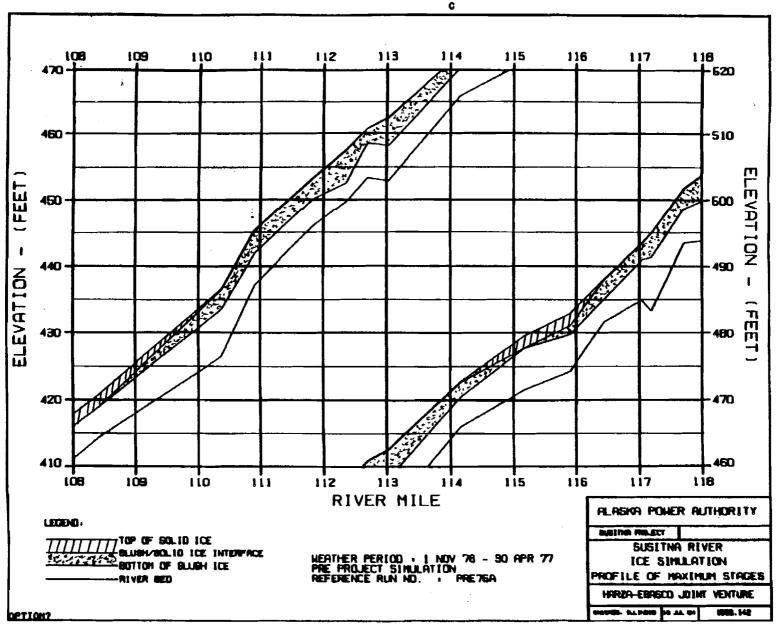
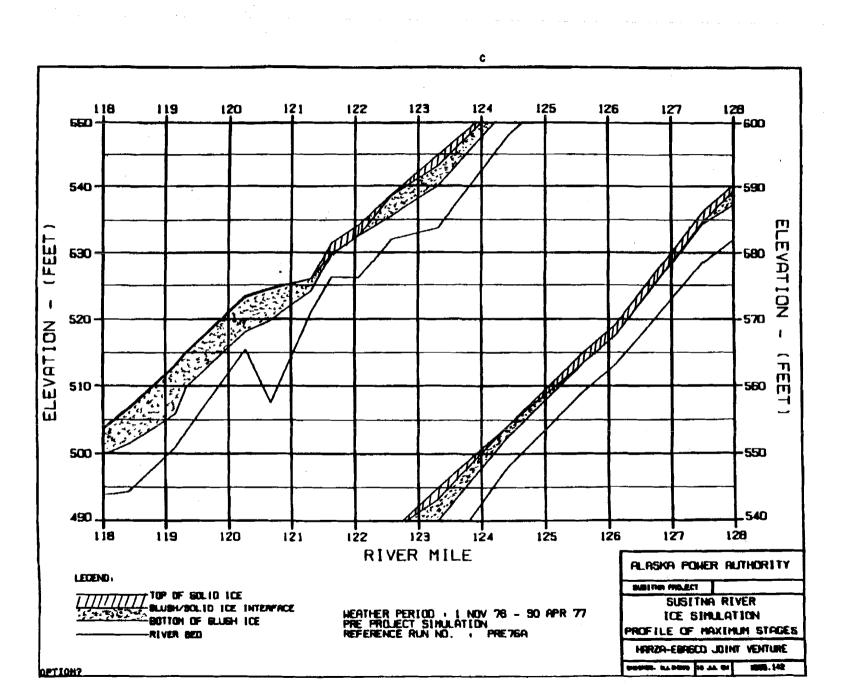


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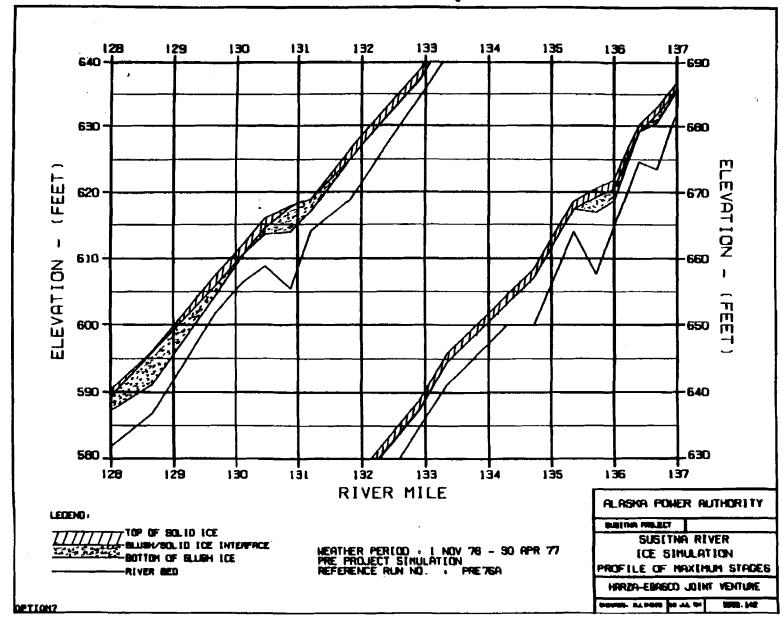




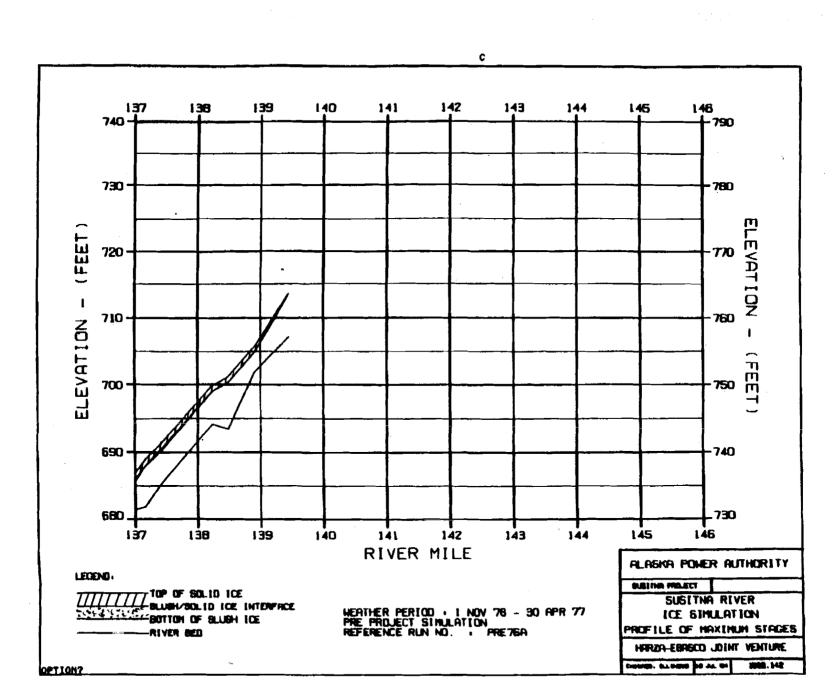


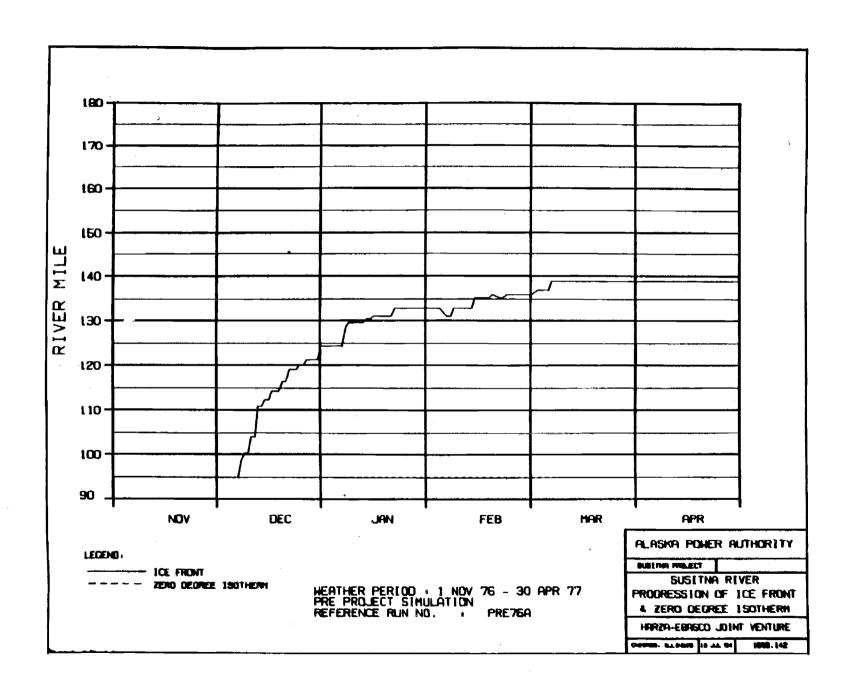


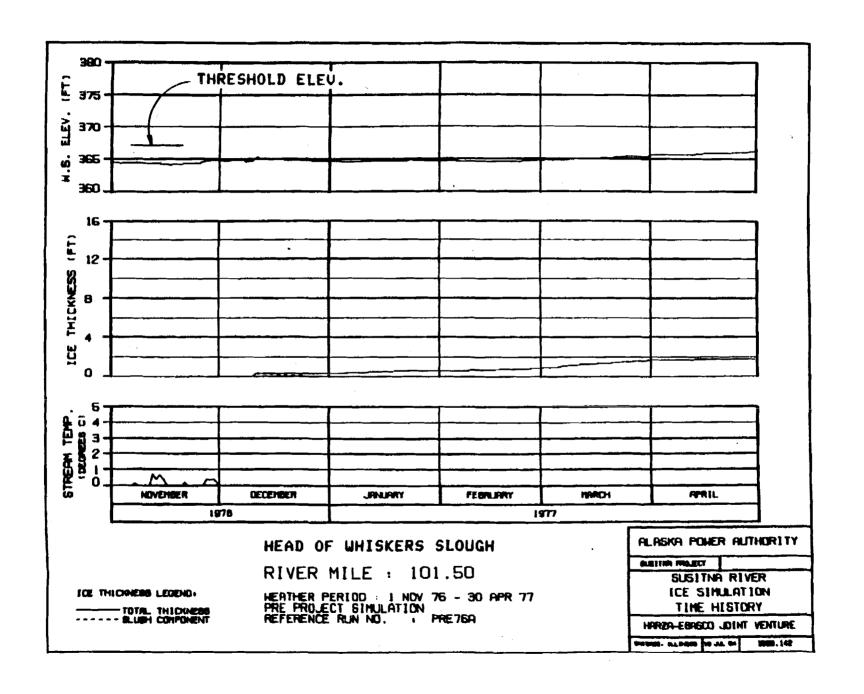


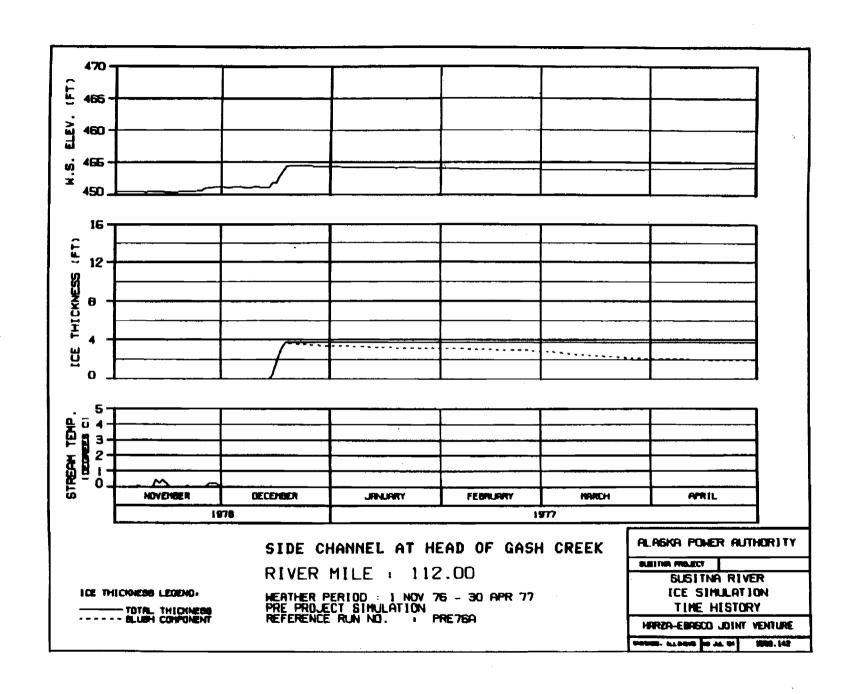


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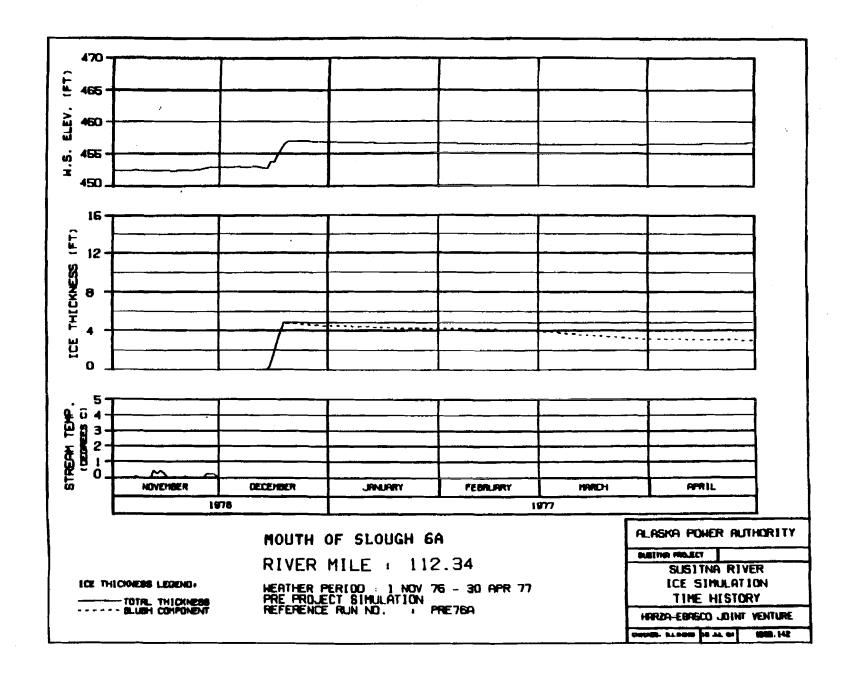


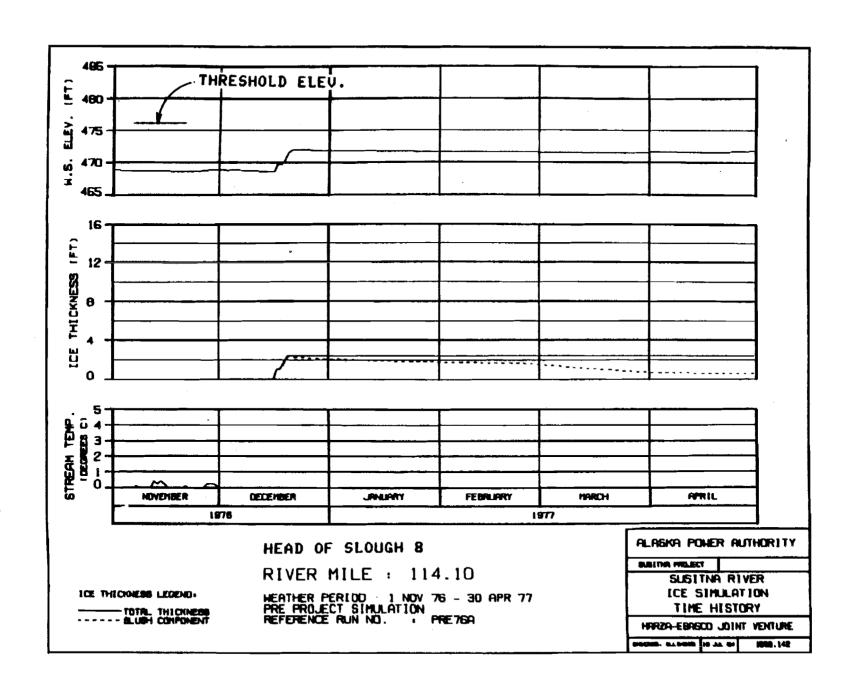




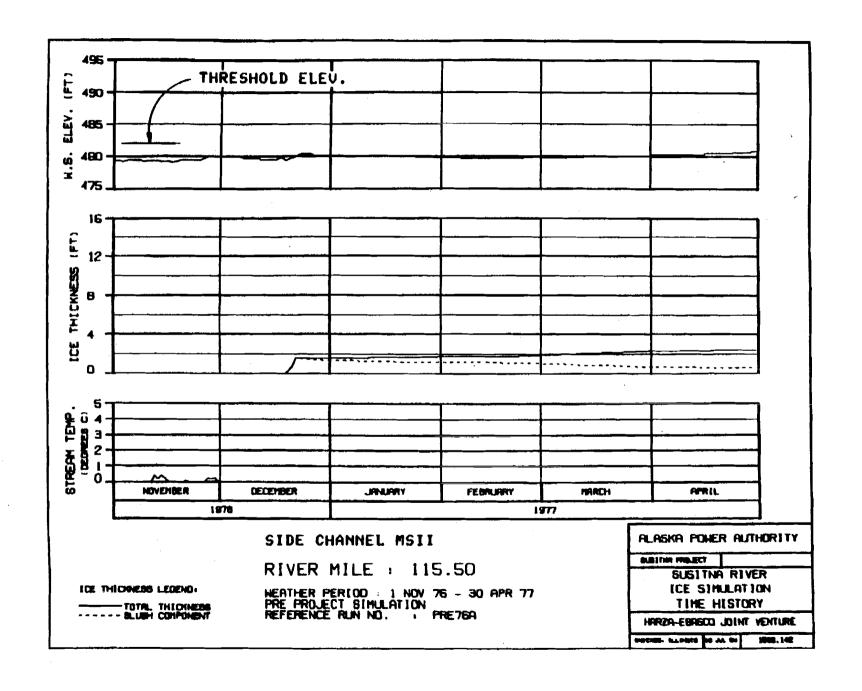


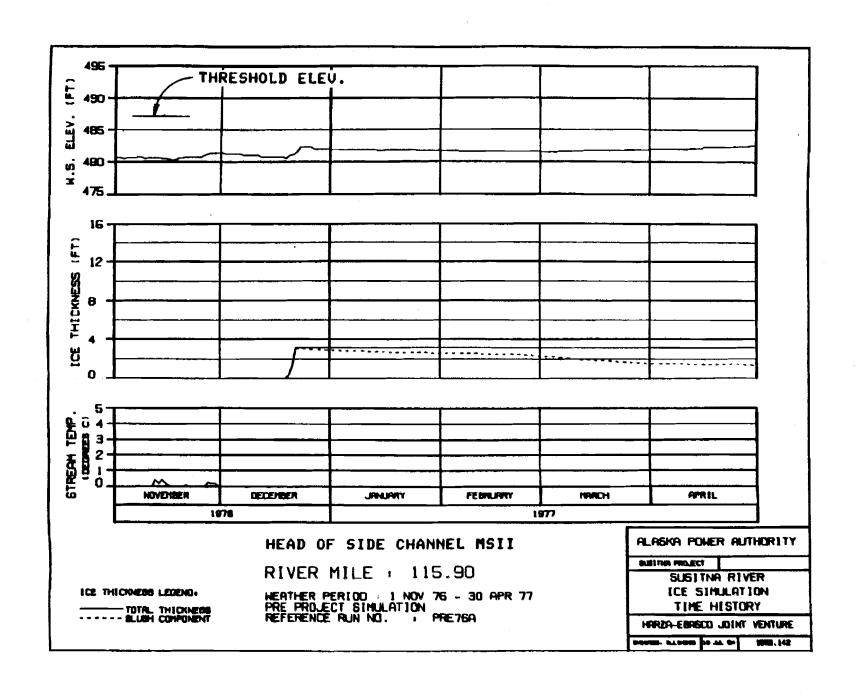
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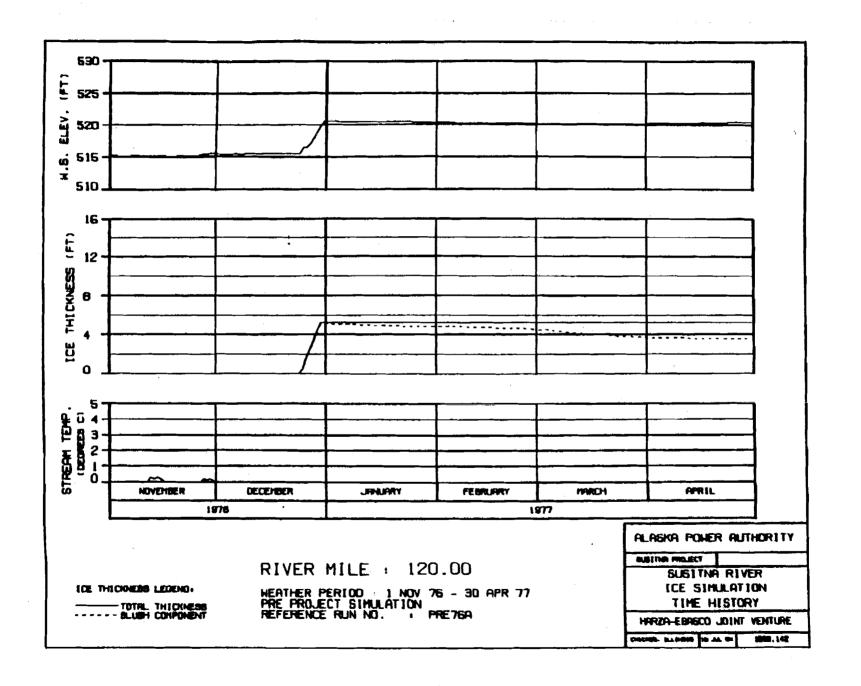


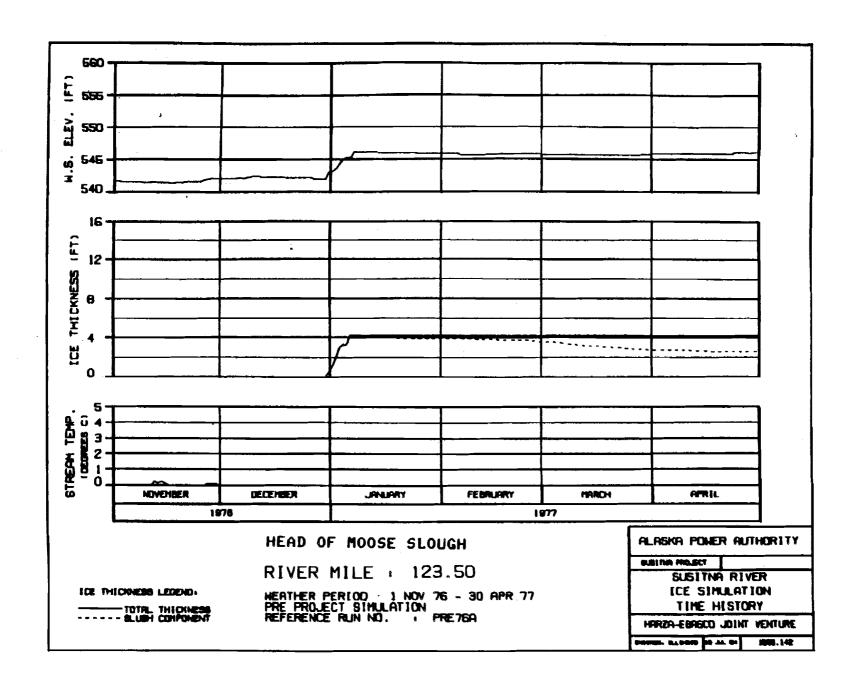


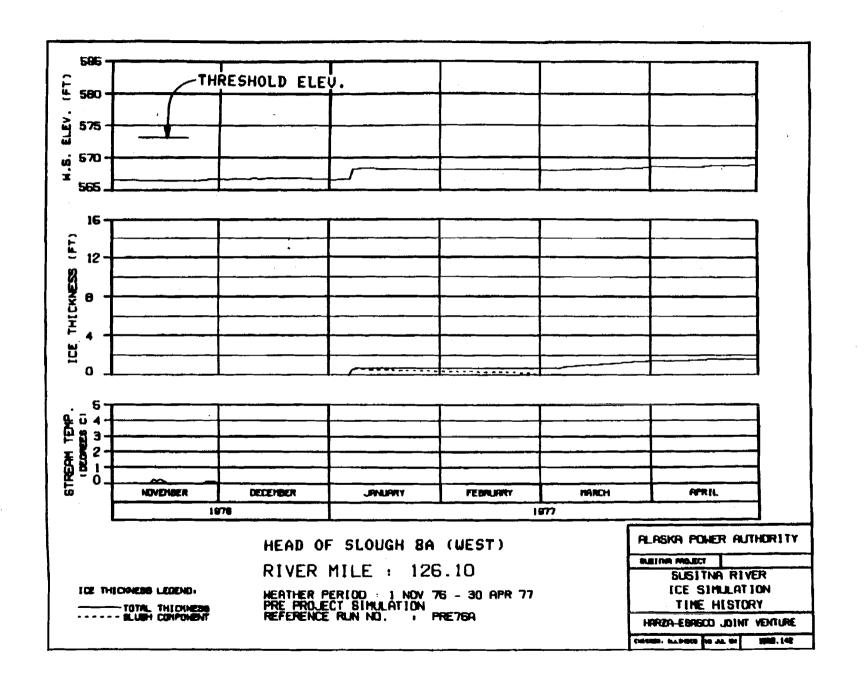
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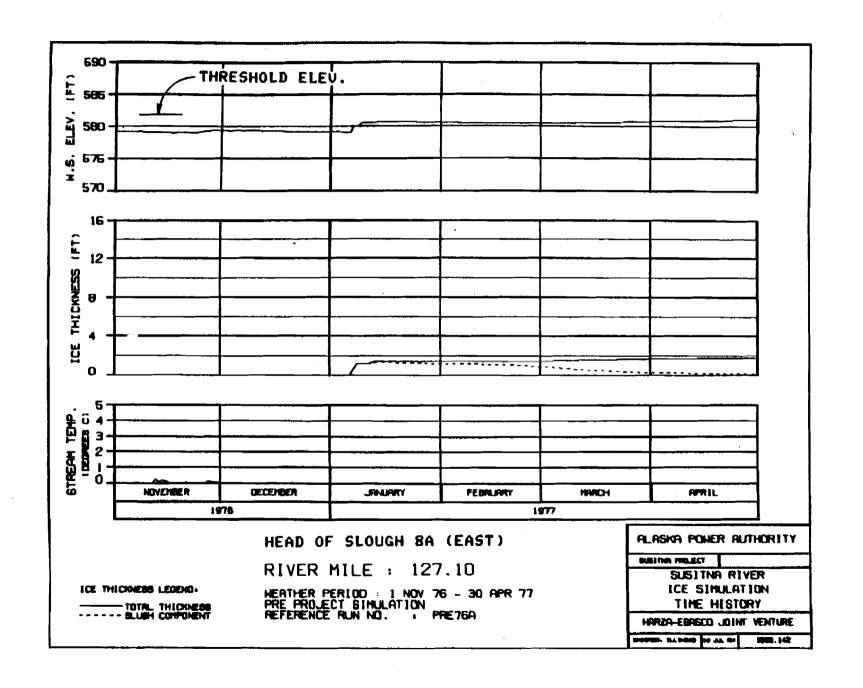


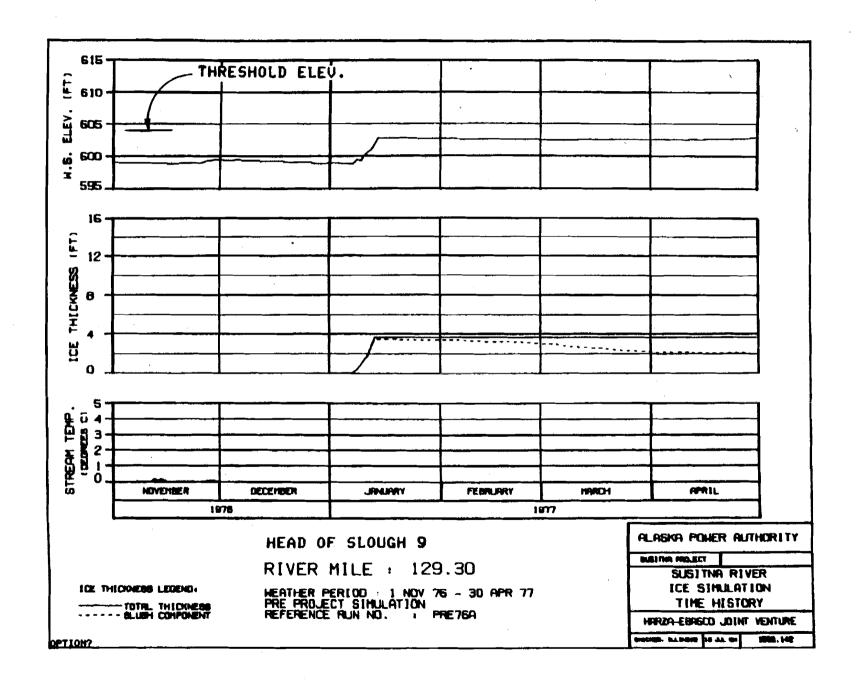


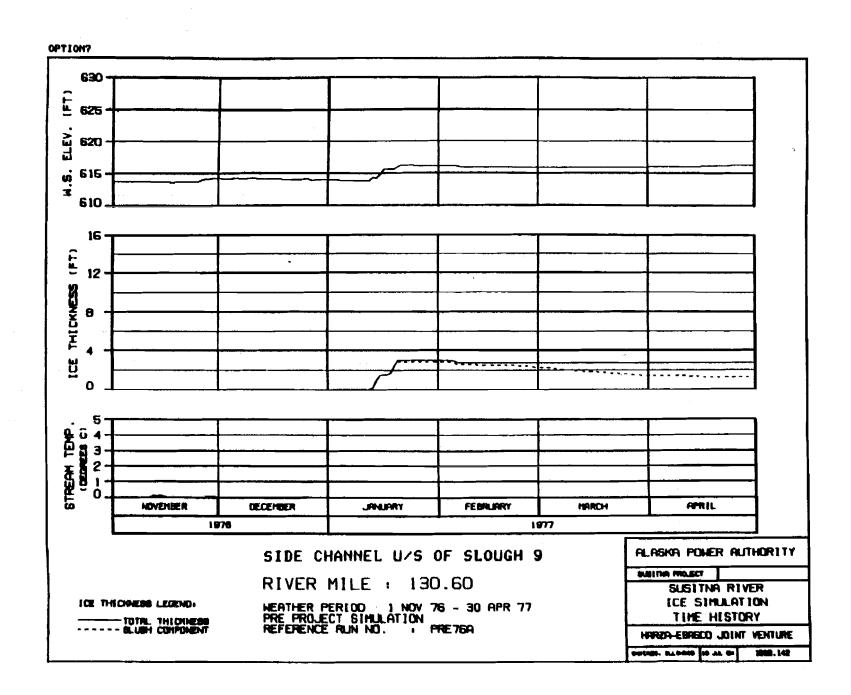


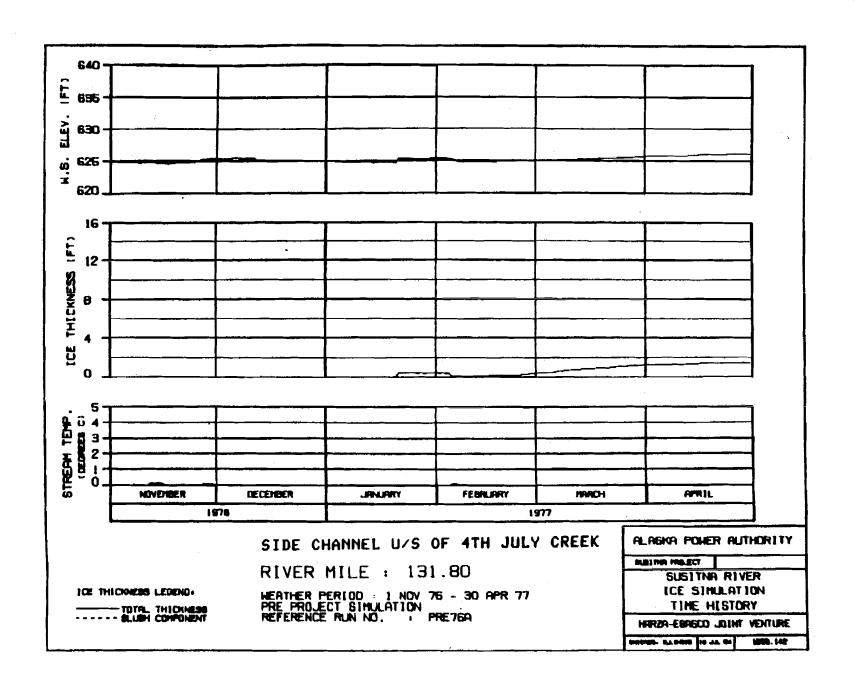


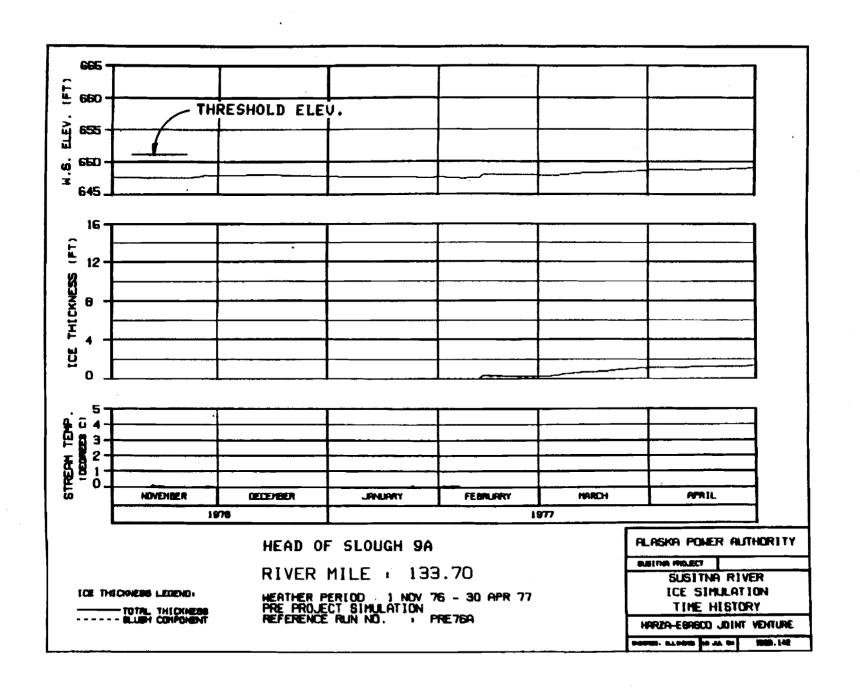


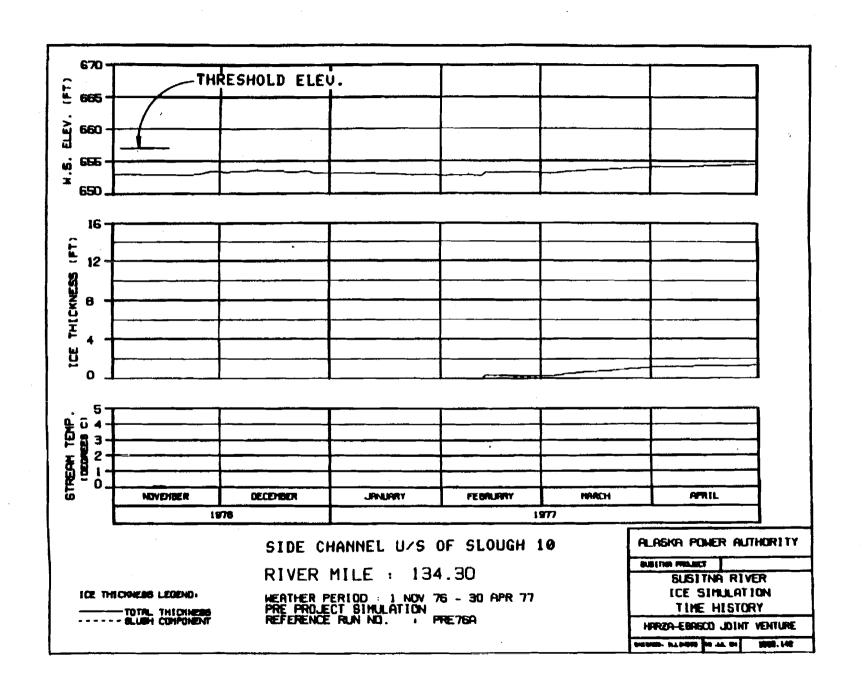


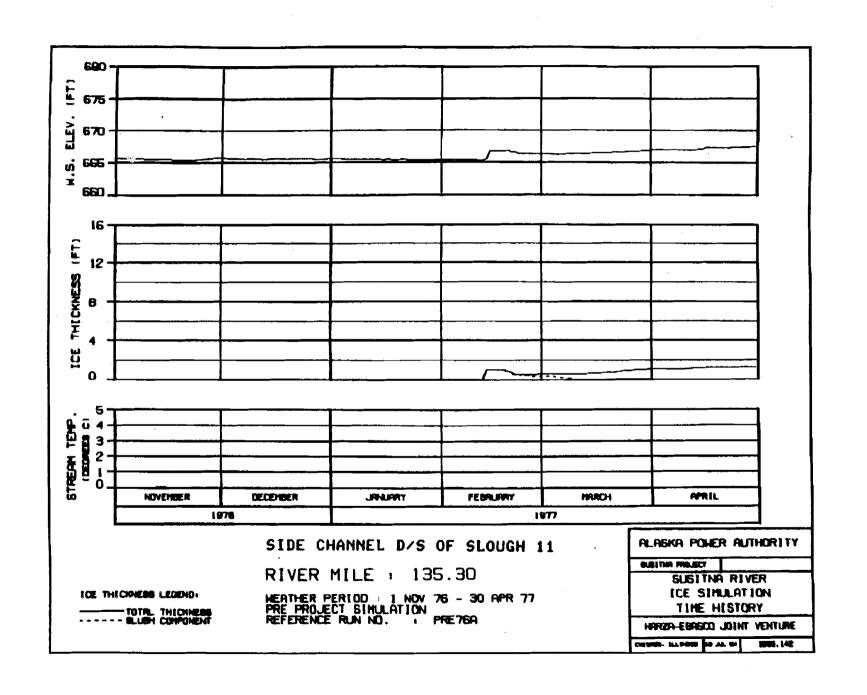












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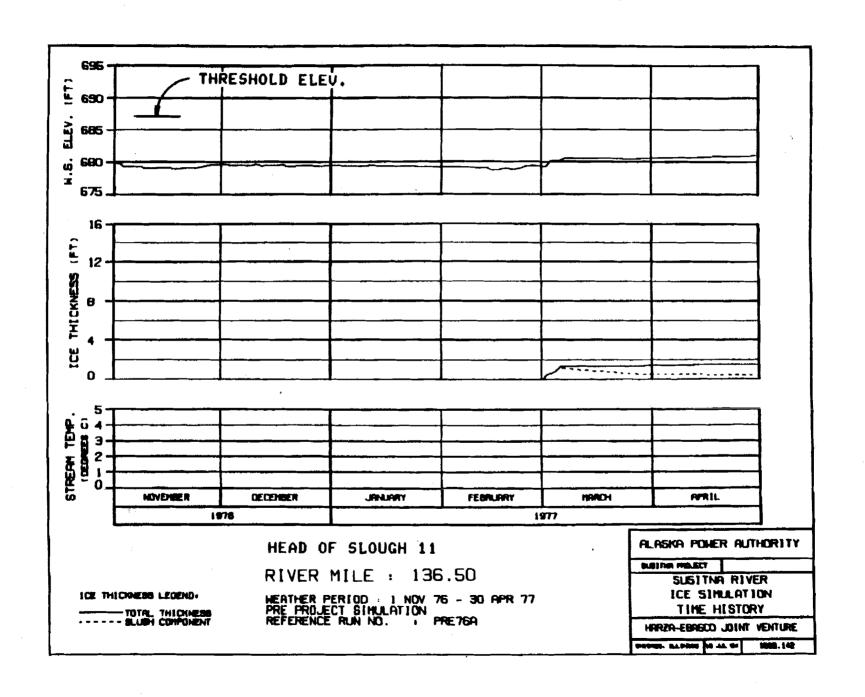
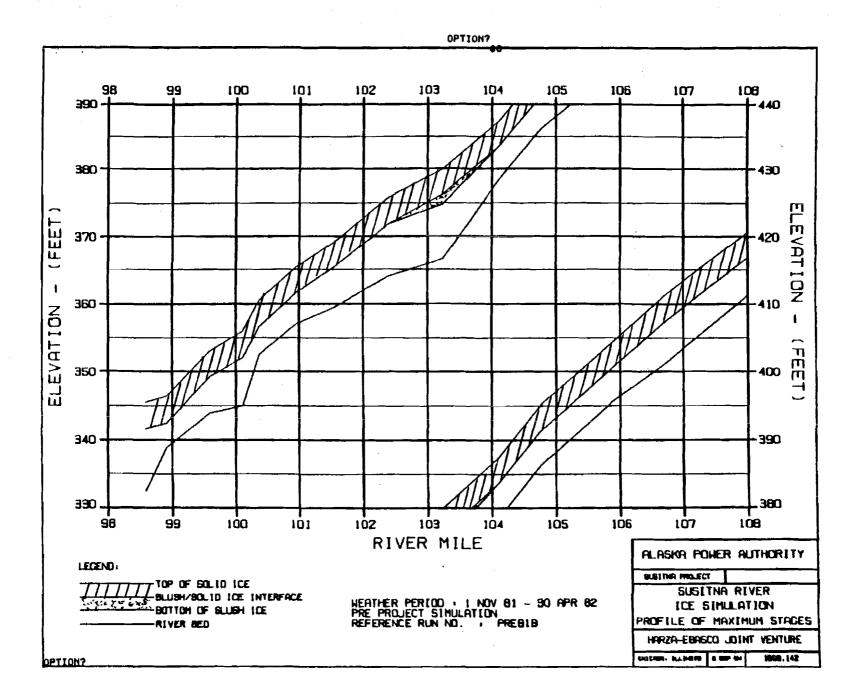
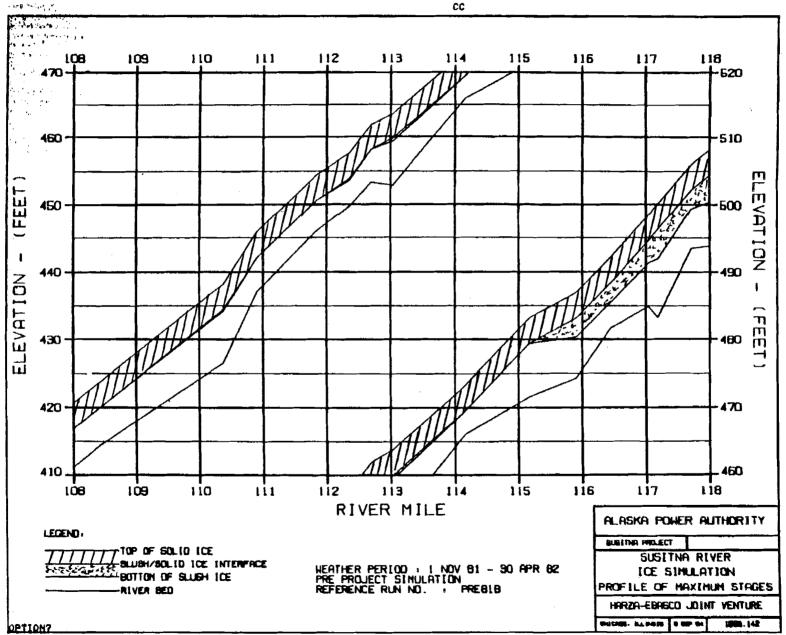
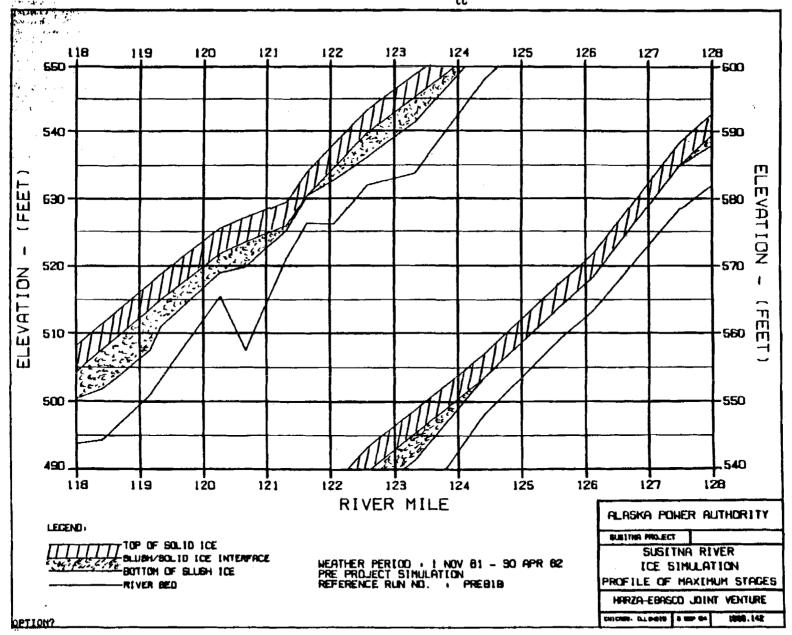


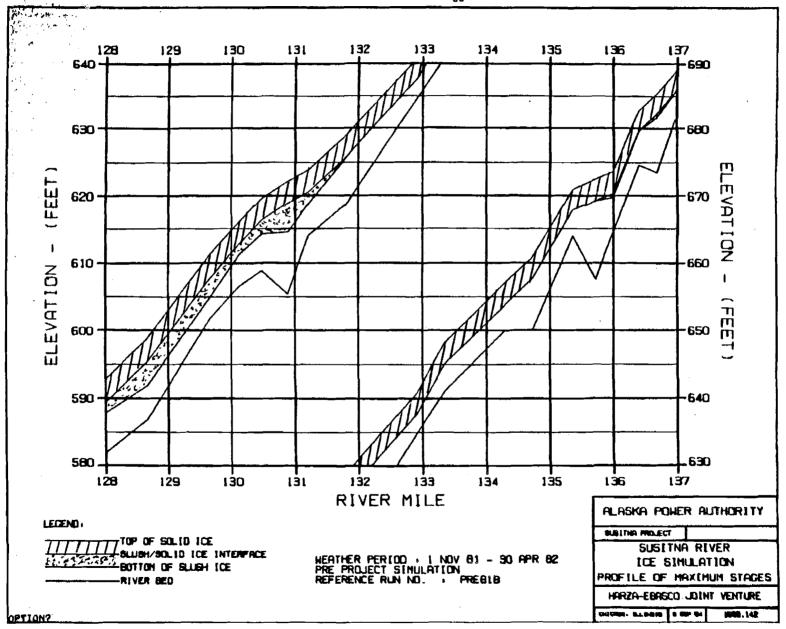
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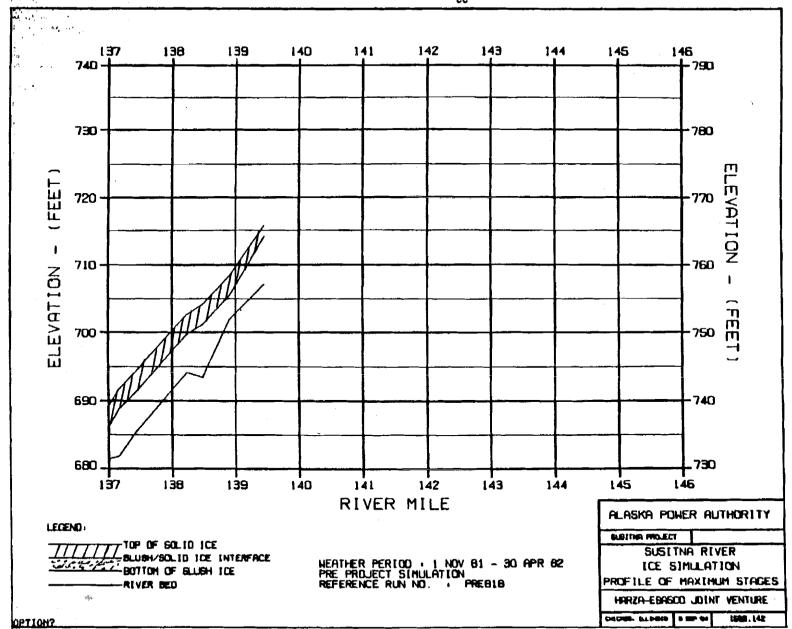


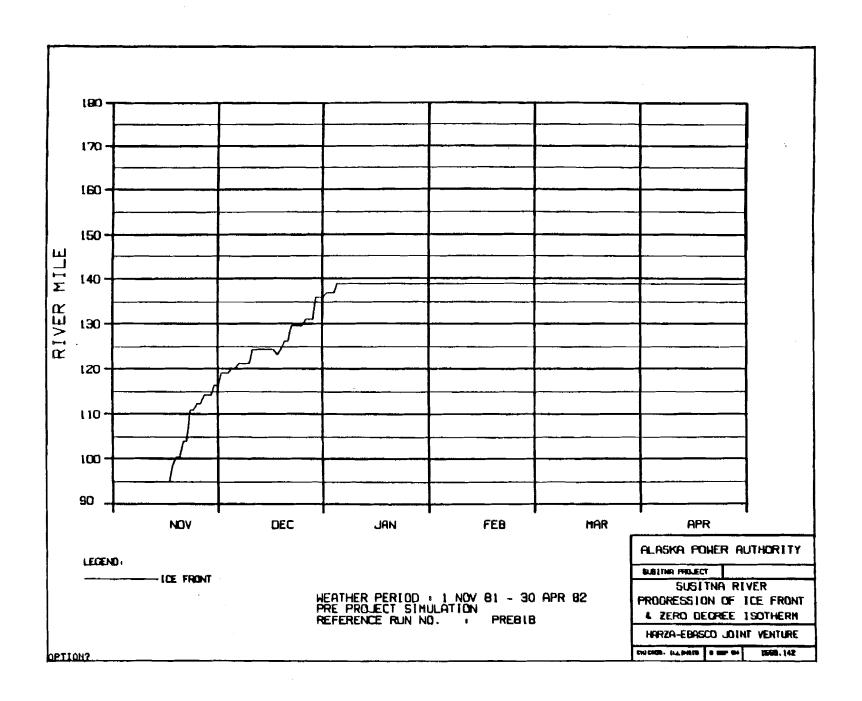


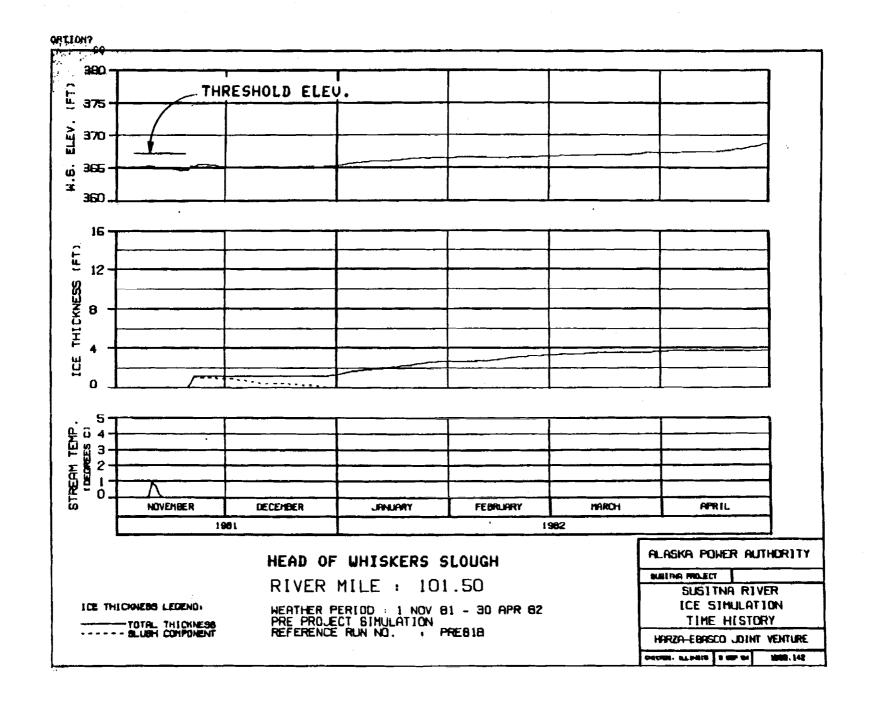


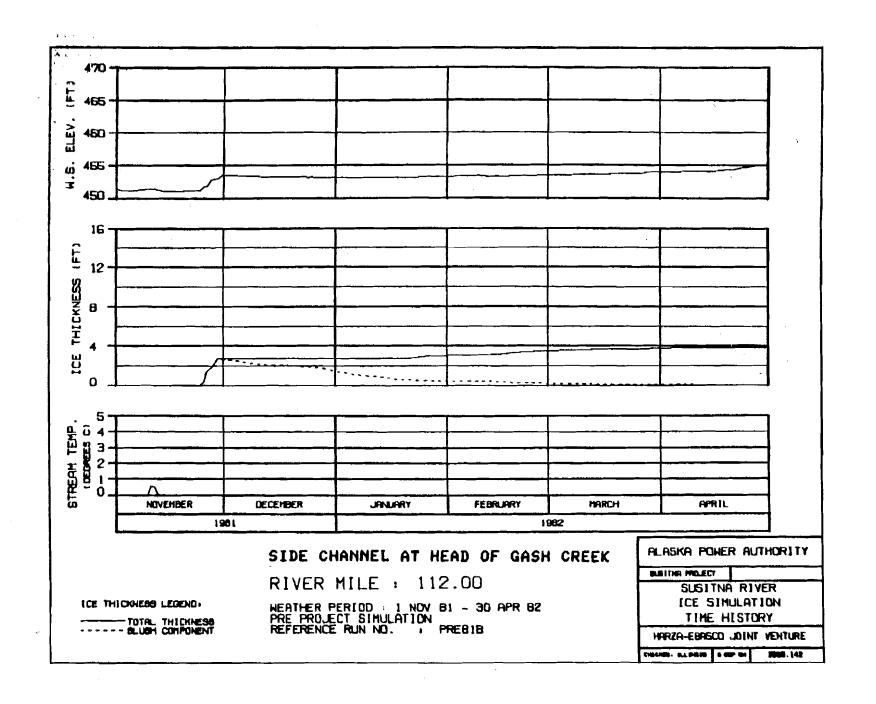




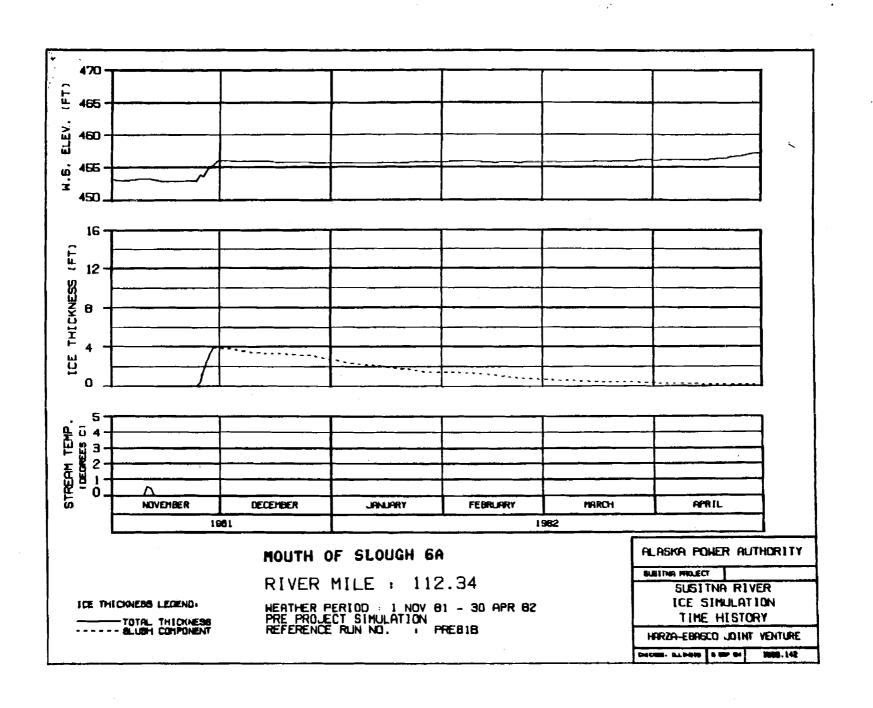


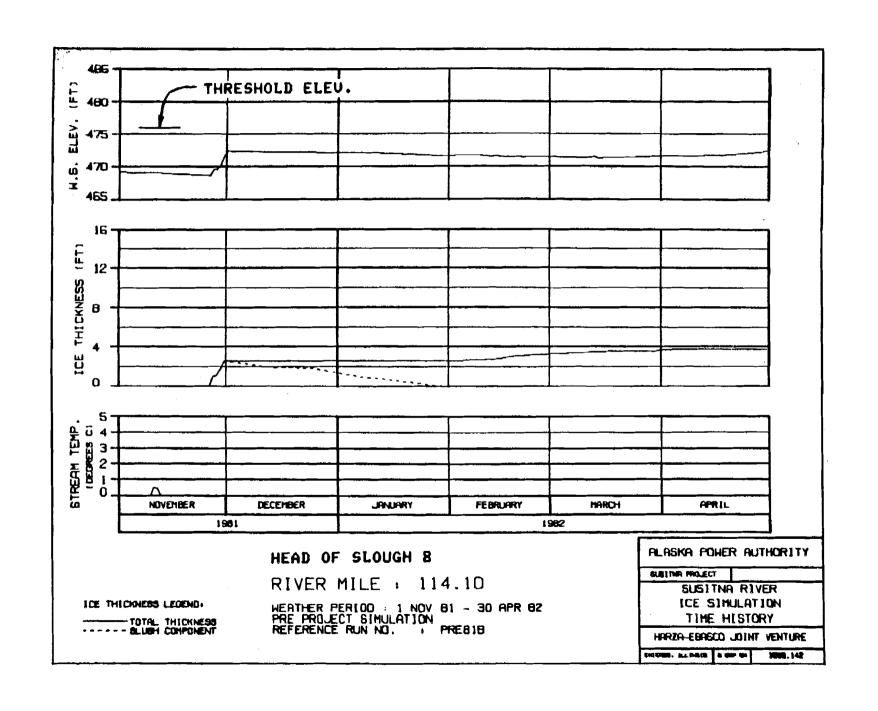


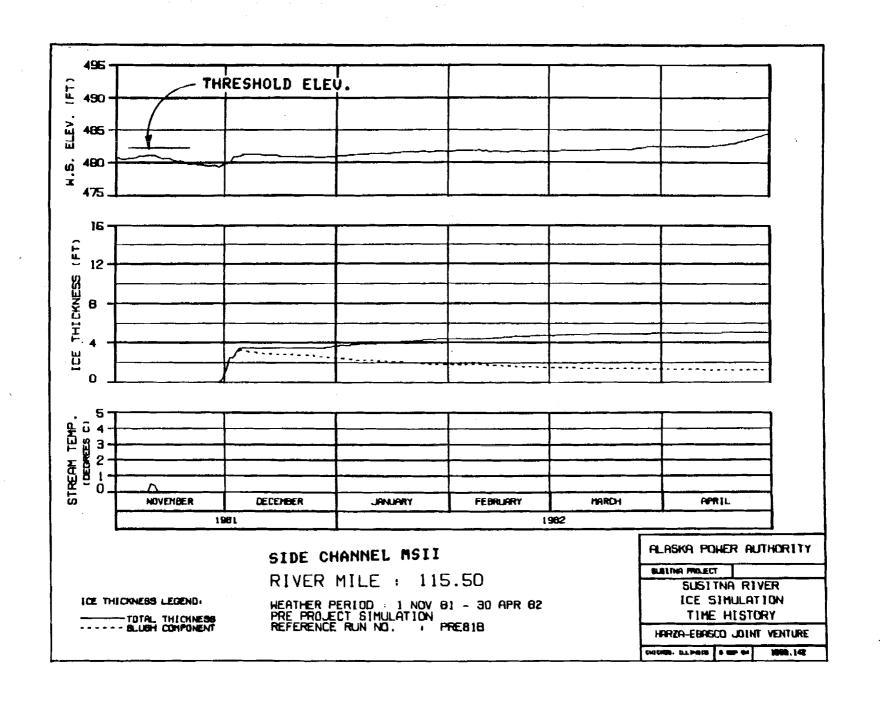


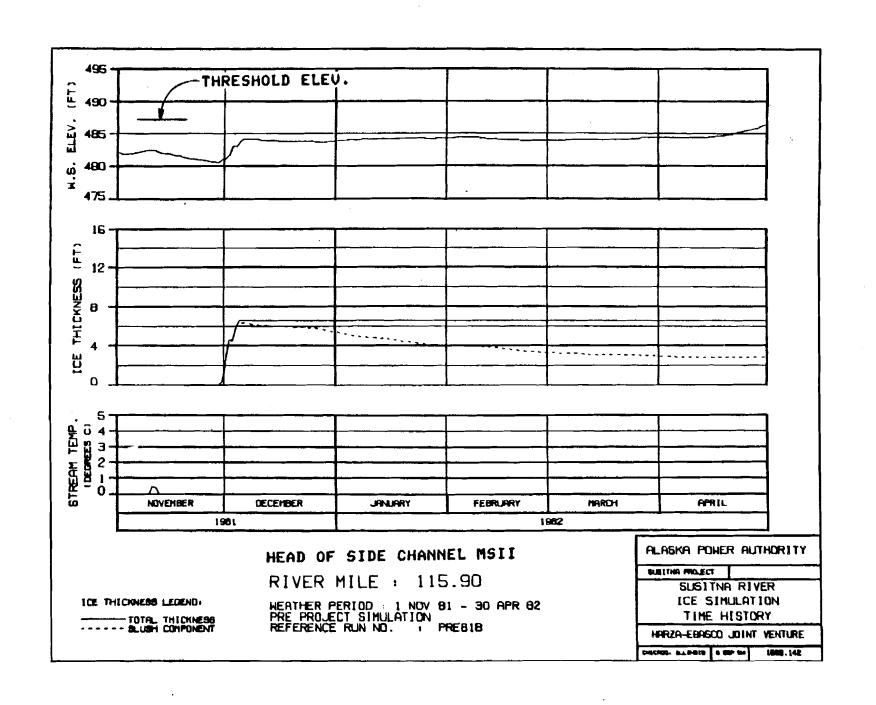


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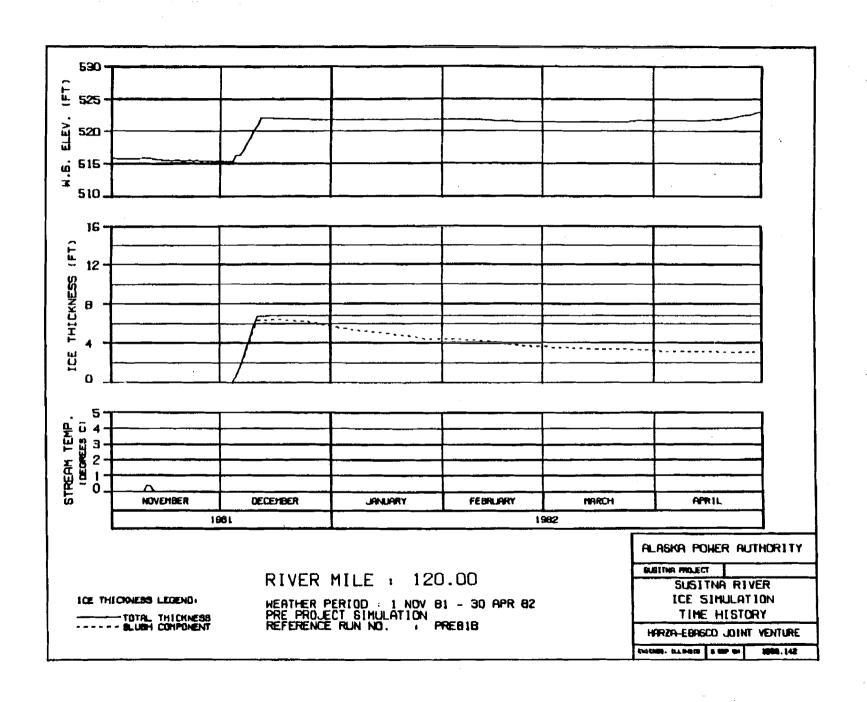


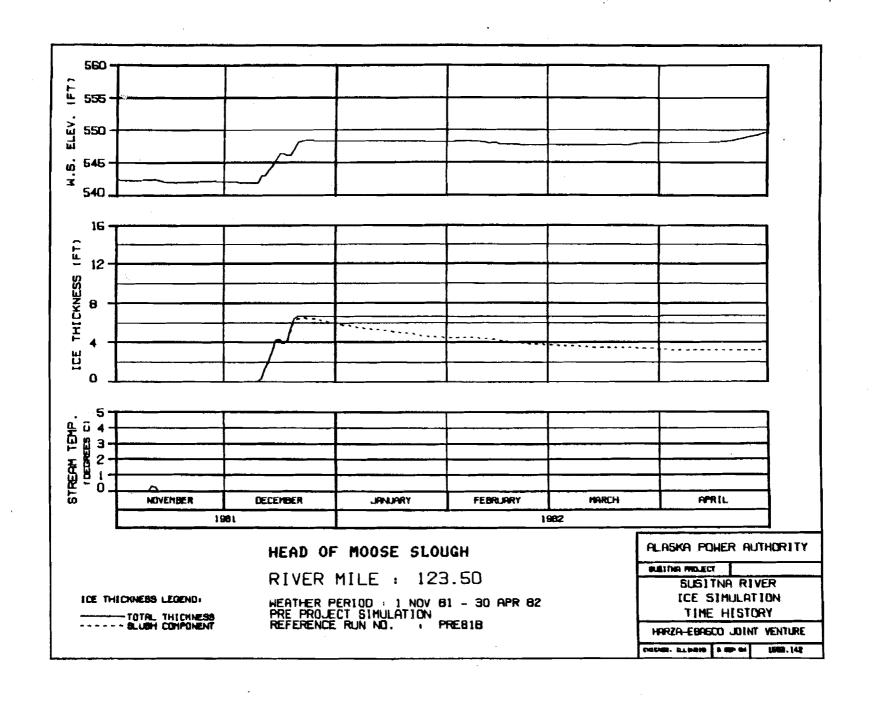


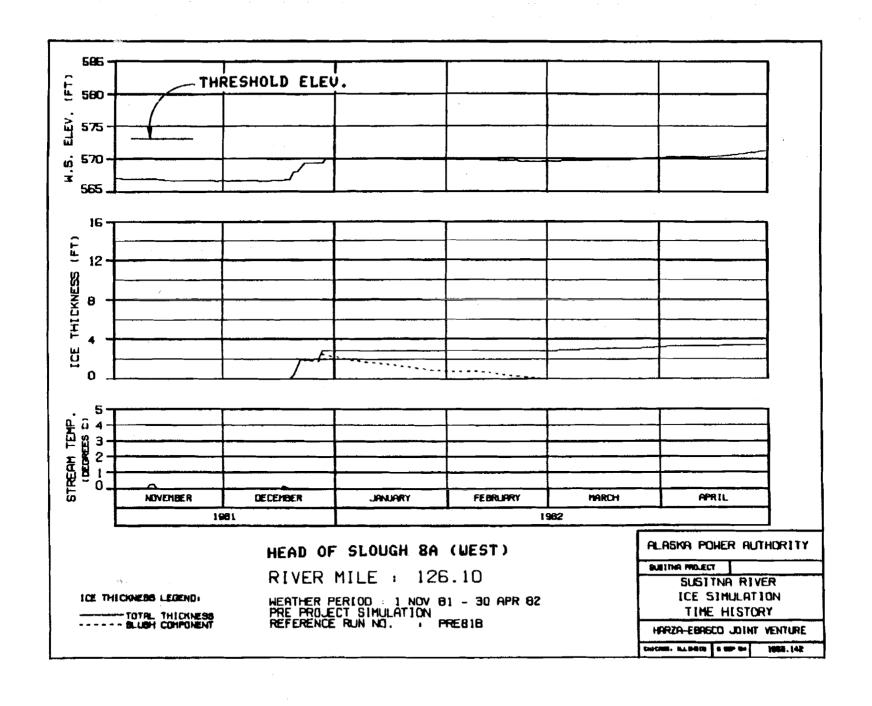


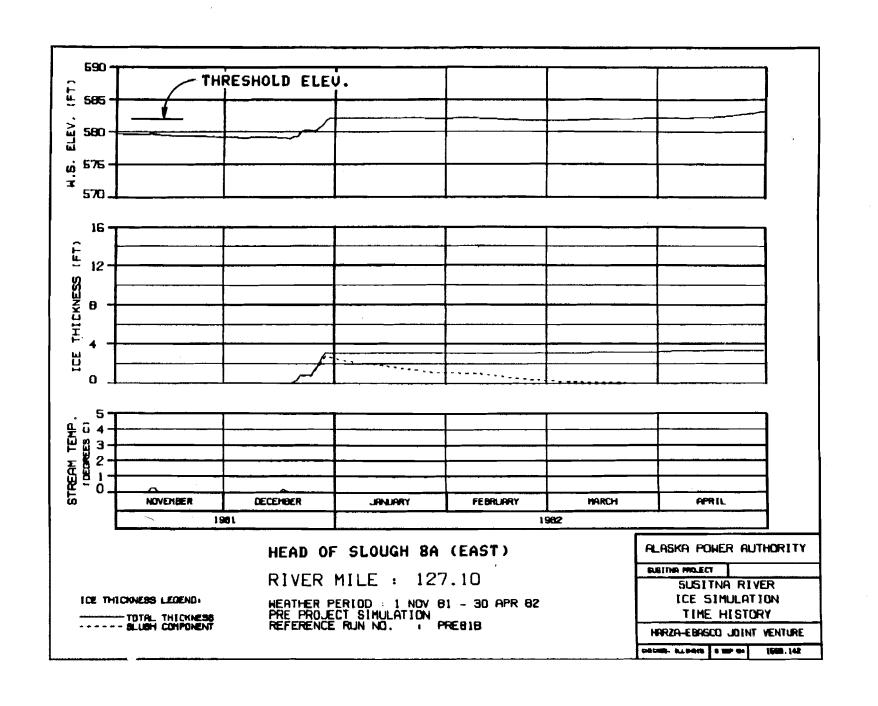


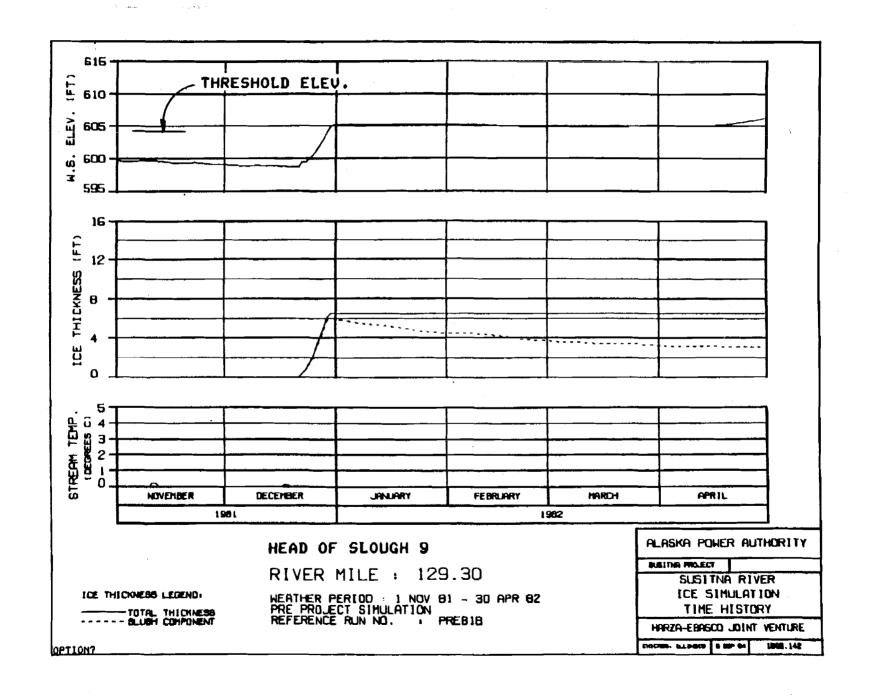
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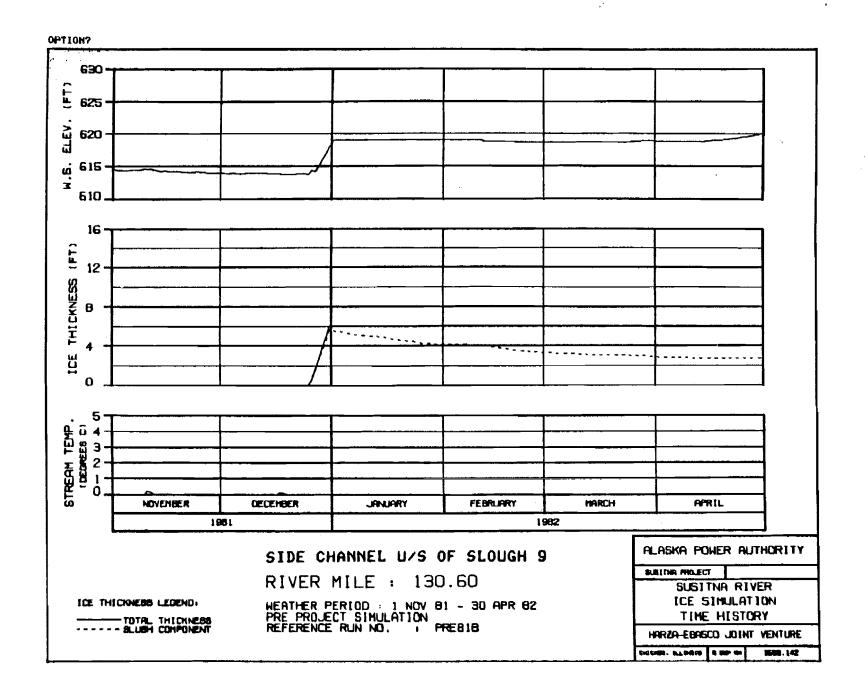


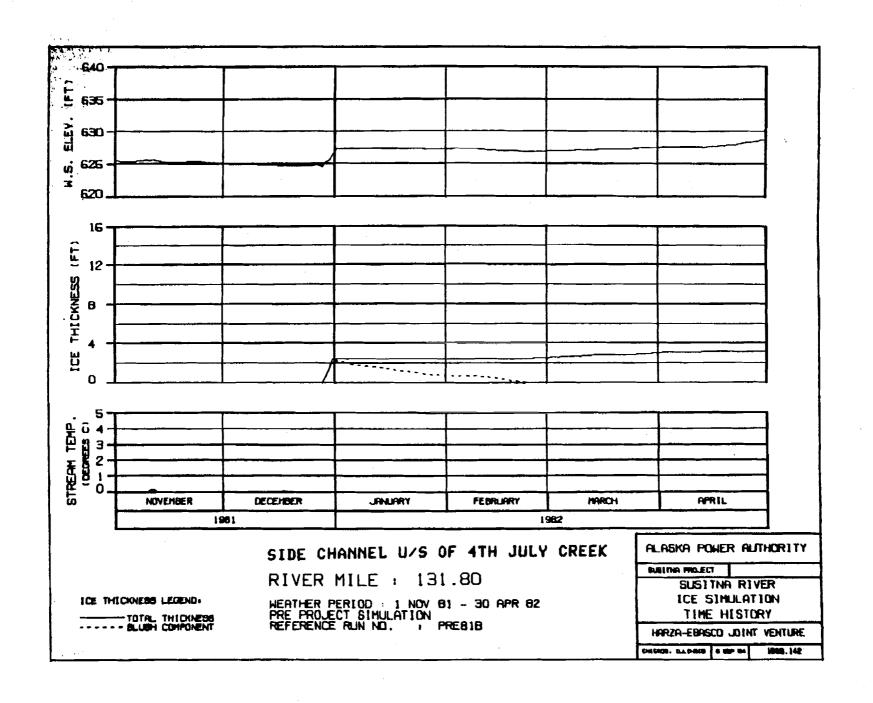


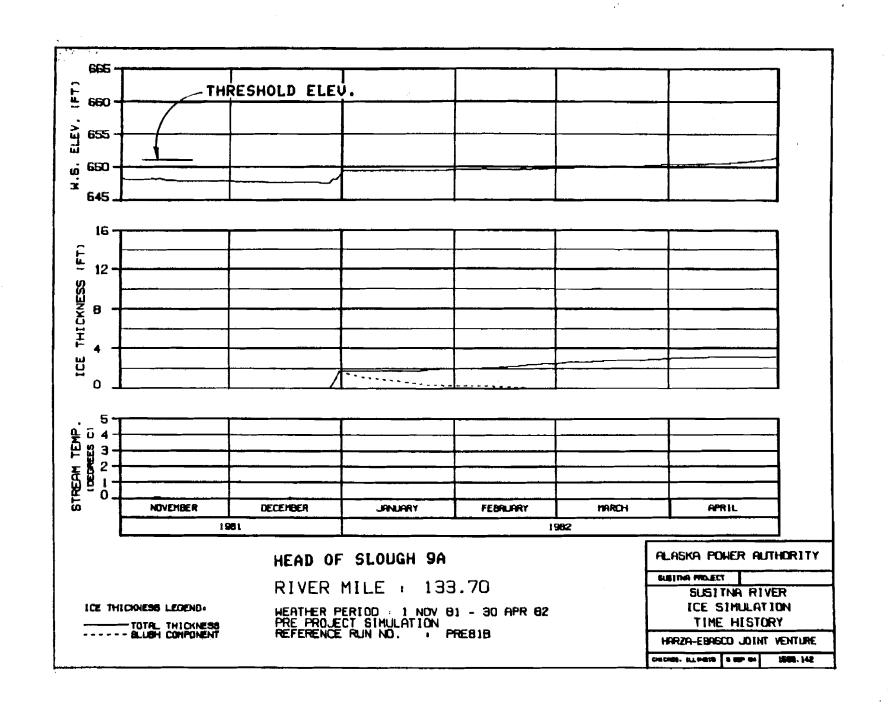


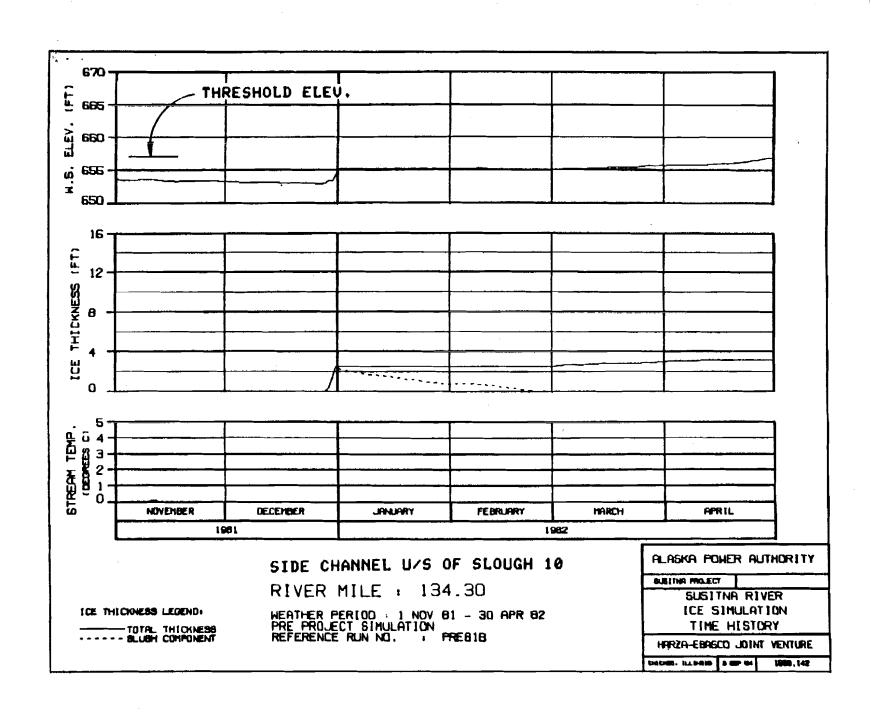


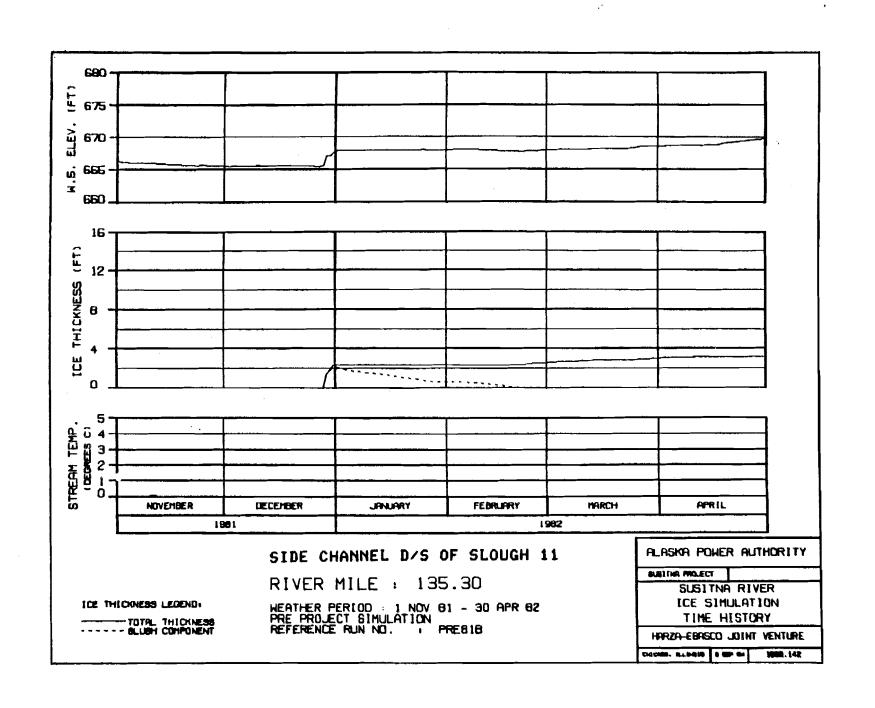












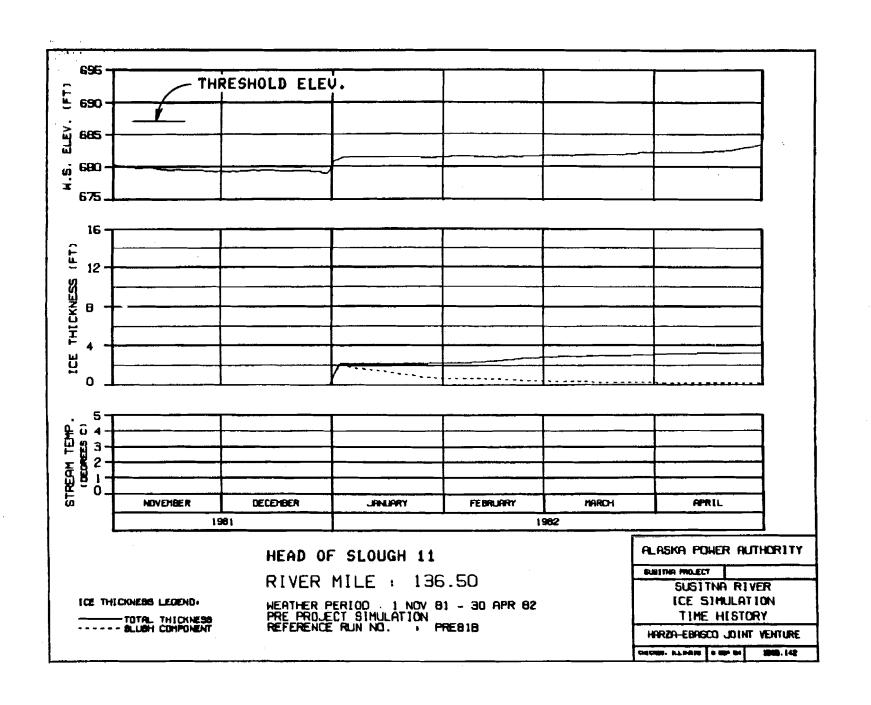
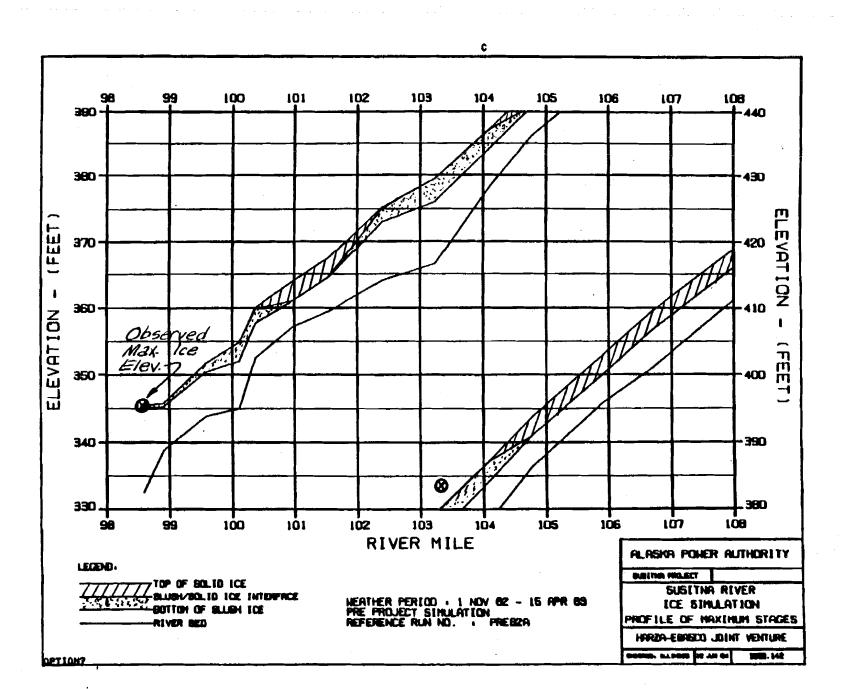
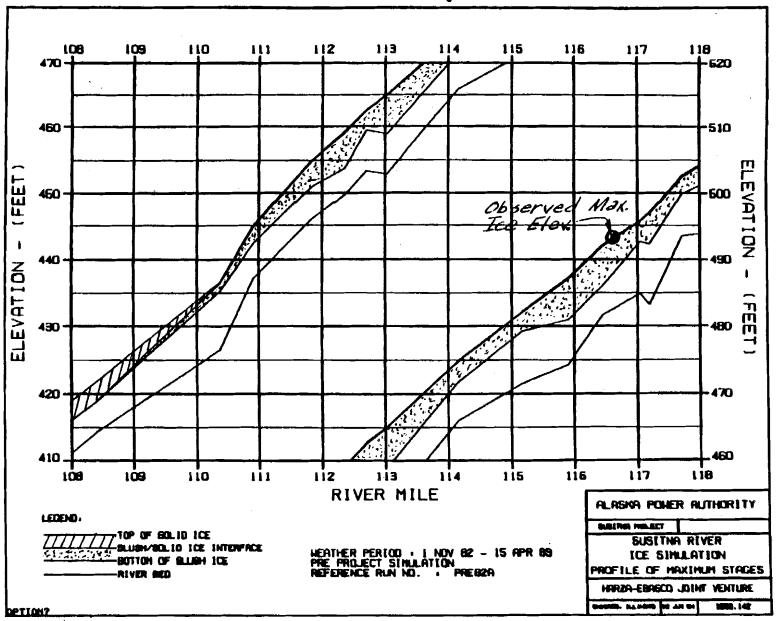


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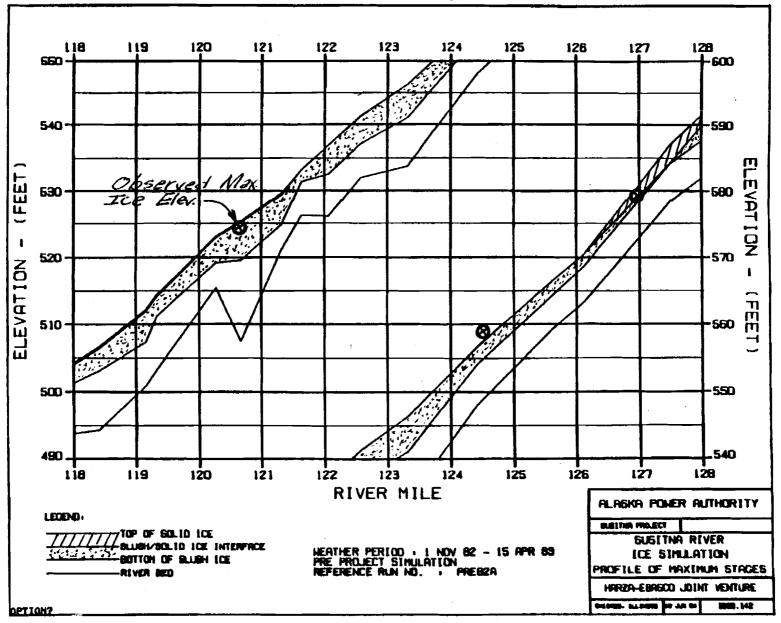




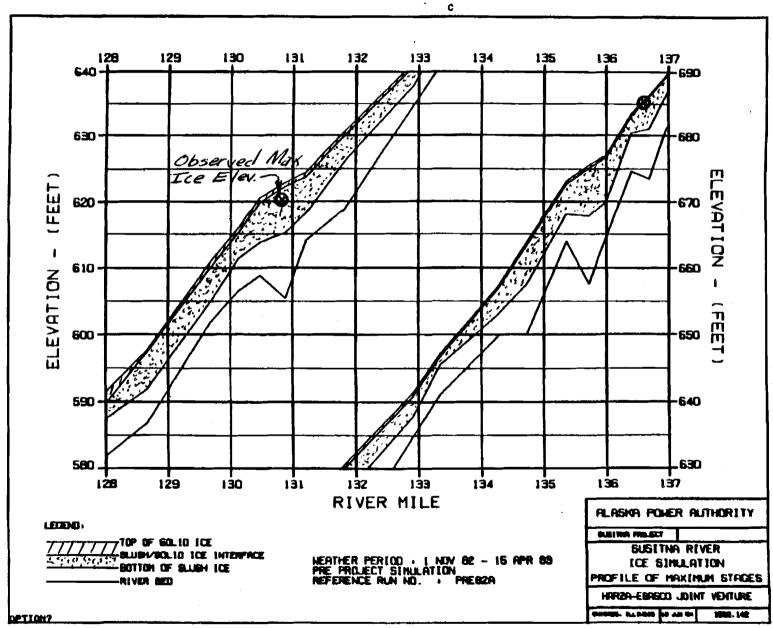


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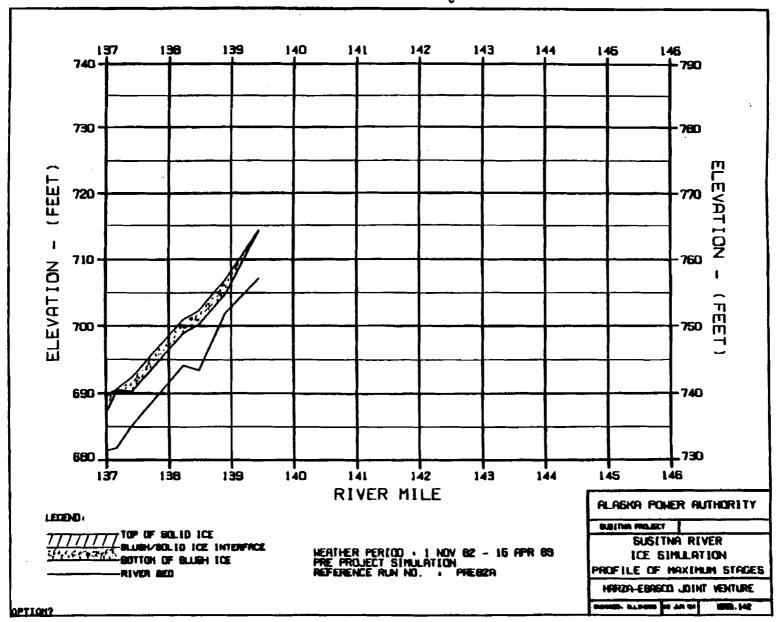




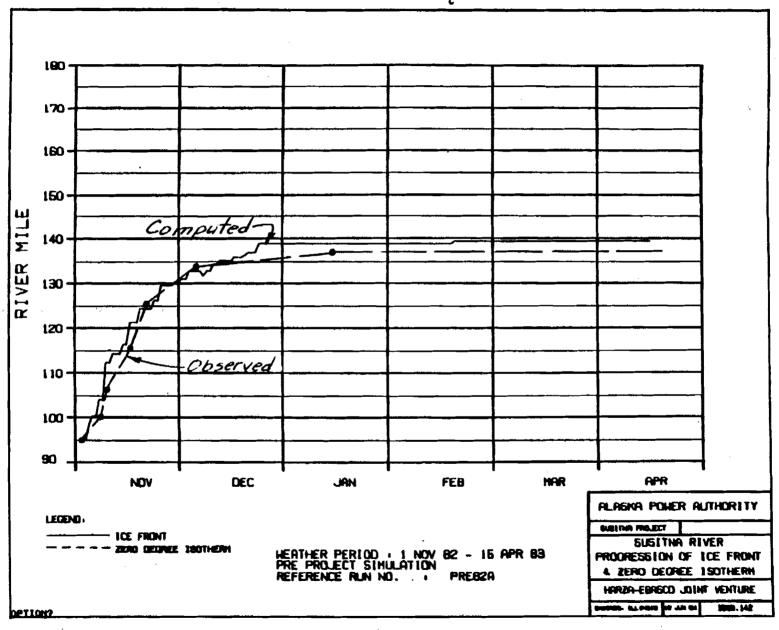


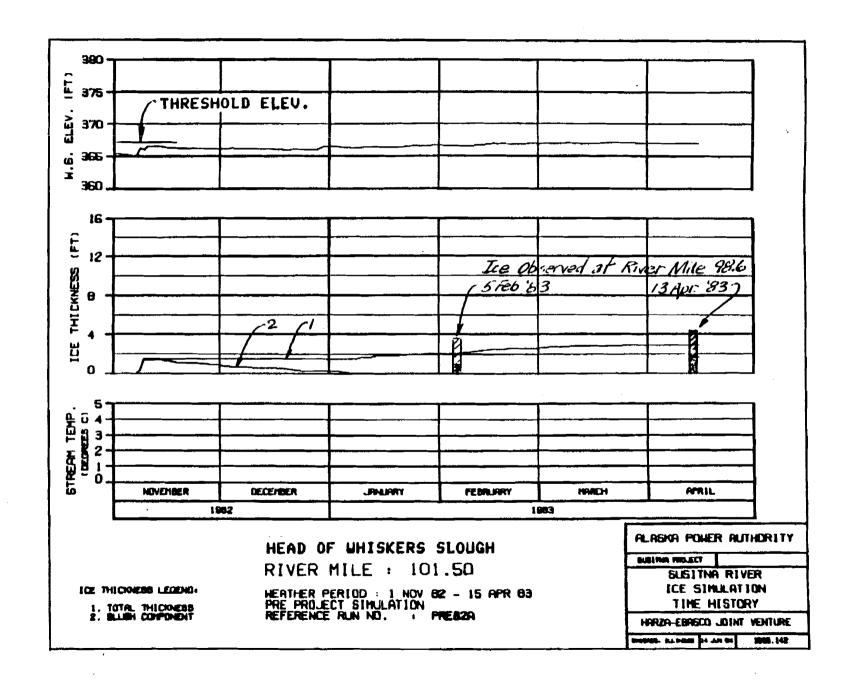
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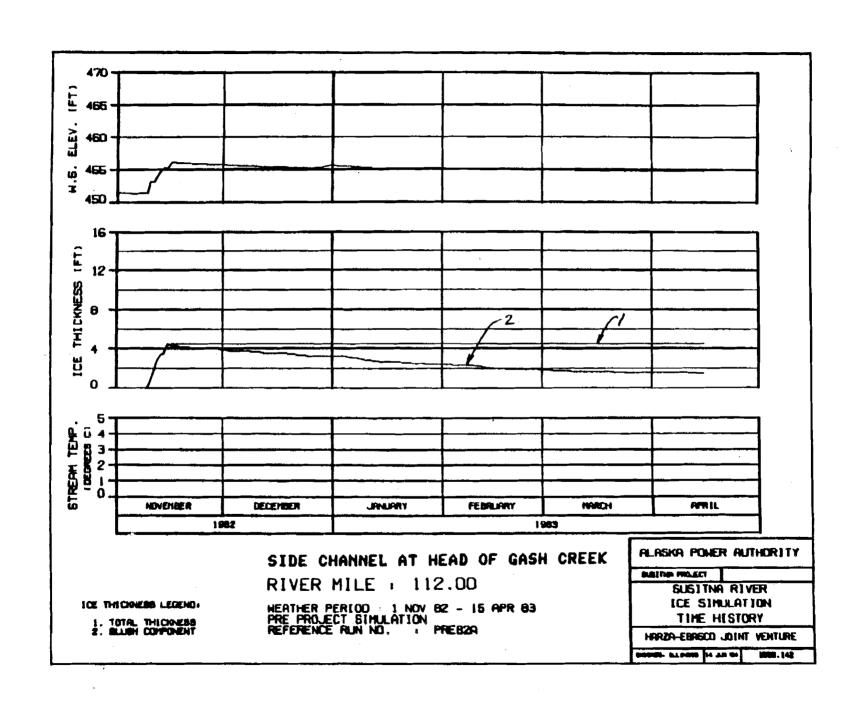


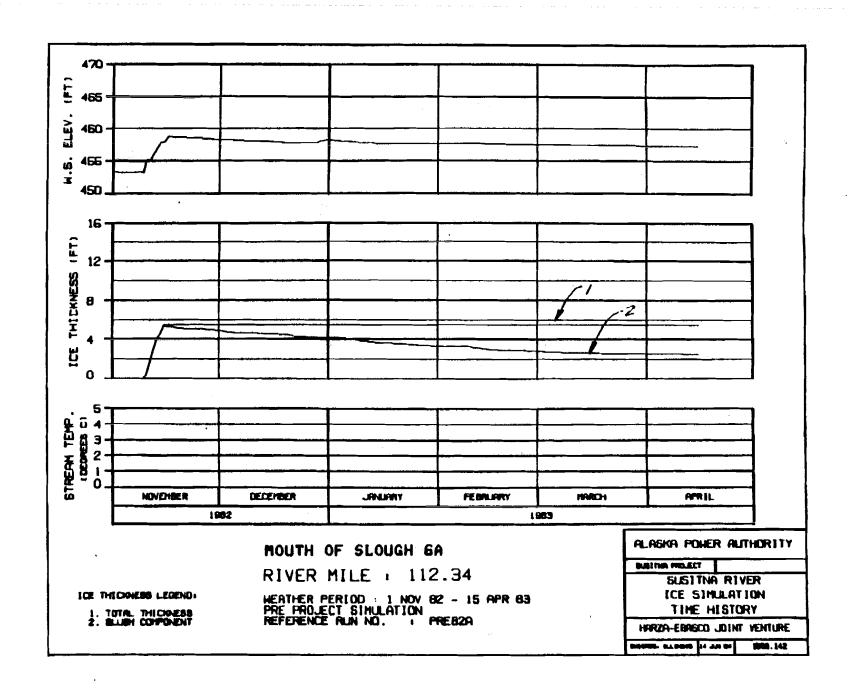


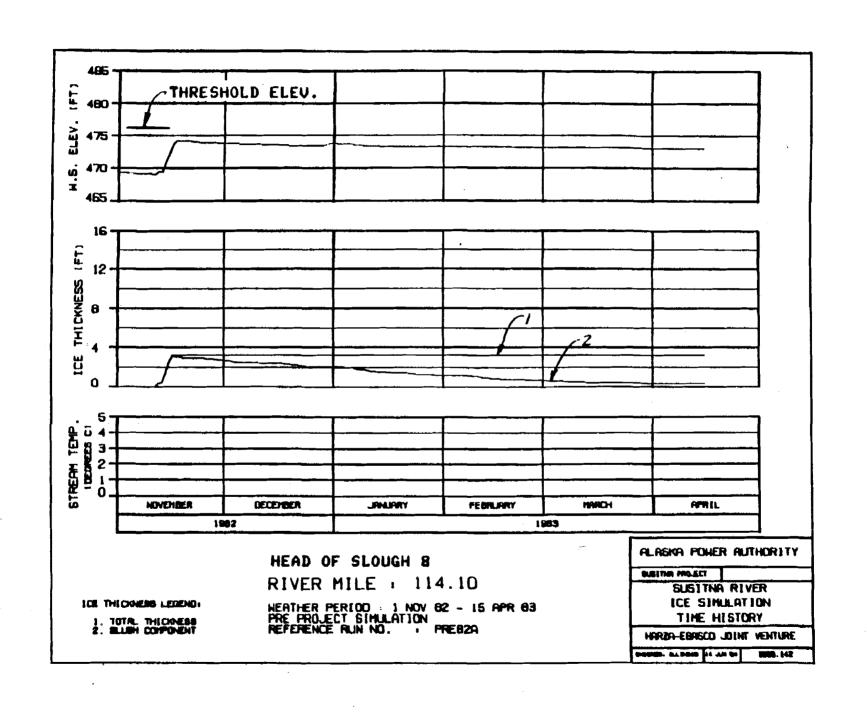


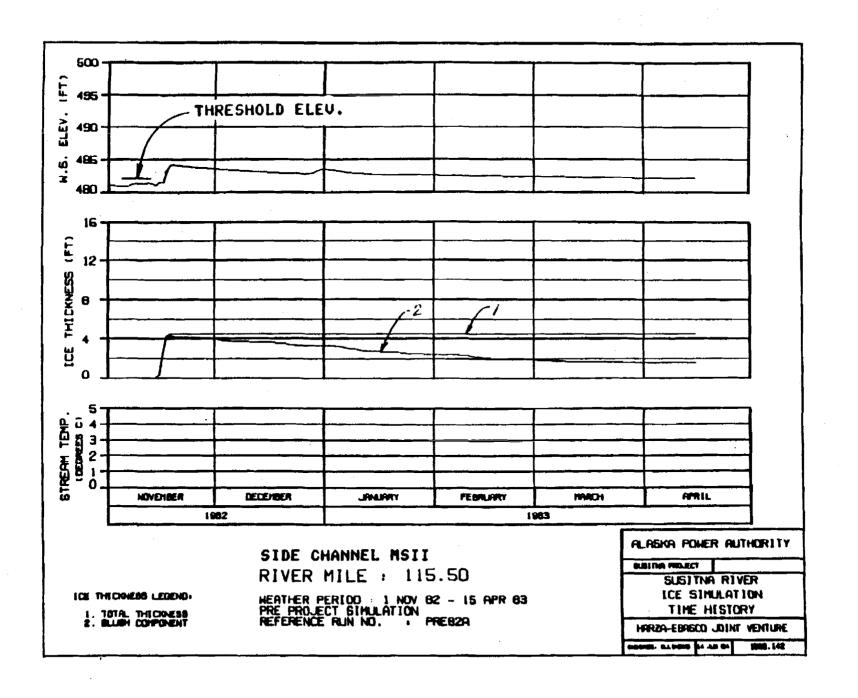


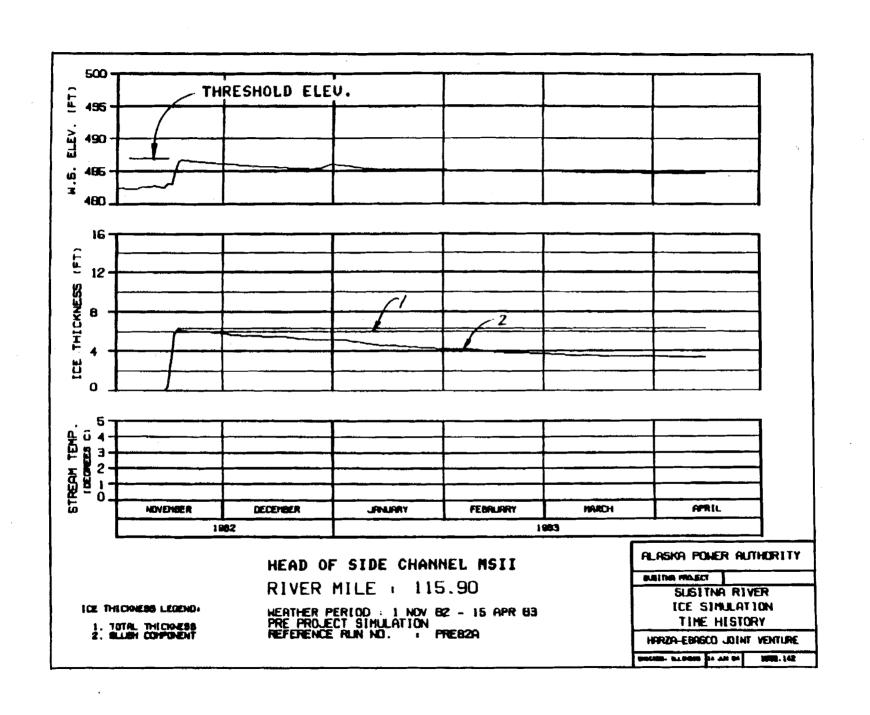


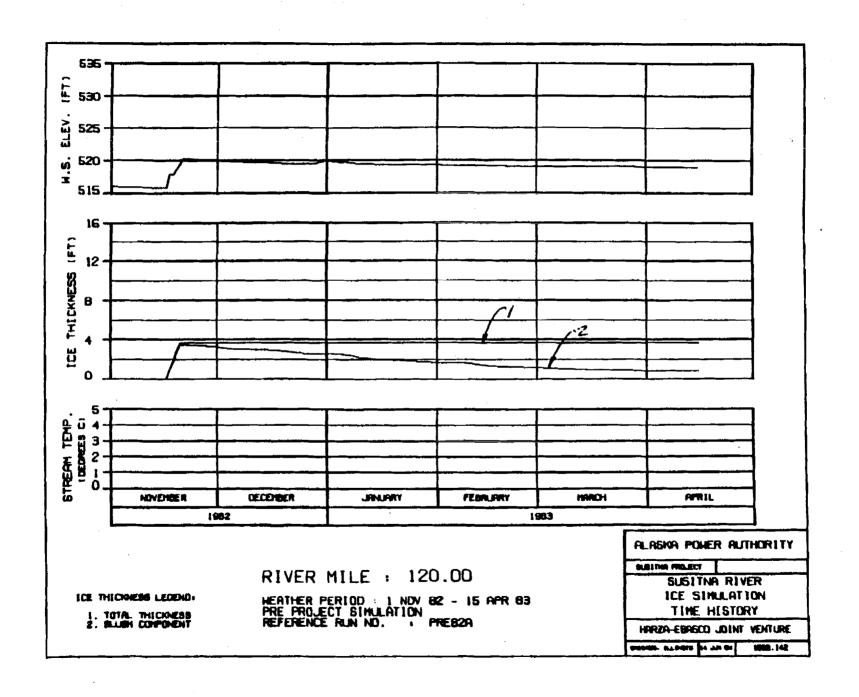


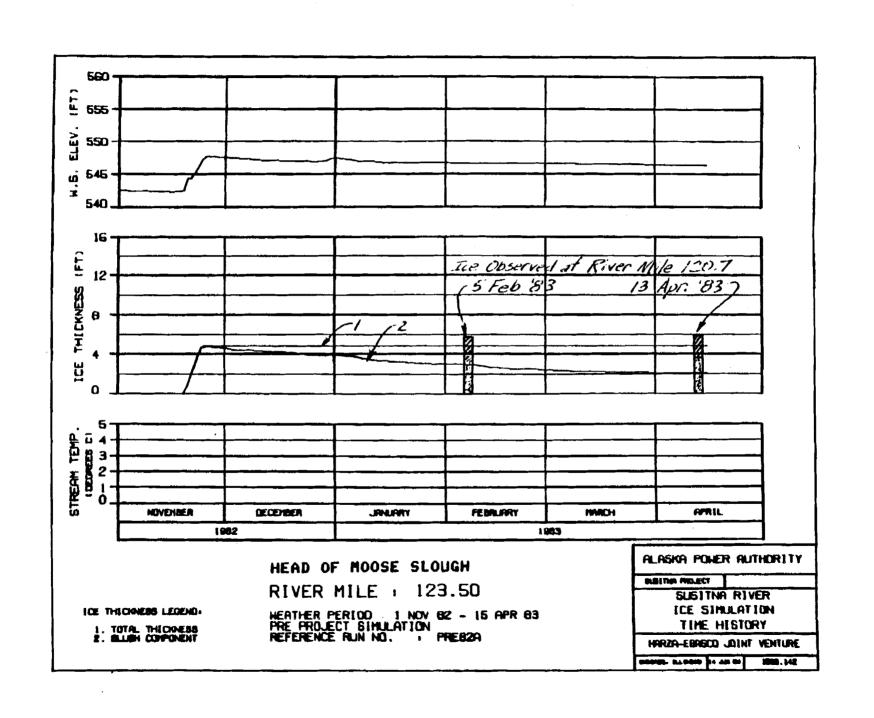


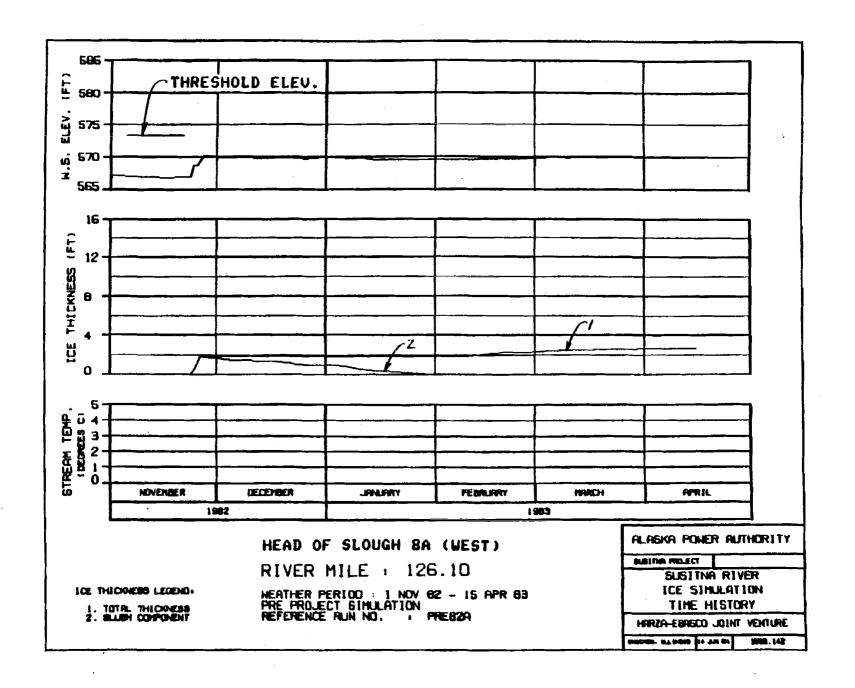


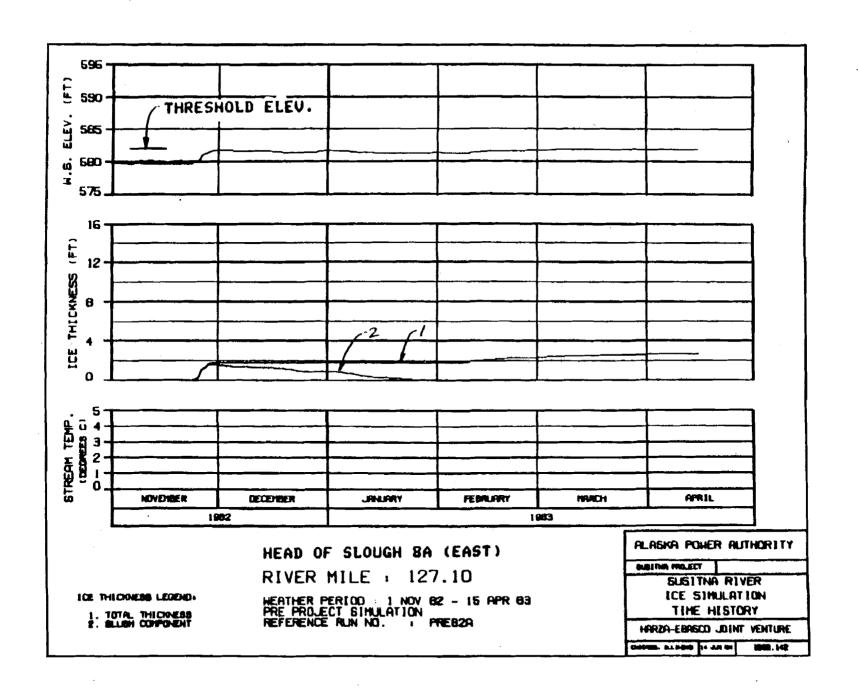


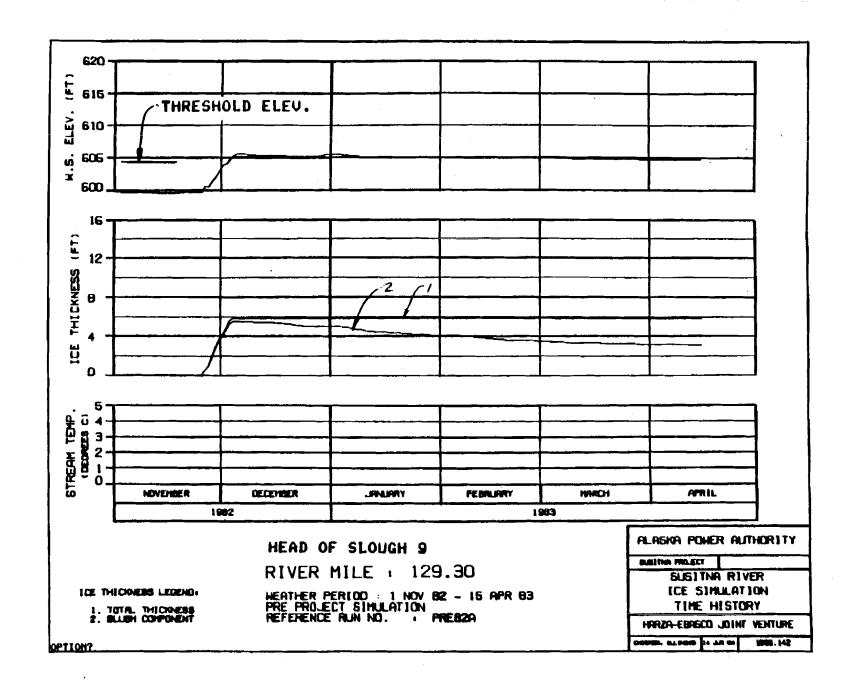


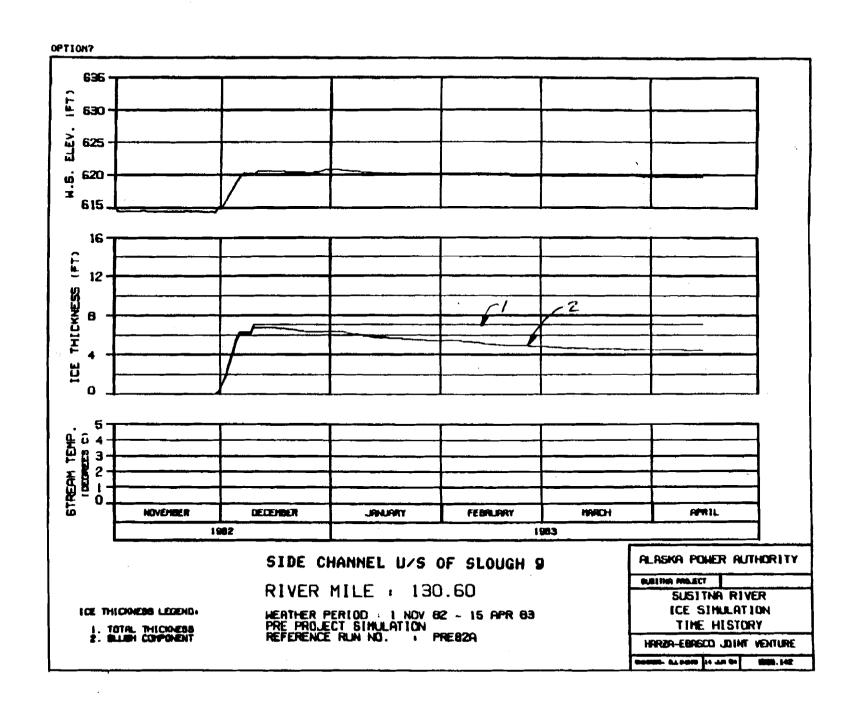


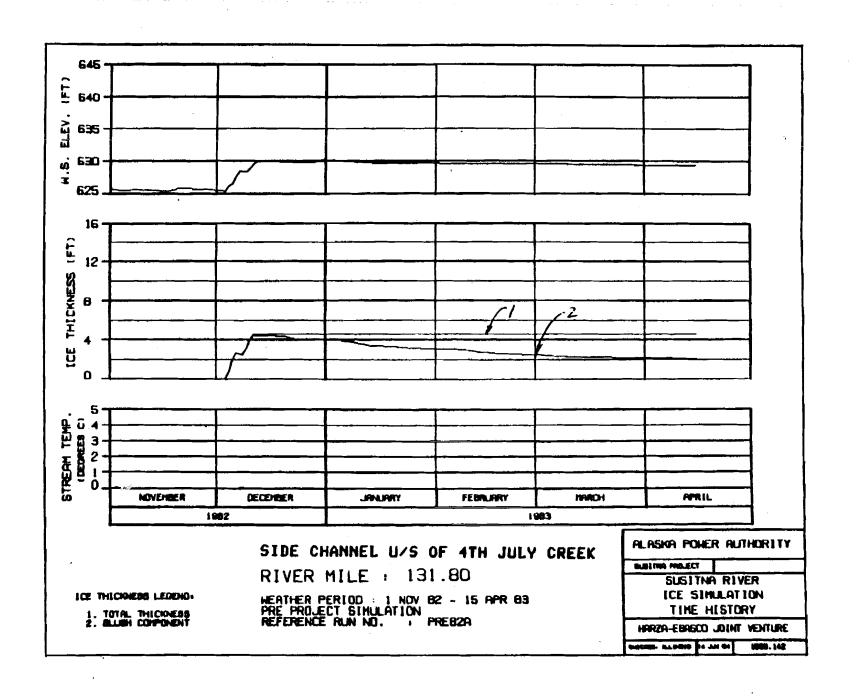


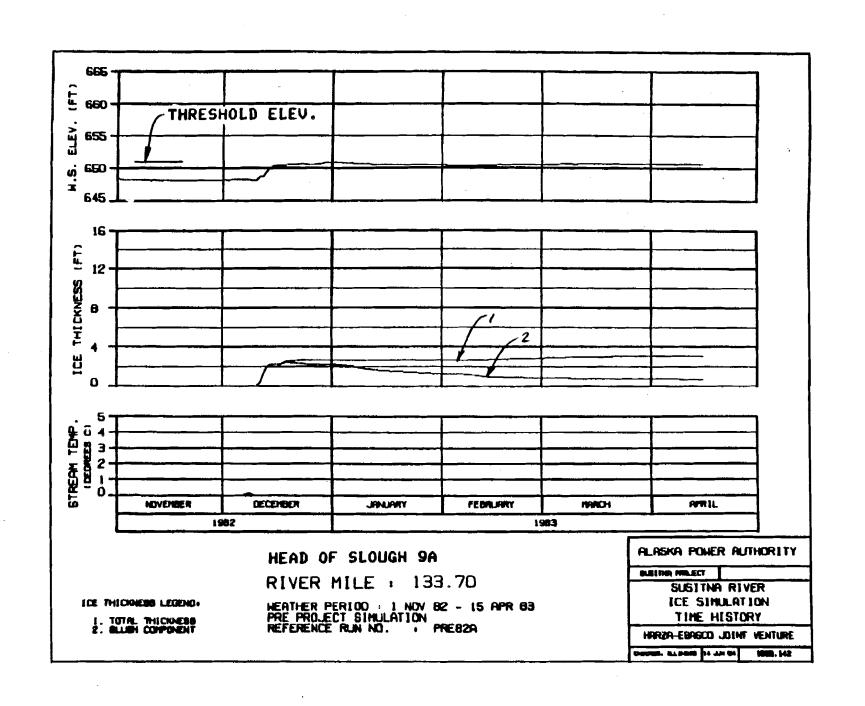


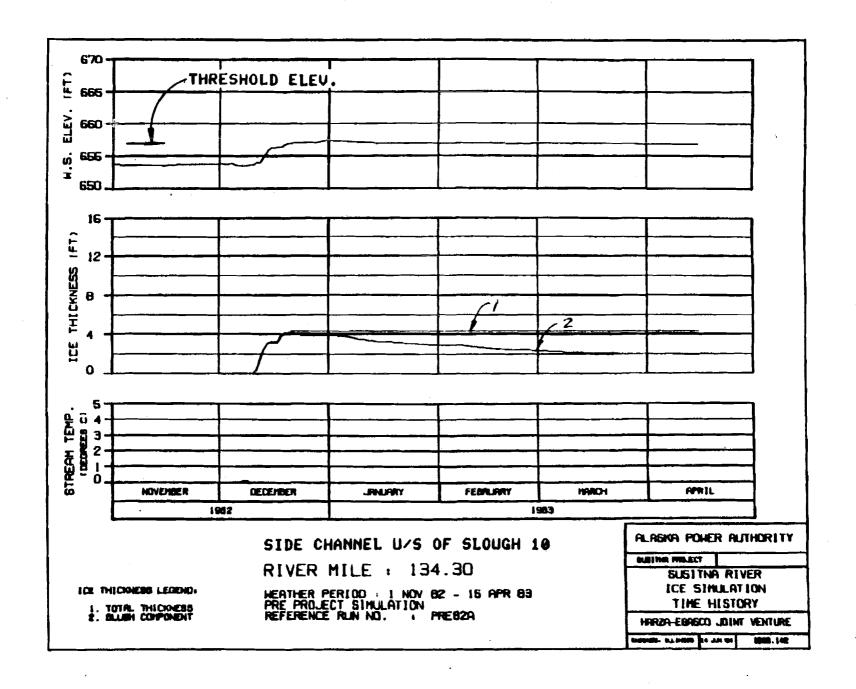


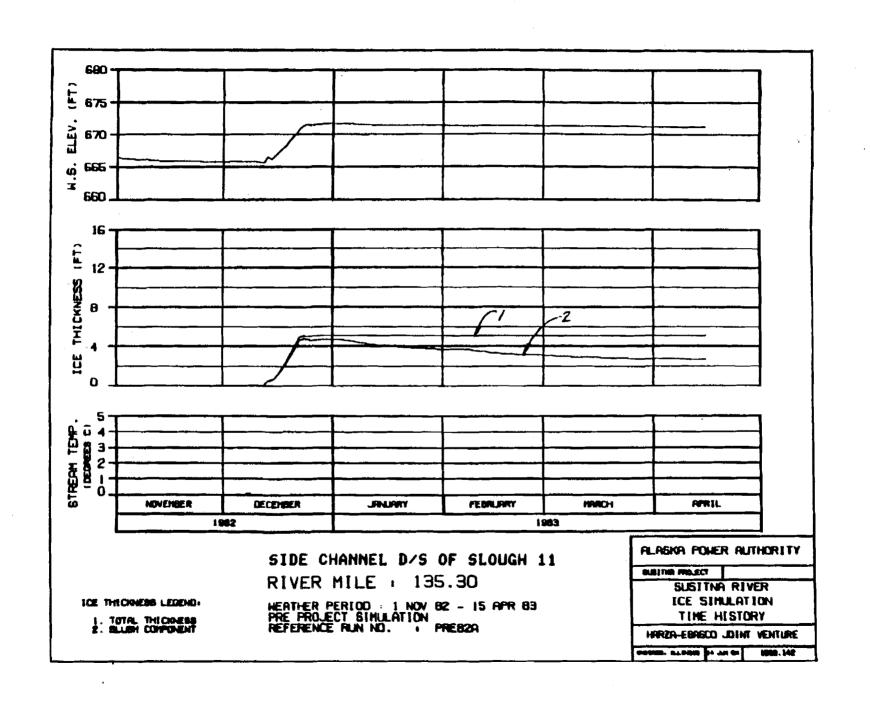












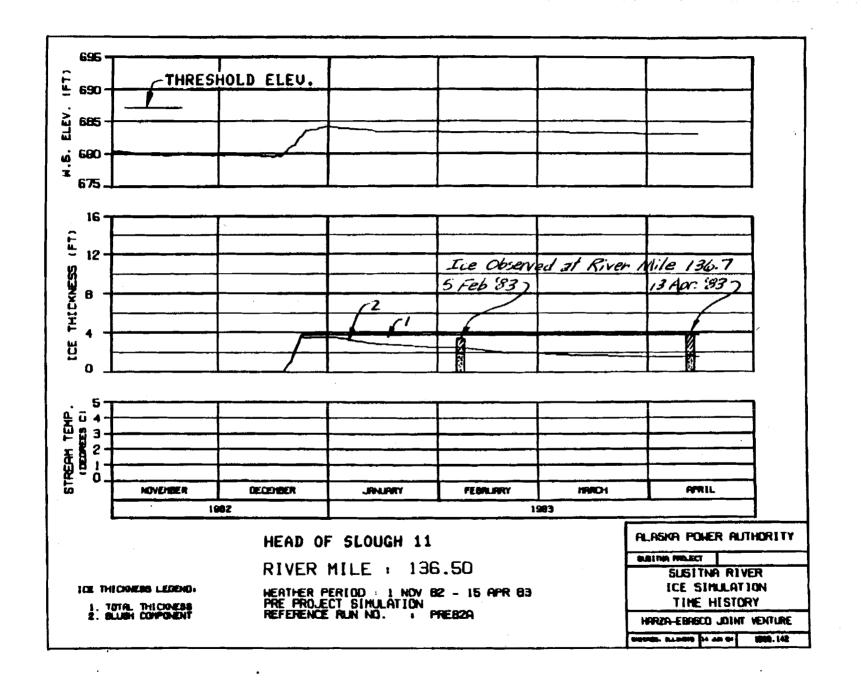
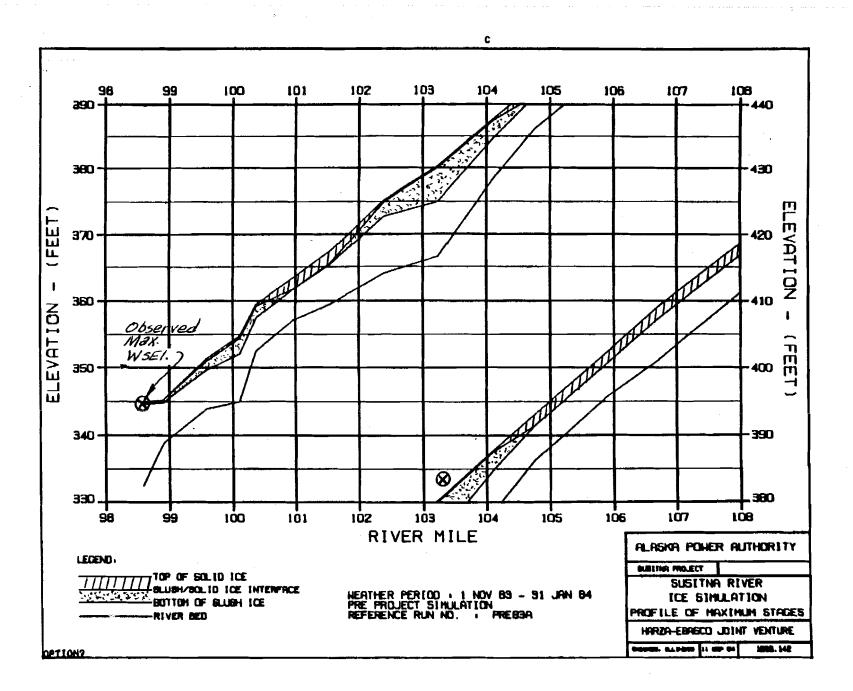
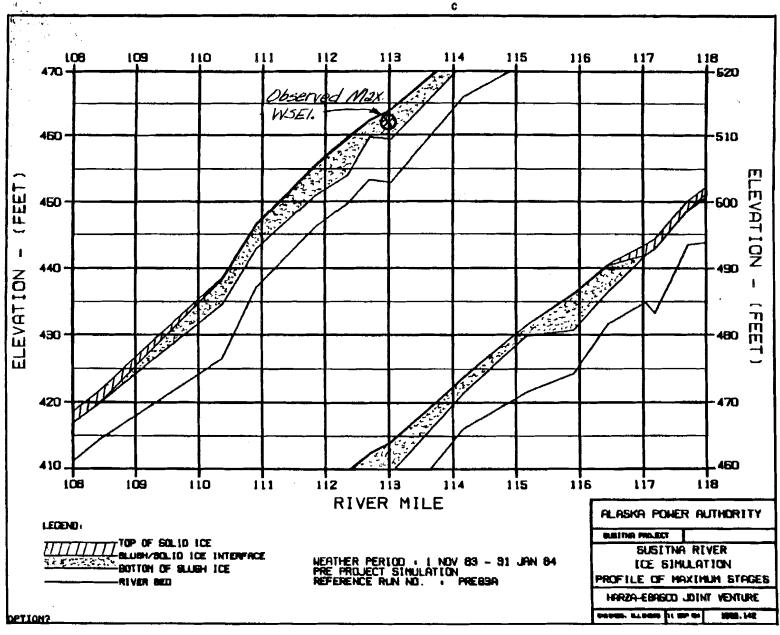
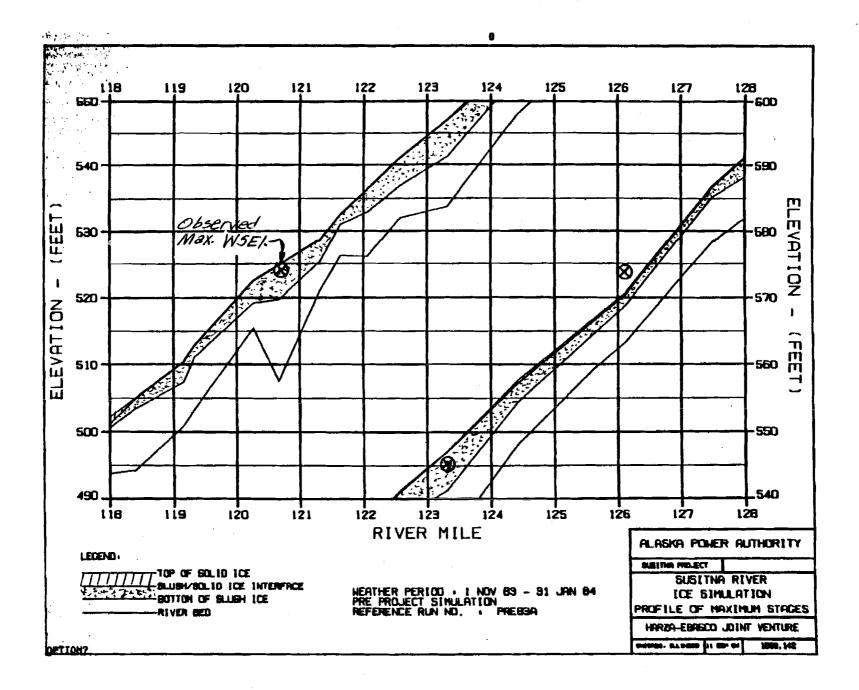


EXHIBIT E

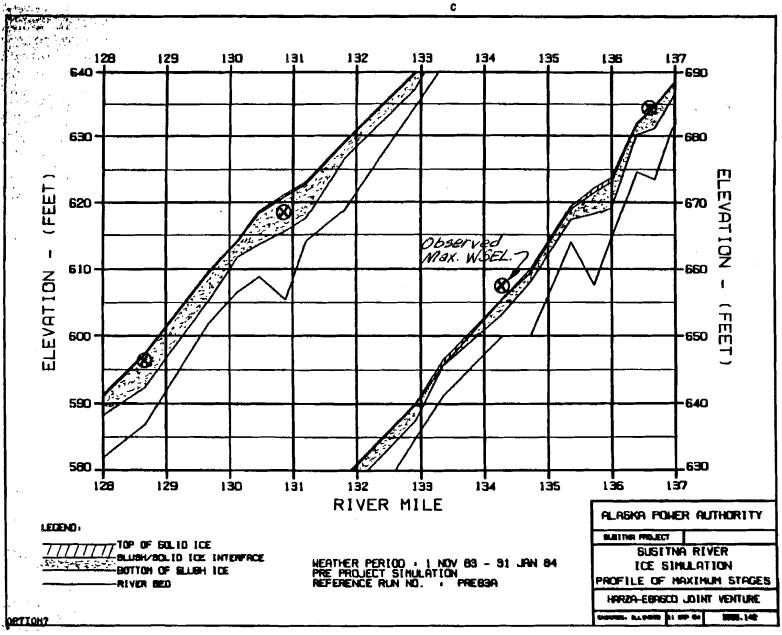




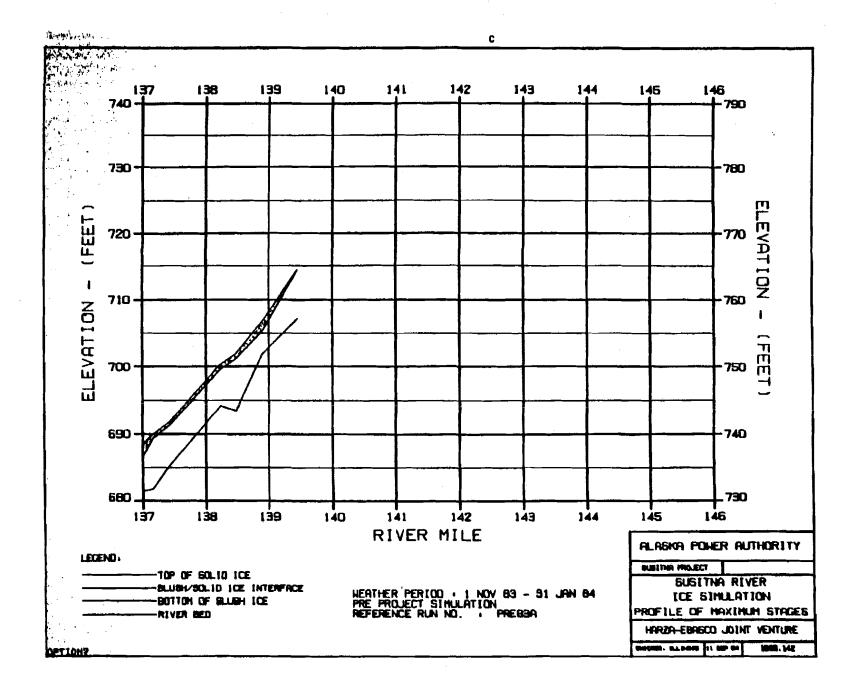


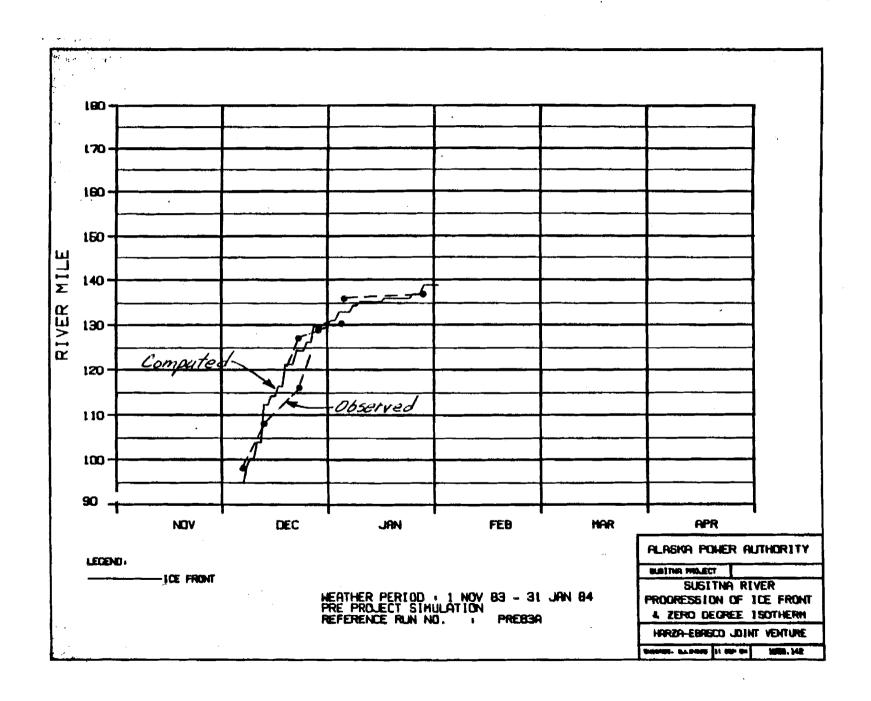


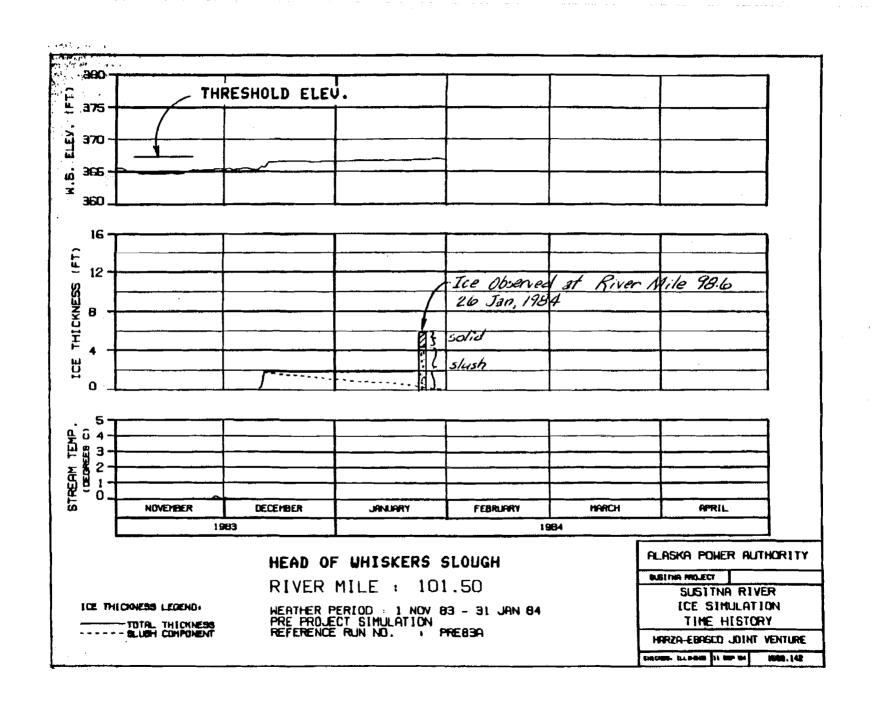


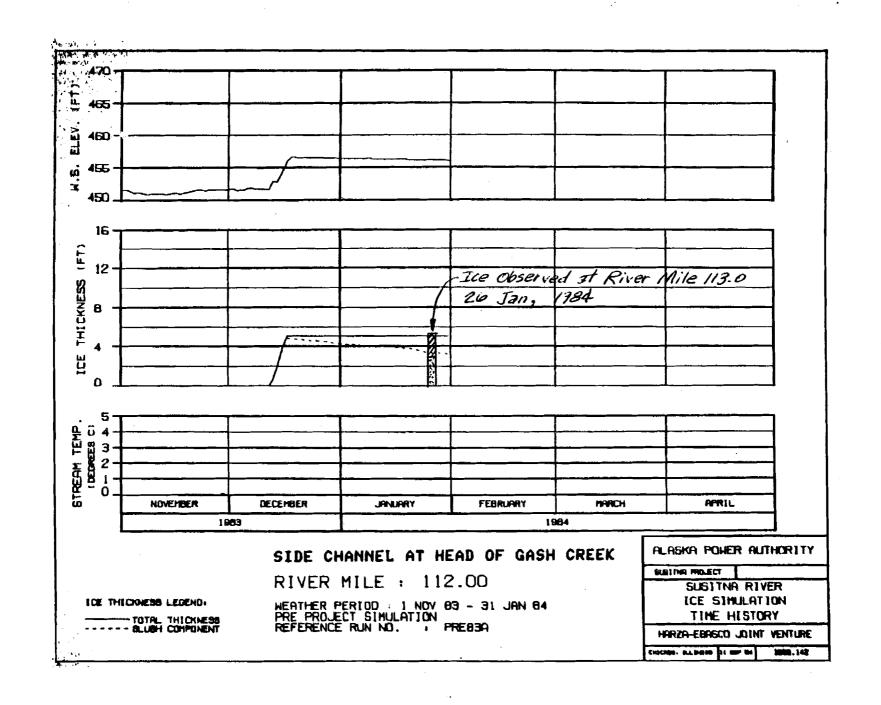


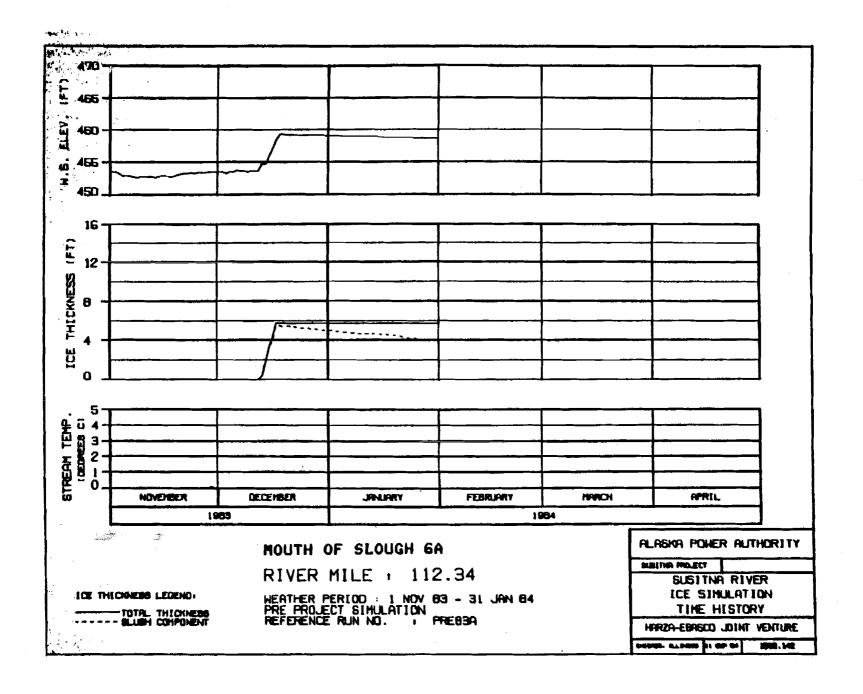
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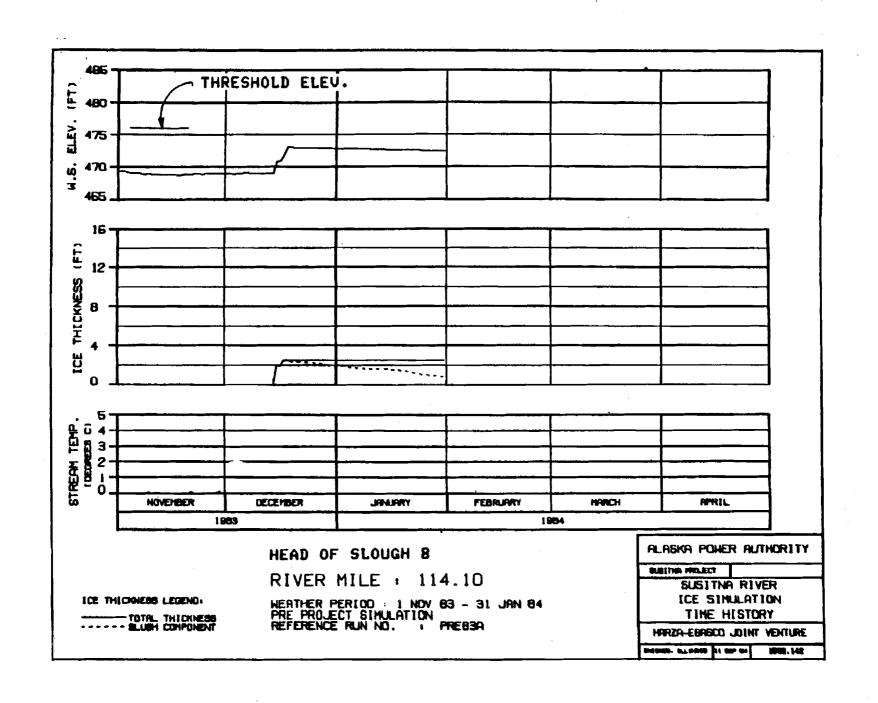


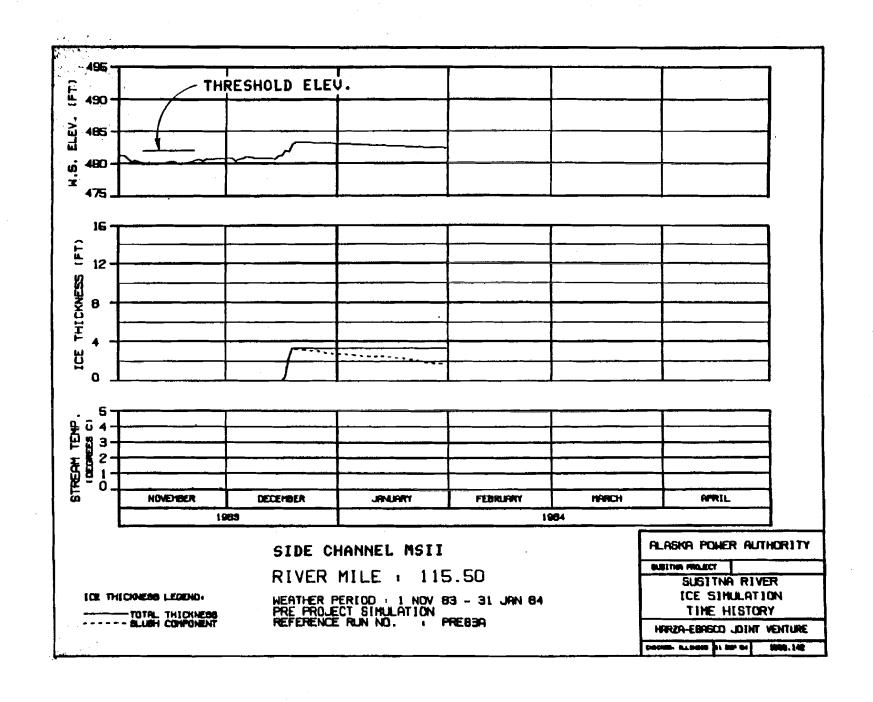


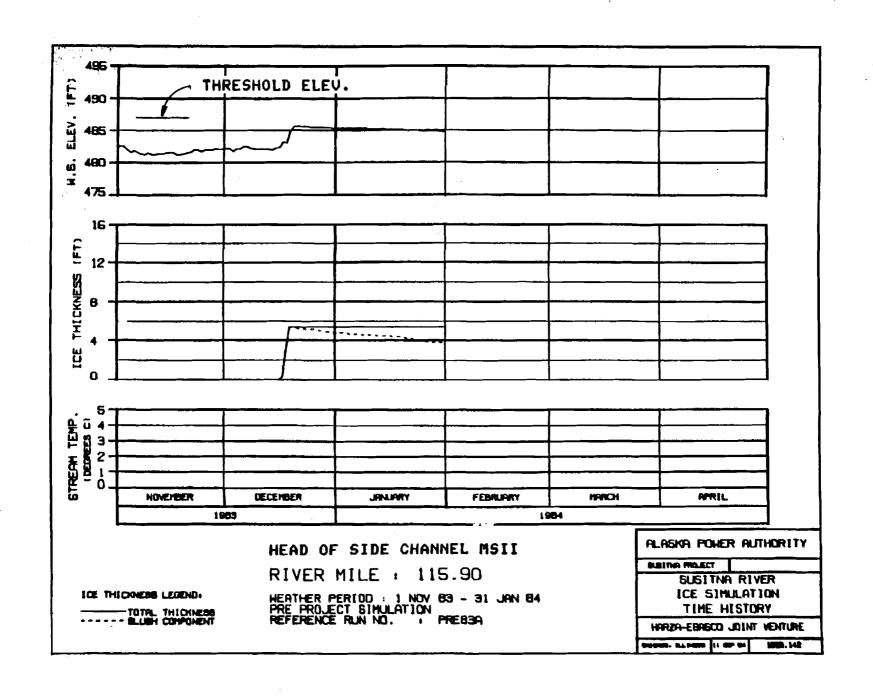


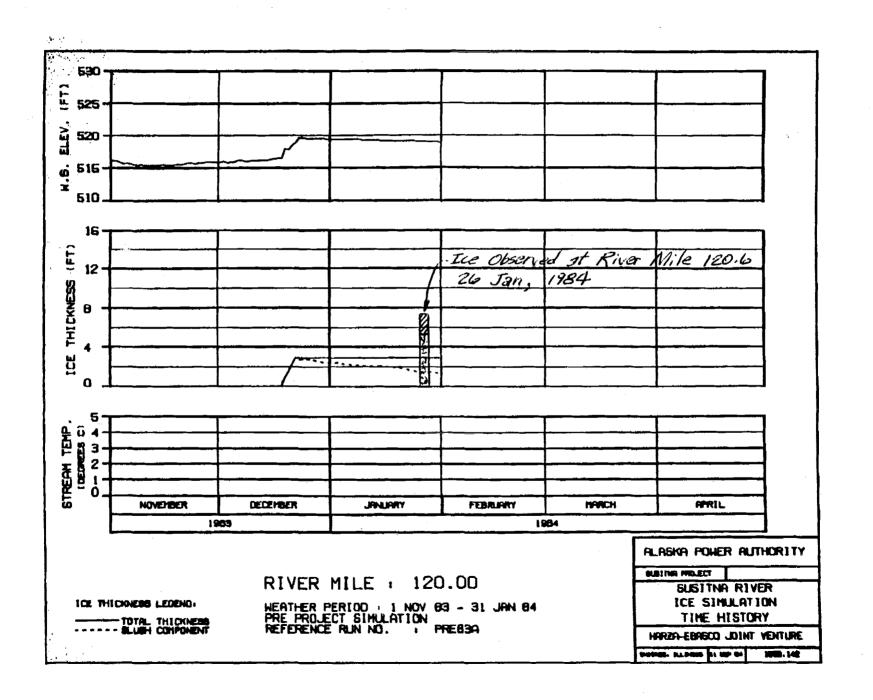


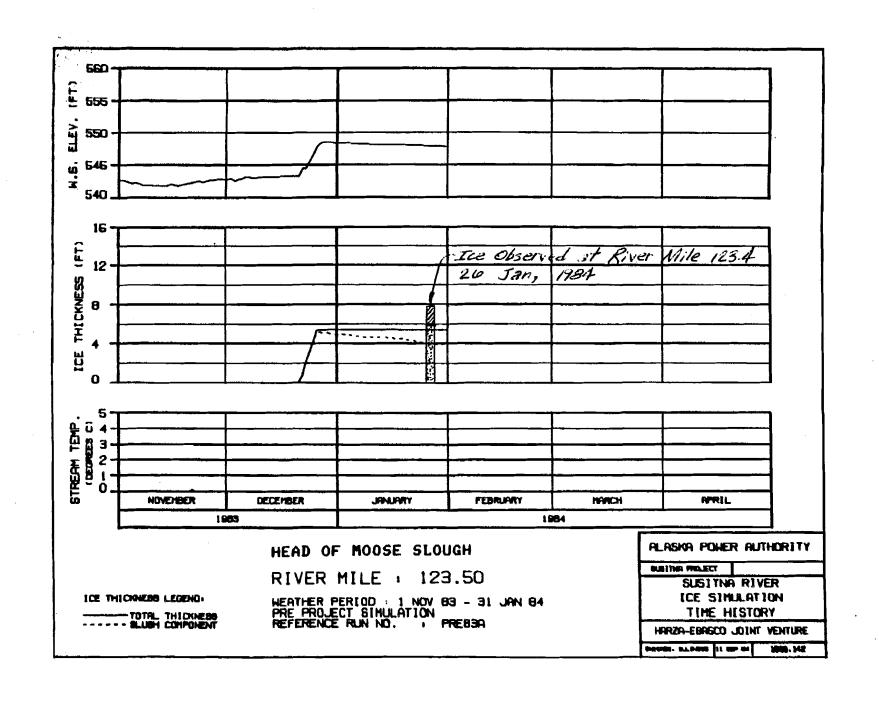




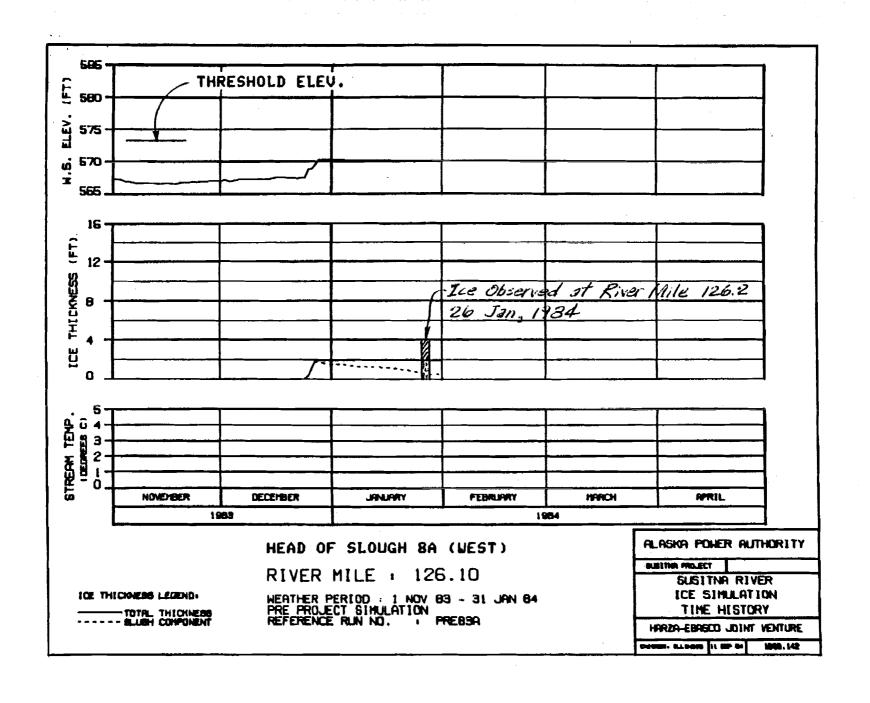


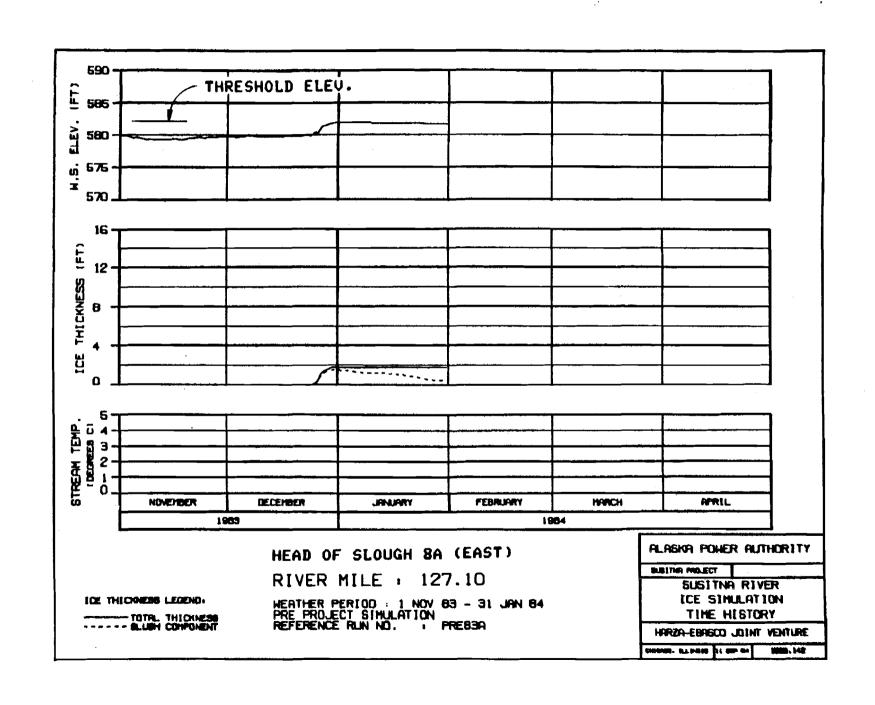




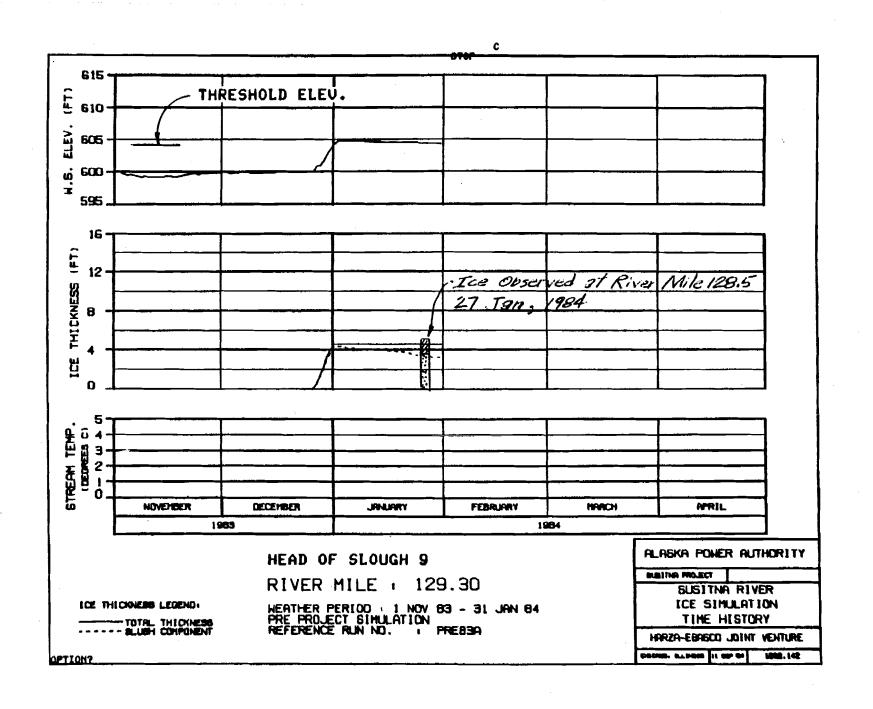


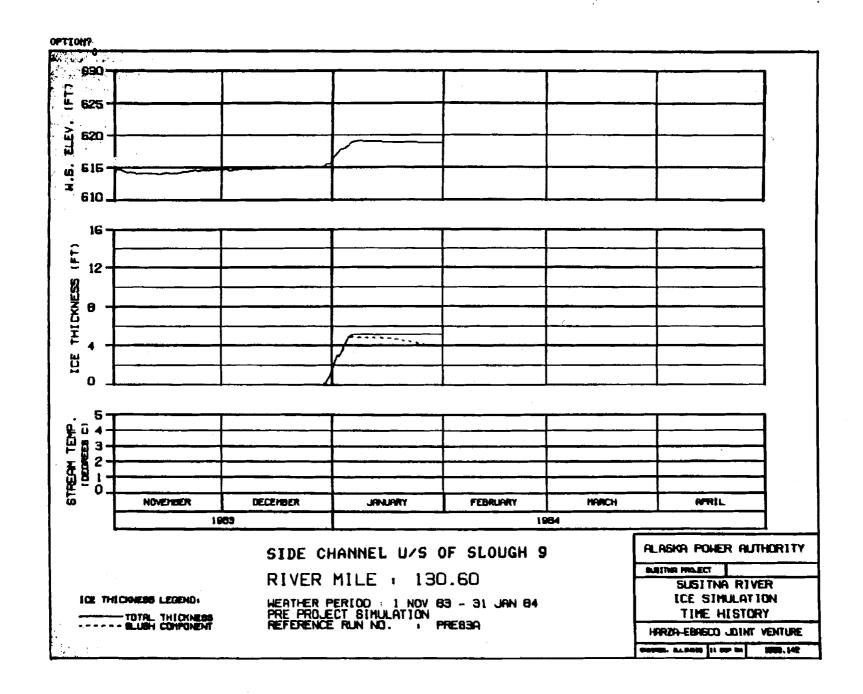
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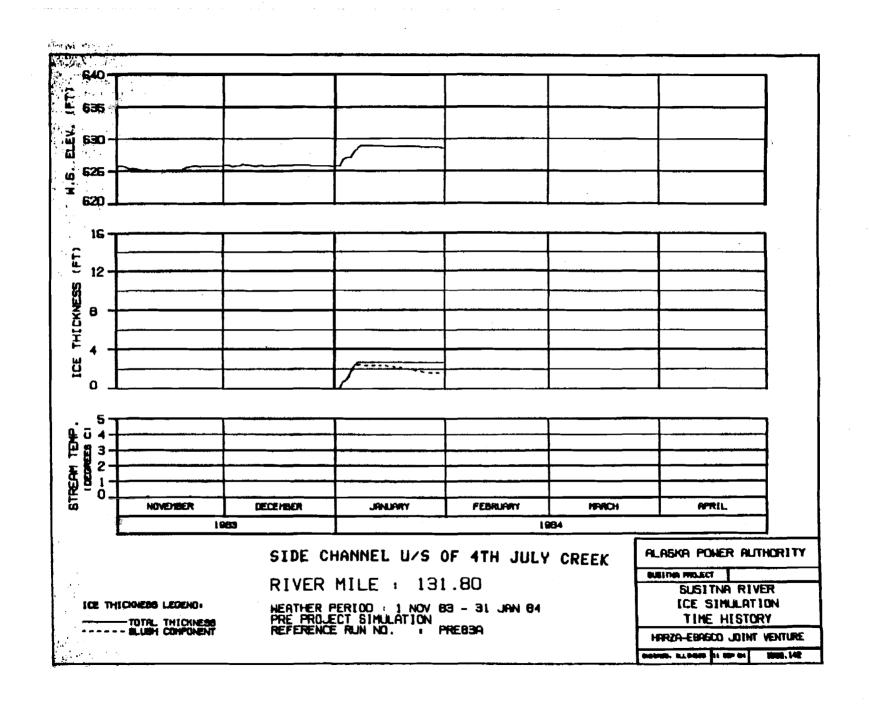


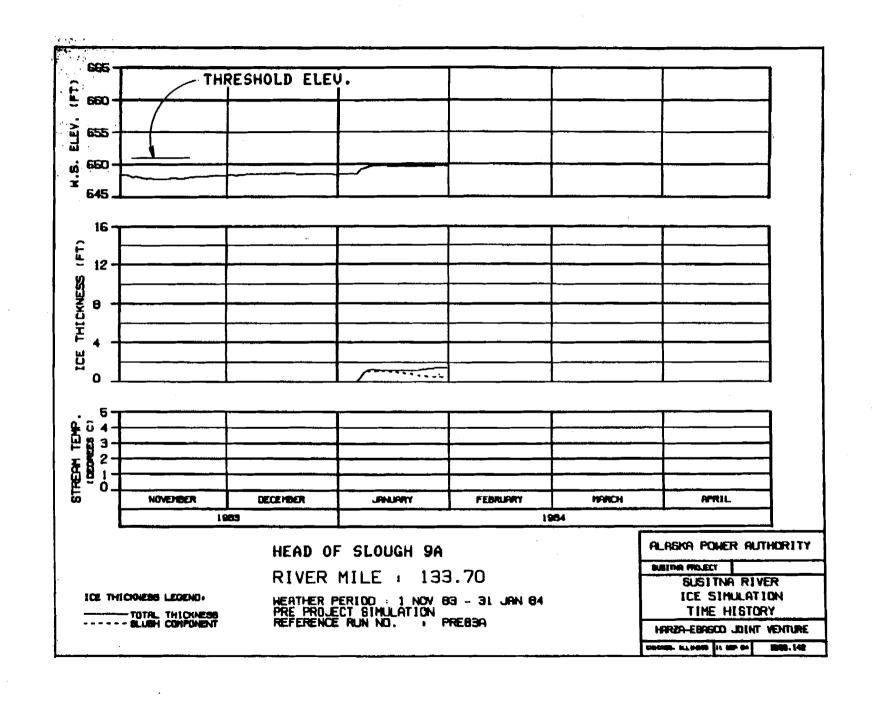
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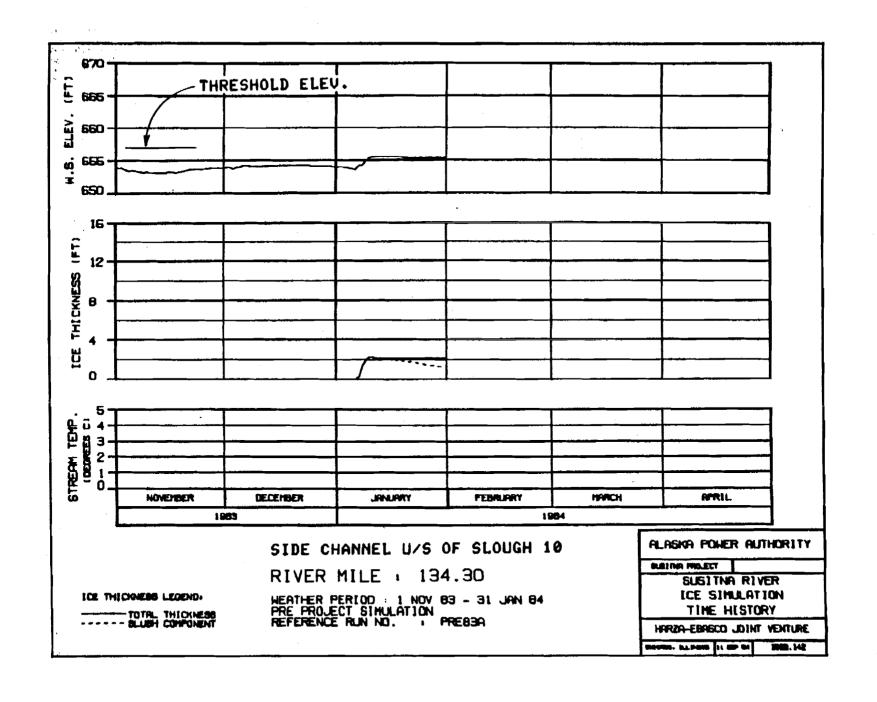


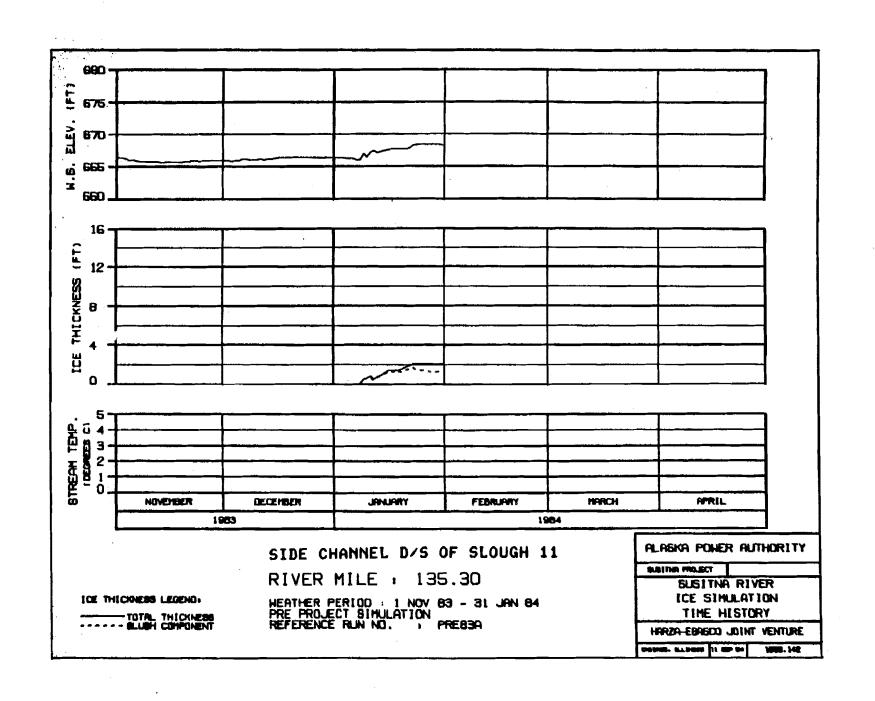


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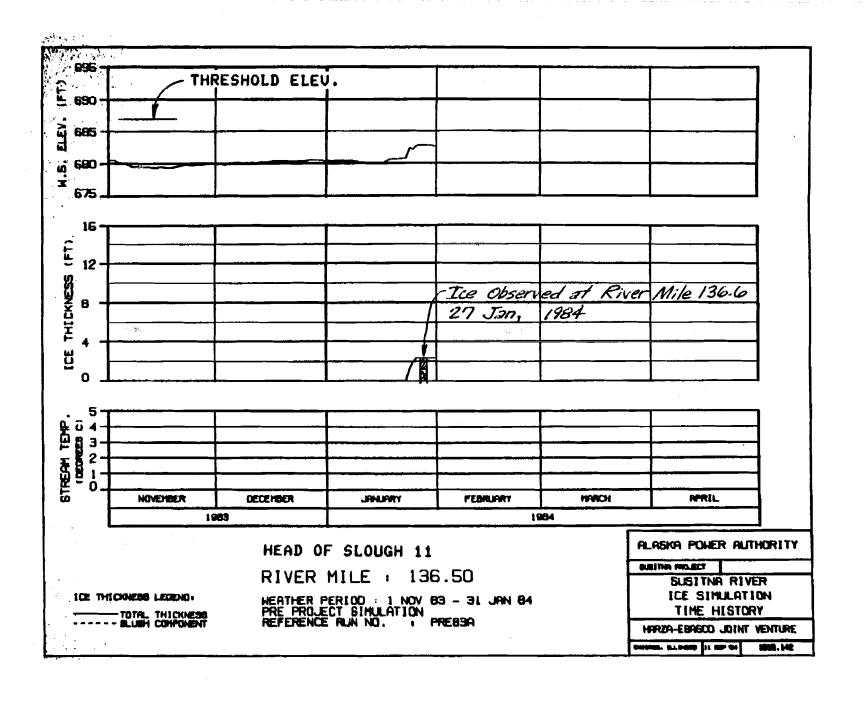
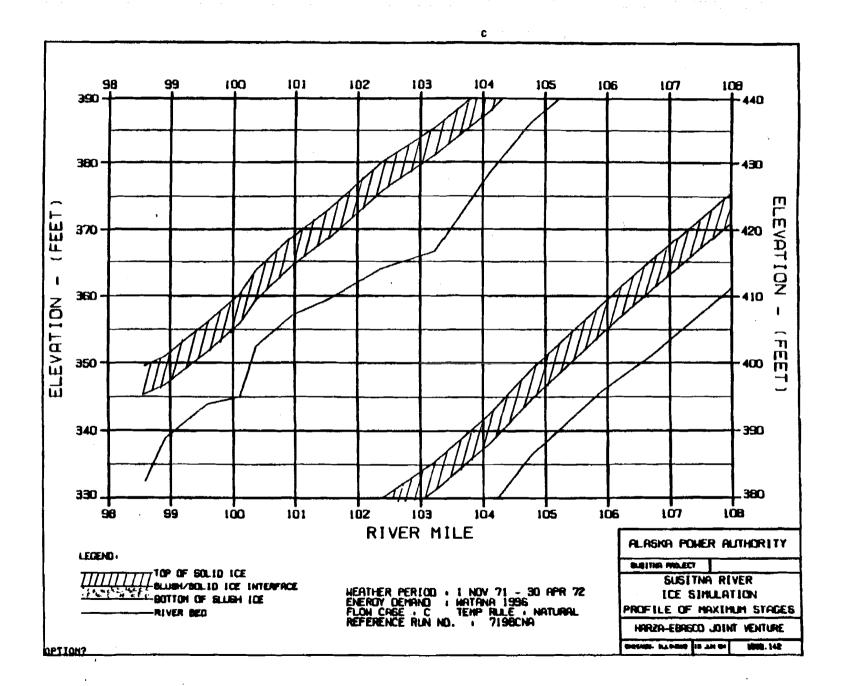
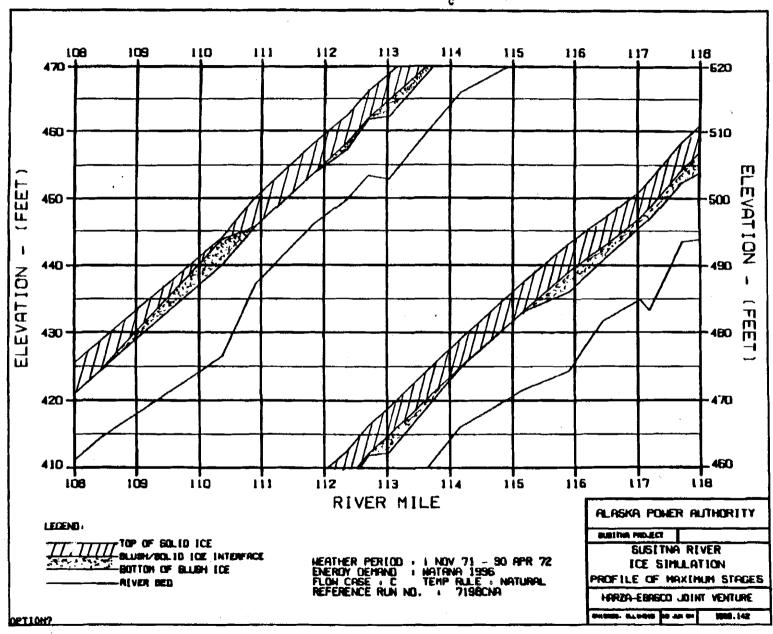


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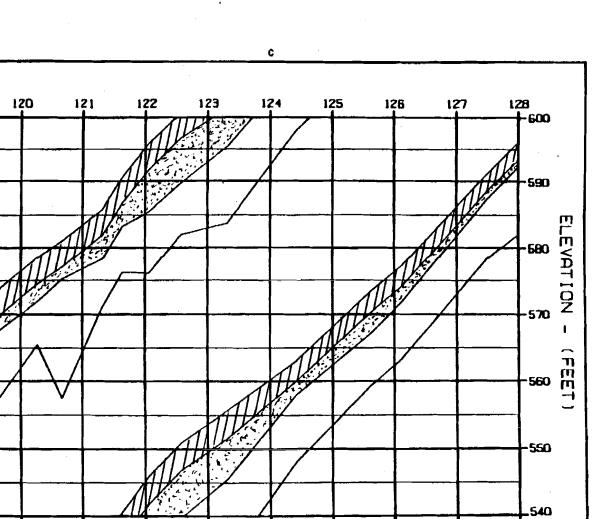


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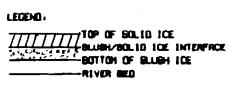




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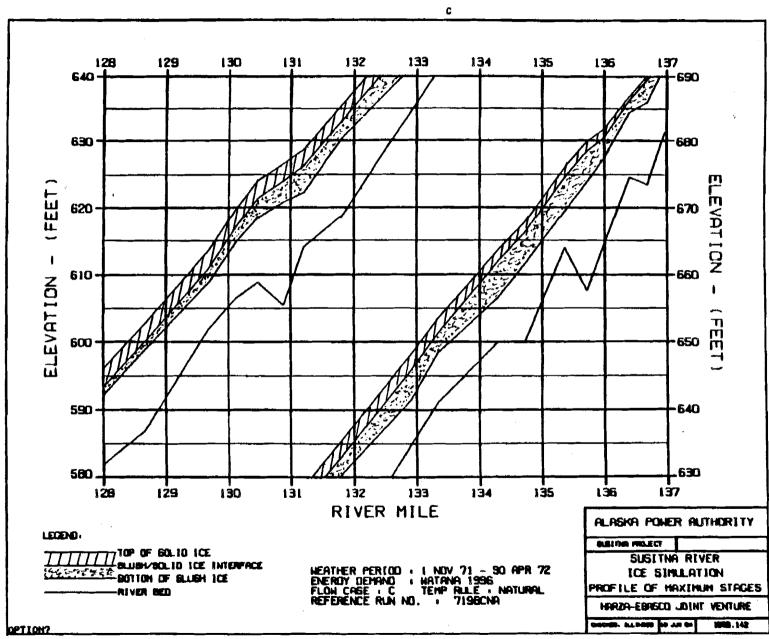
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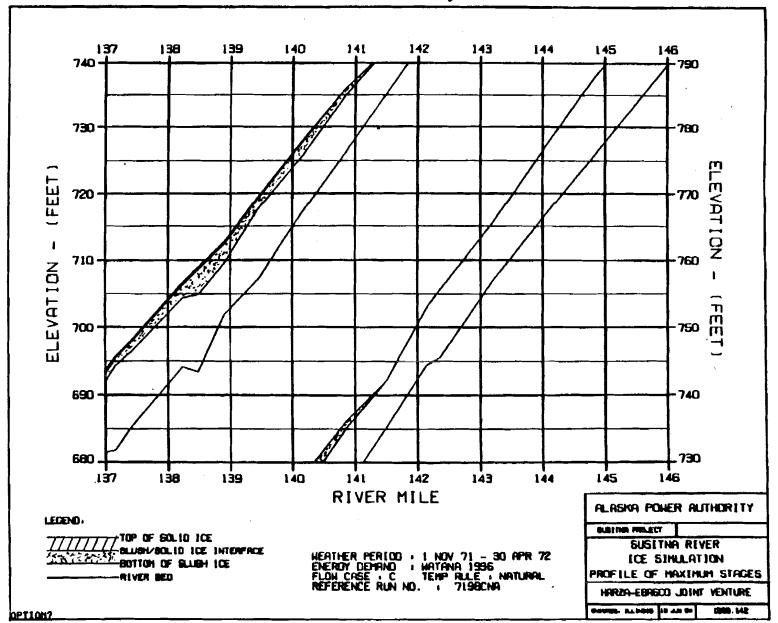
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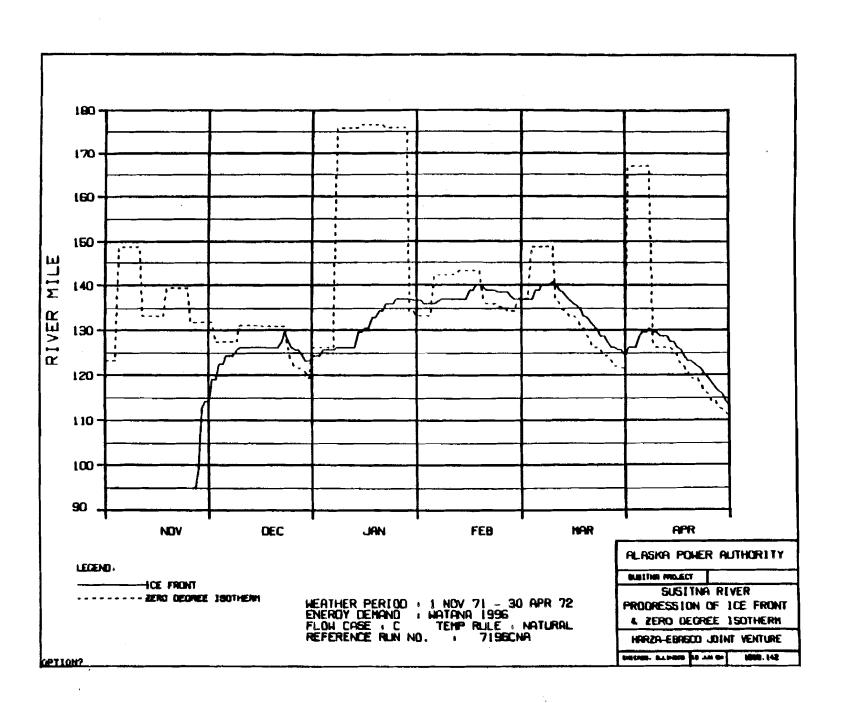
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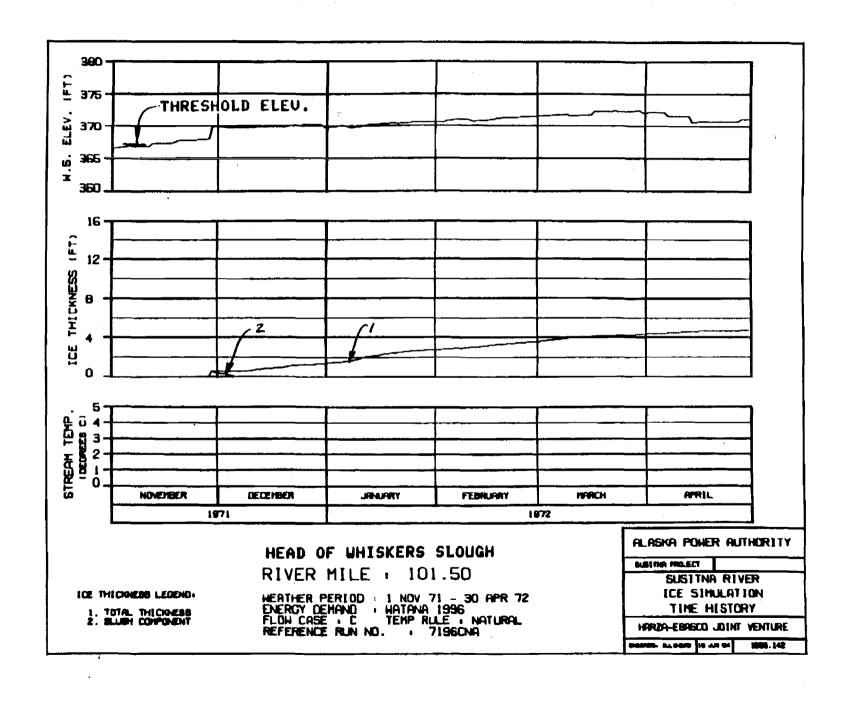


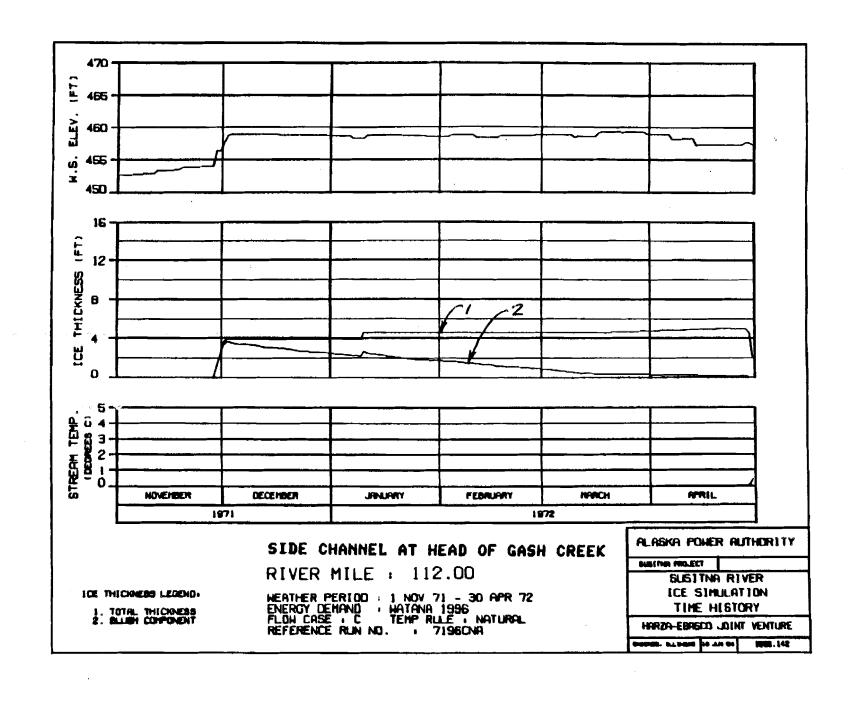


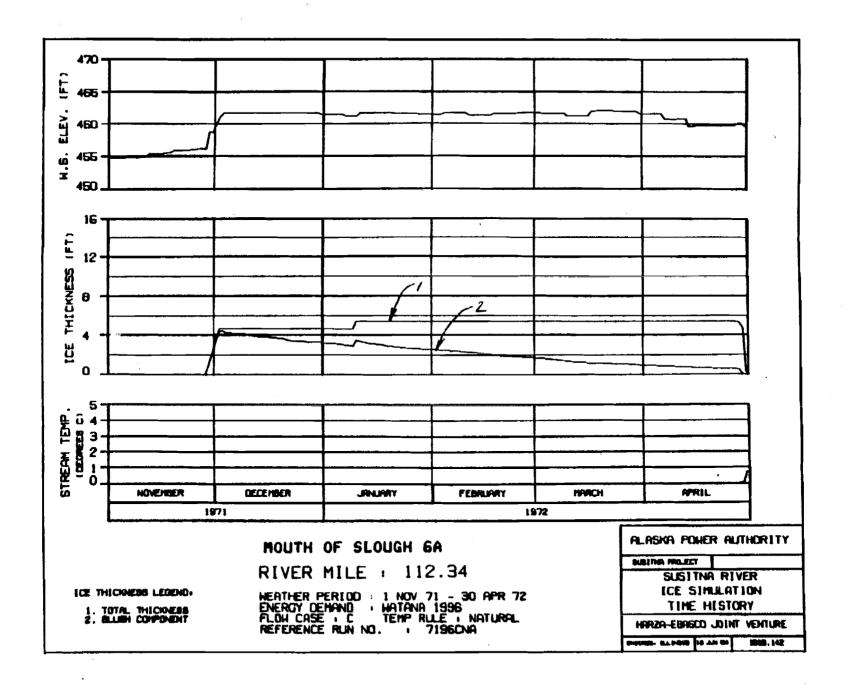


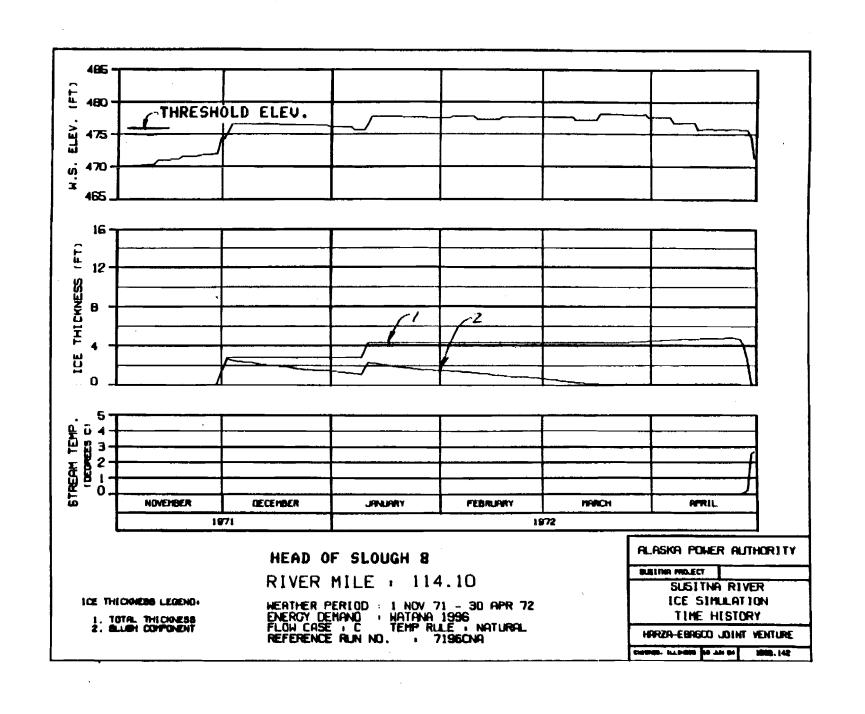


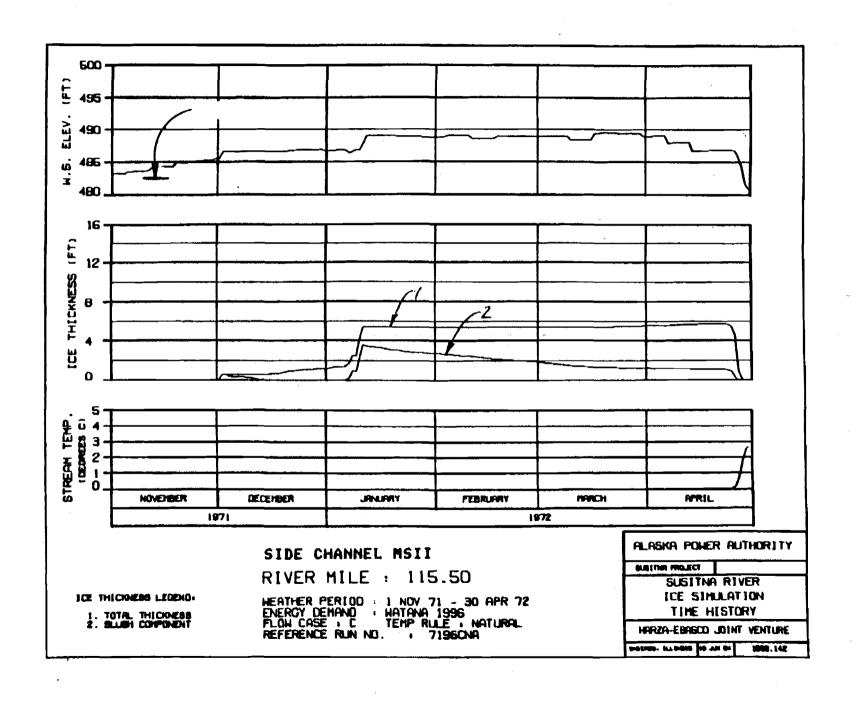
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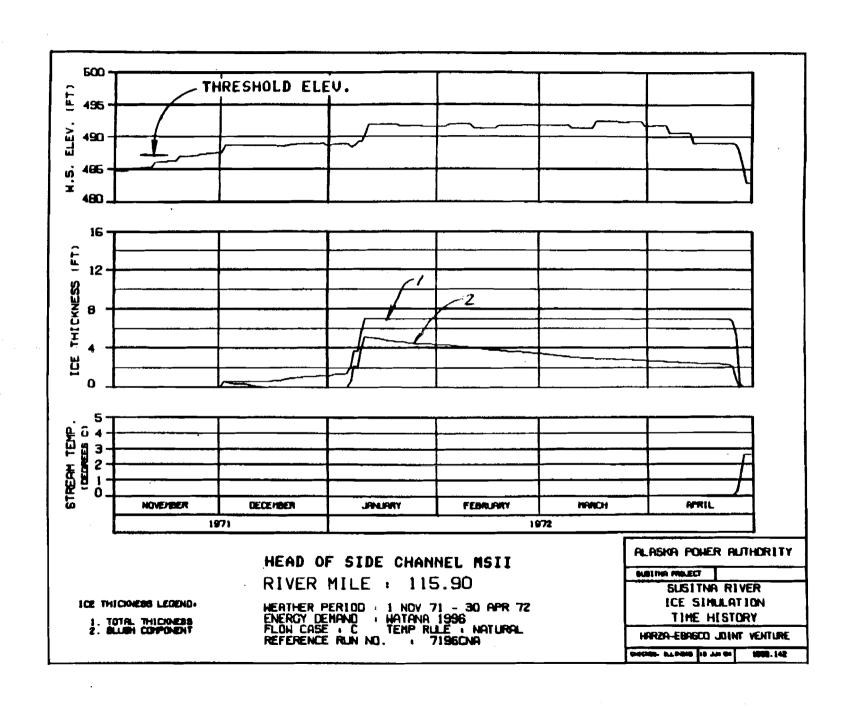


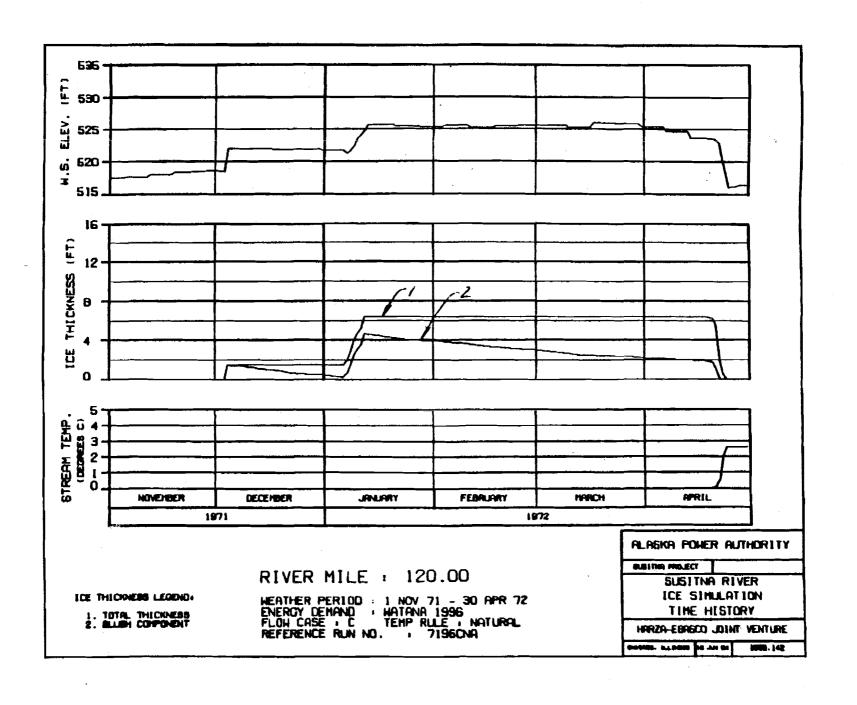


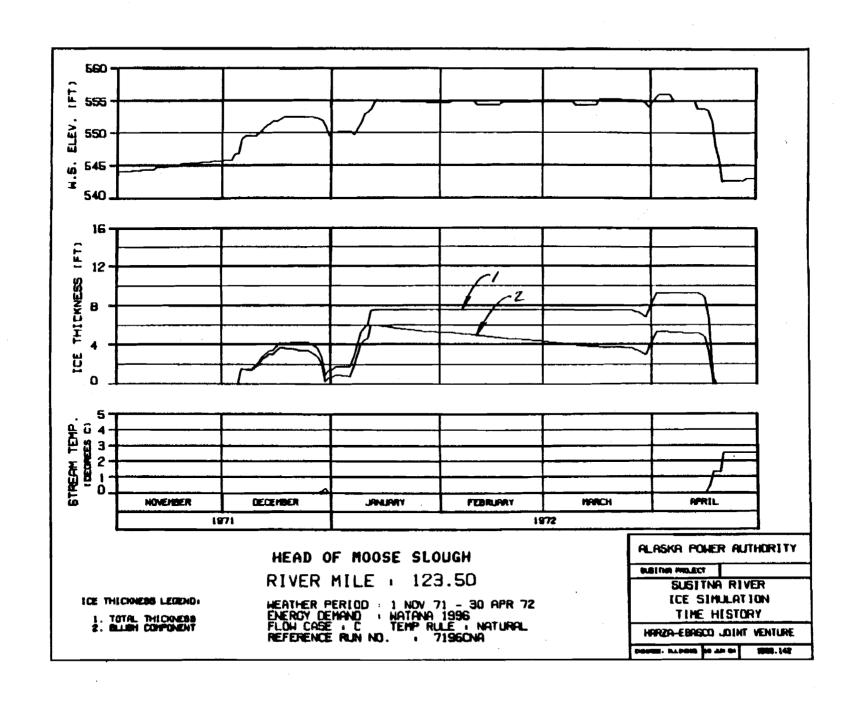


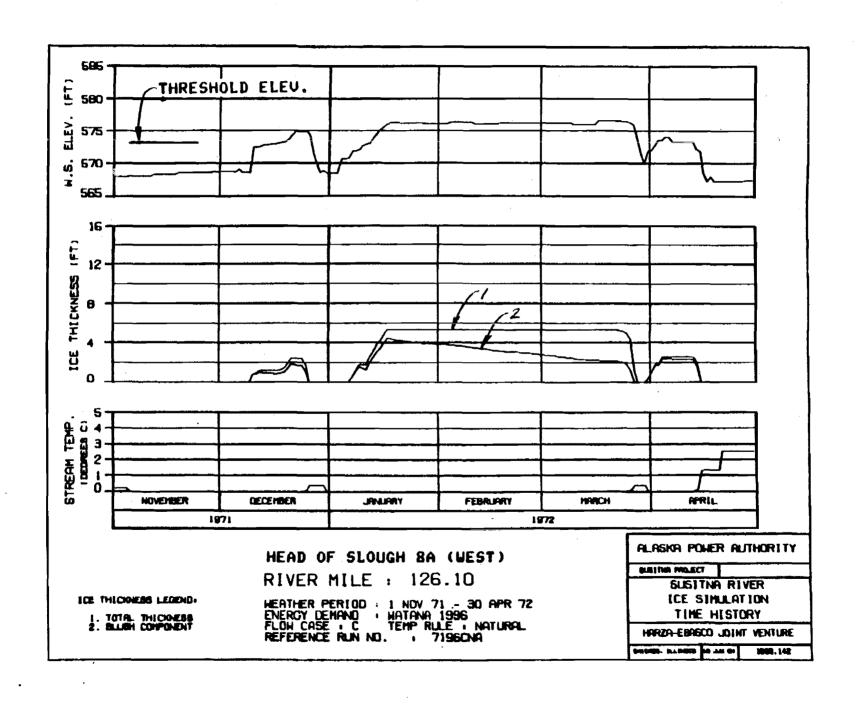


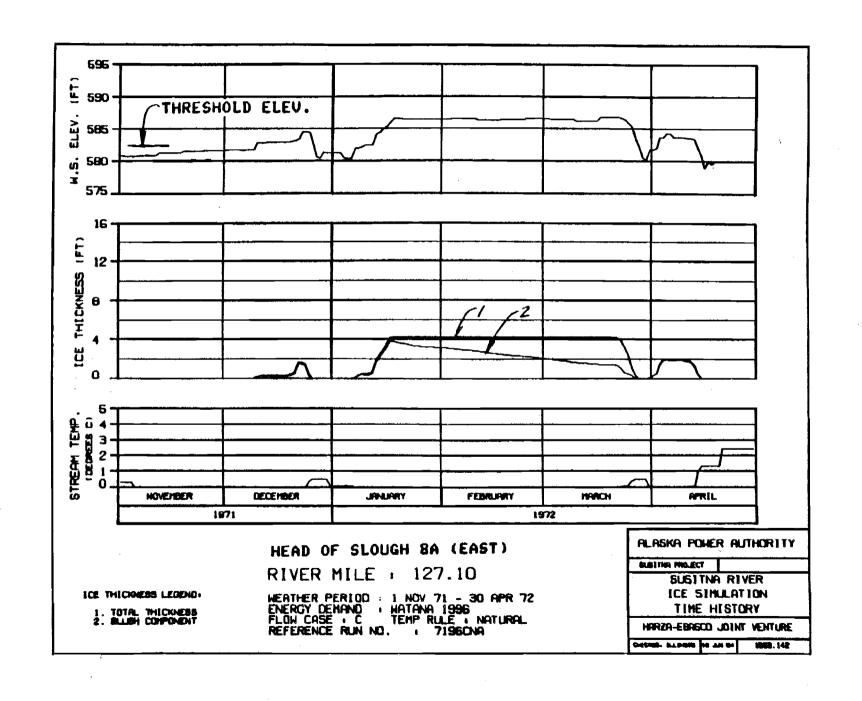


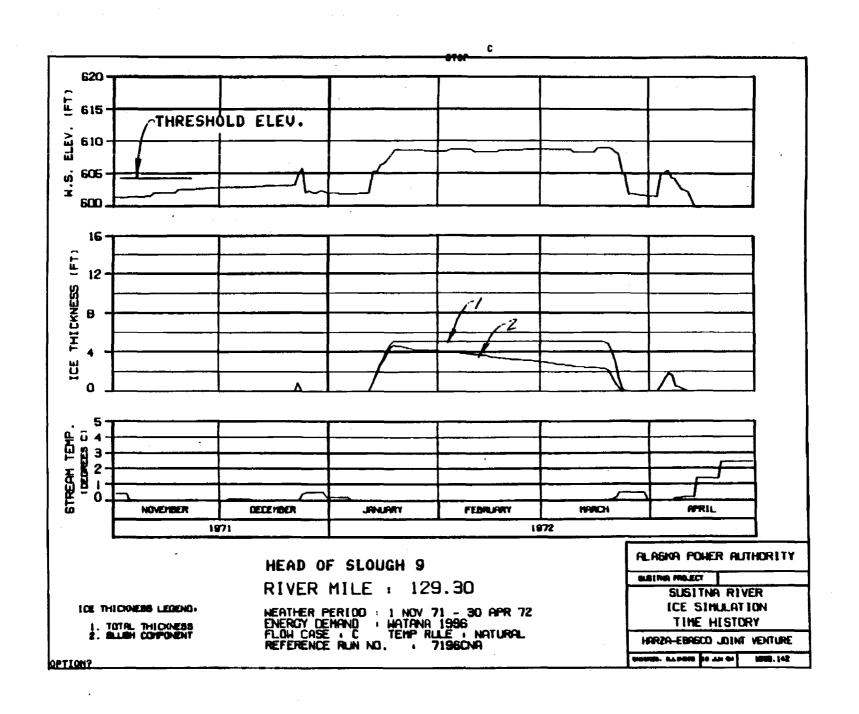


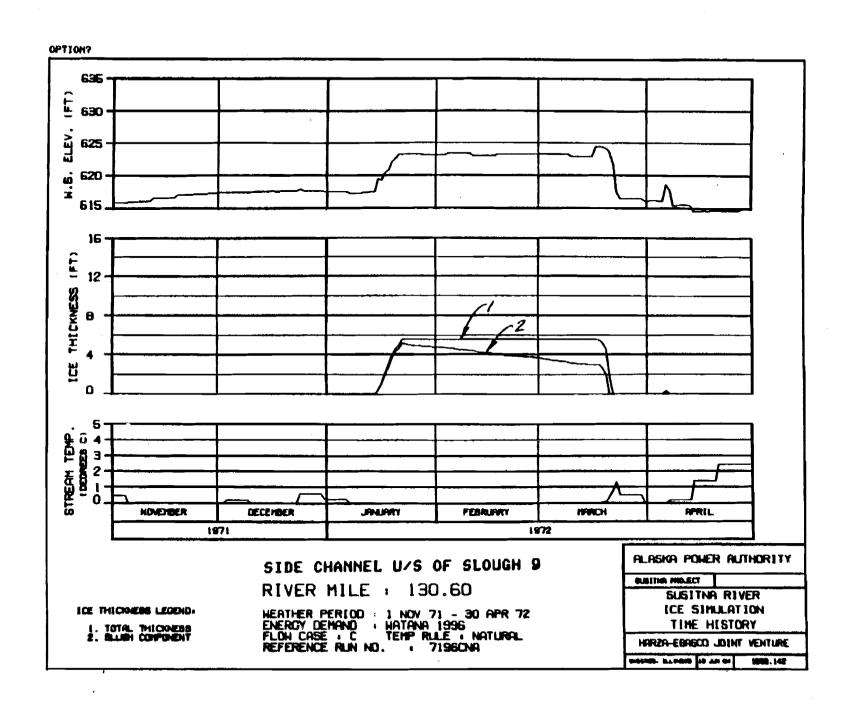


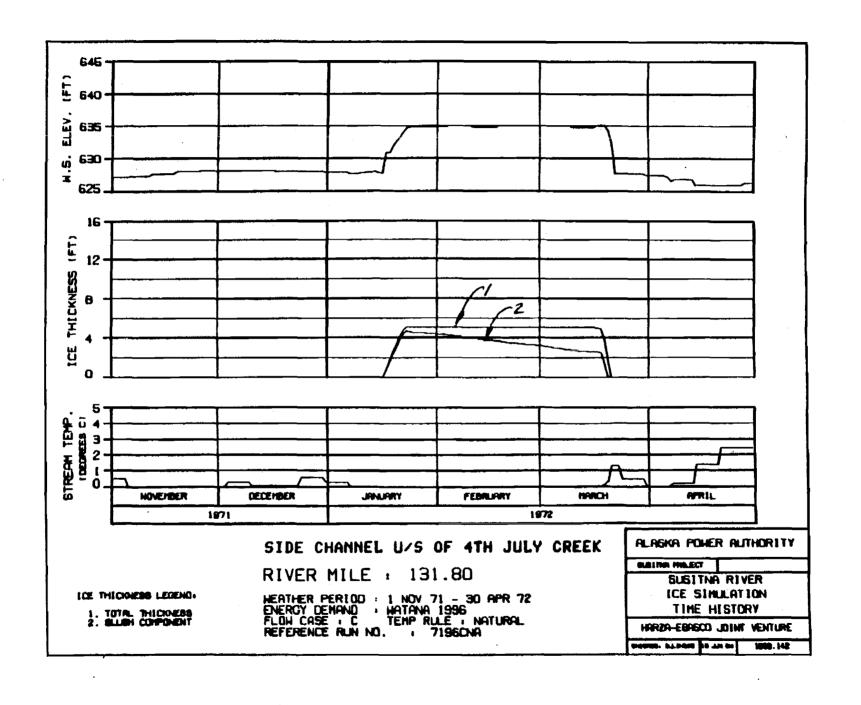


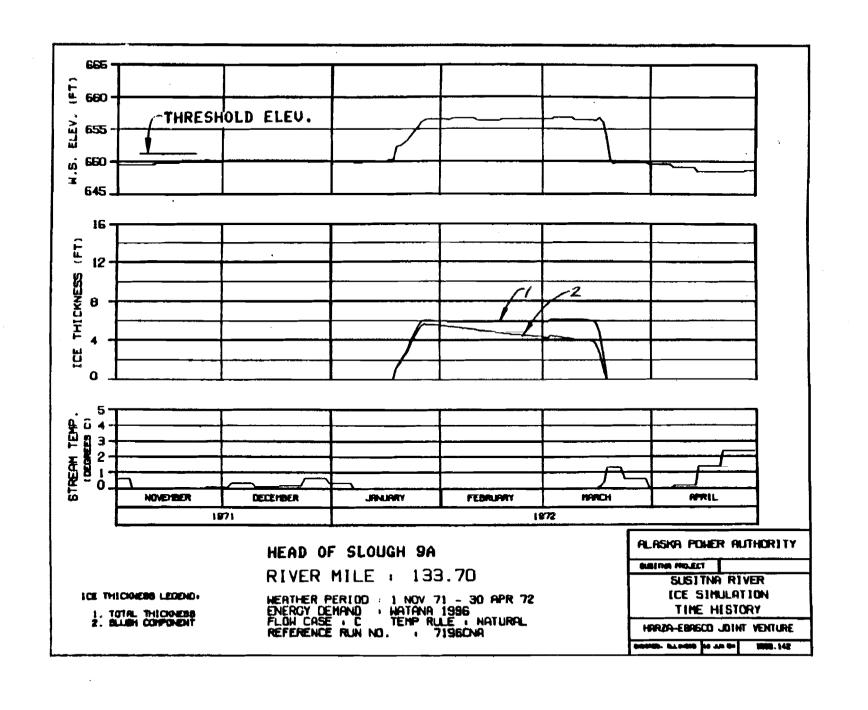


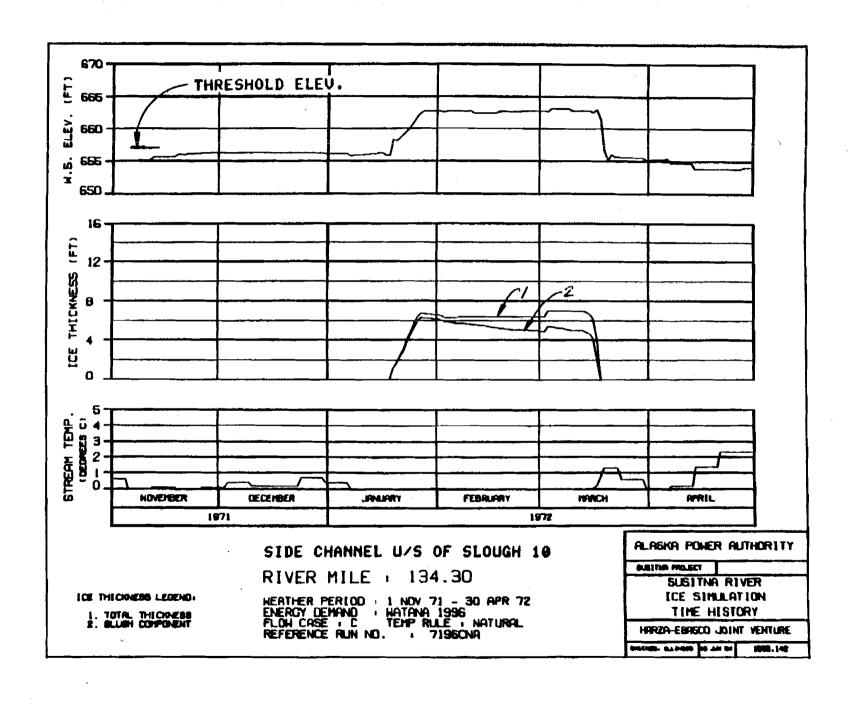


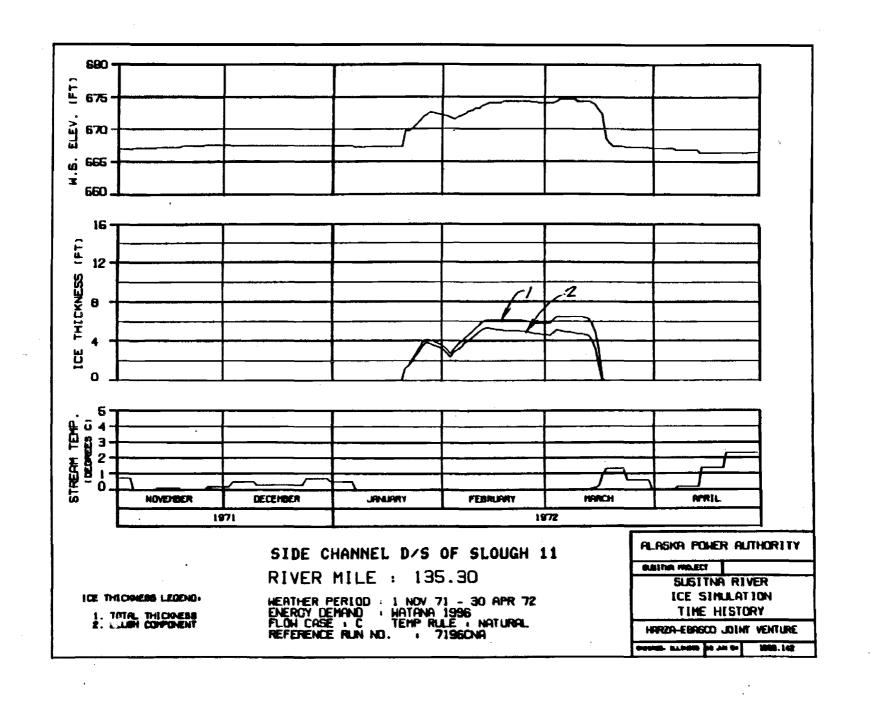


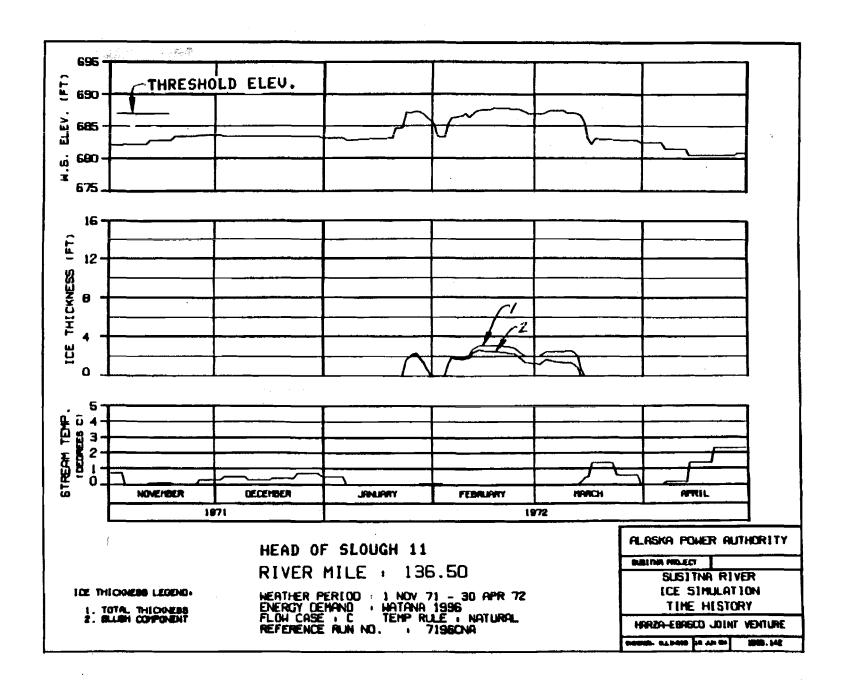


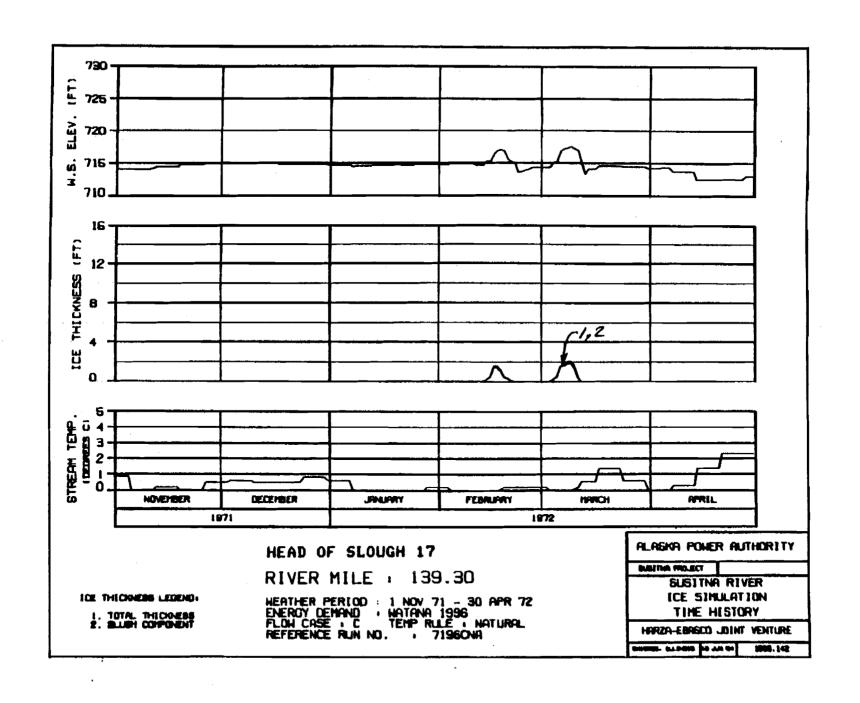




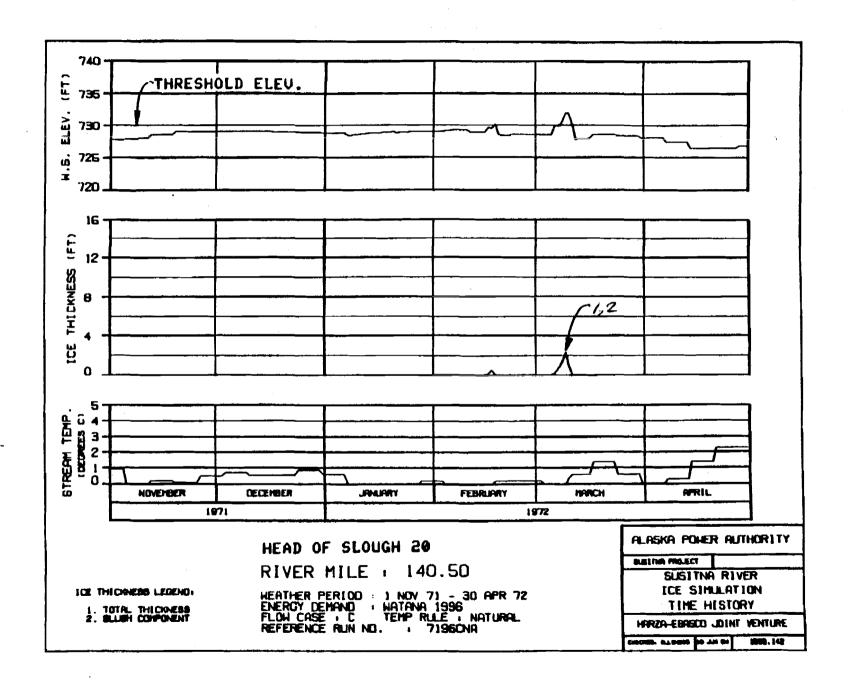


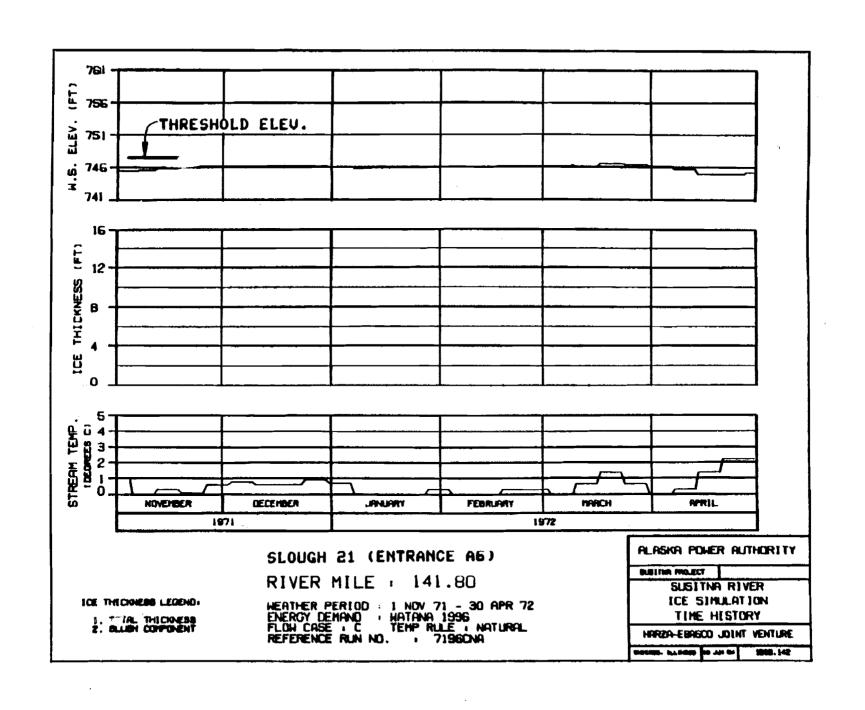


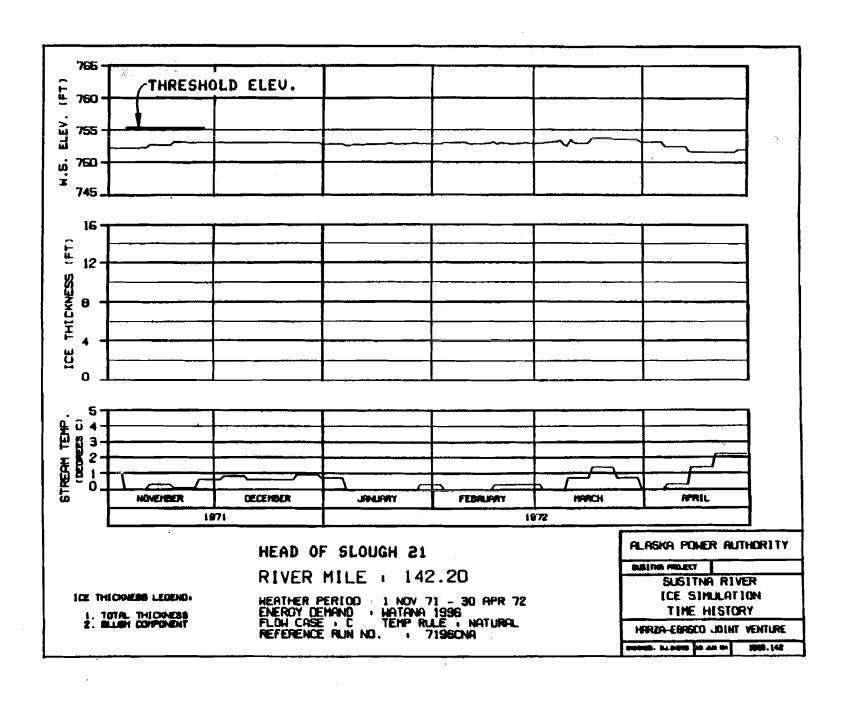




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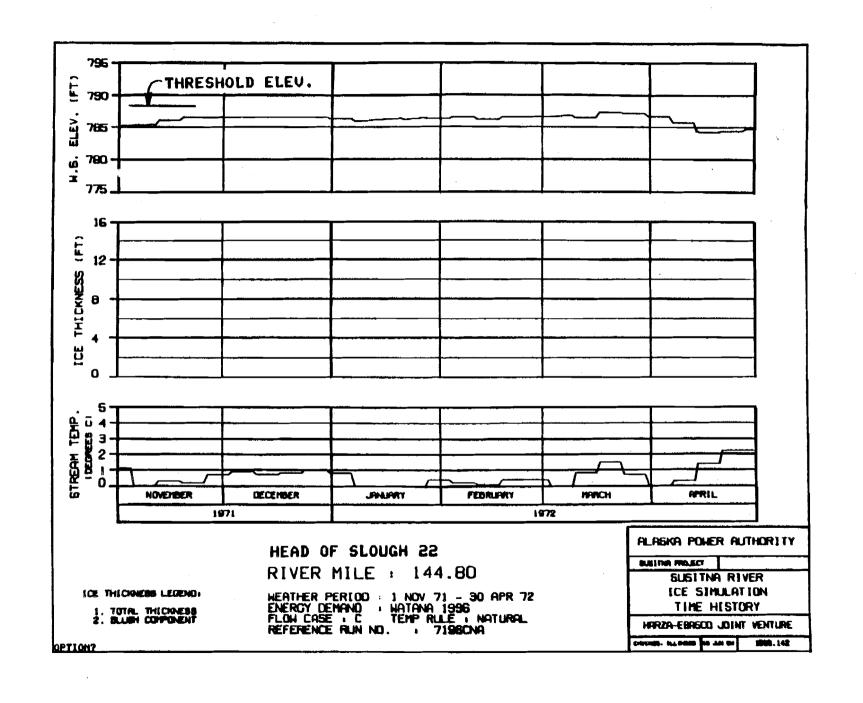
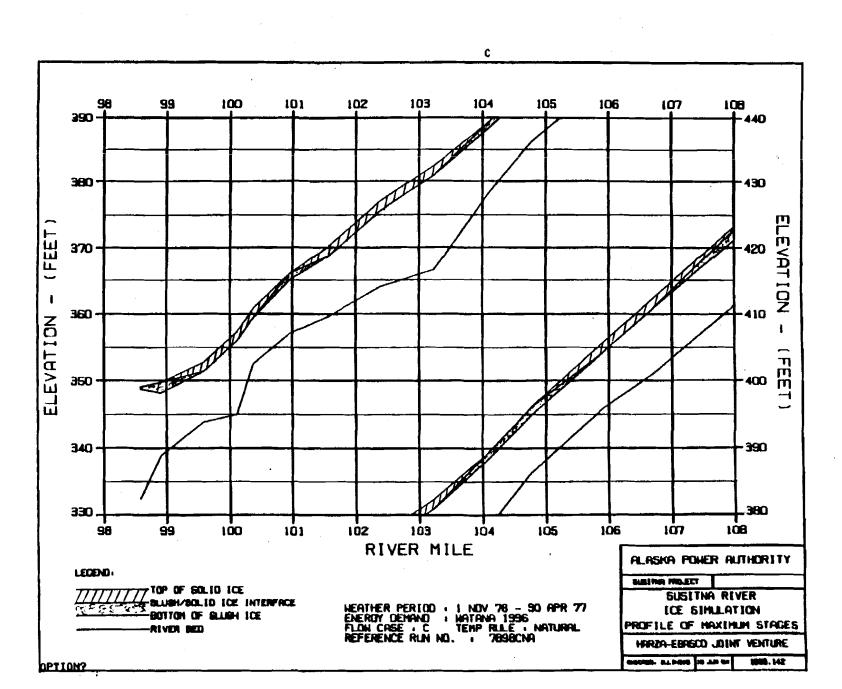
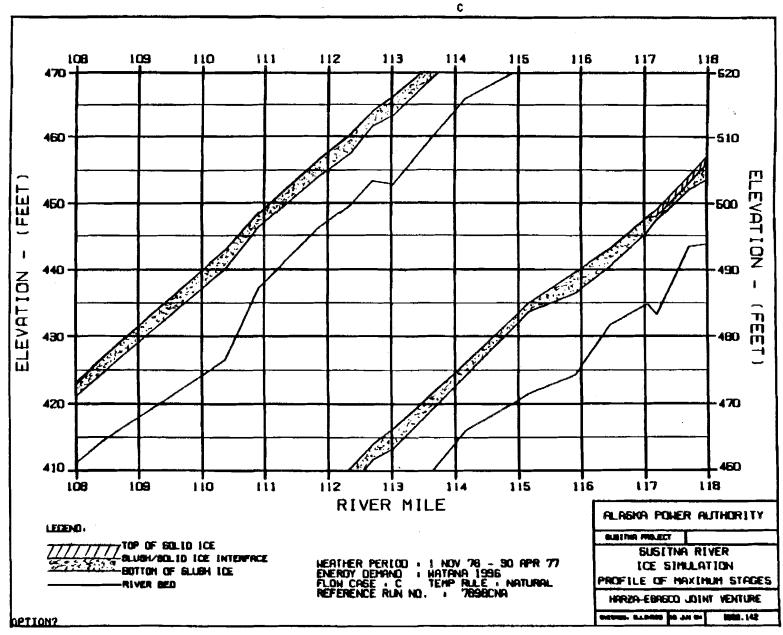


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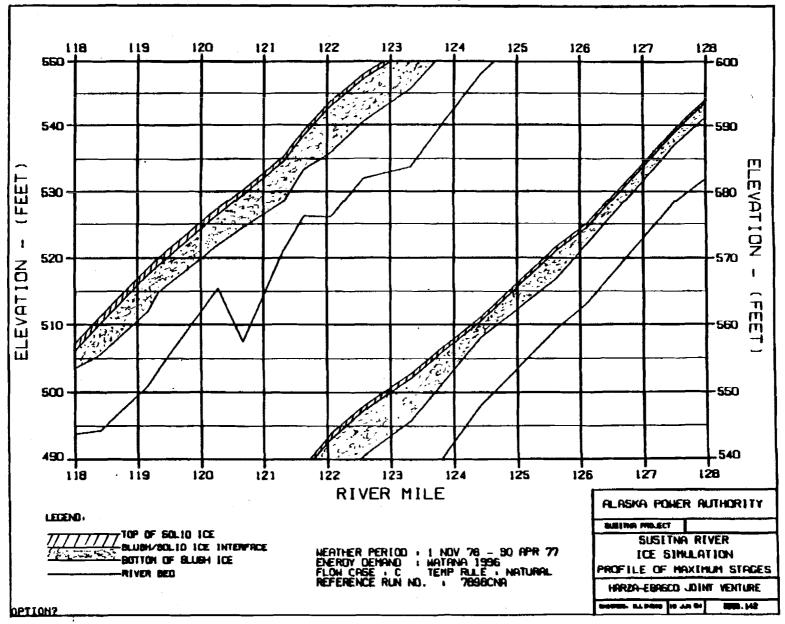




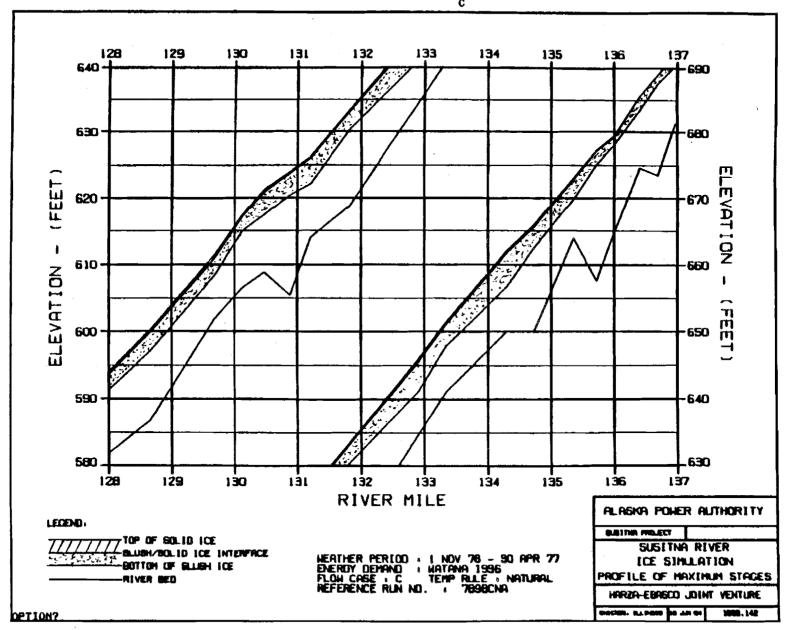


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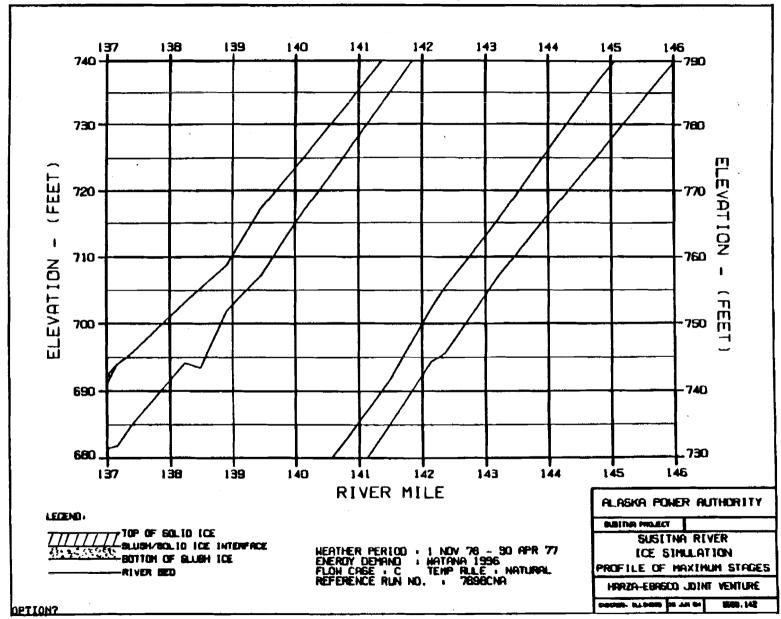


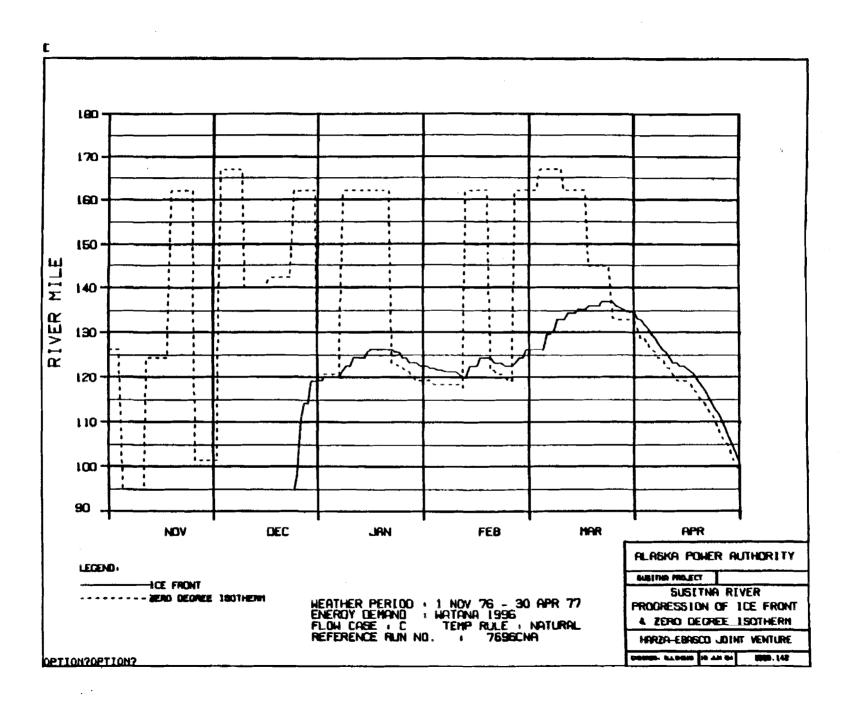




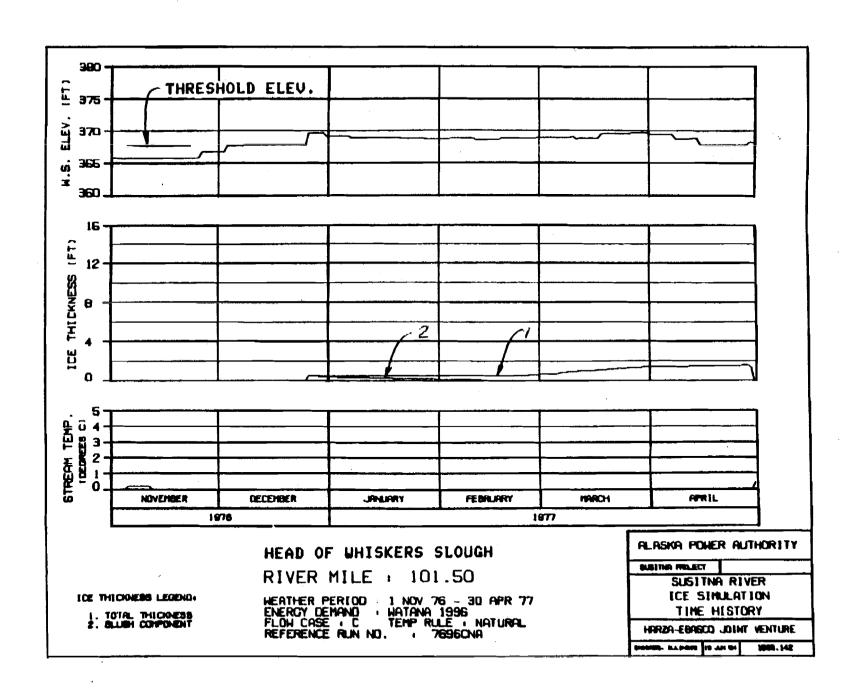
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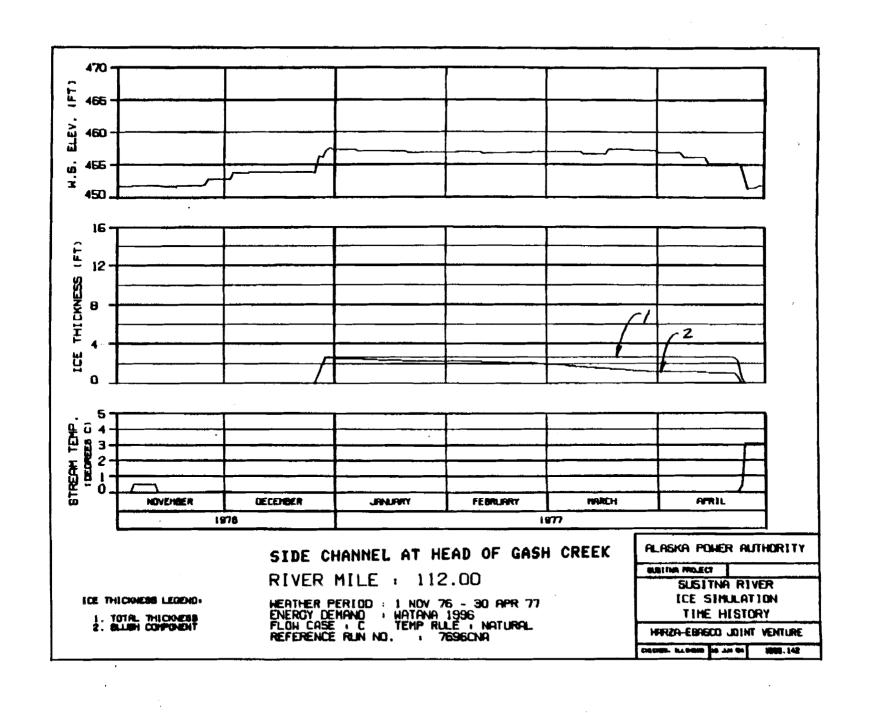


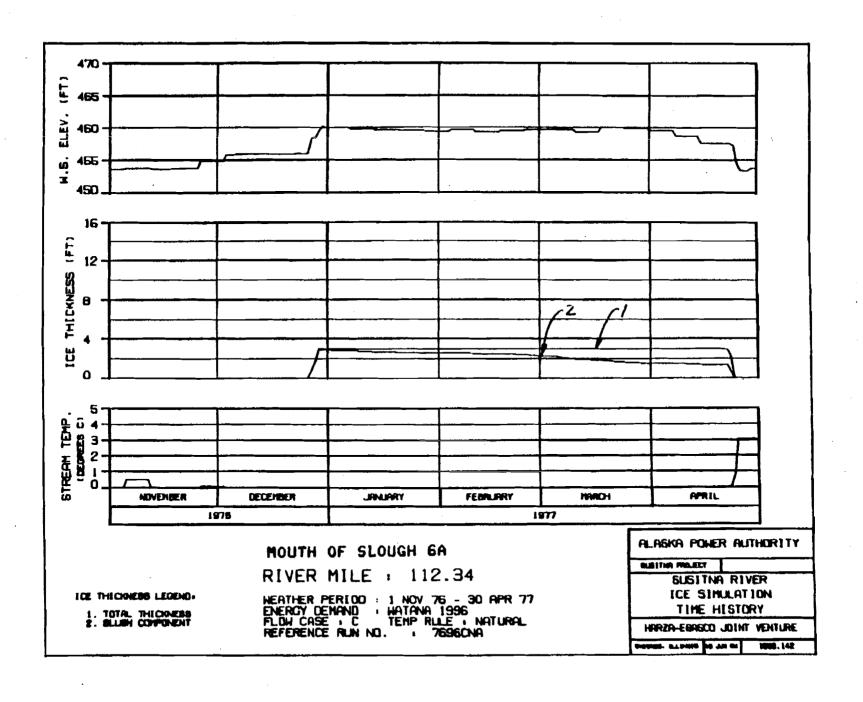


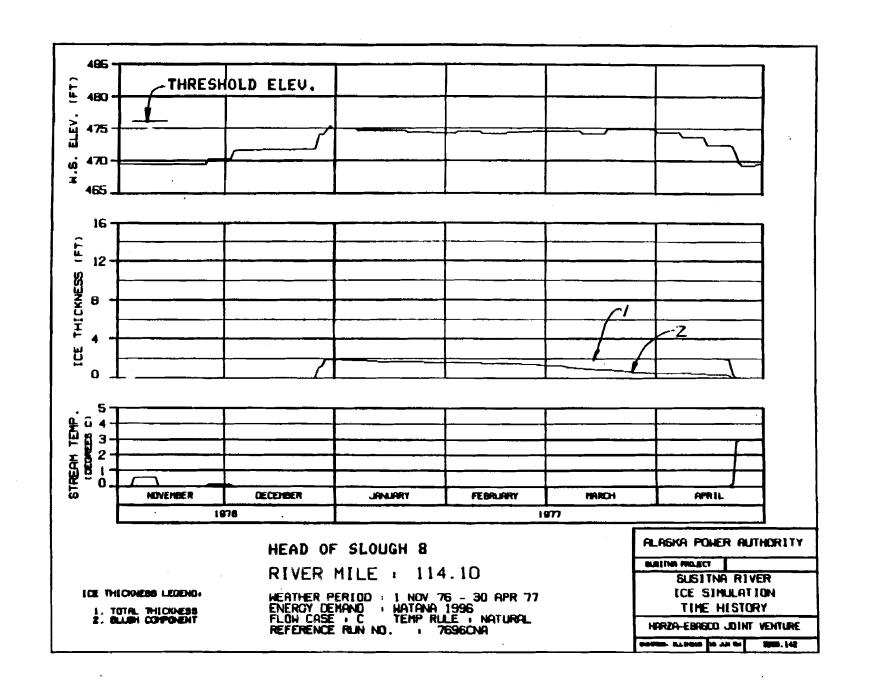


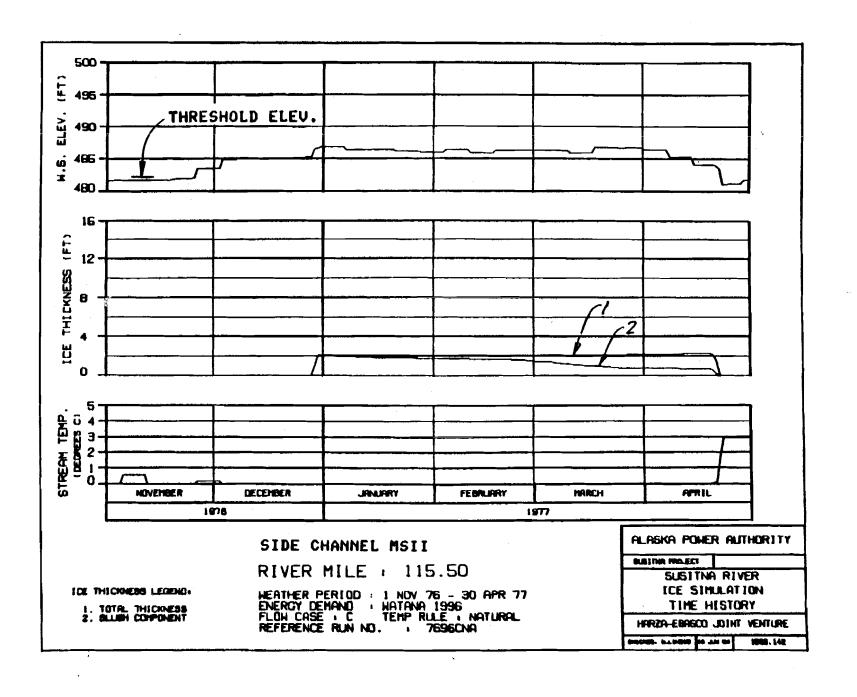
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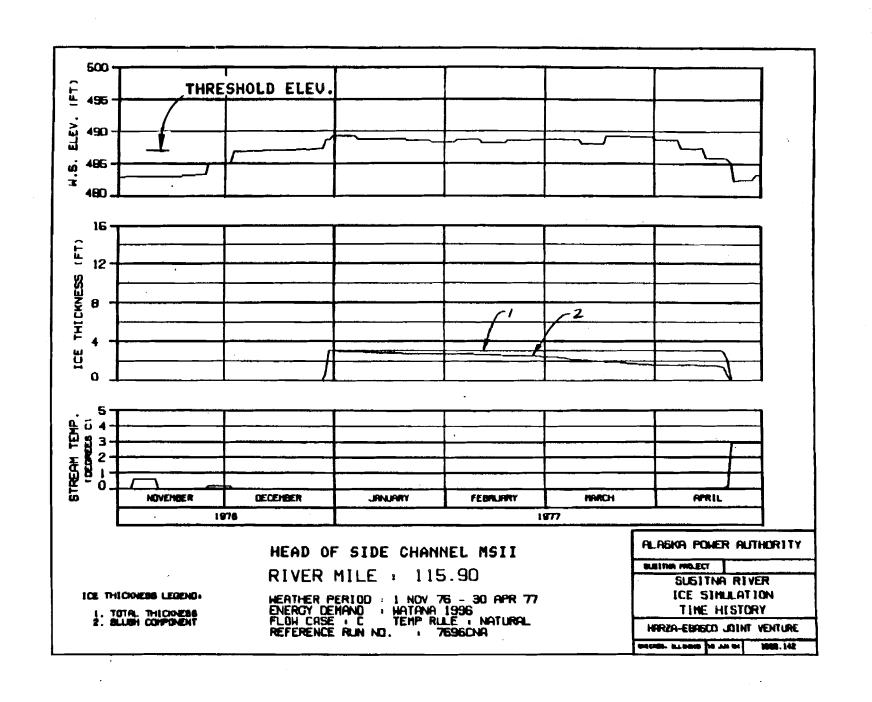


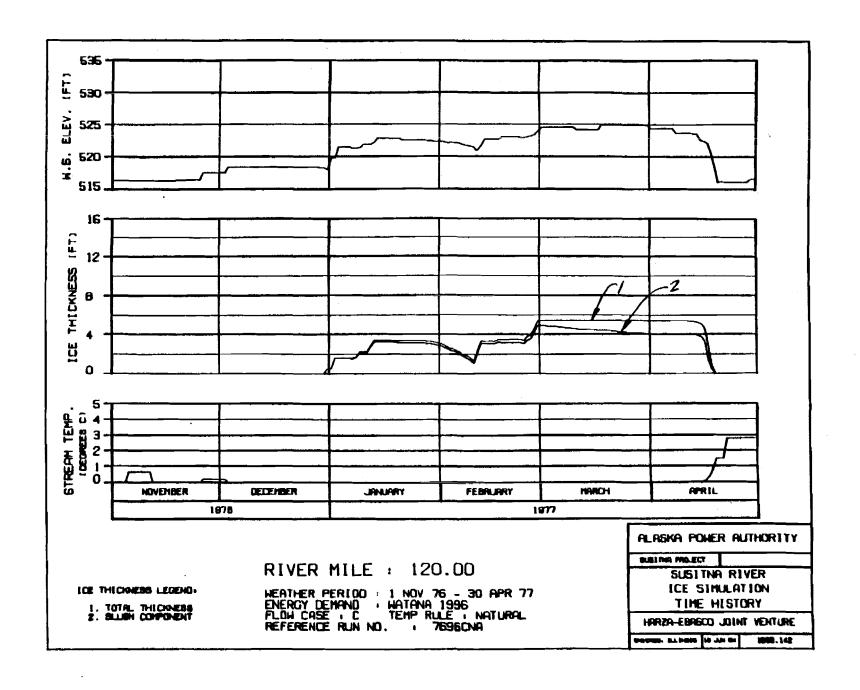


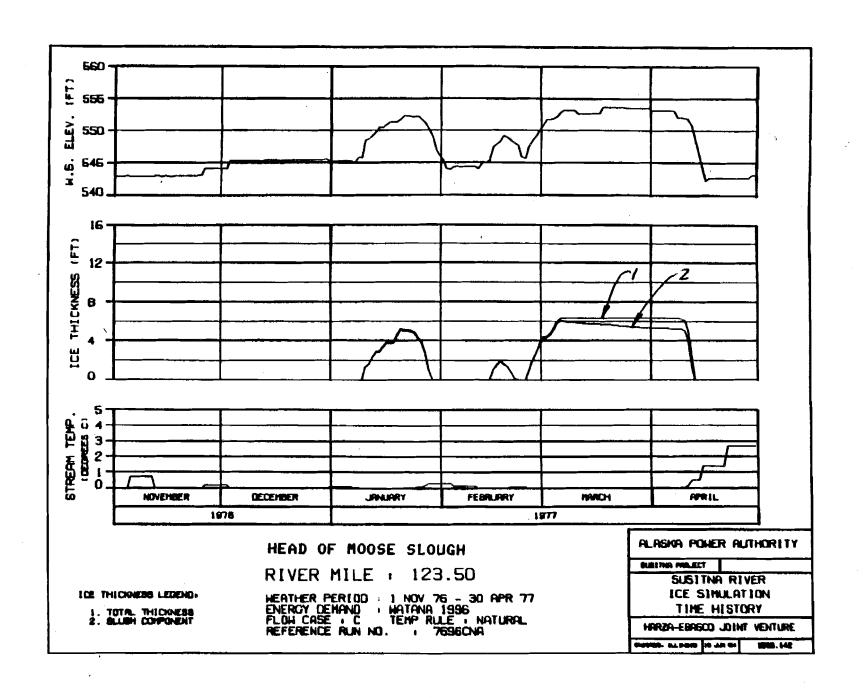


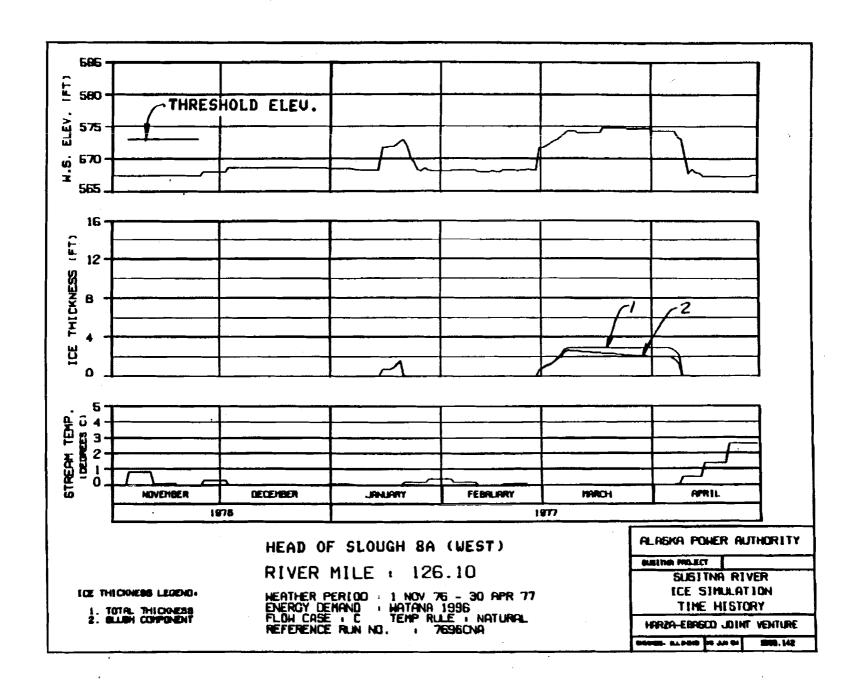


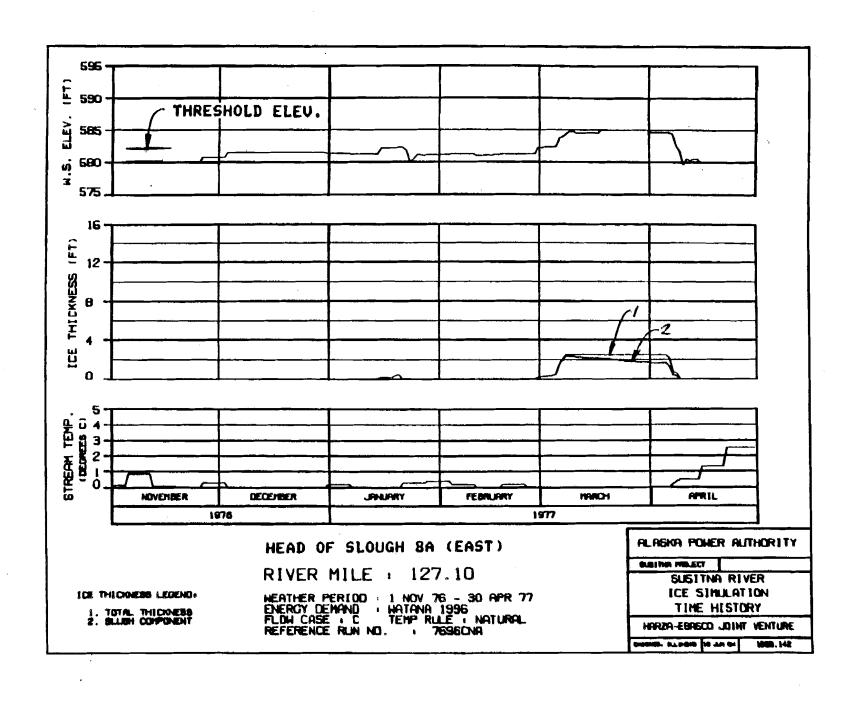




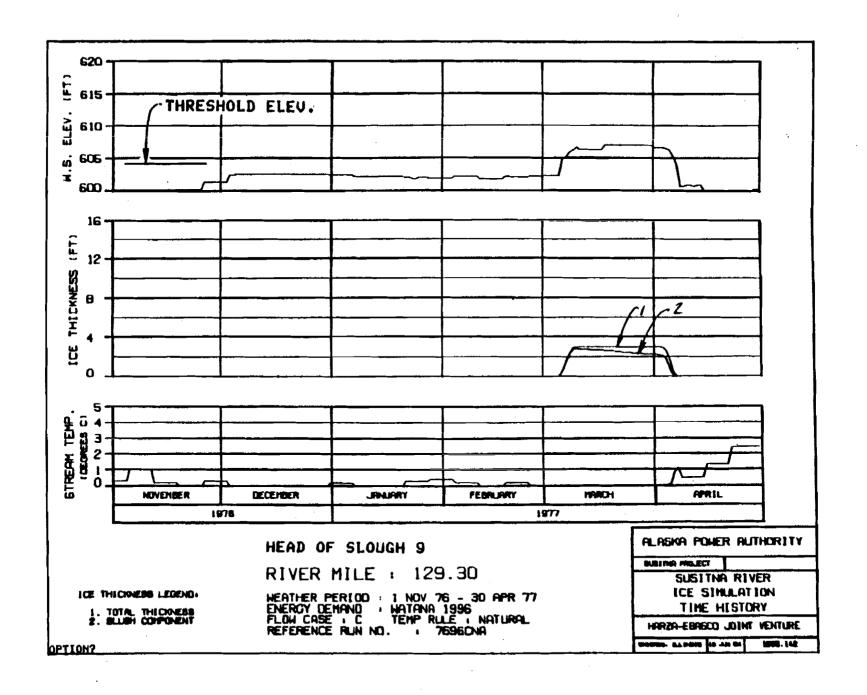


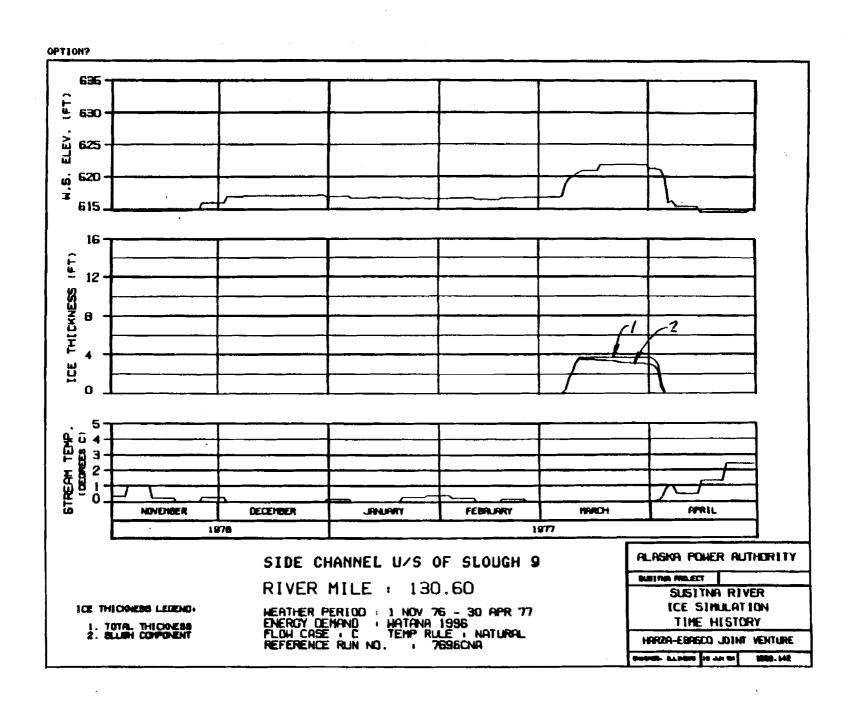


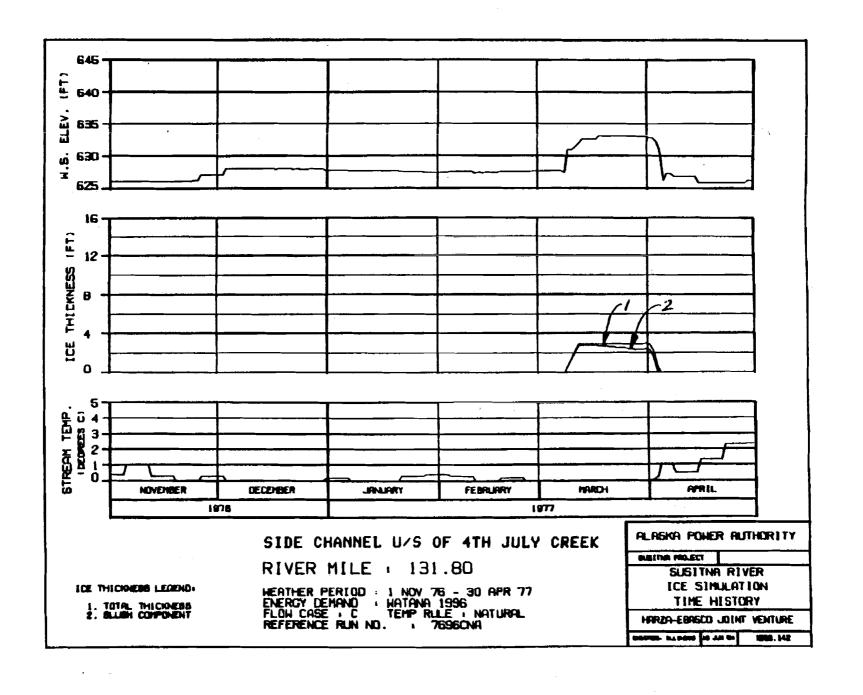


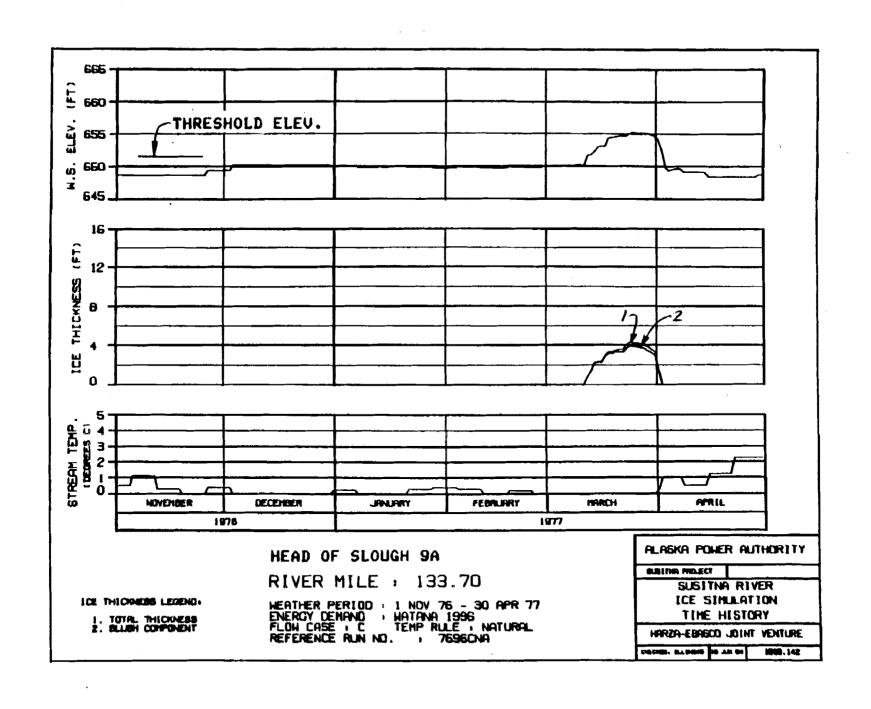


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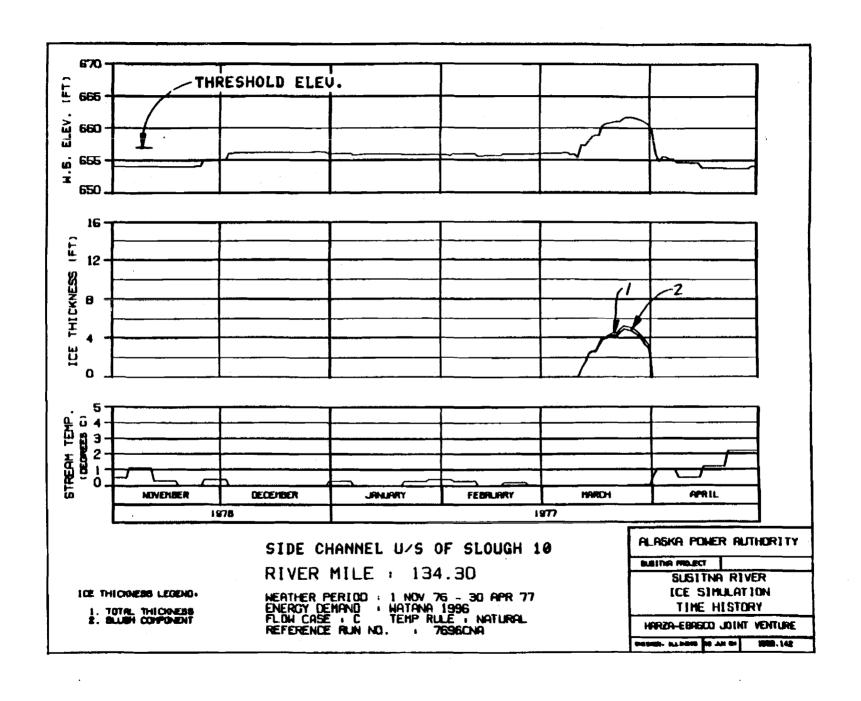


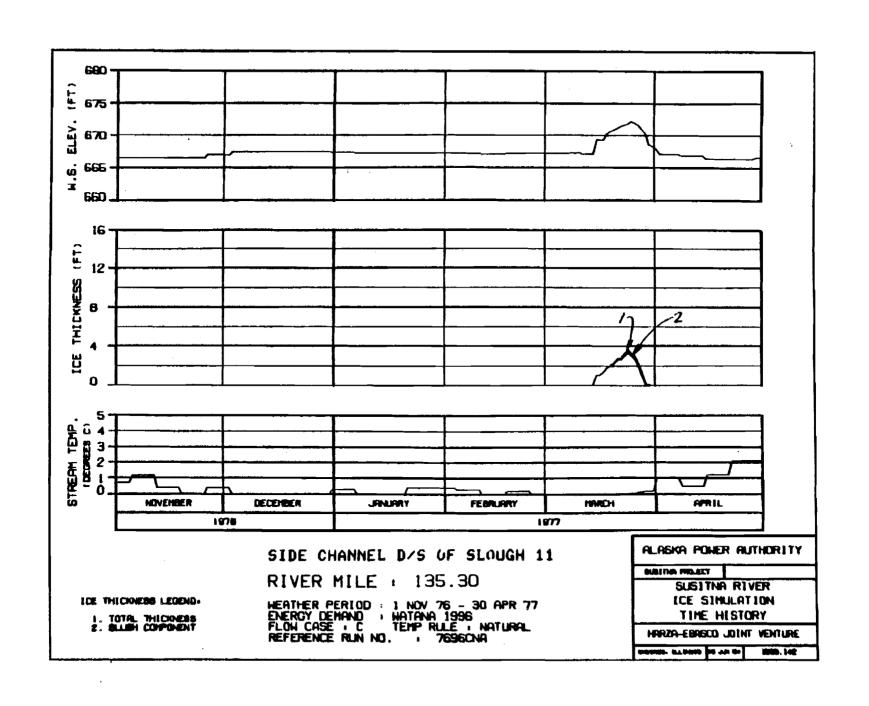




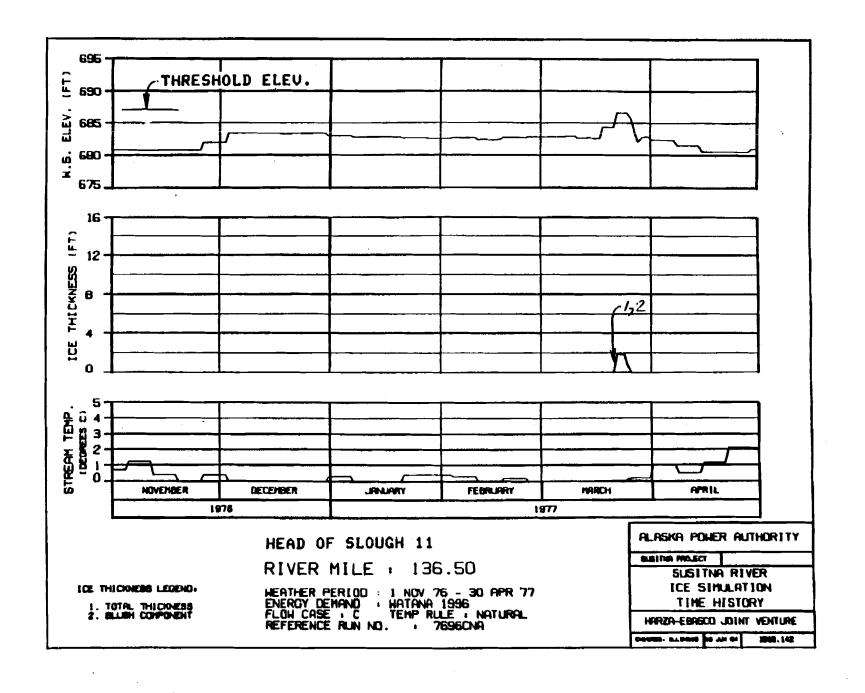


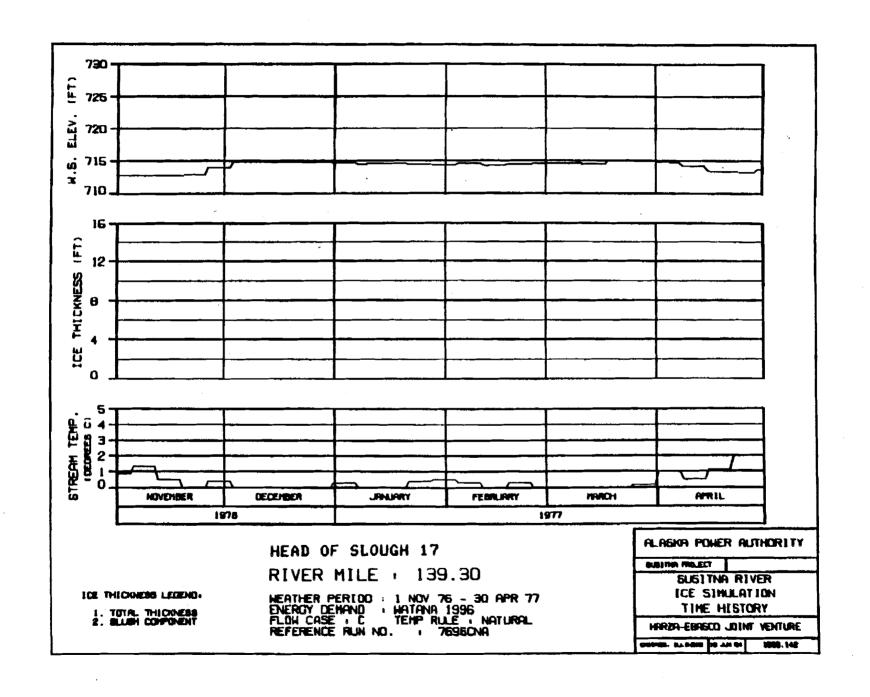
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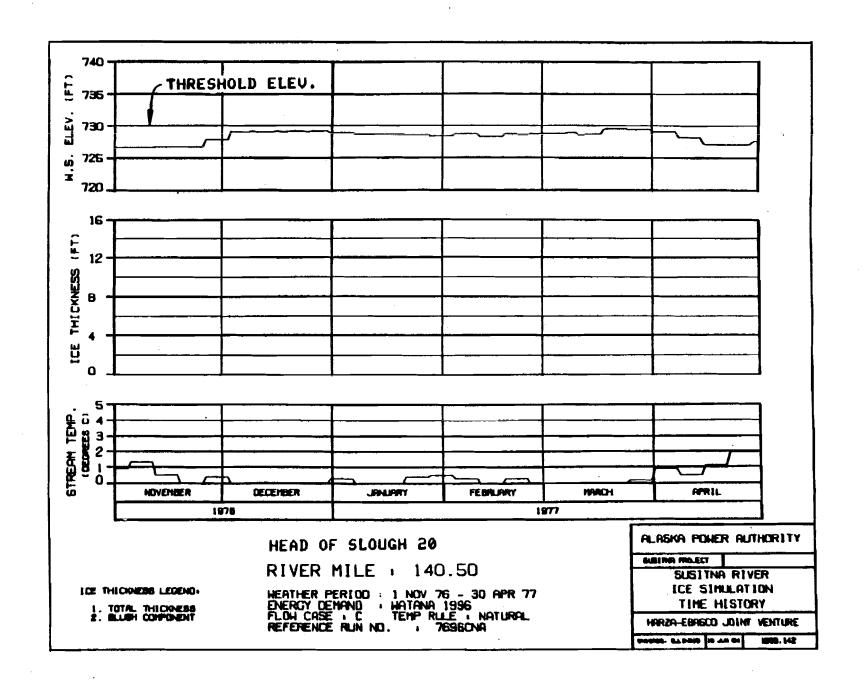


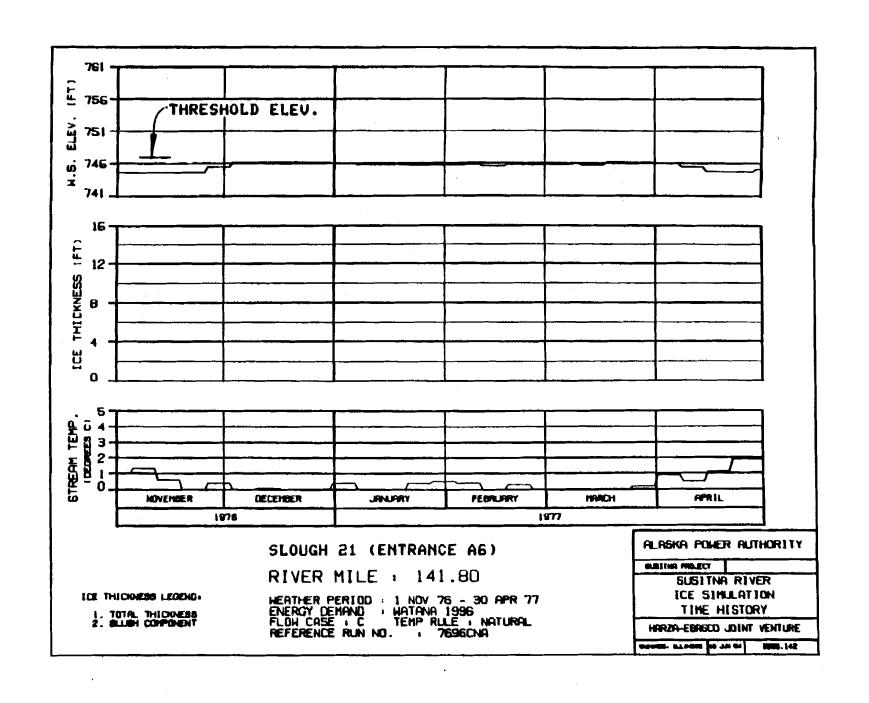
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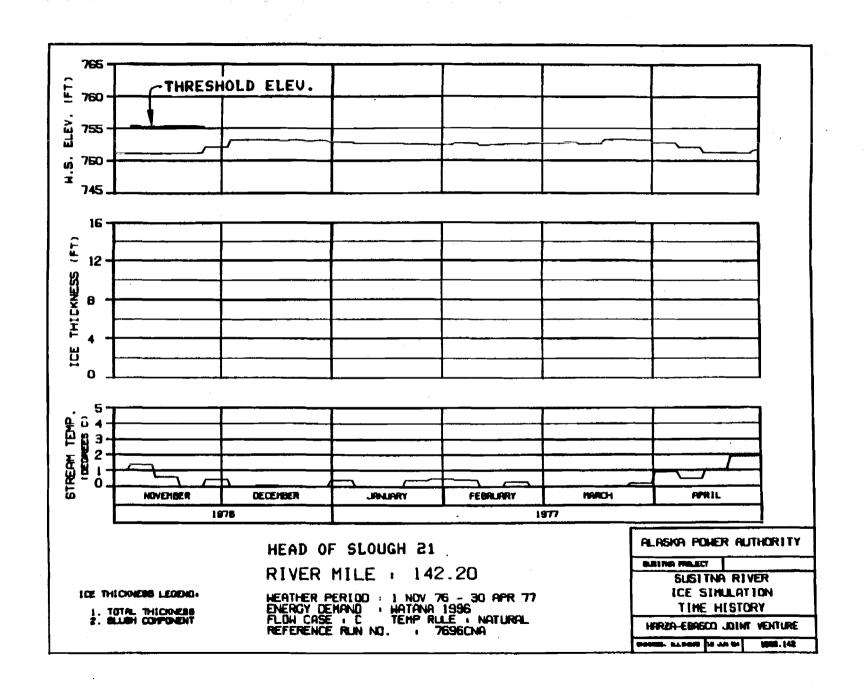




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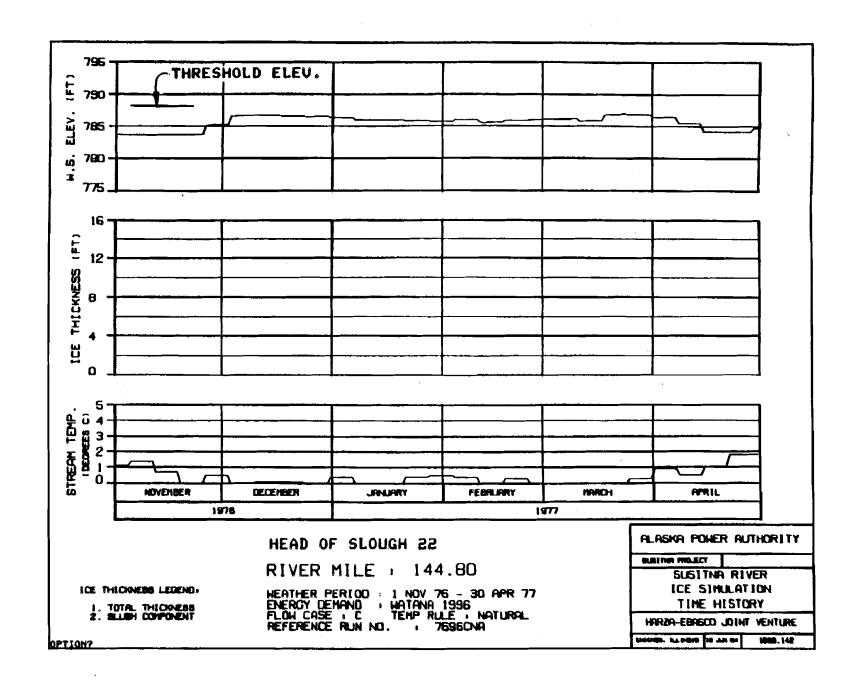
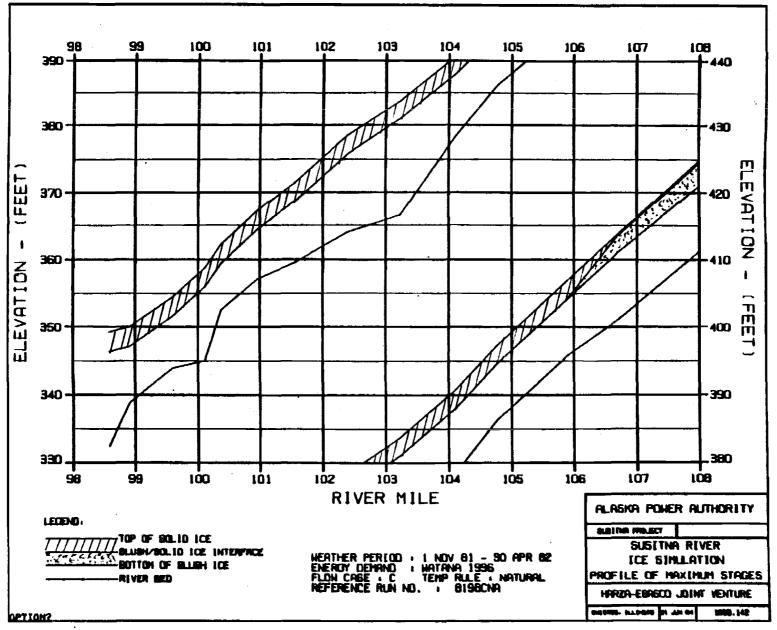
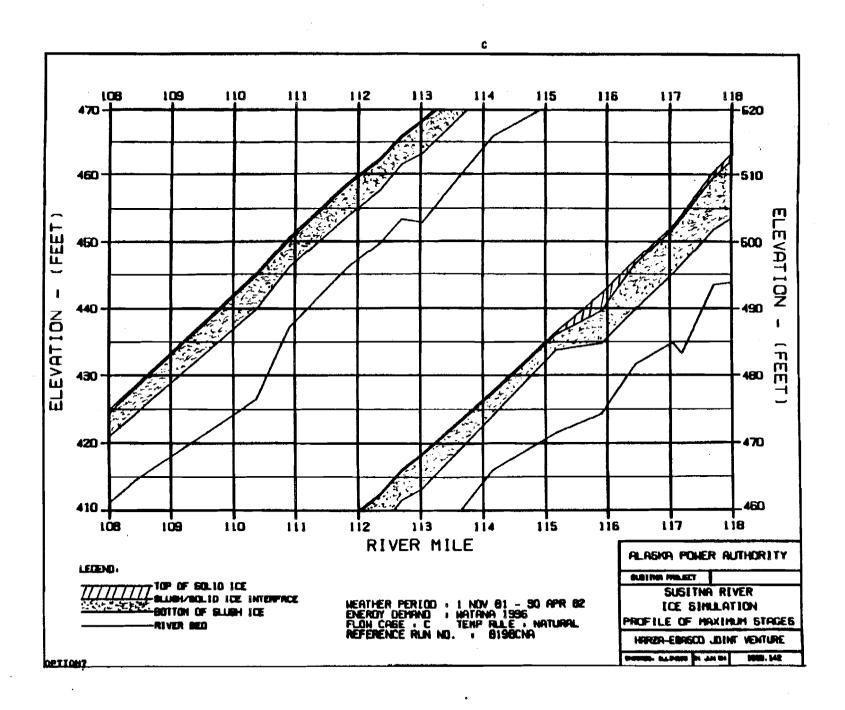


EXHIBIT H





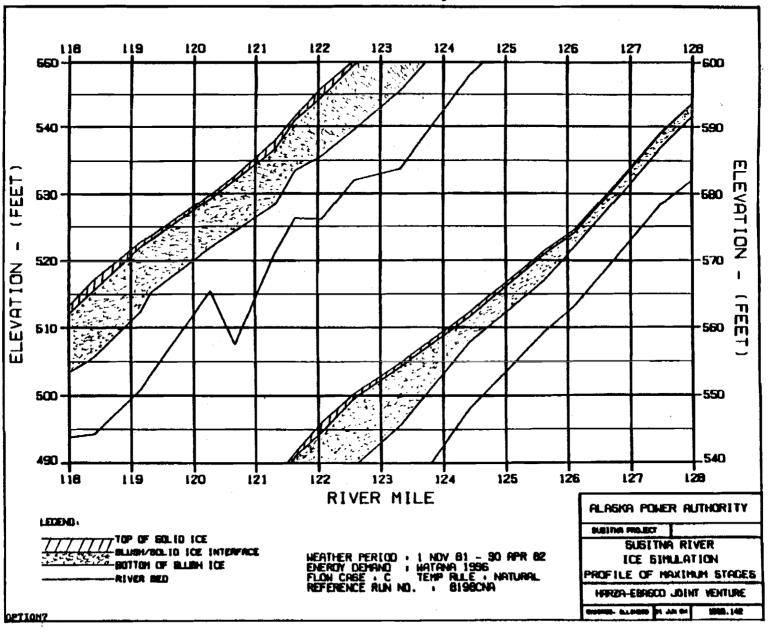




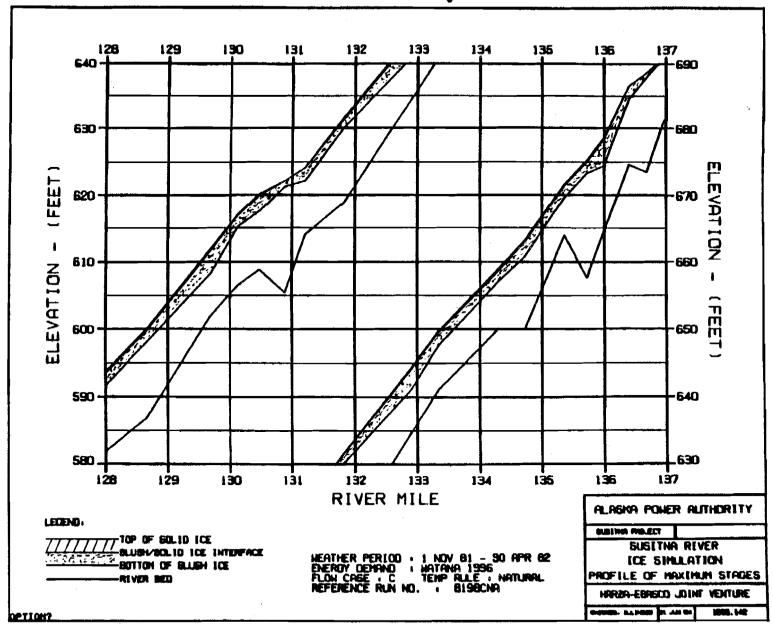
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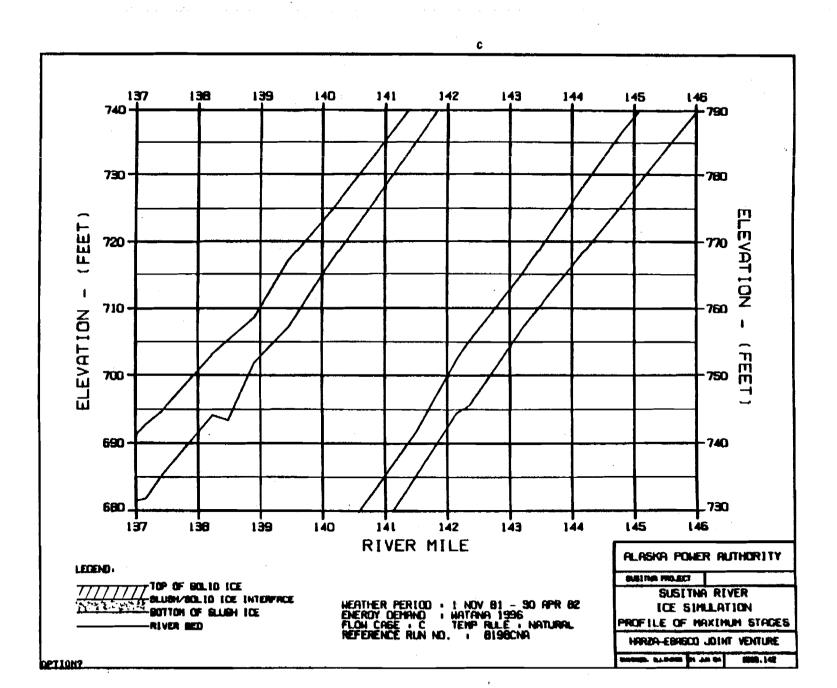
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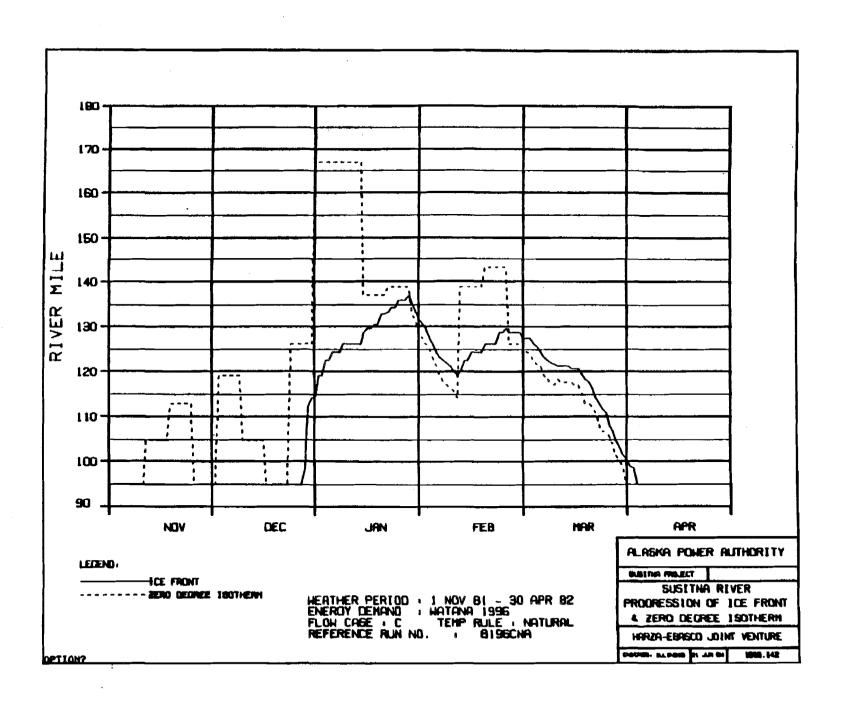




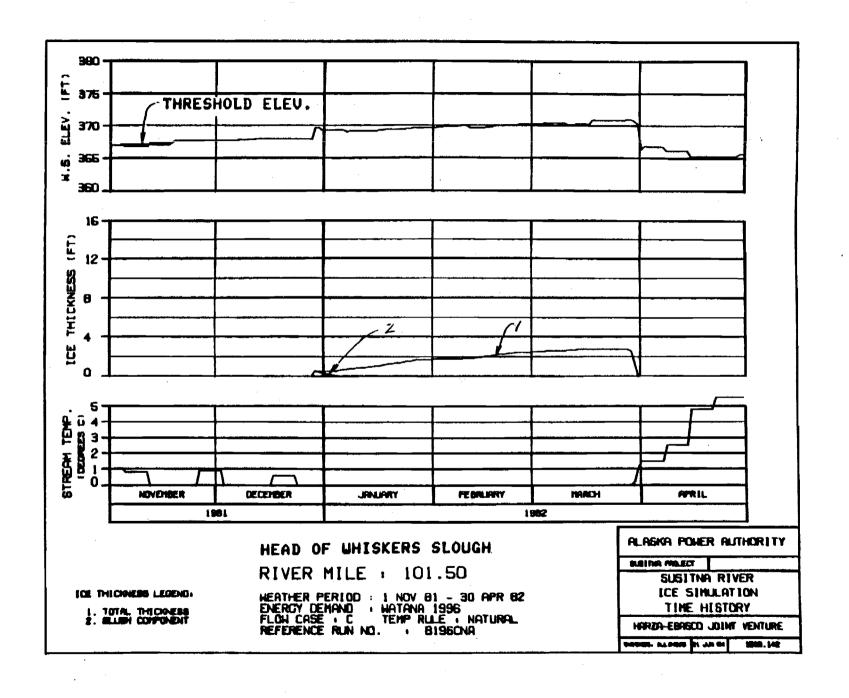


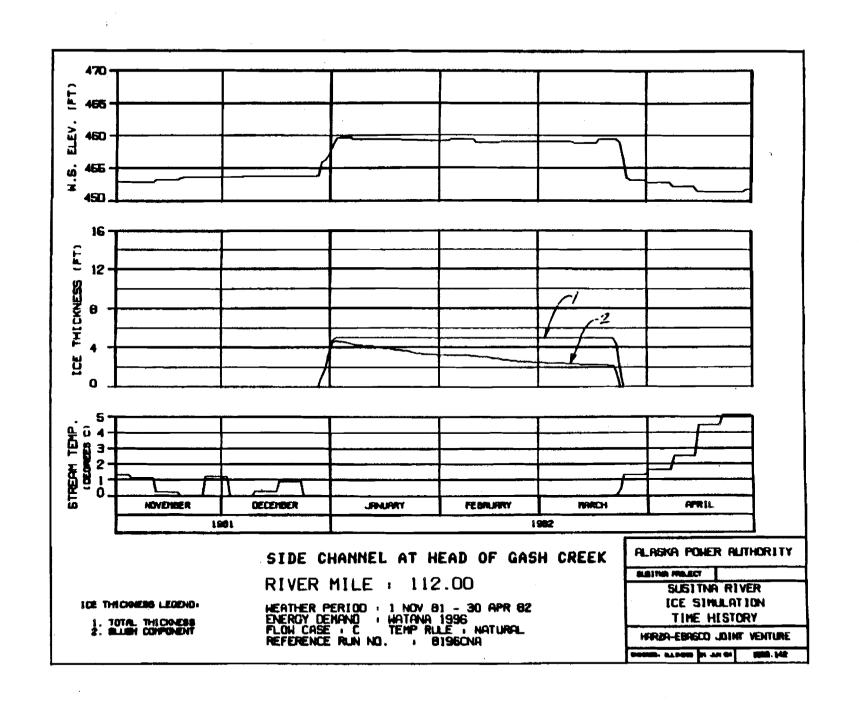


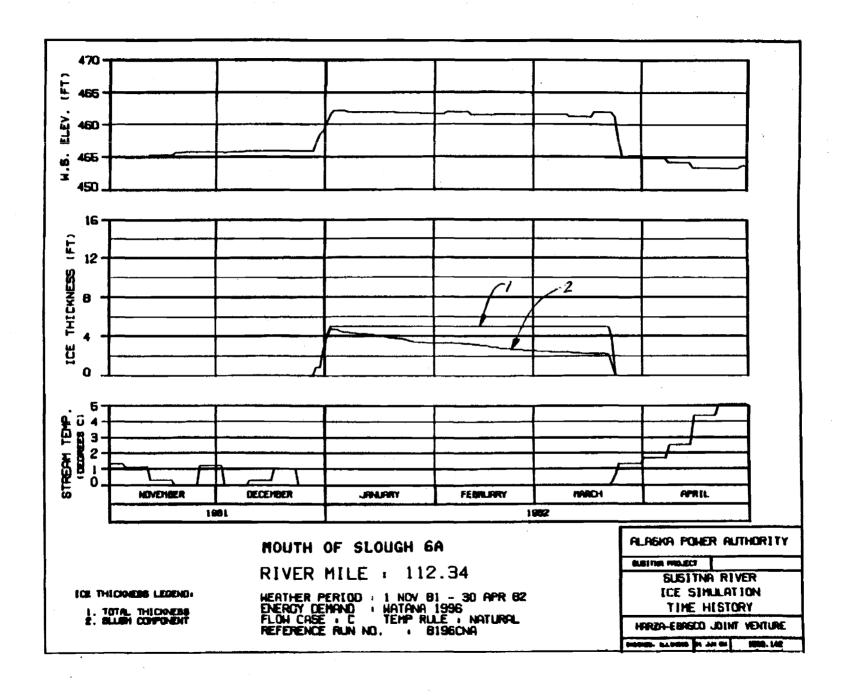


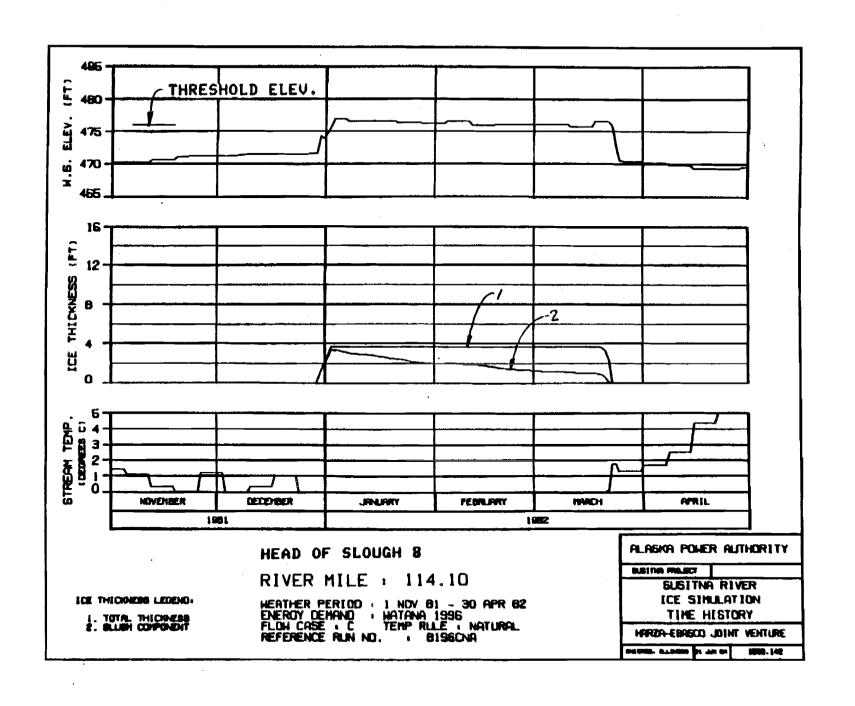


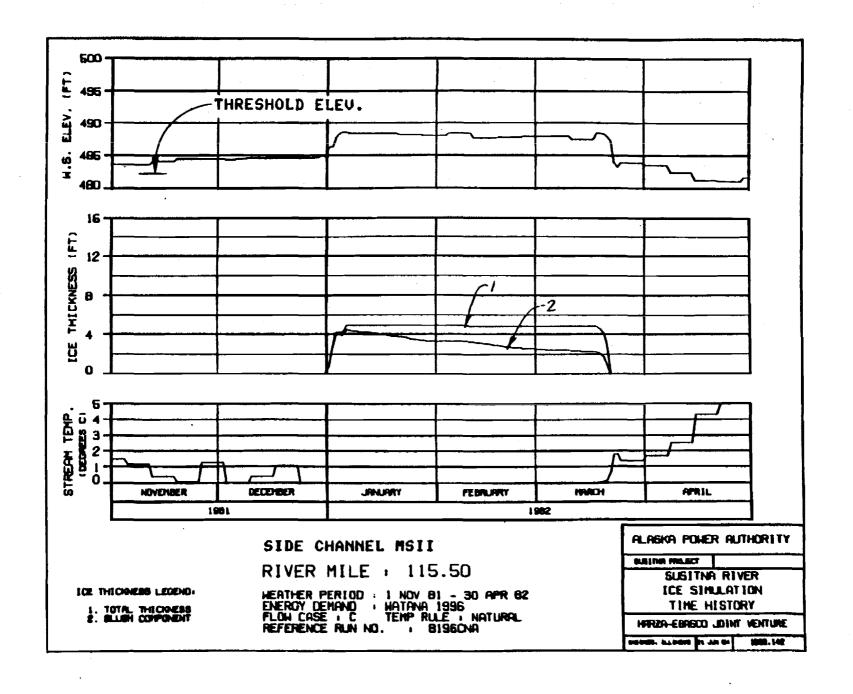
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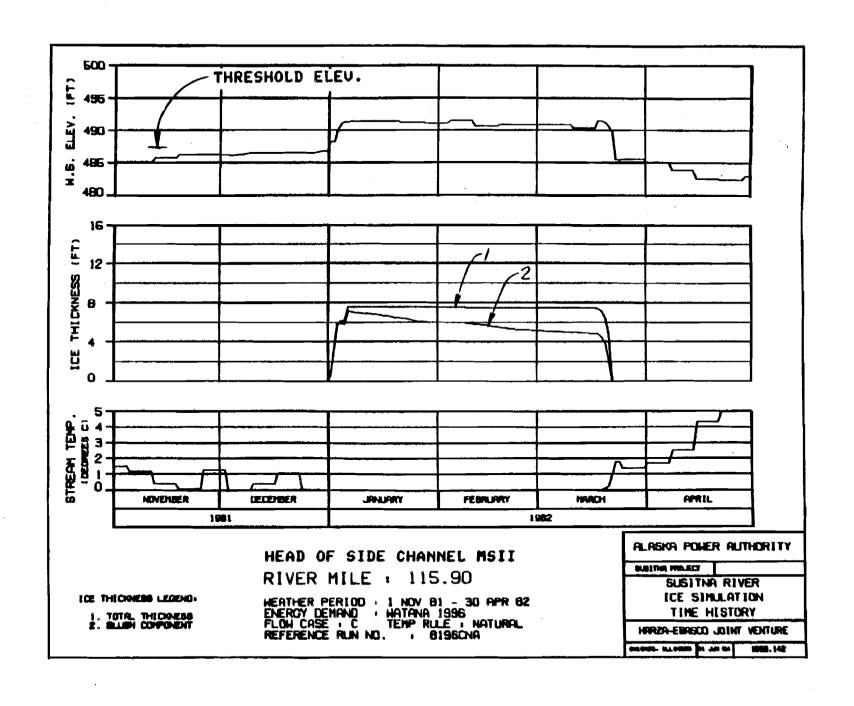


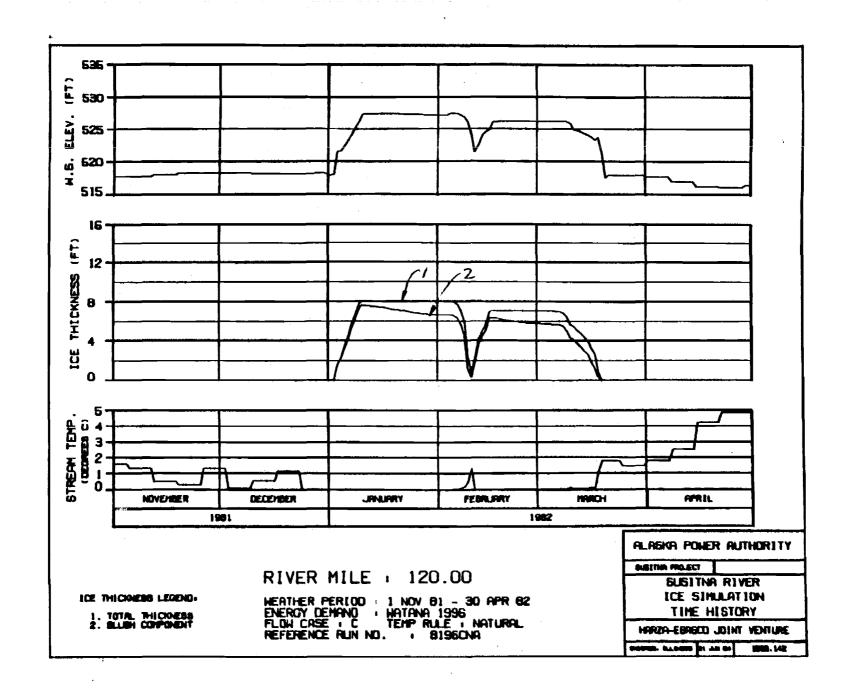


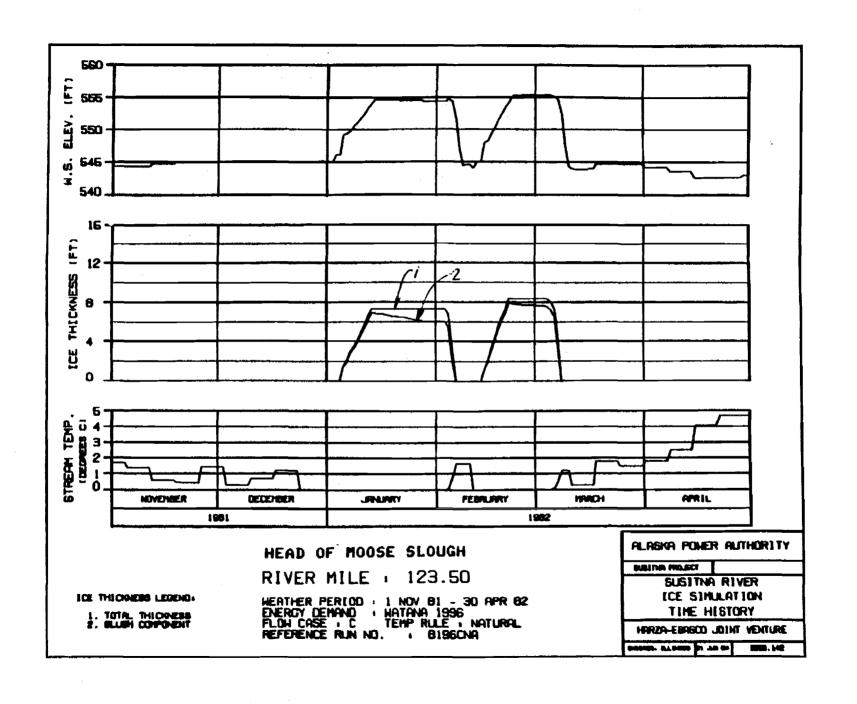


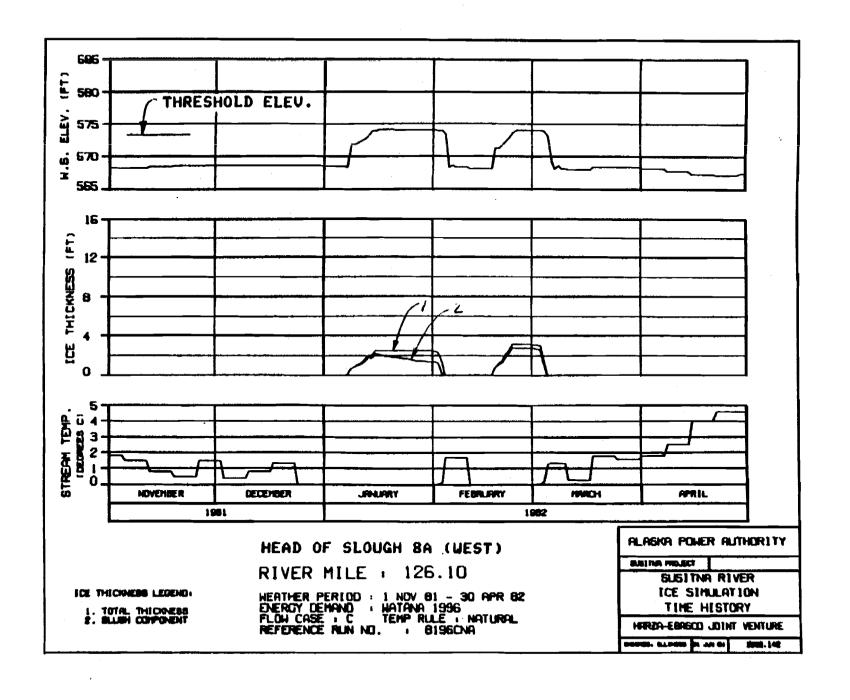


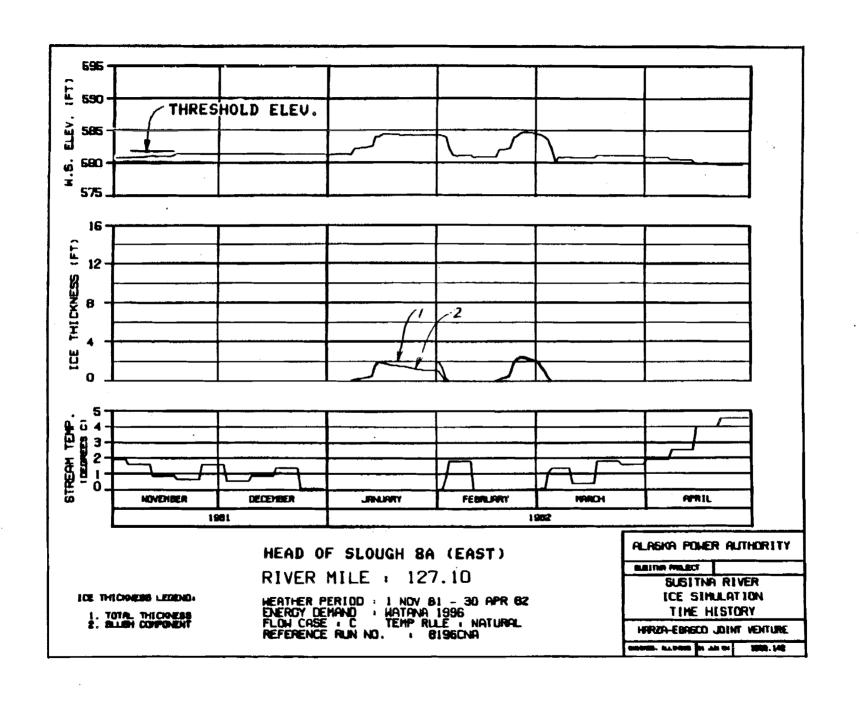


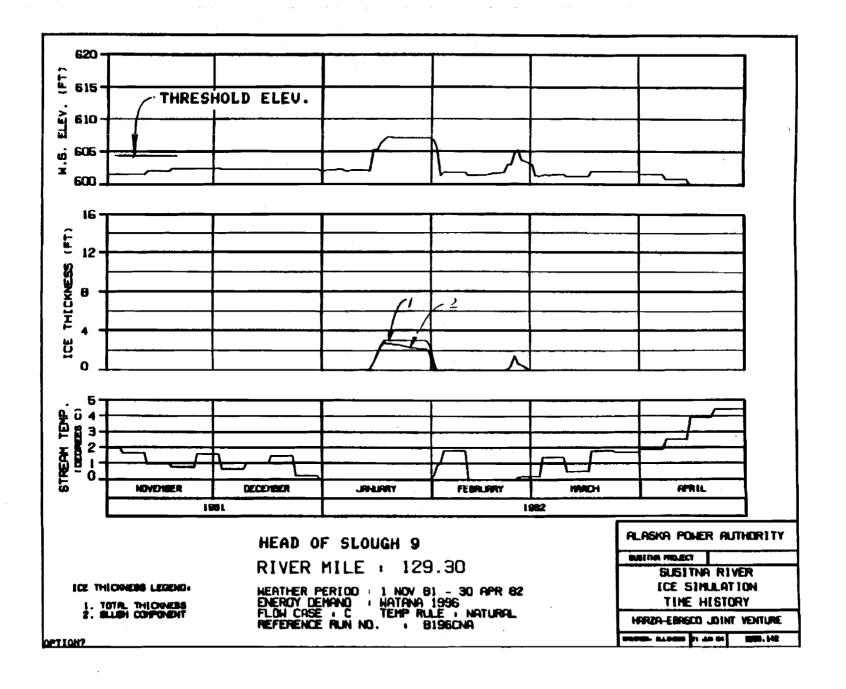


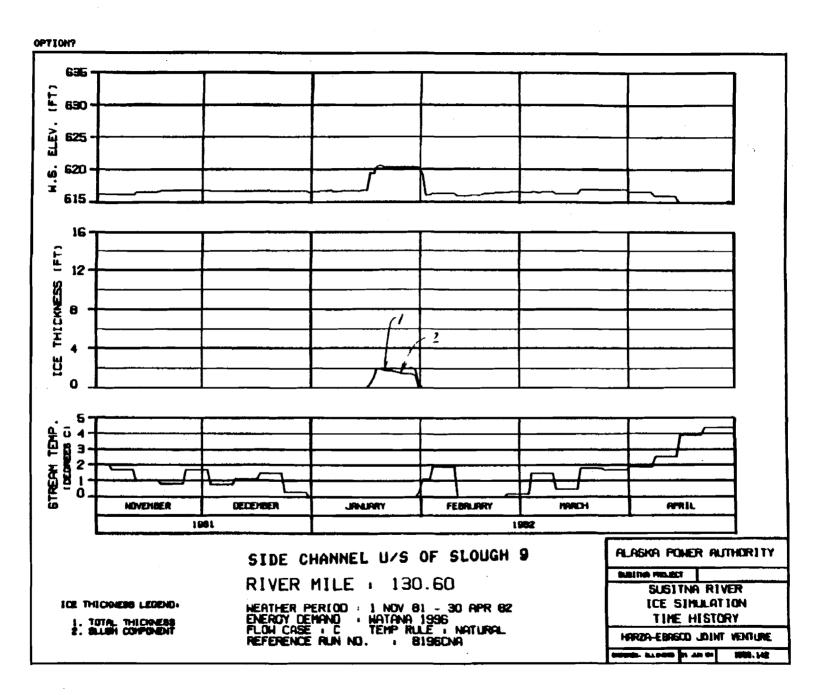




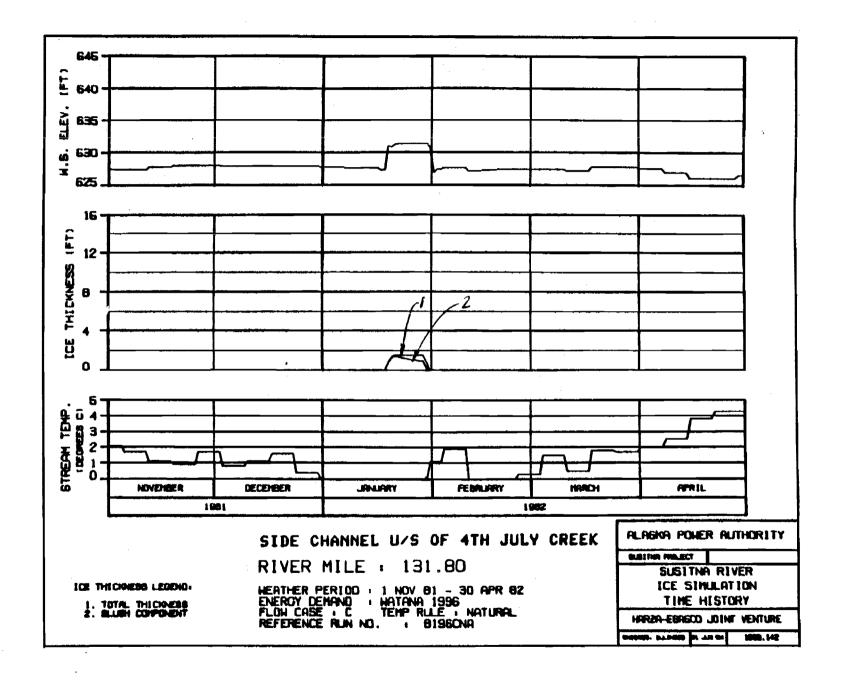


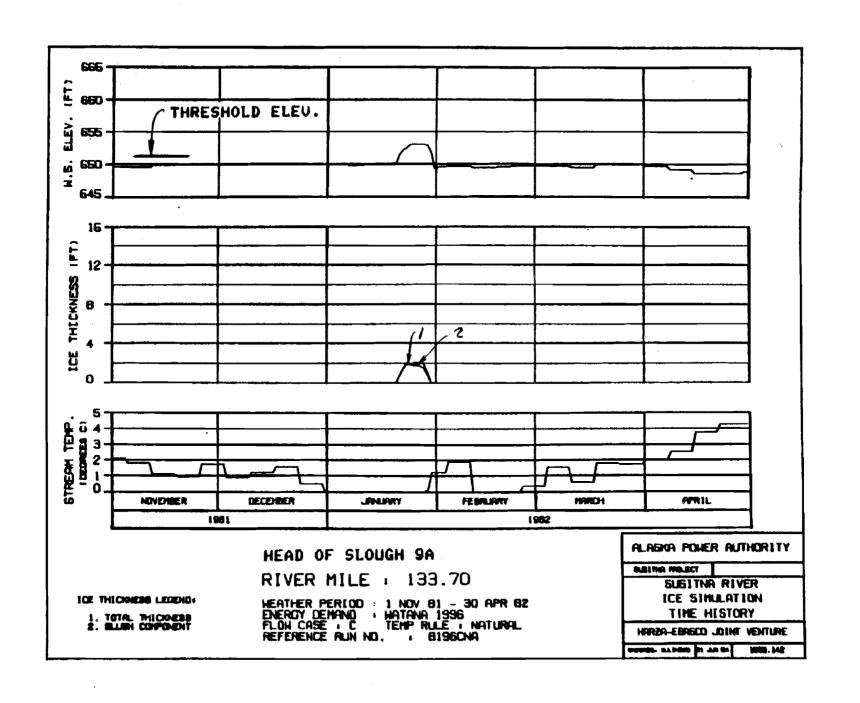


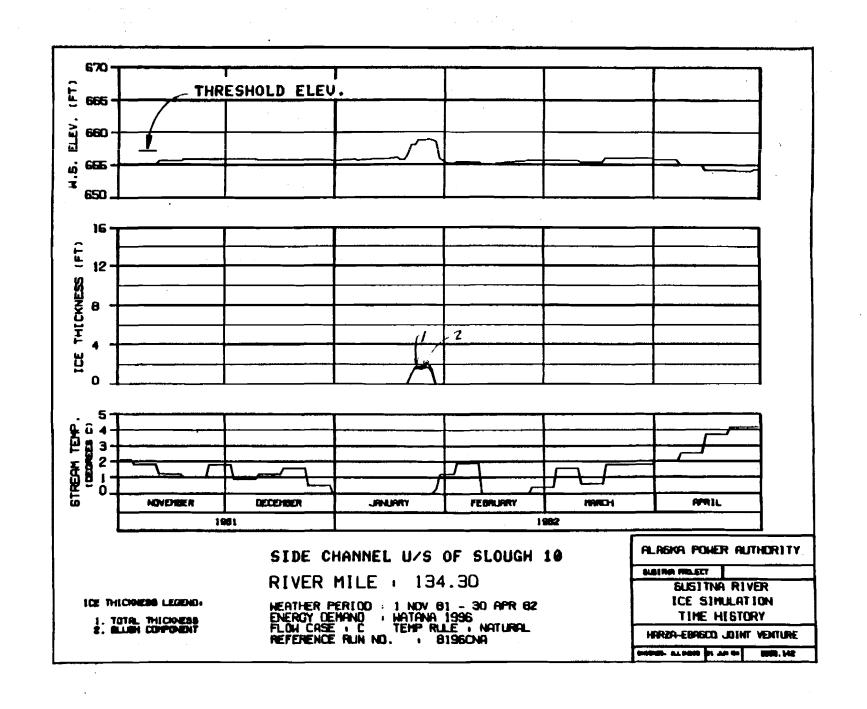


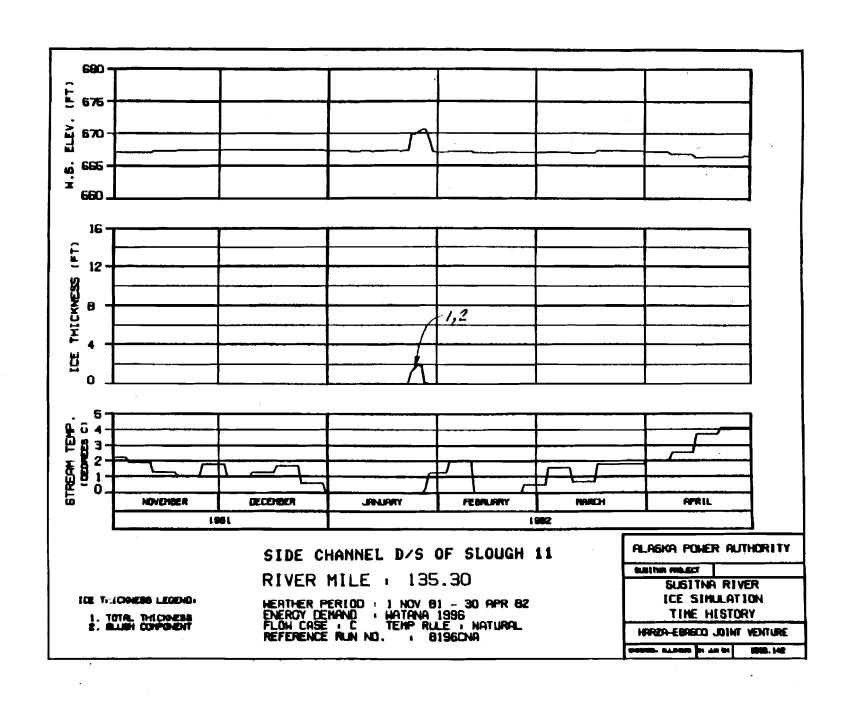


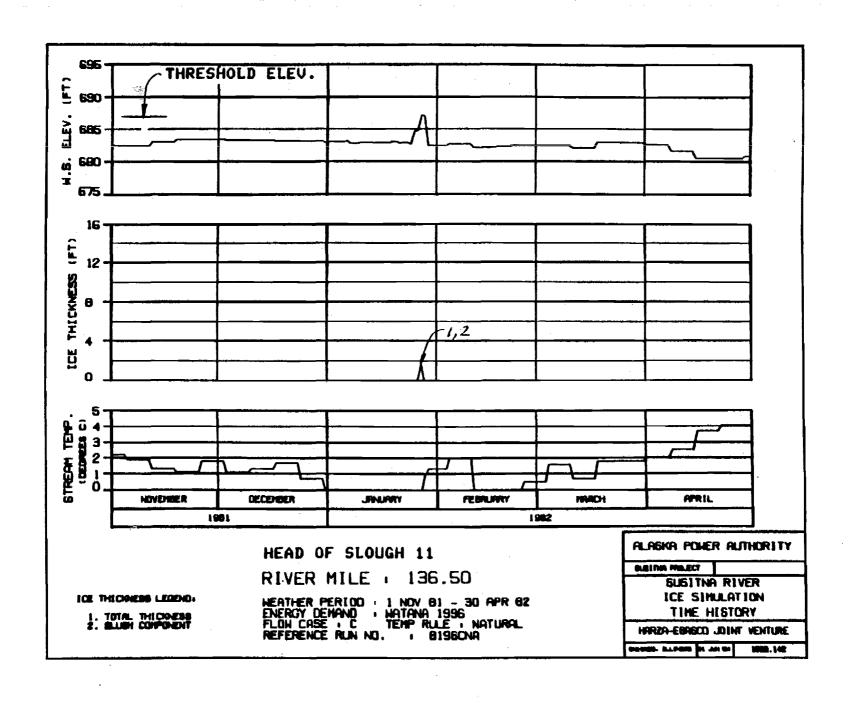
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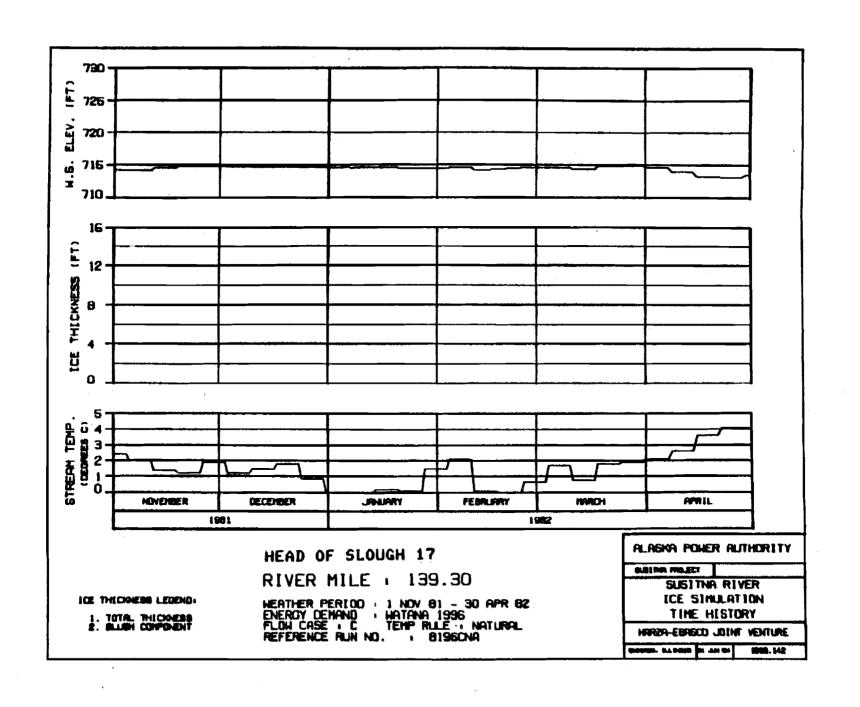


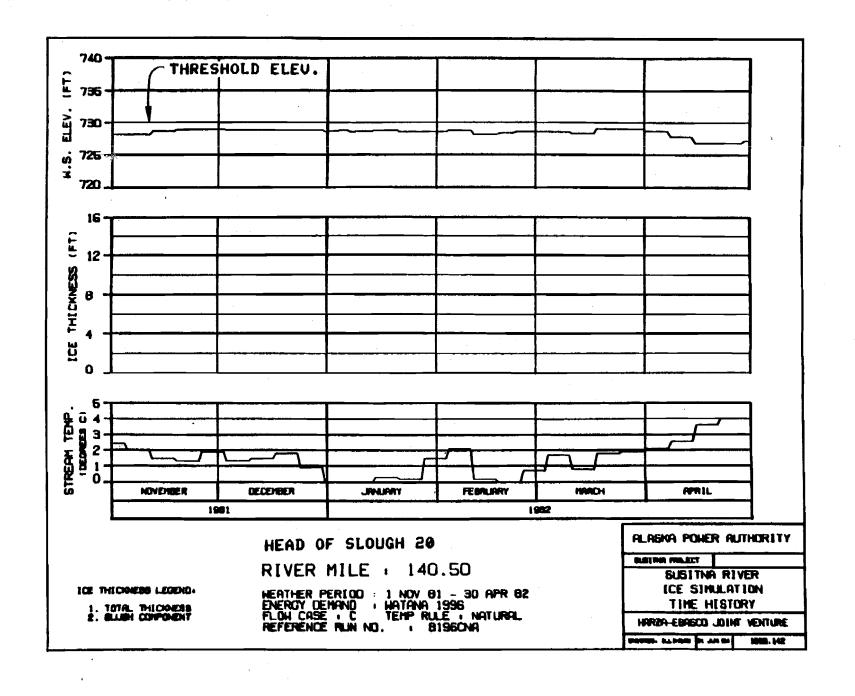


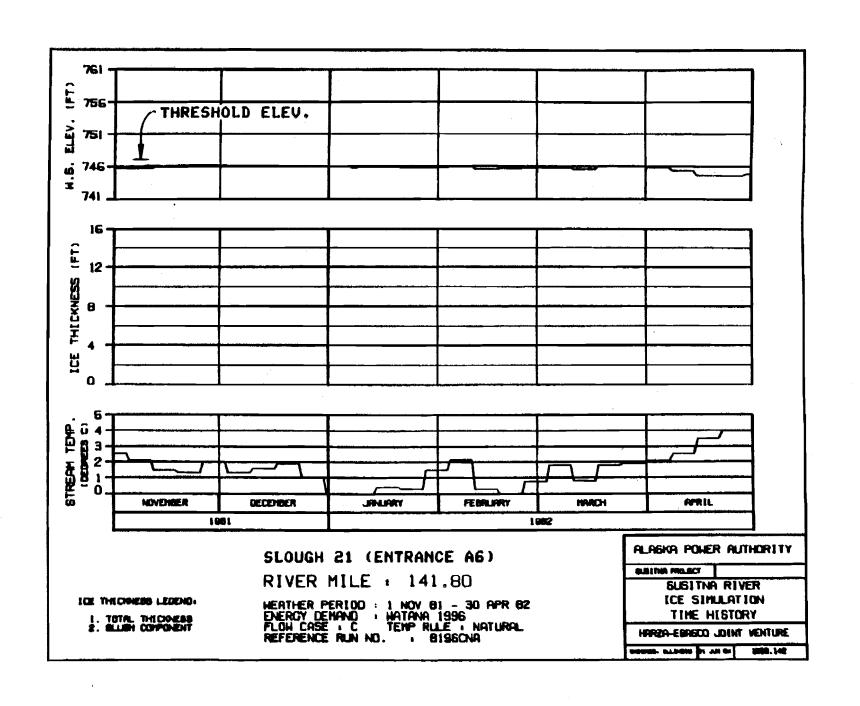
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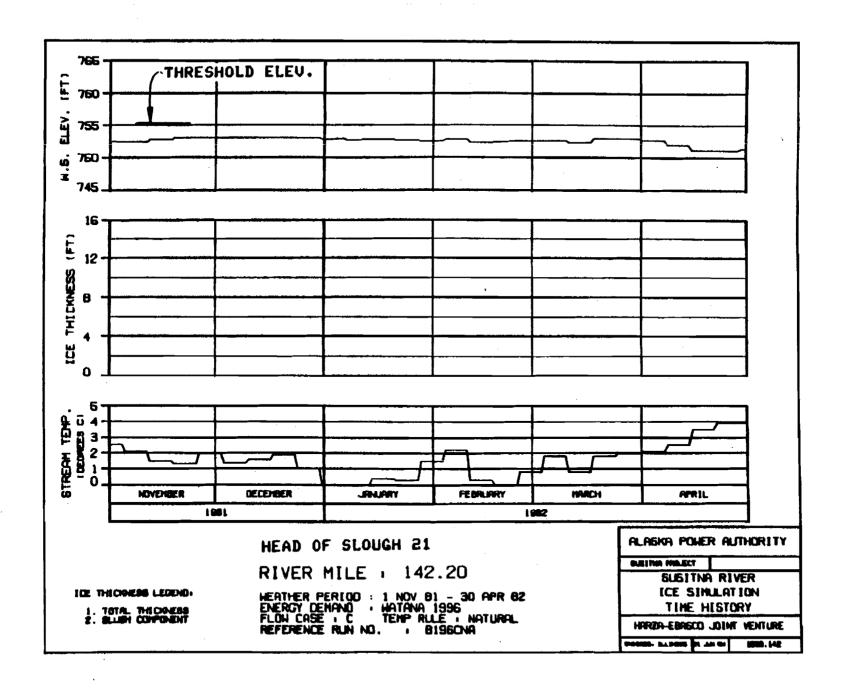




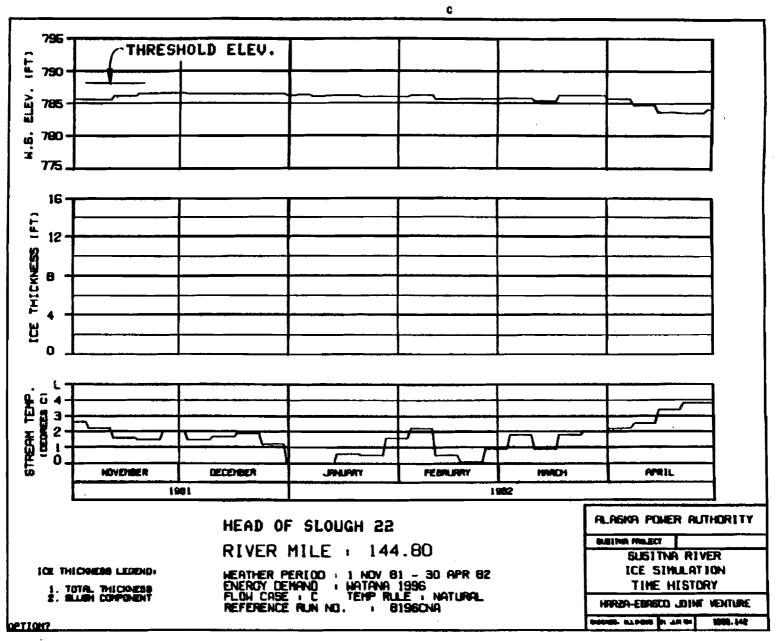




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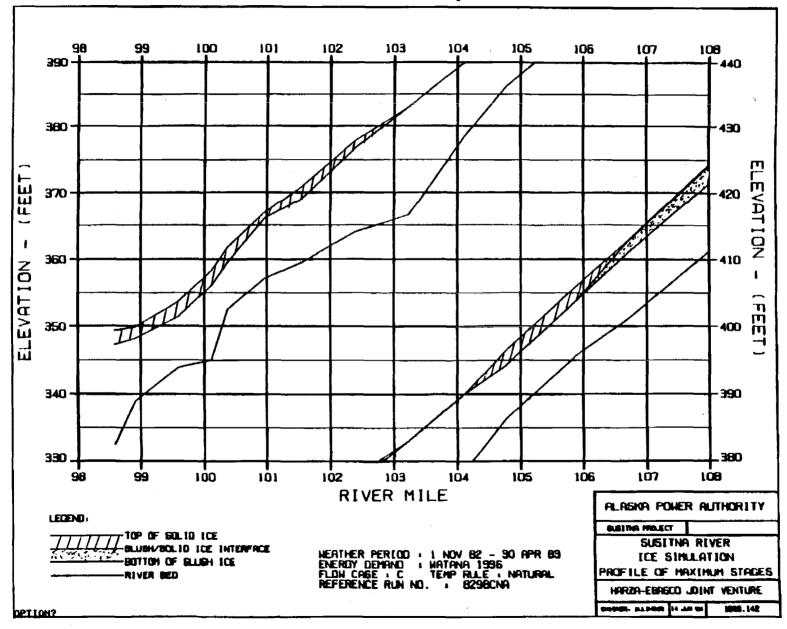


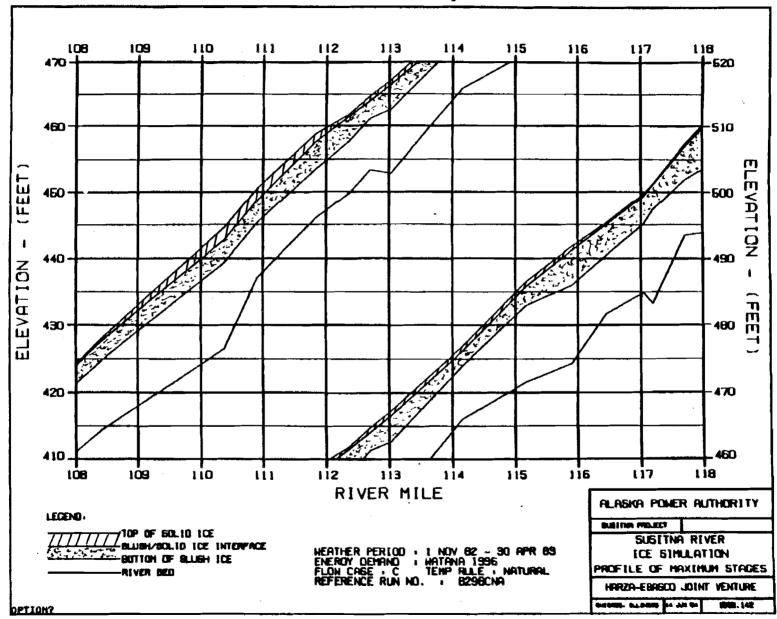


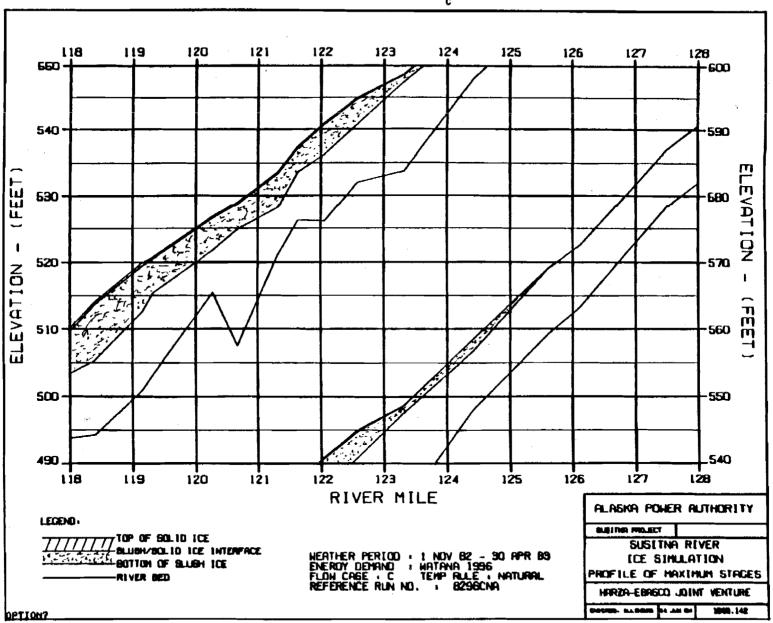
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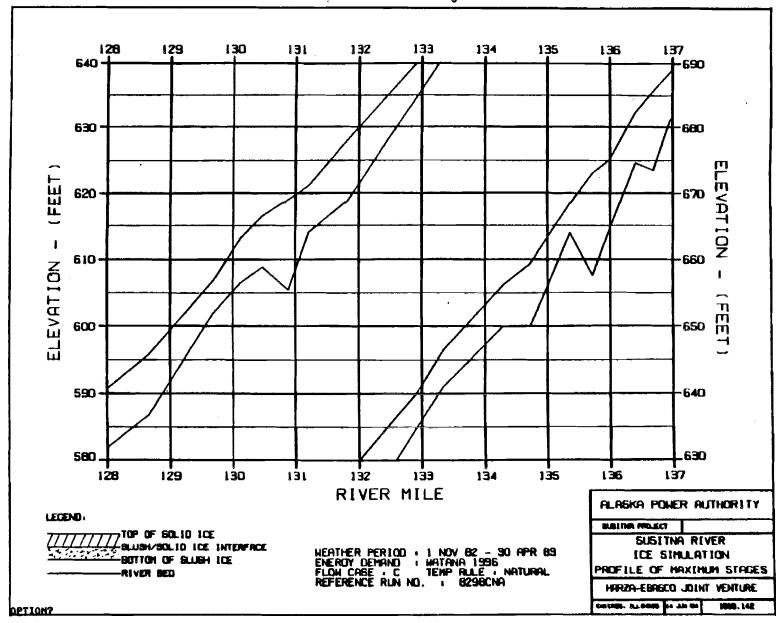




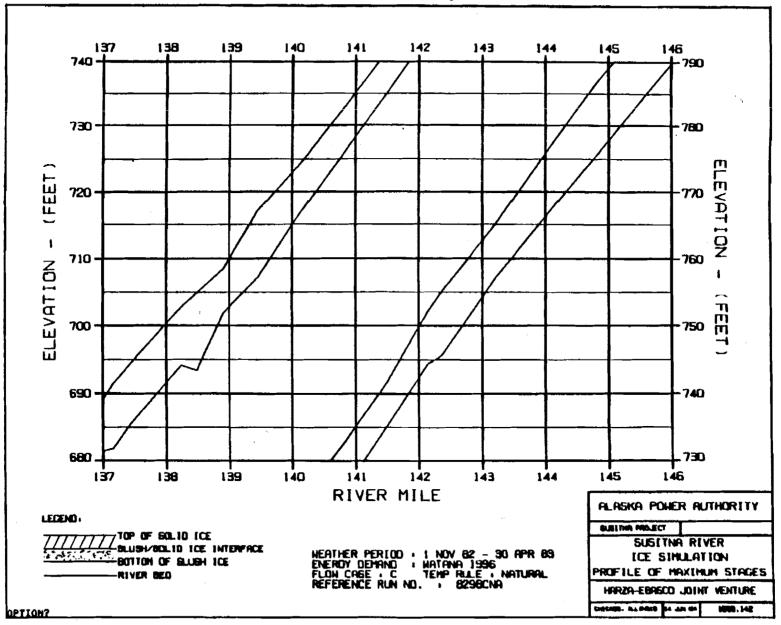


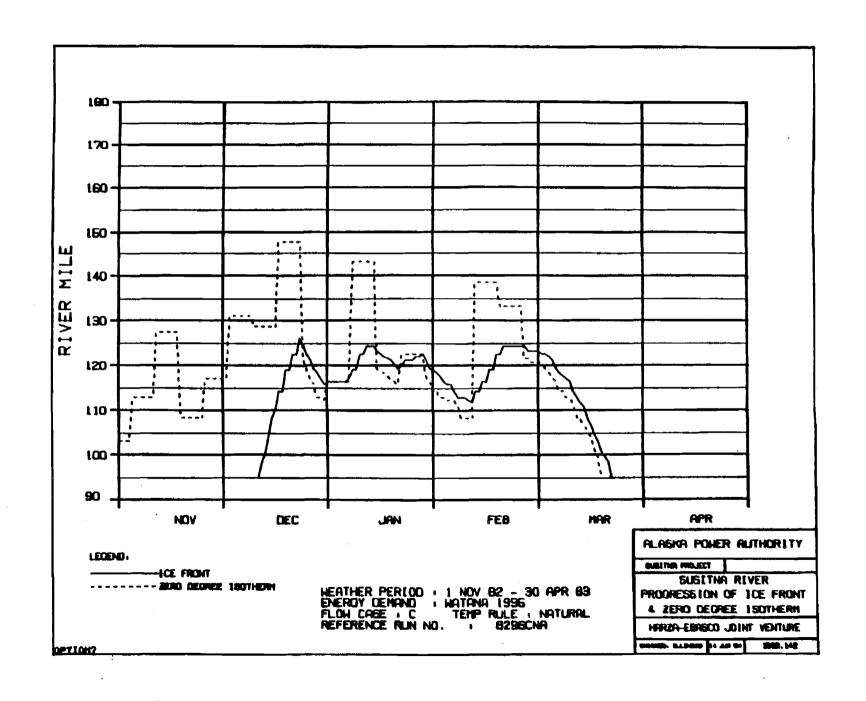


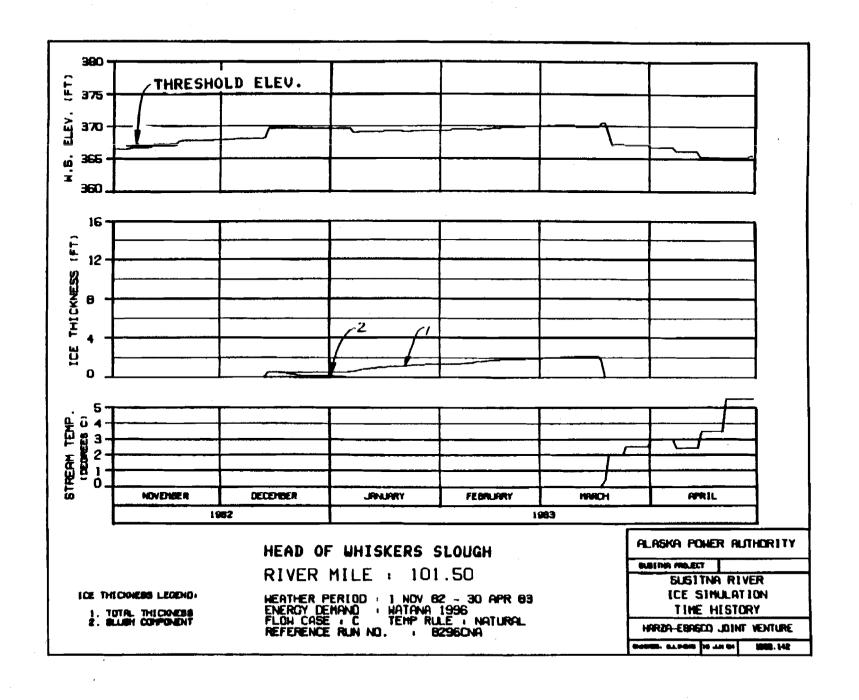
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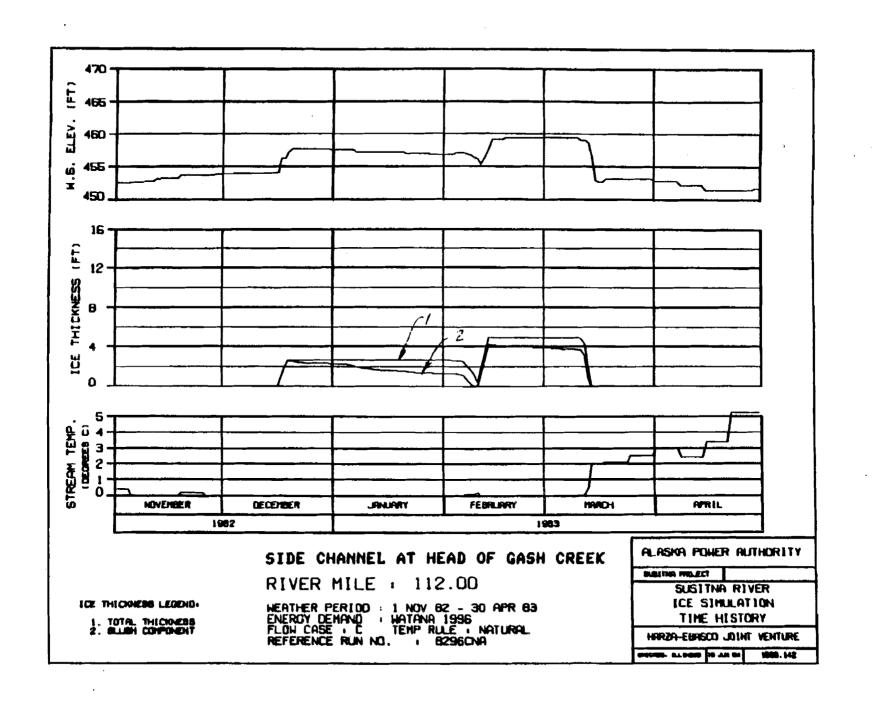




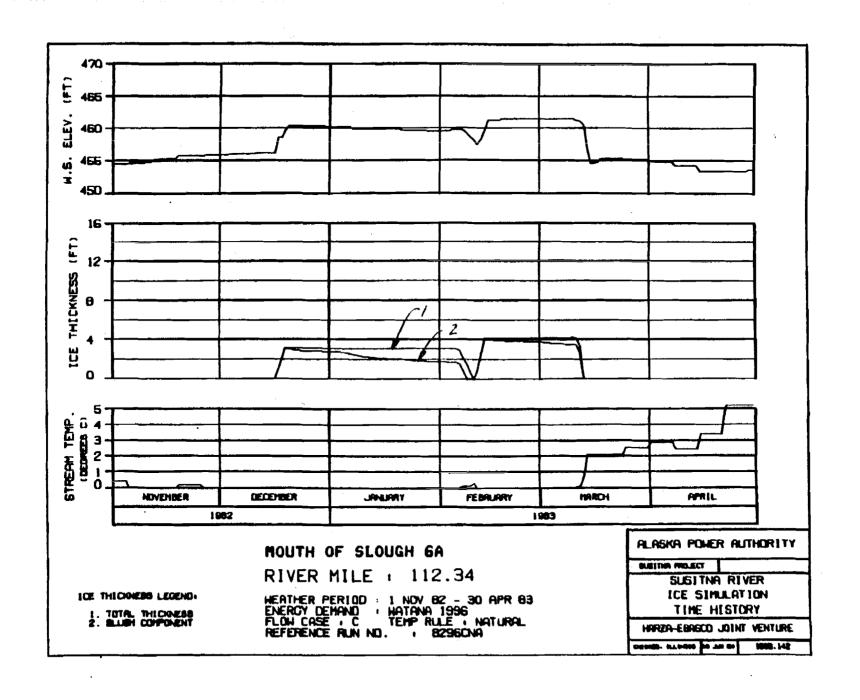


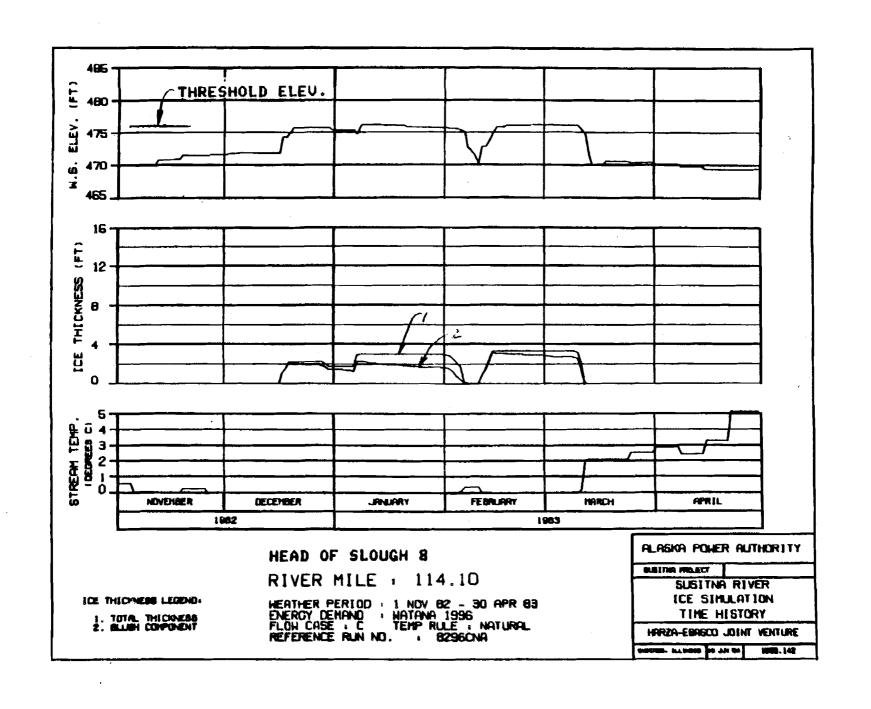


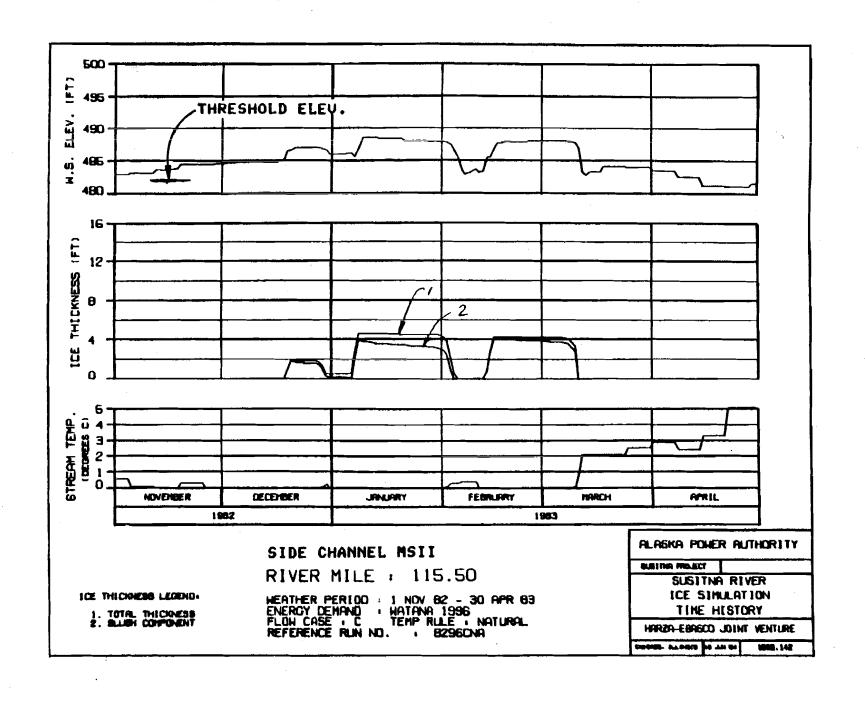


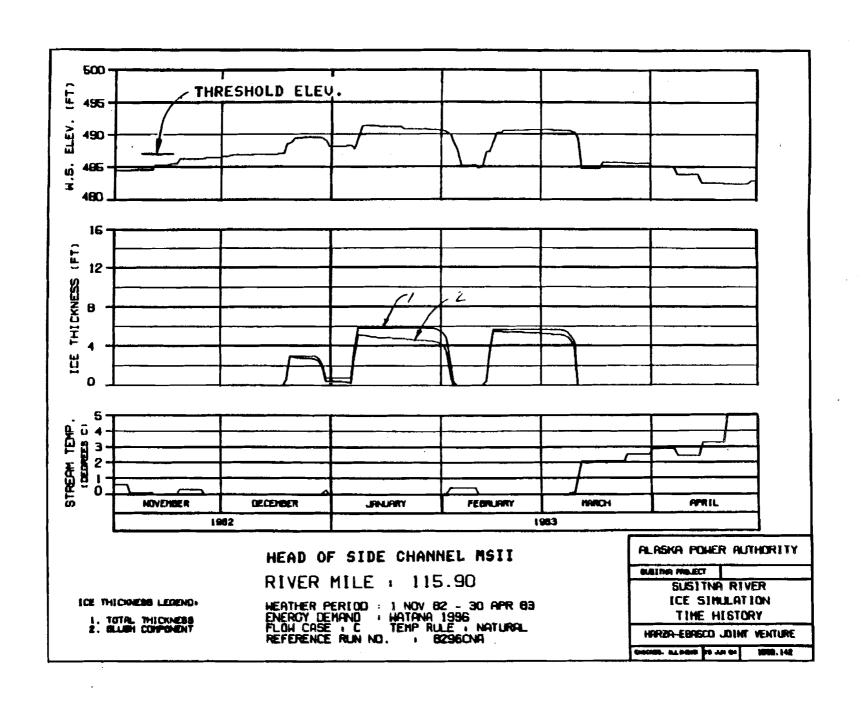


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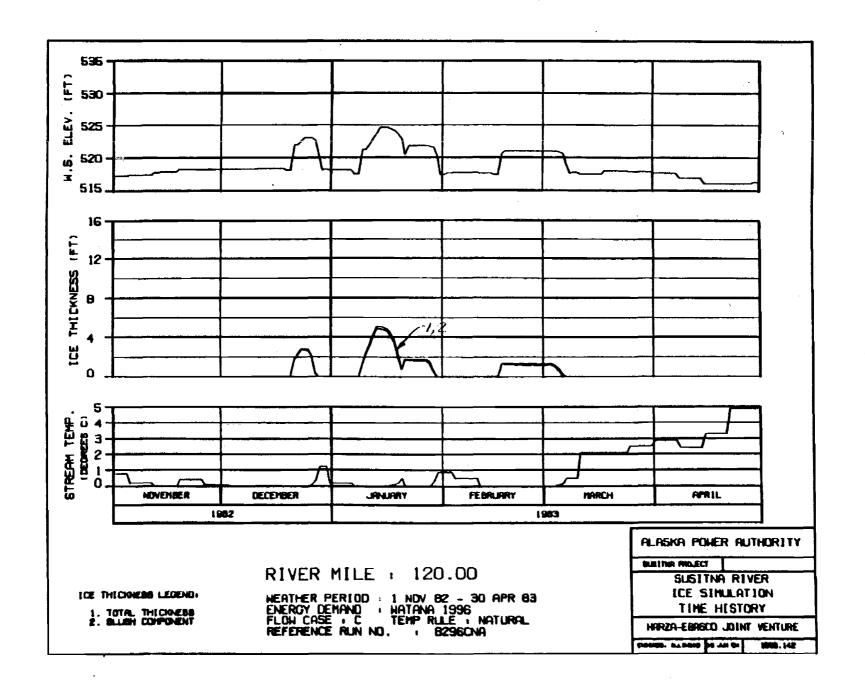


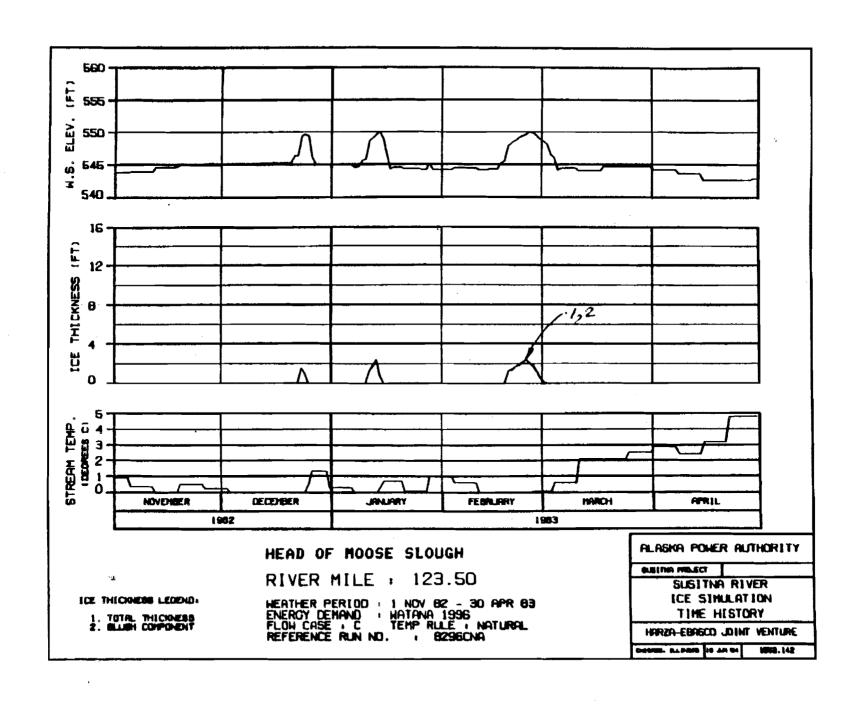


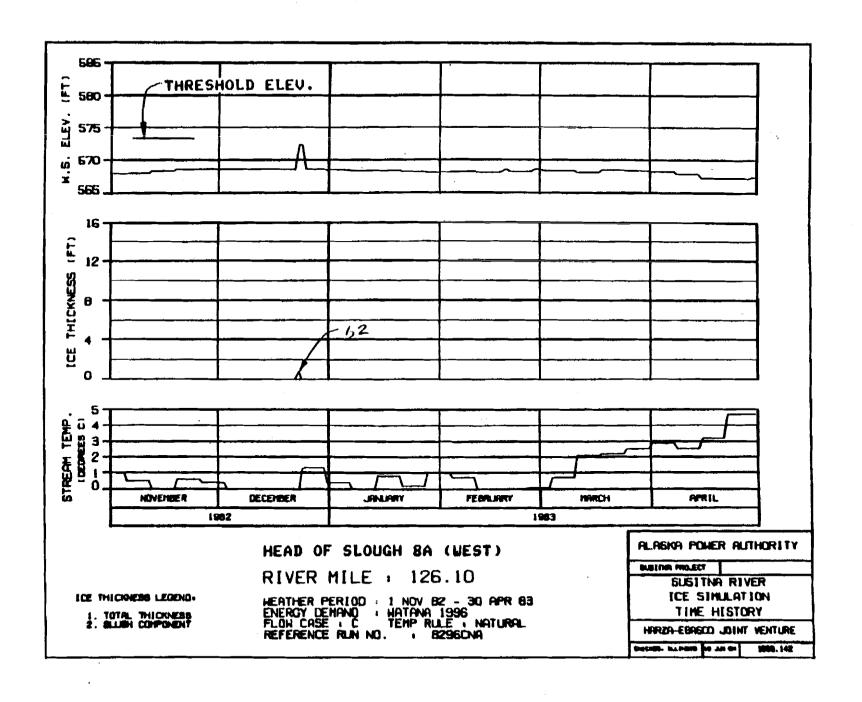


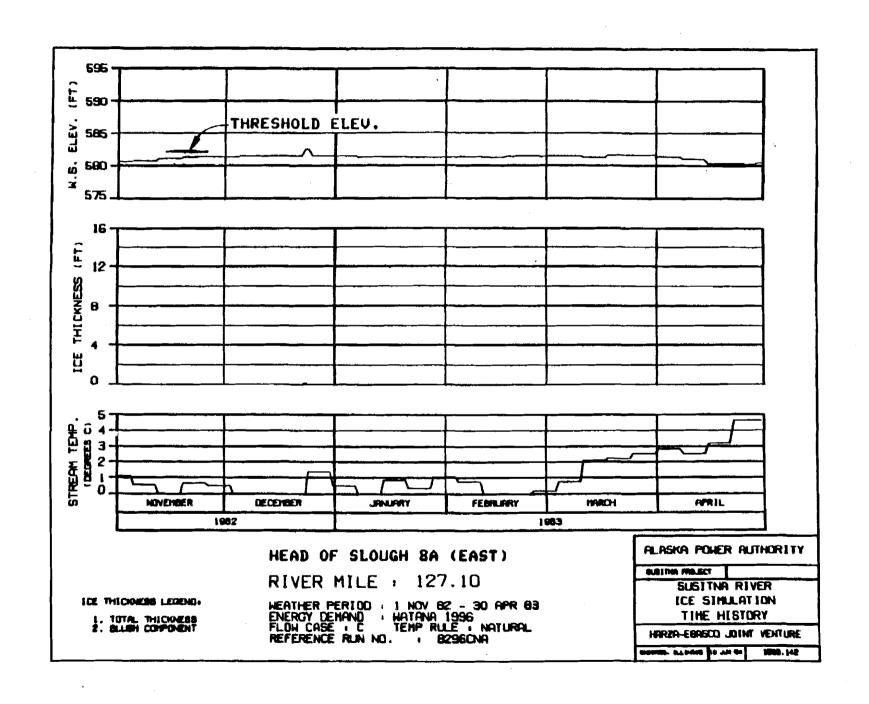


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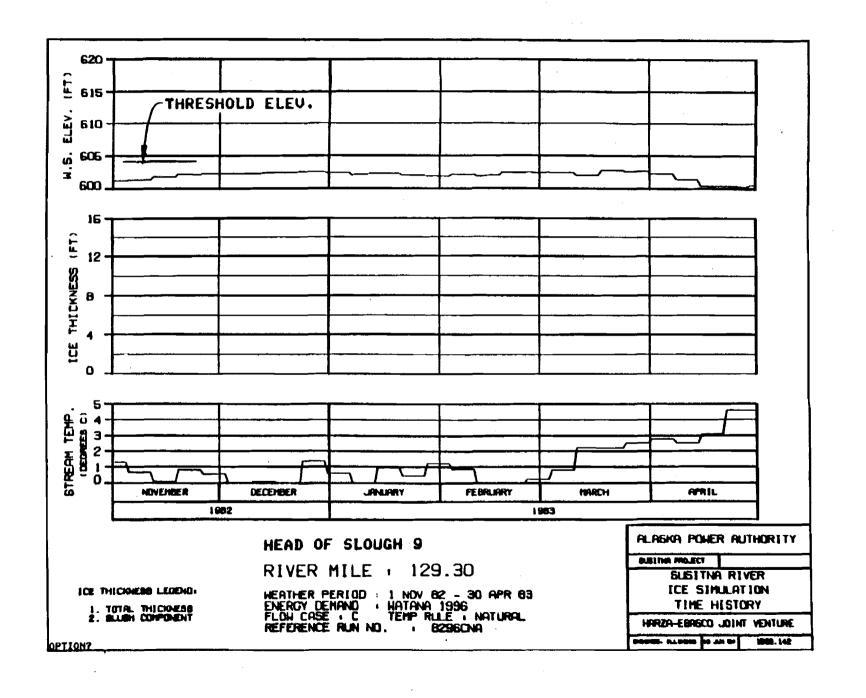


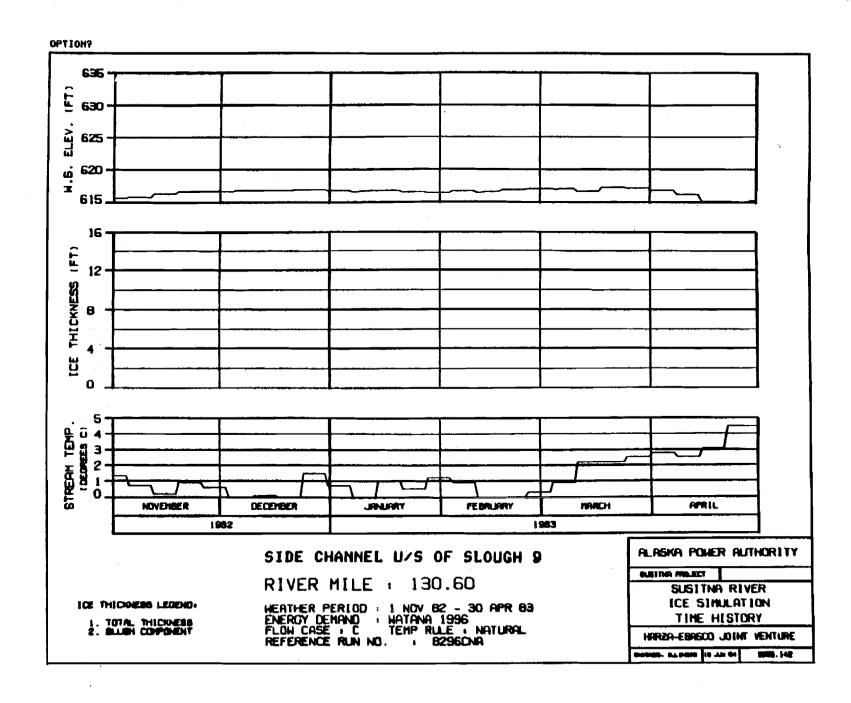




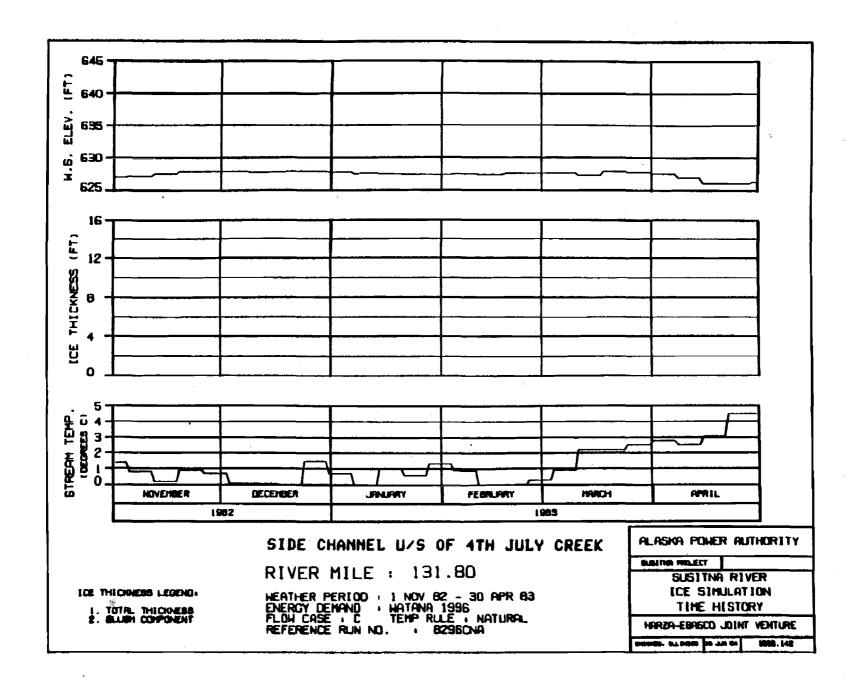


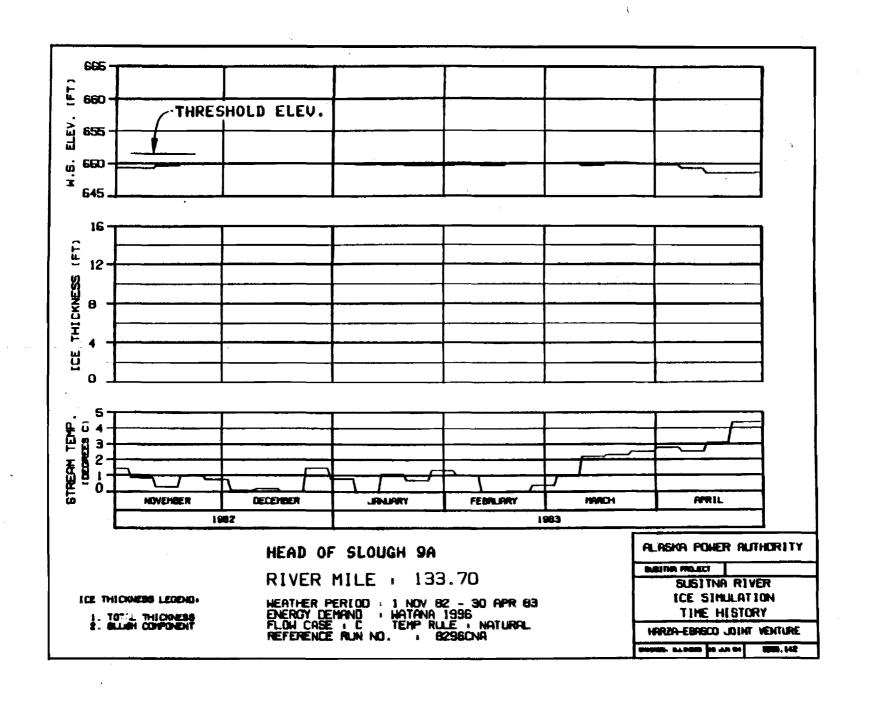
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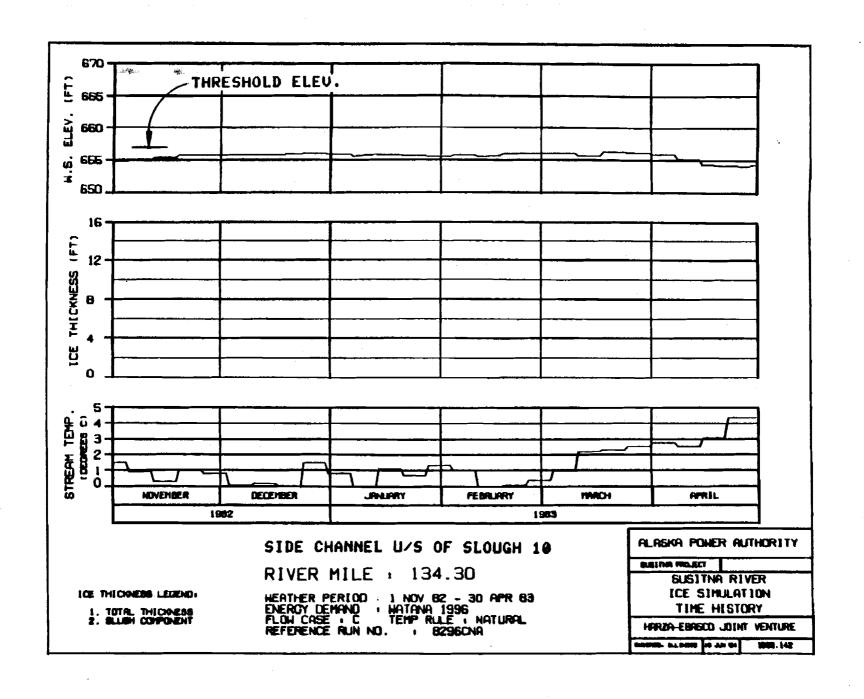


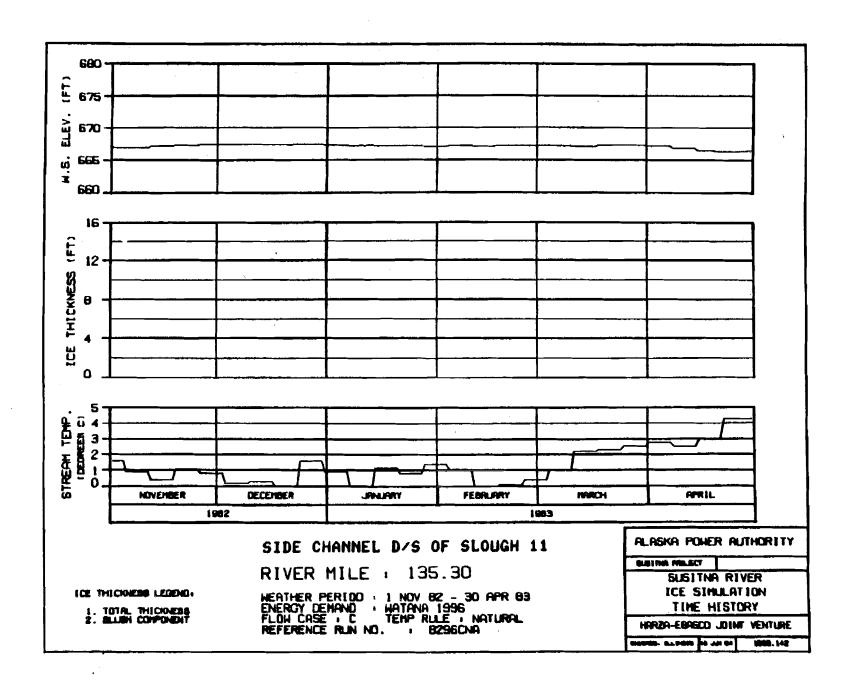
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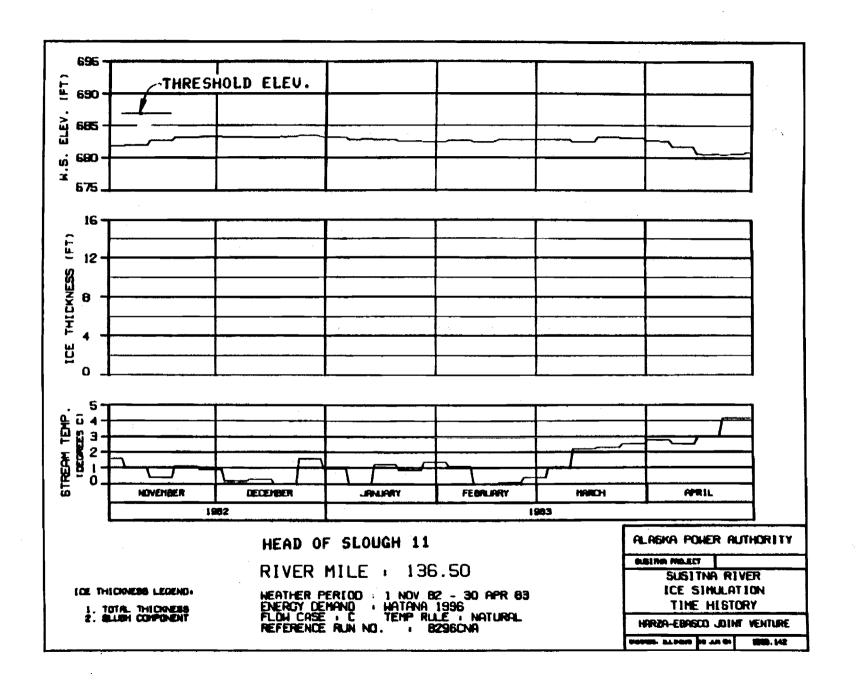


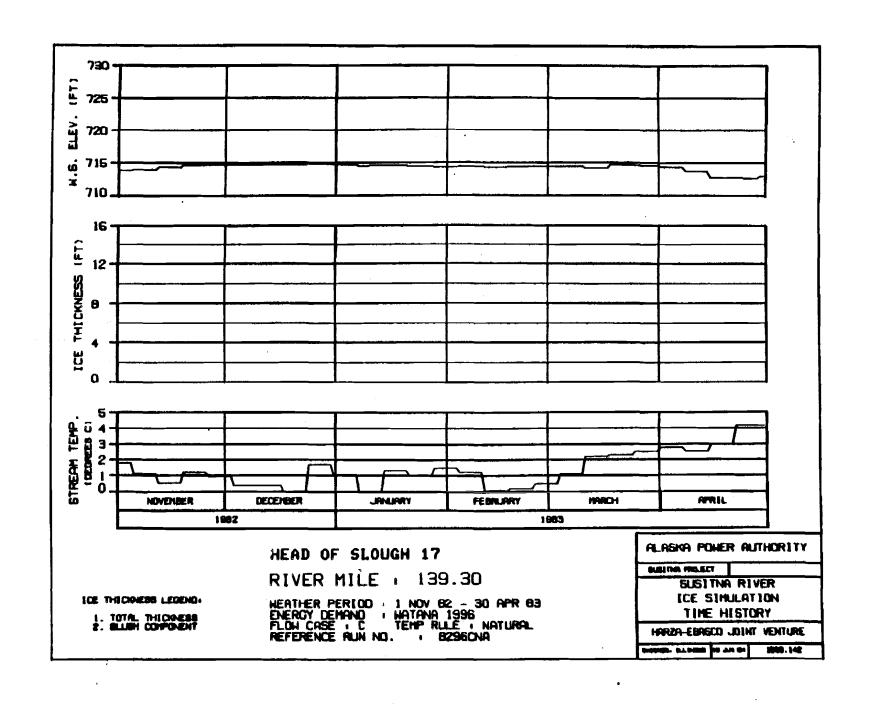
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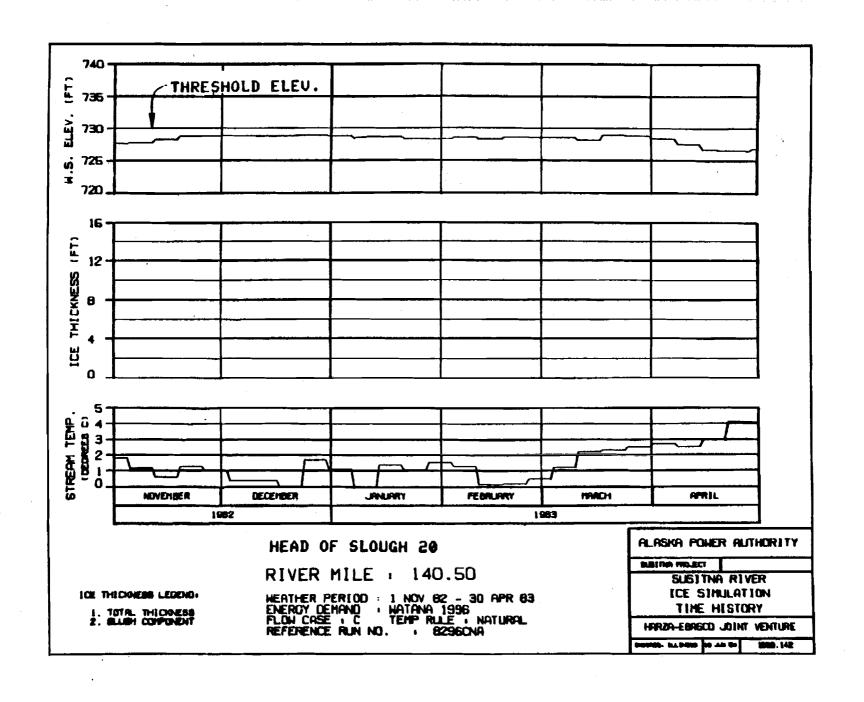


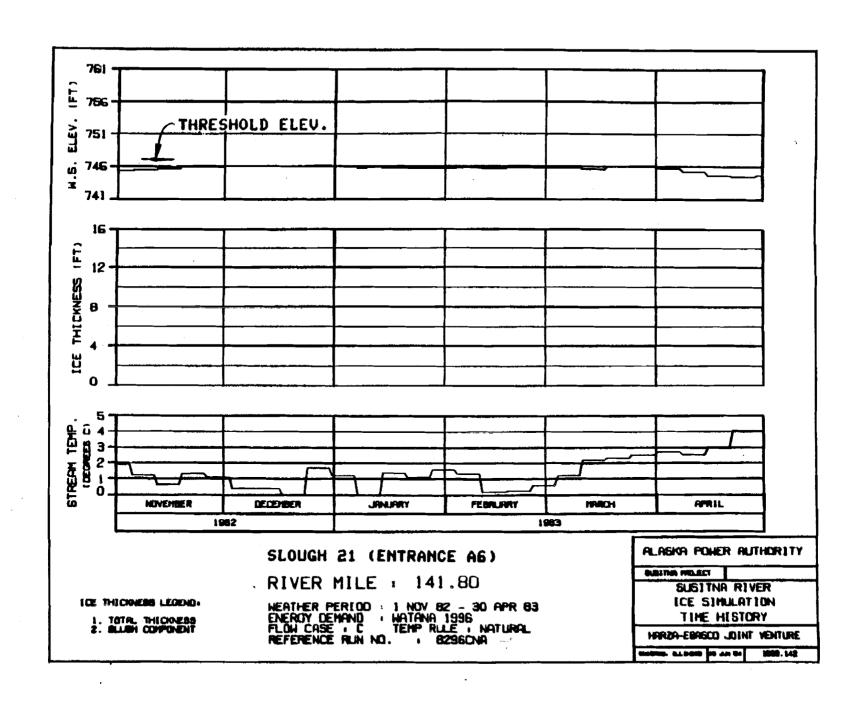


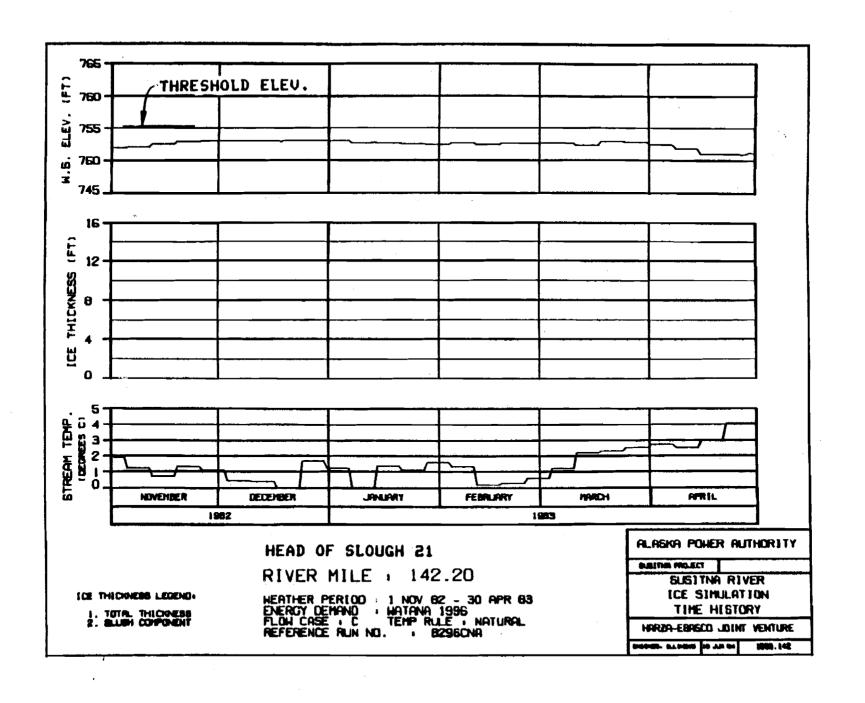
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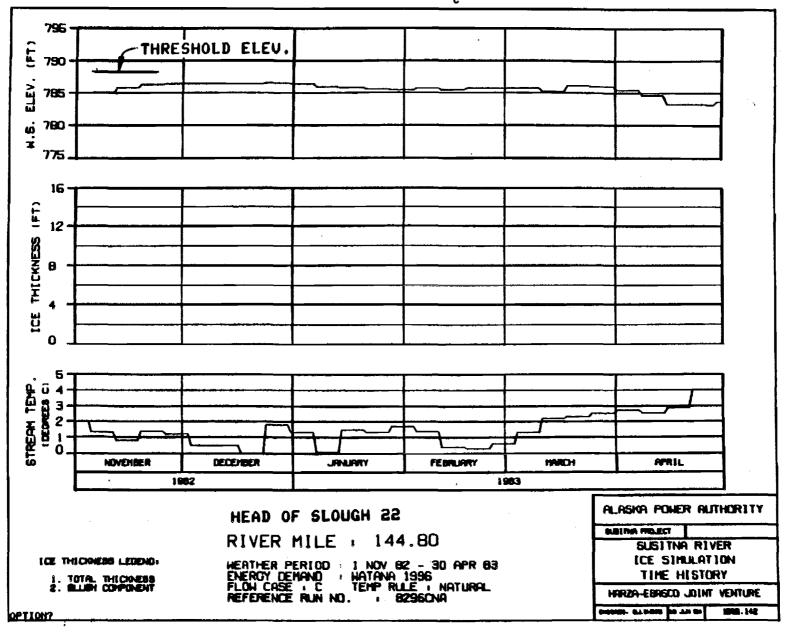








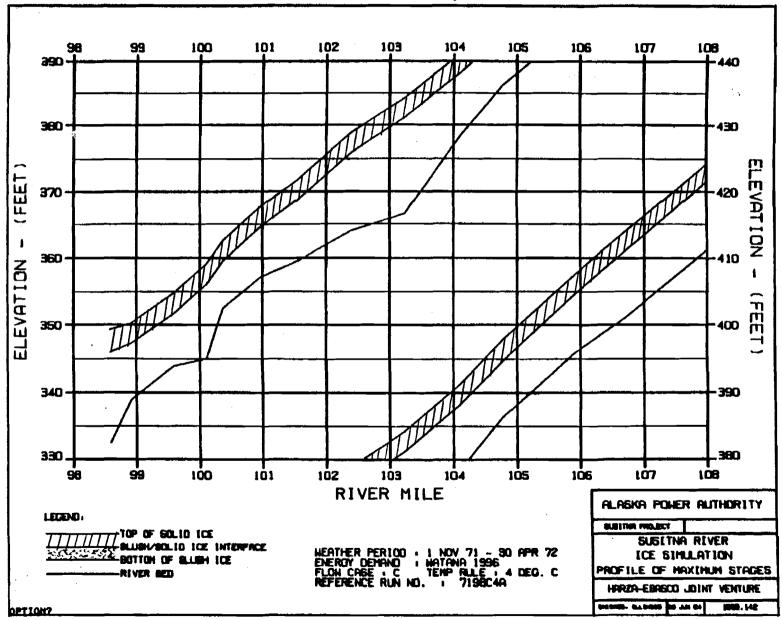


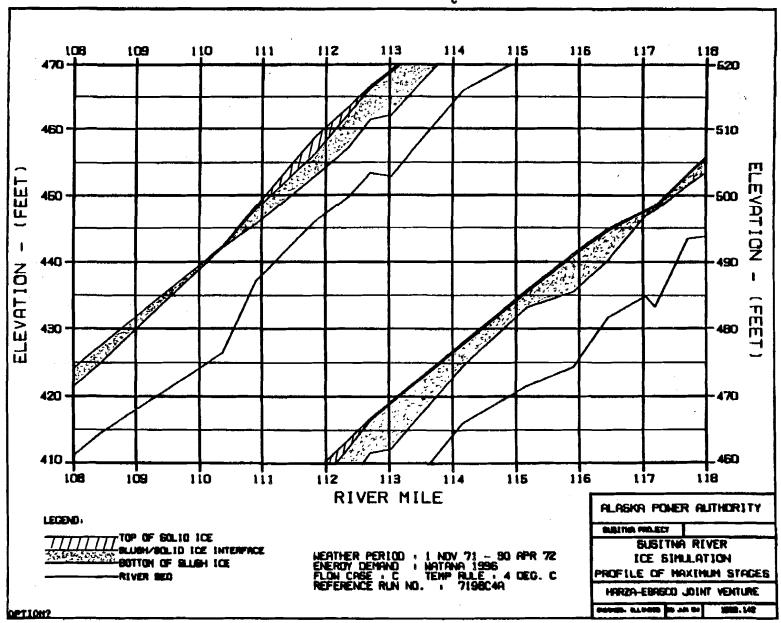


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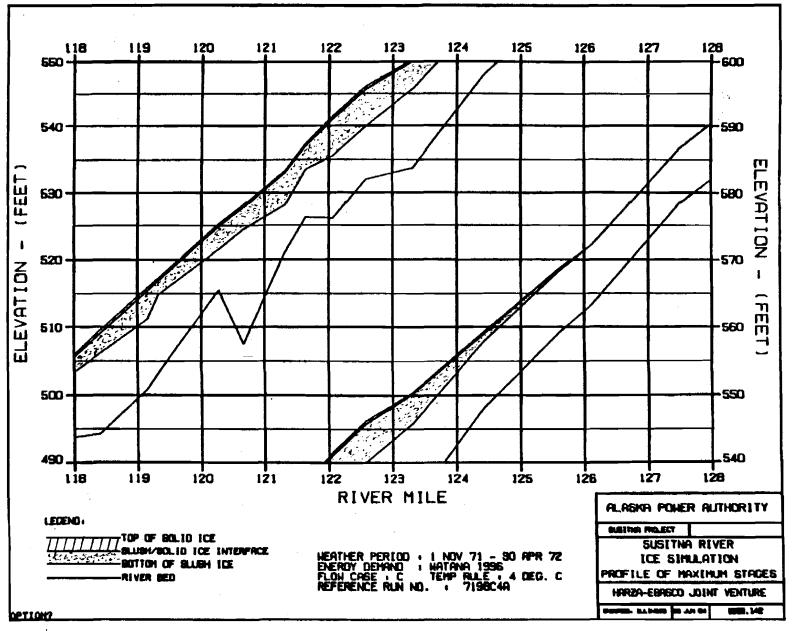
EXHIBIT J



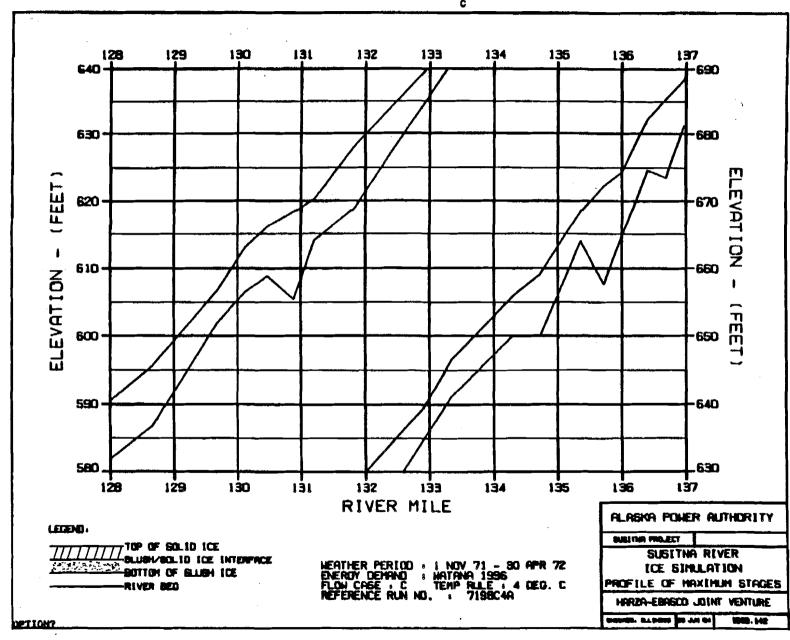




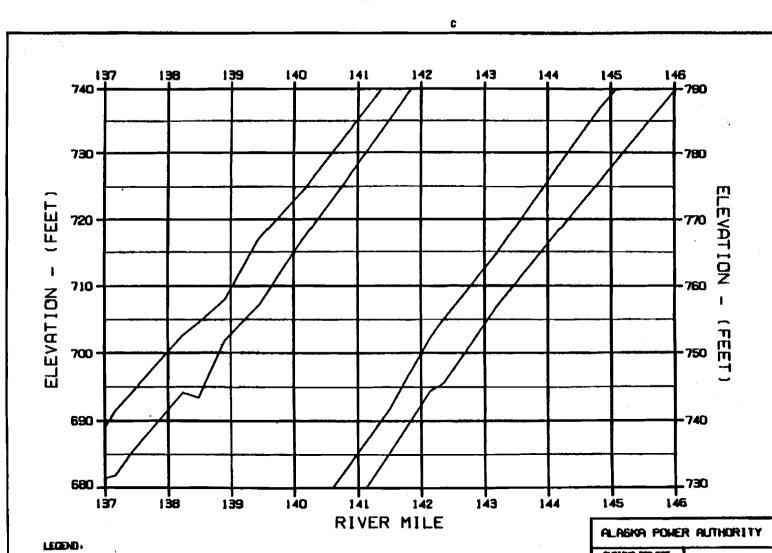








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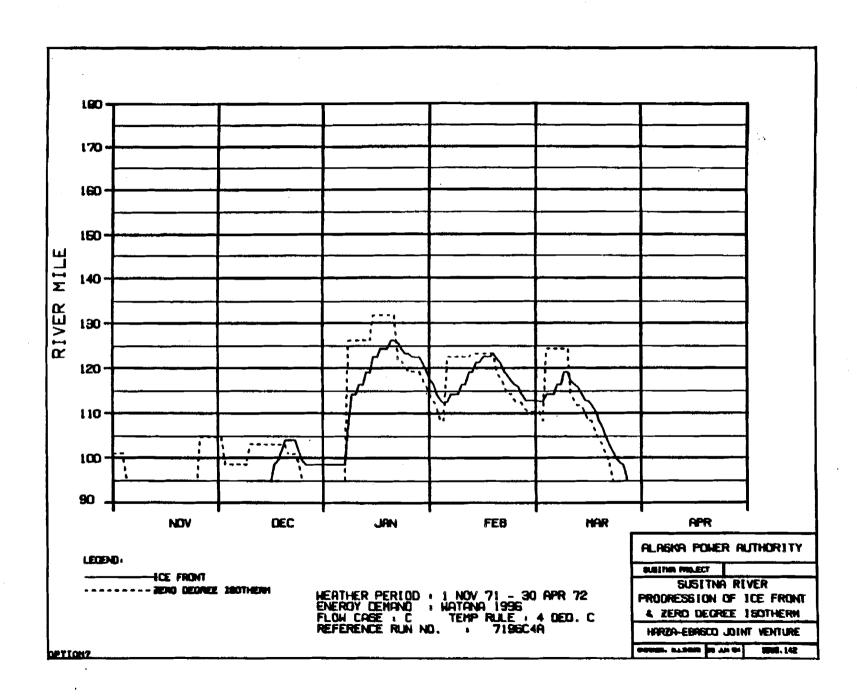
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SUSITNA RIVER ICE SIMULATION PROFILE OF MAXIMUM STAGES

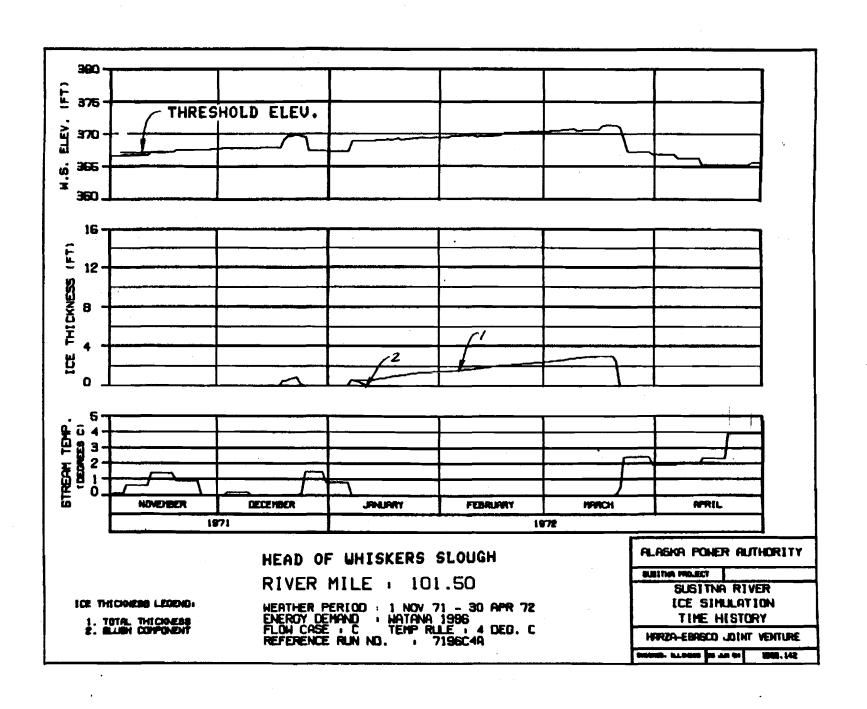
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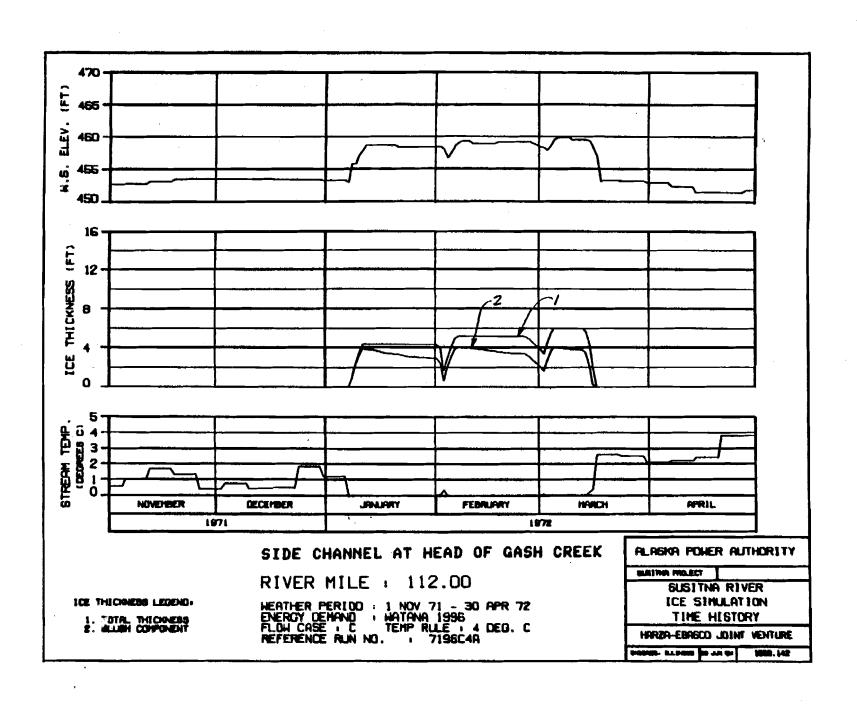
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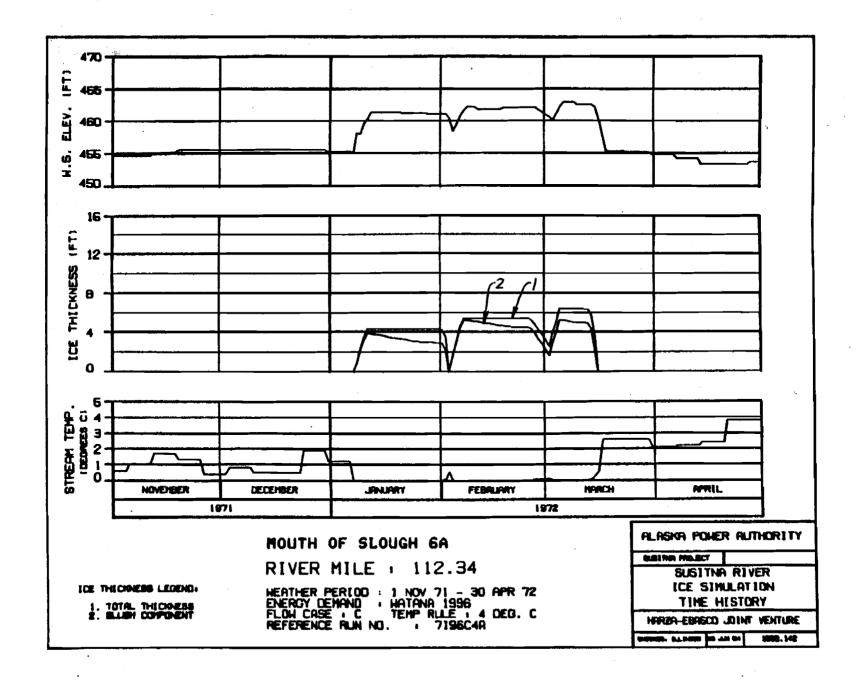
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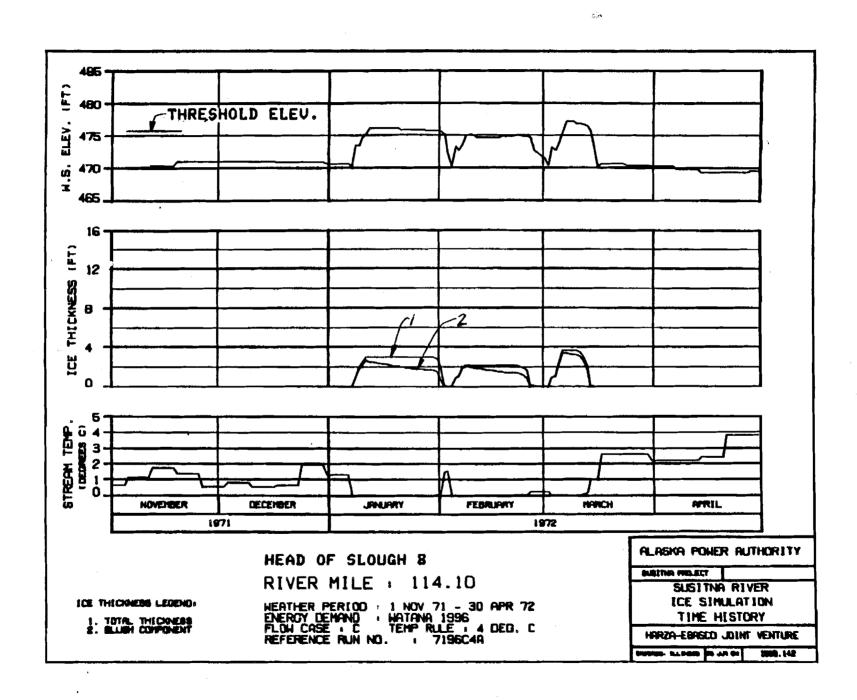


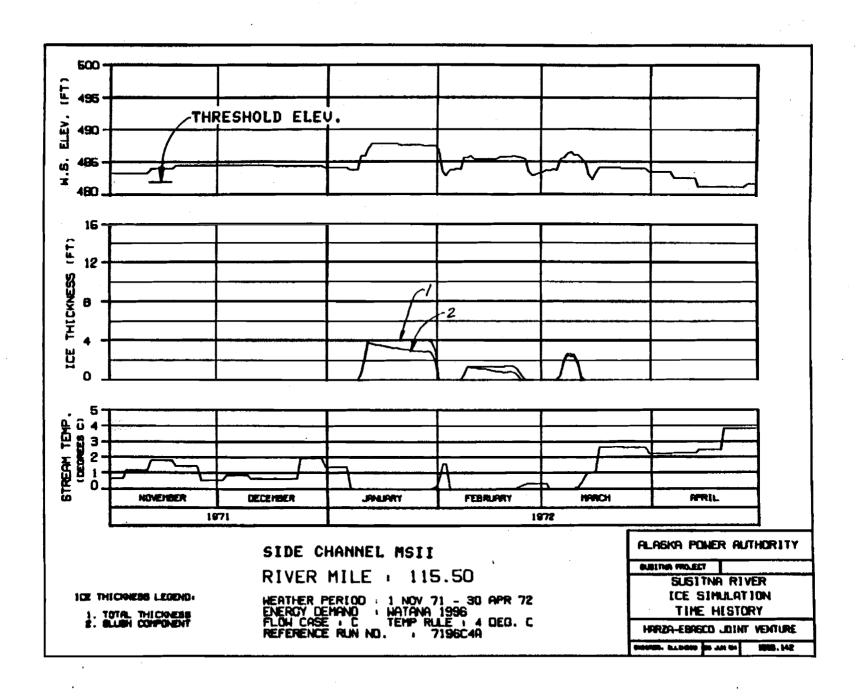
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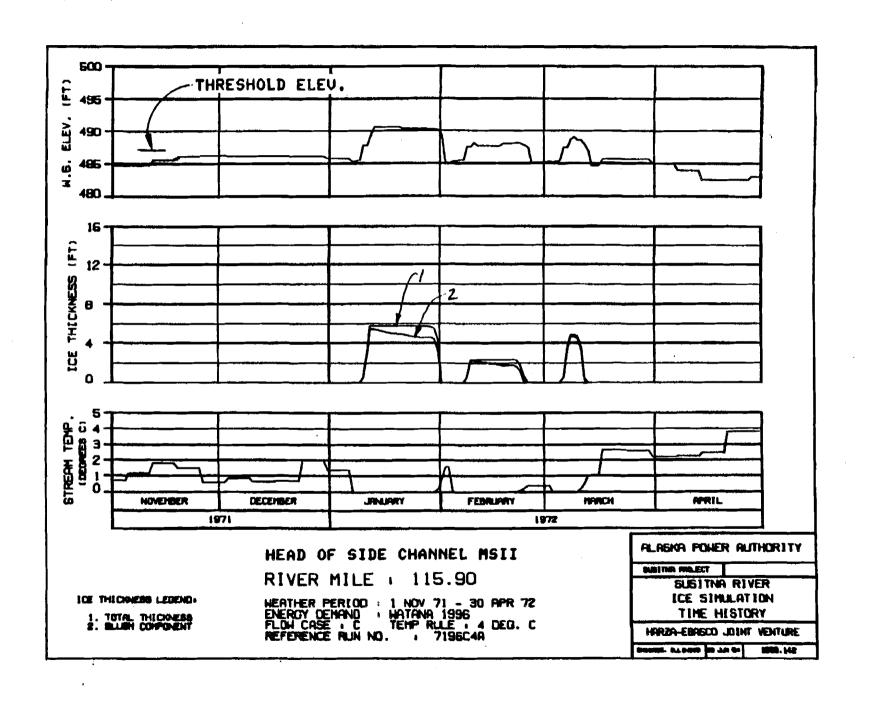


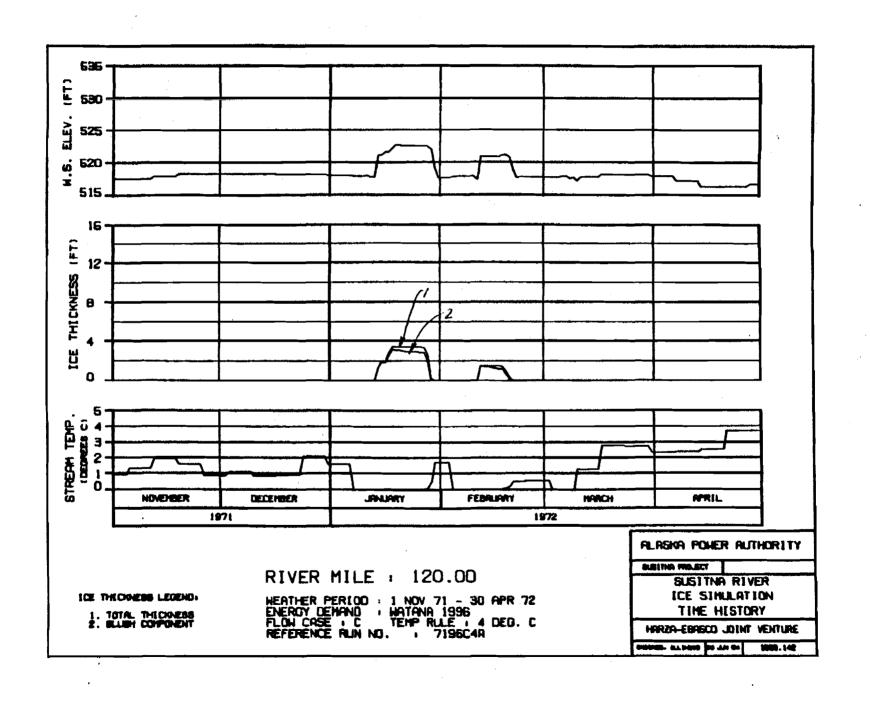


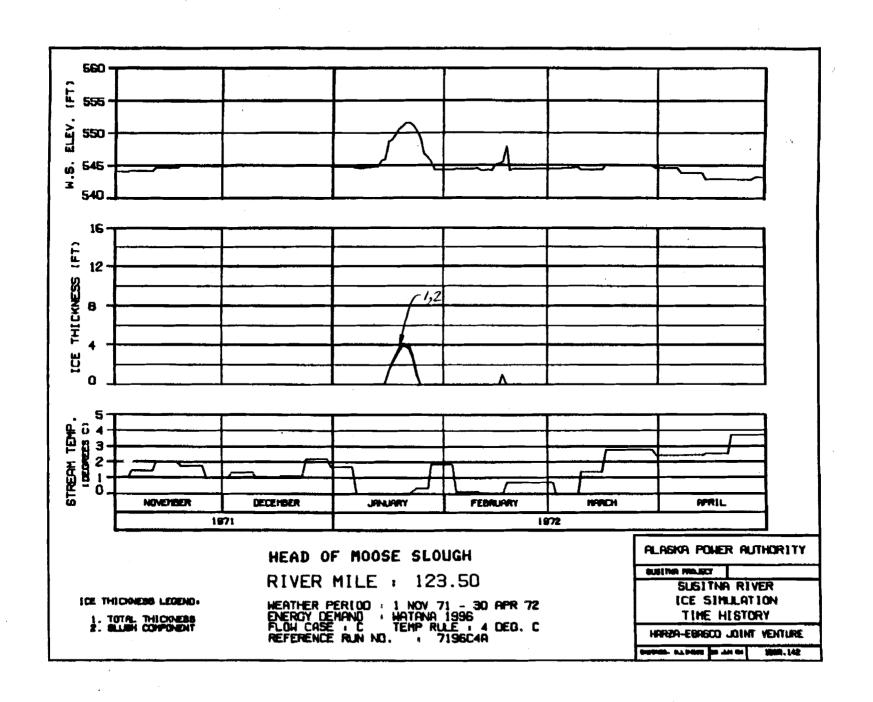


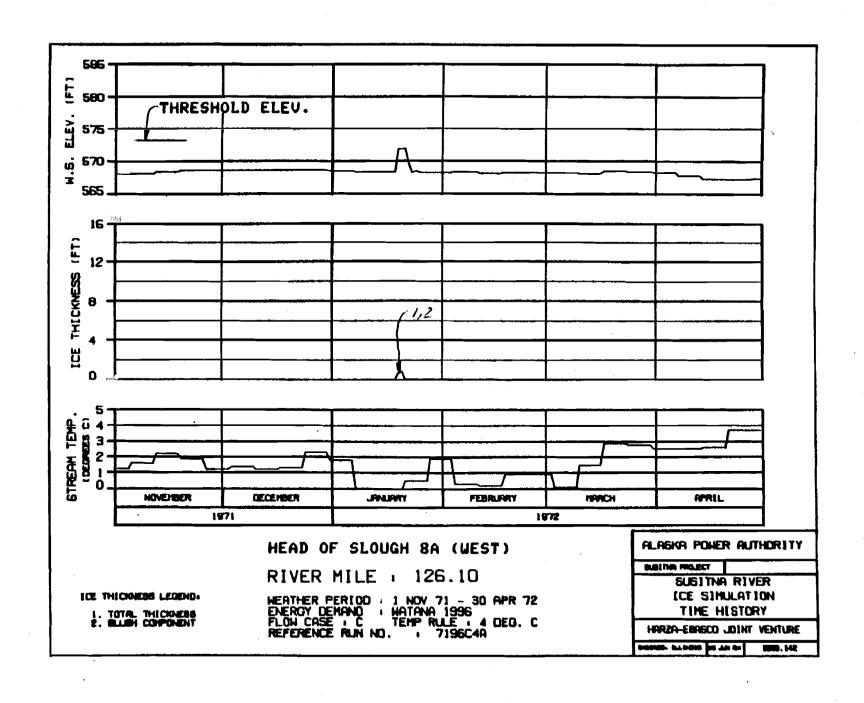


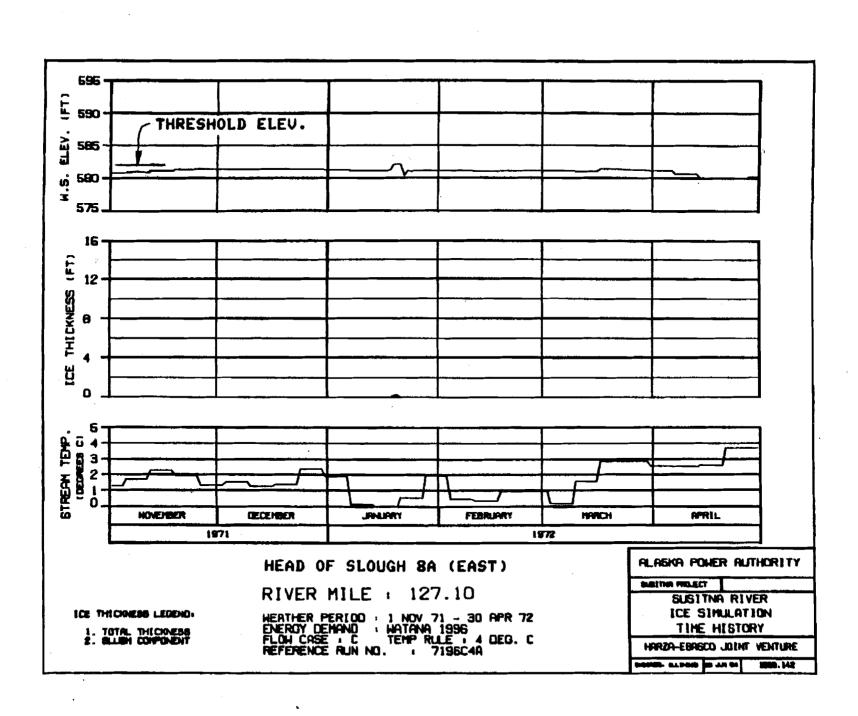


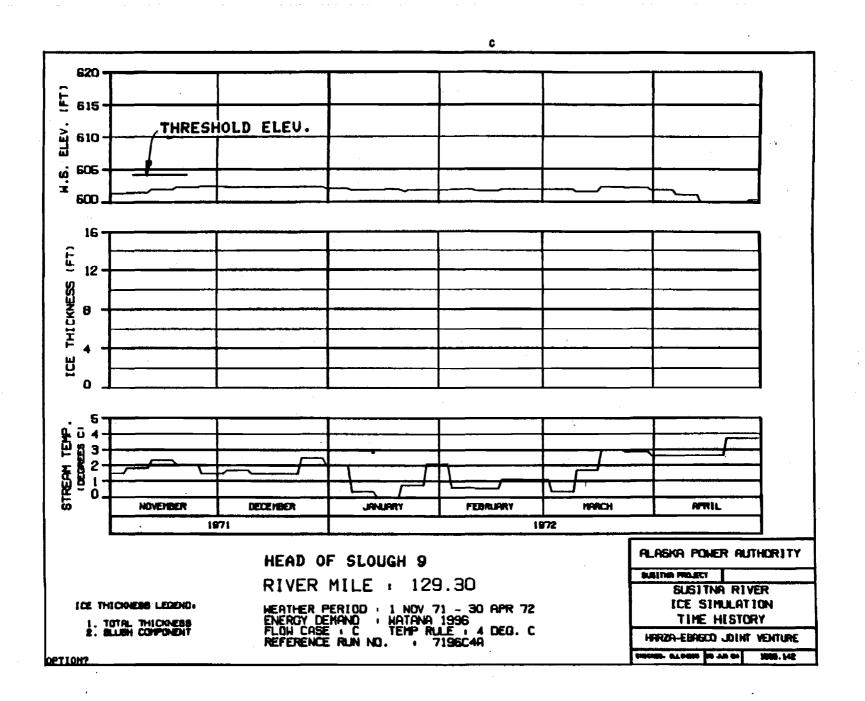


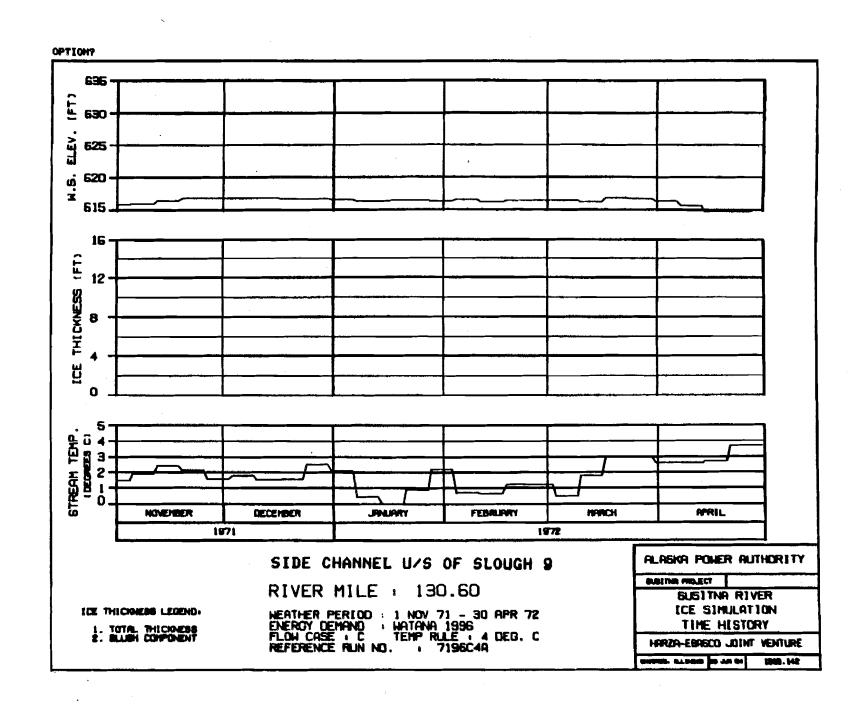




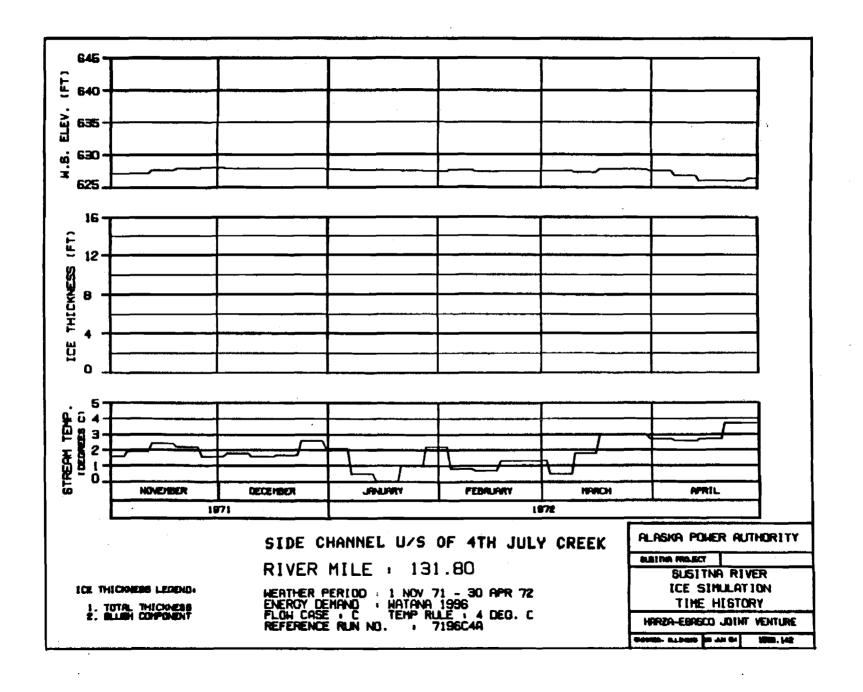


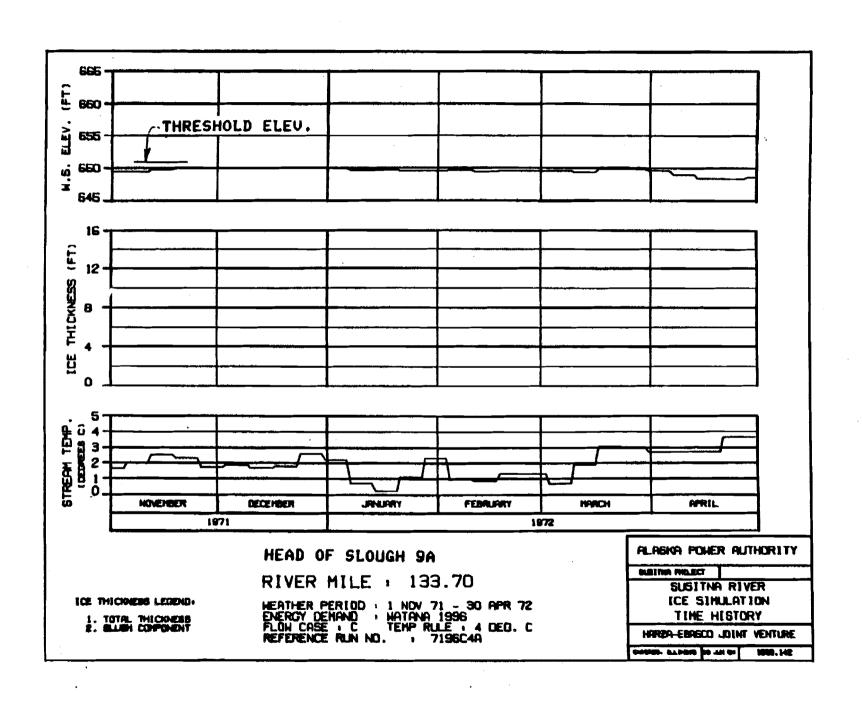


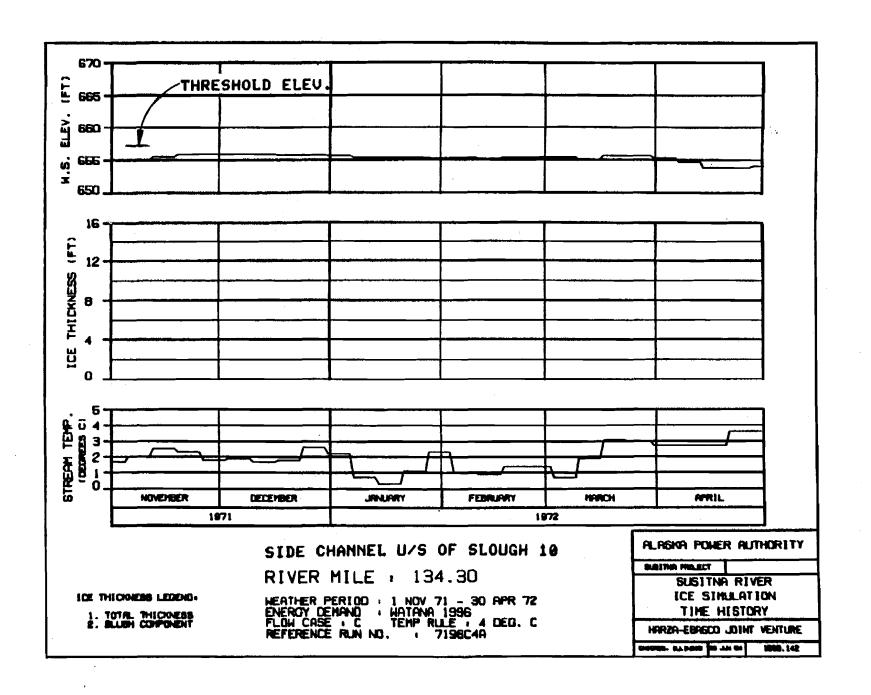


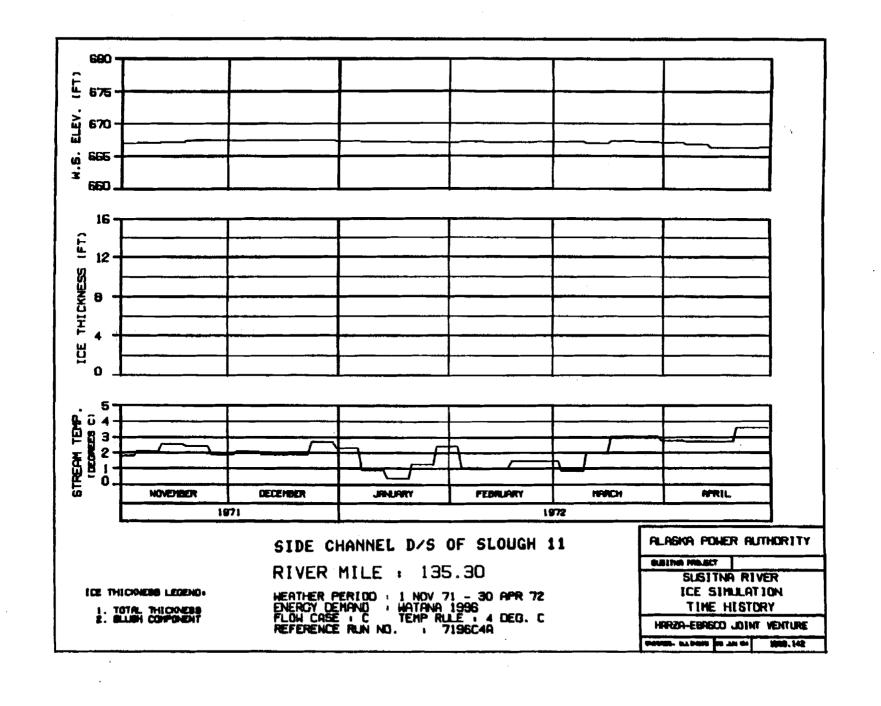


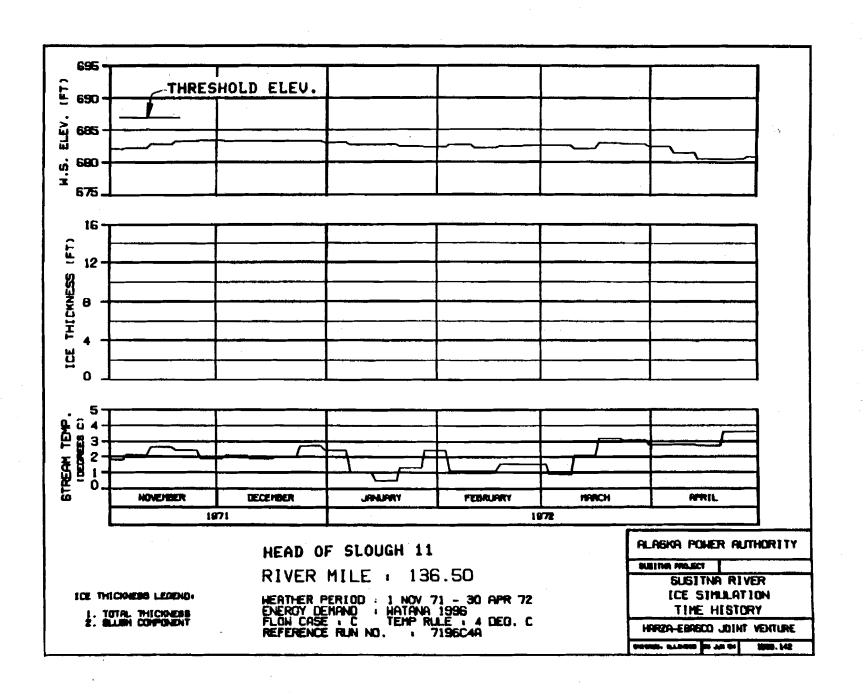
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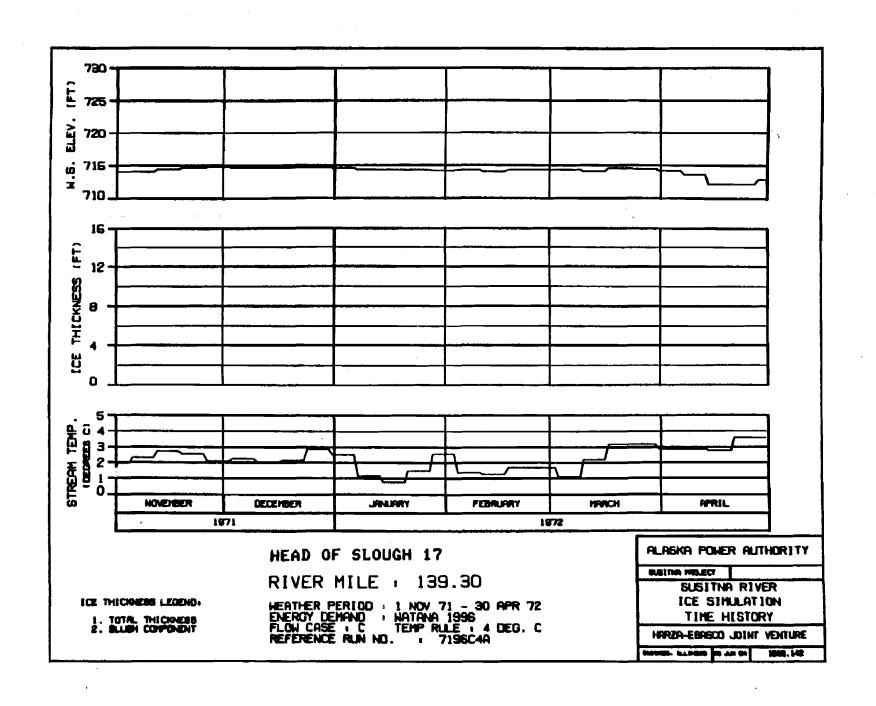


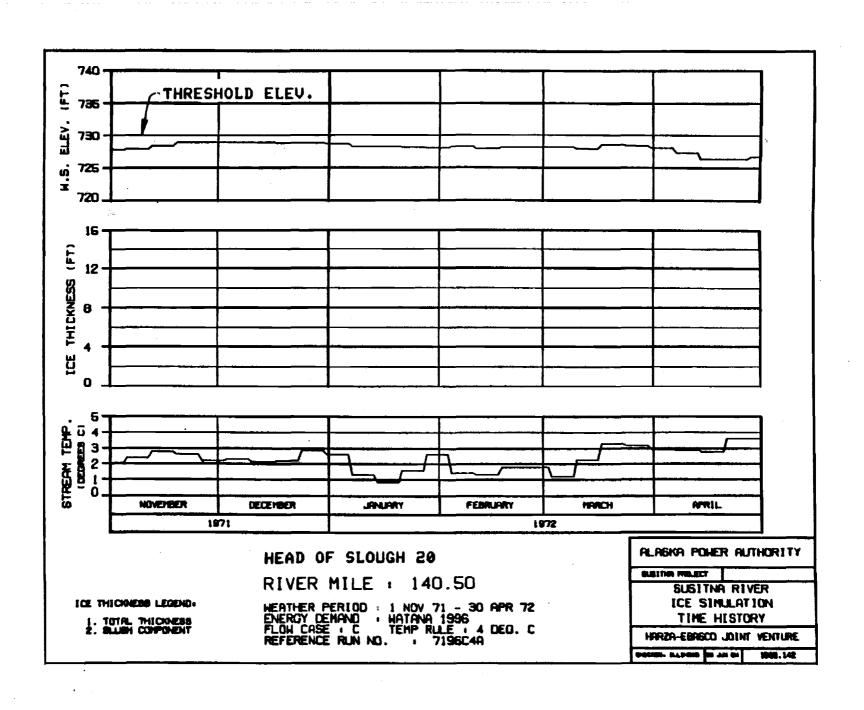


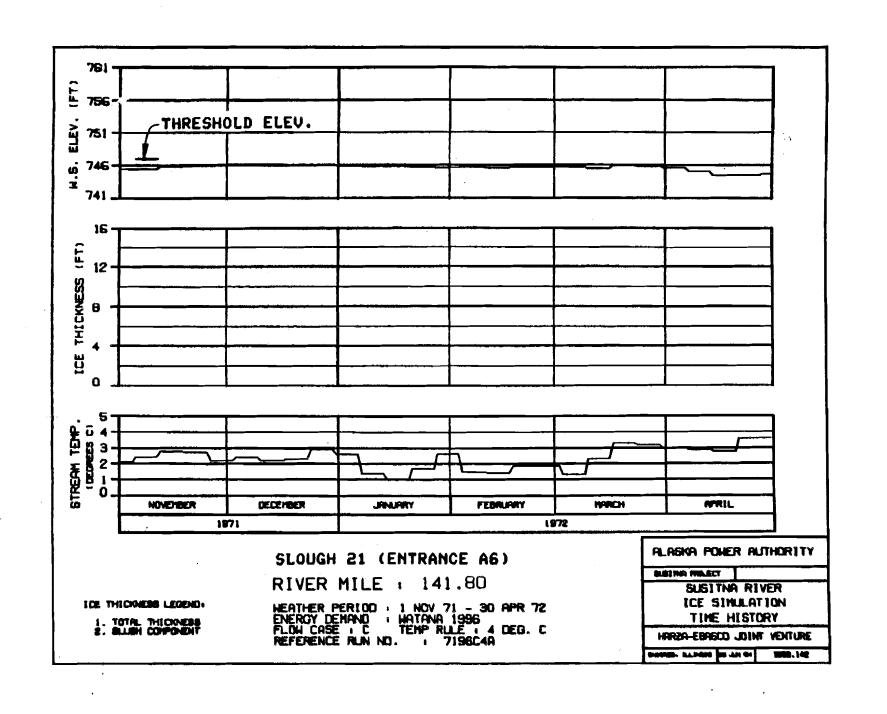




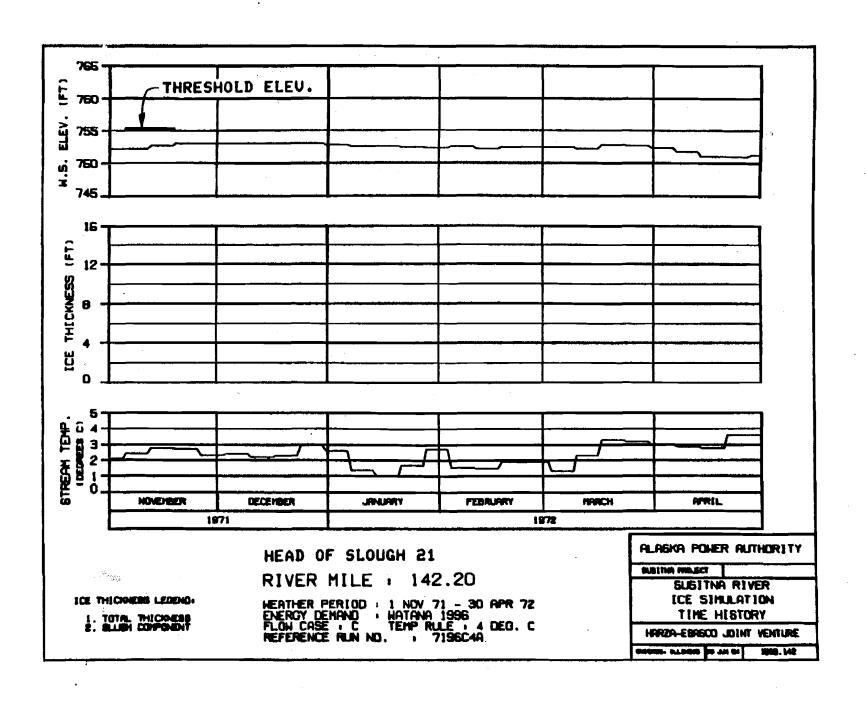








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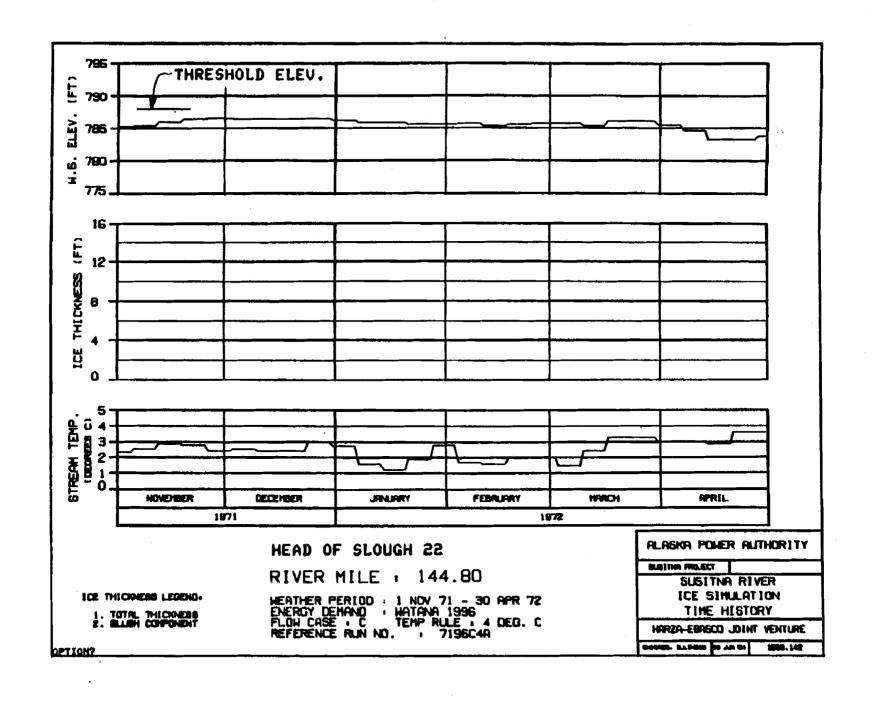
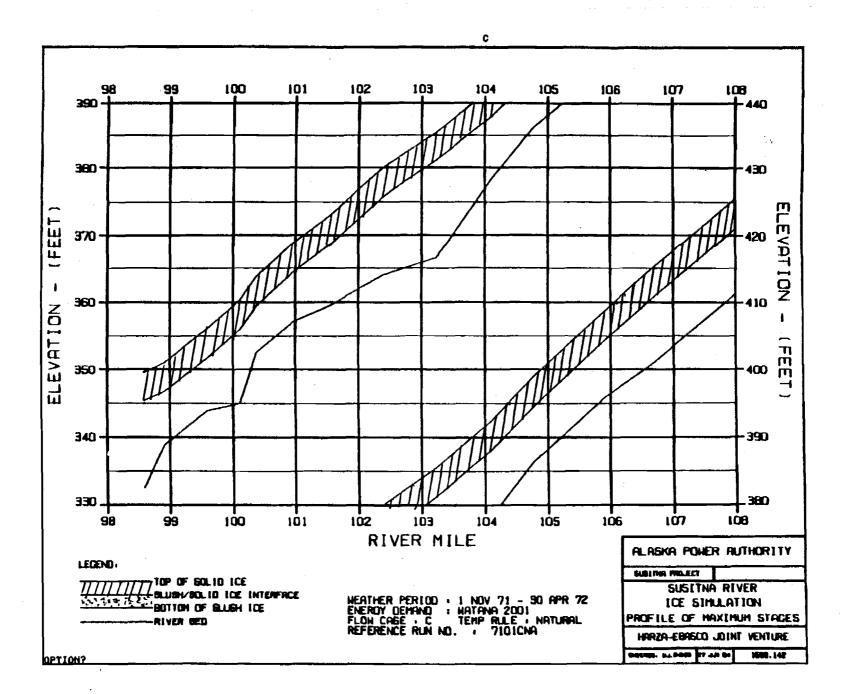
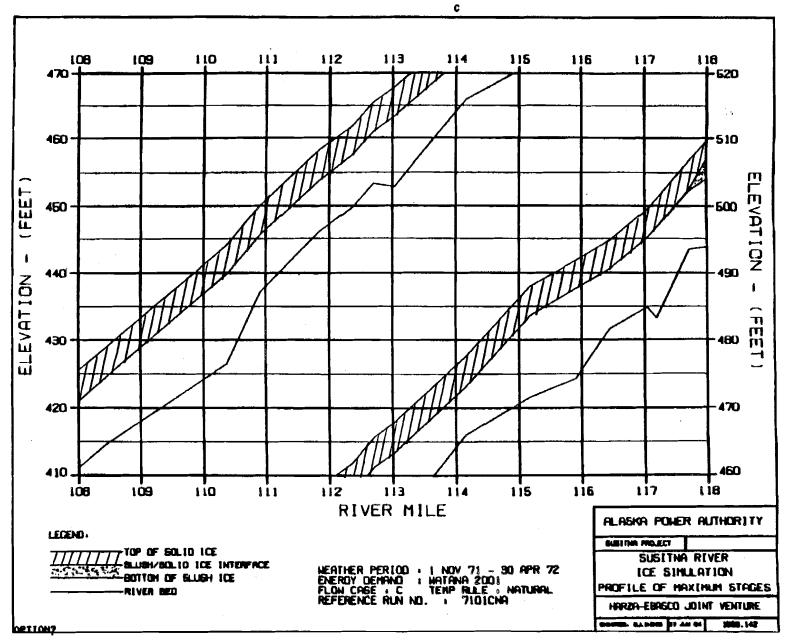


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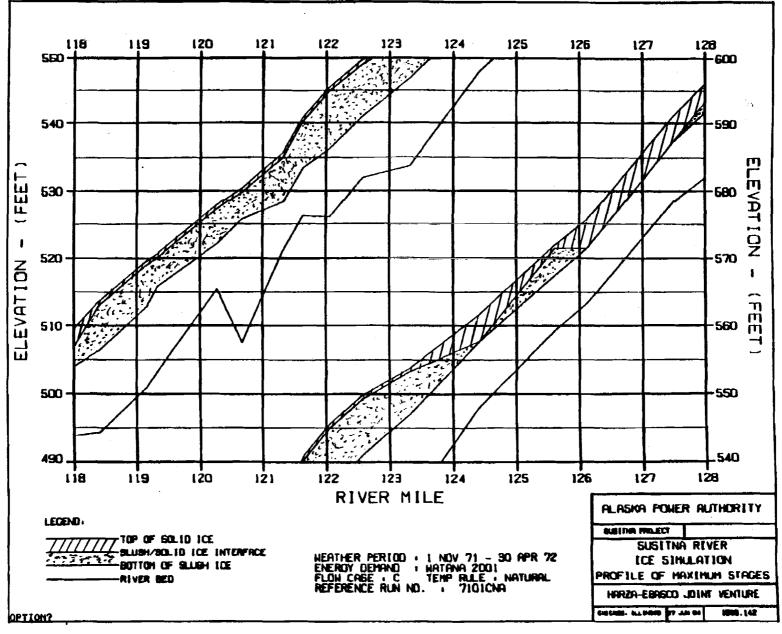




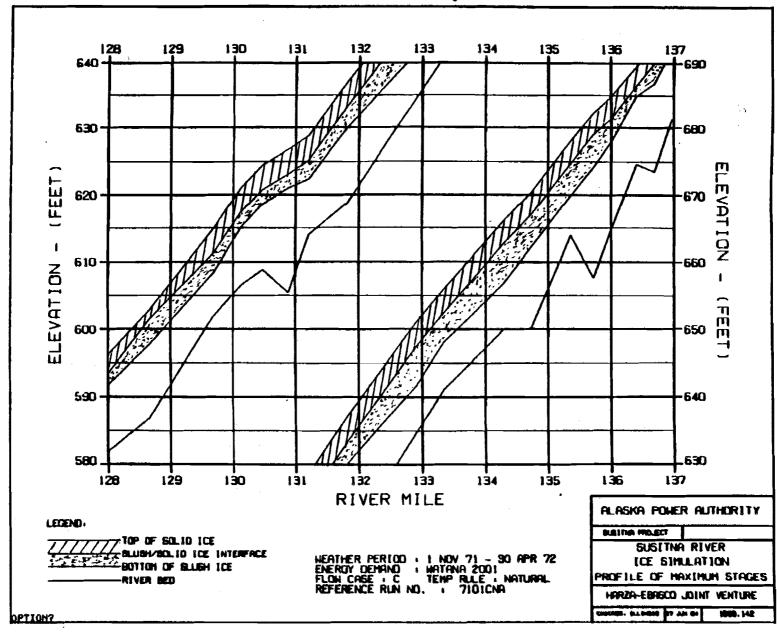


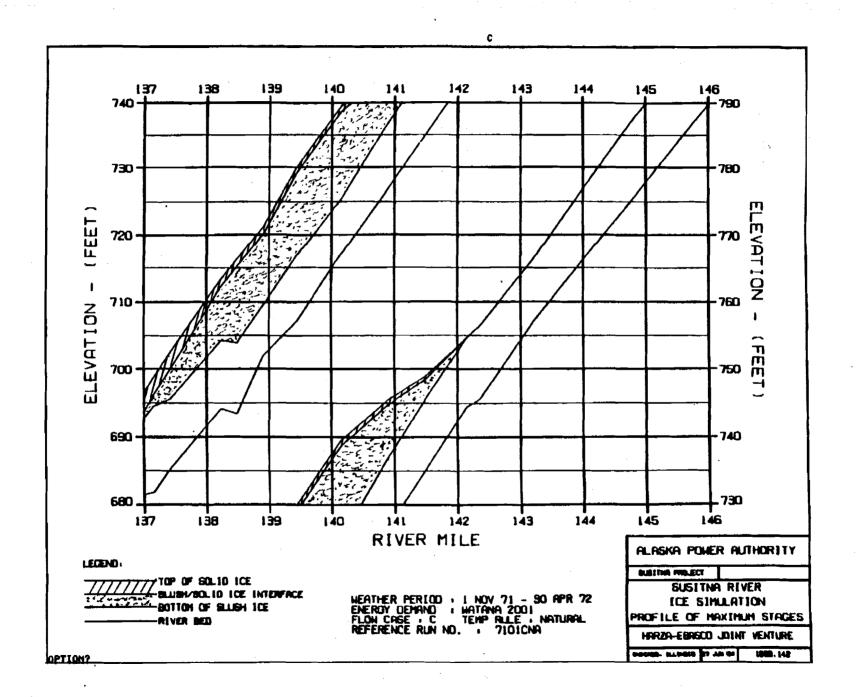
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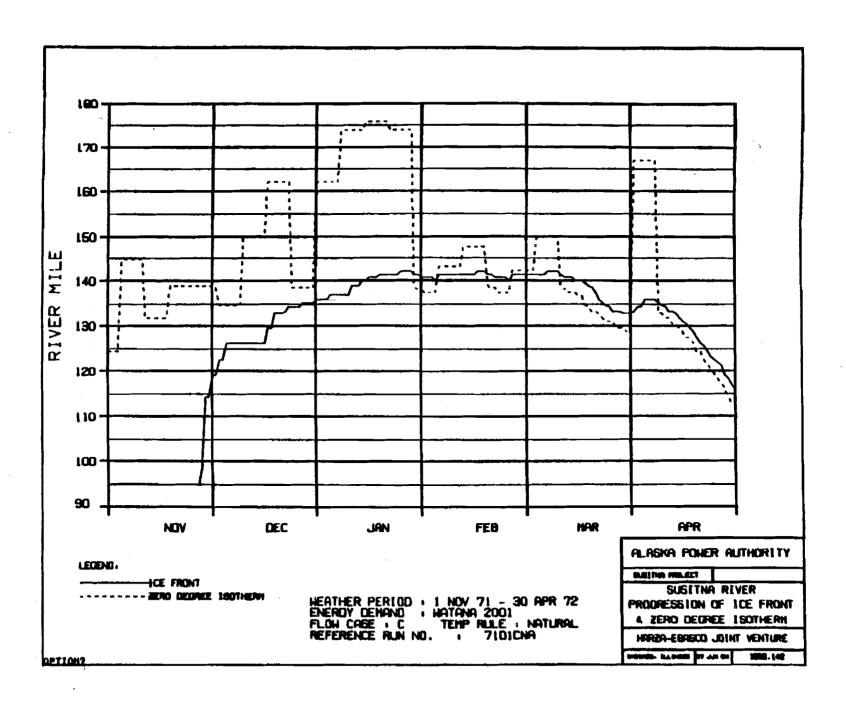


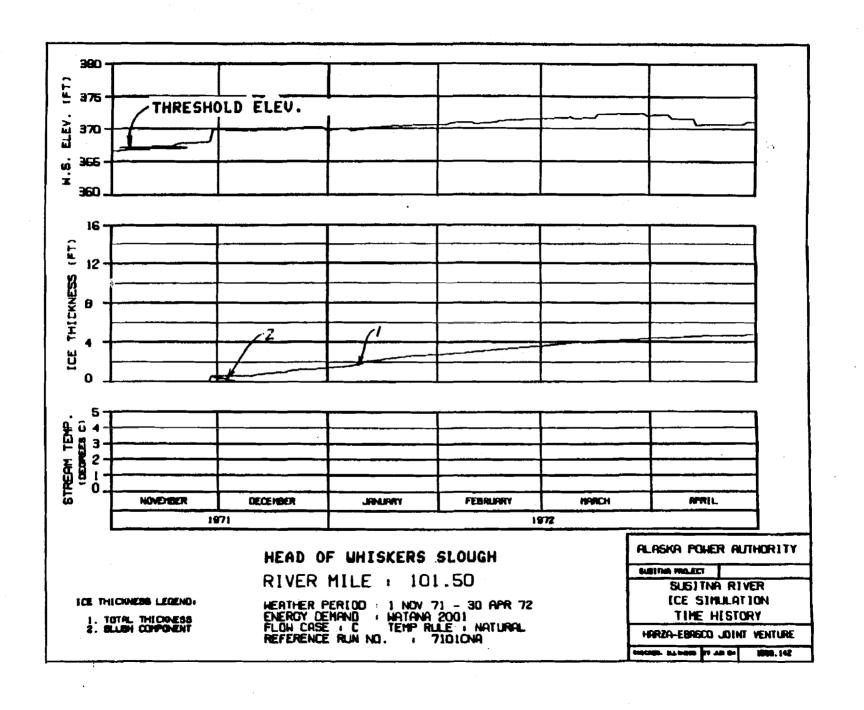


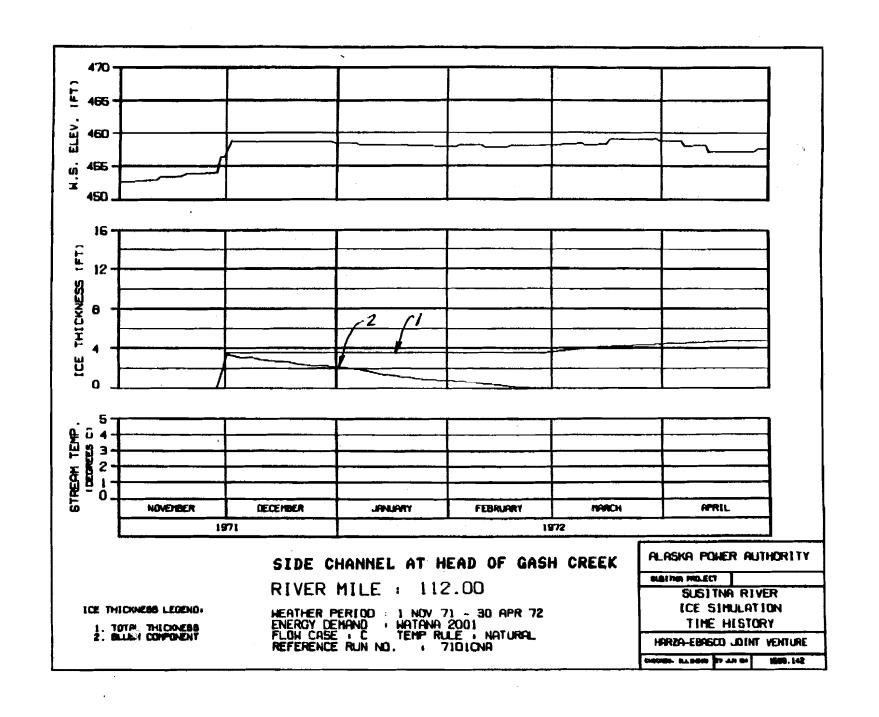


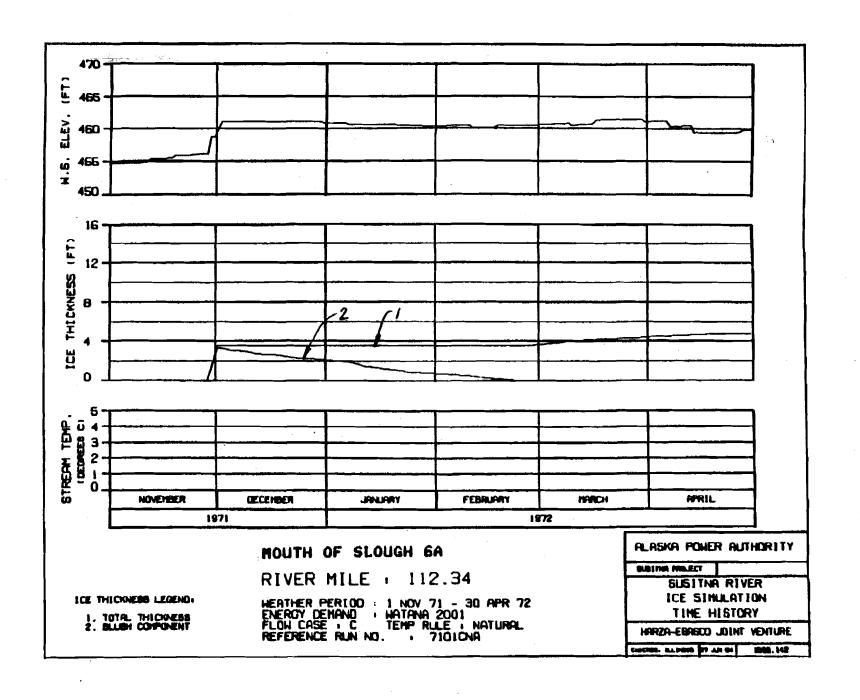


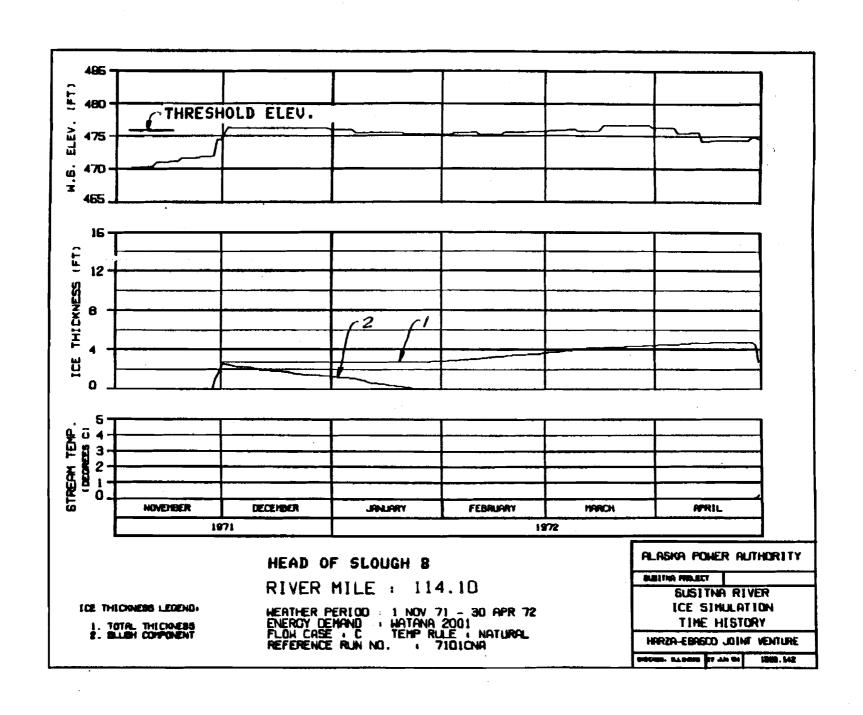




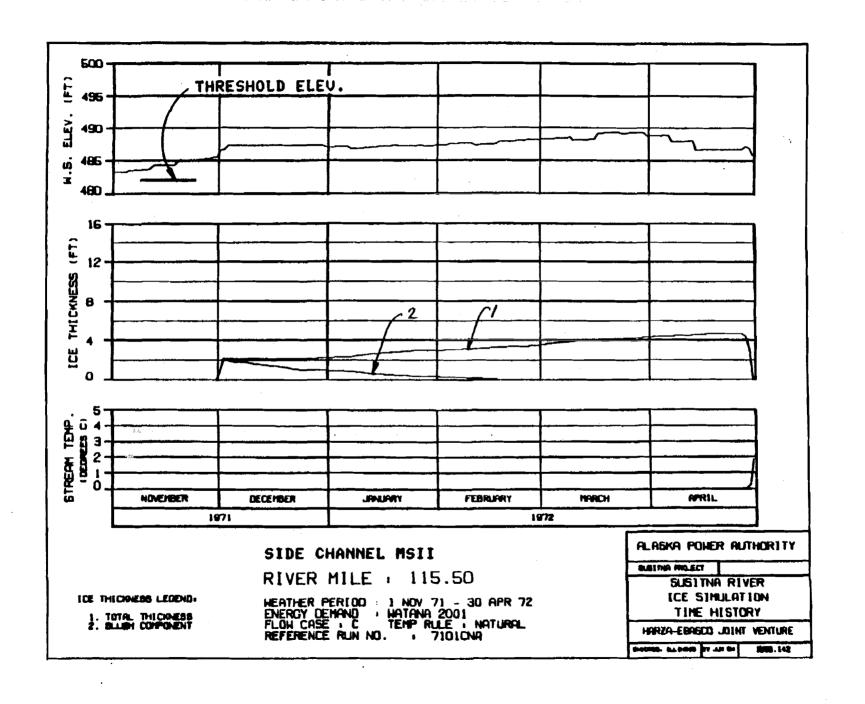


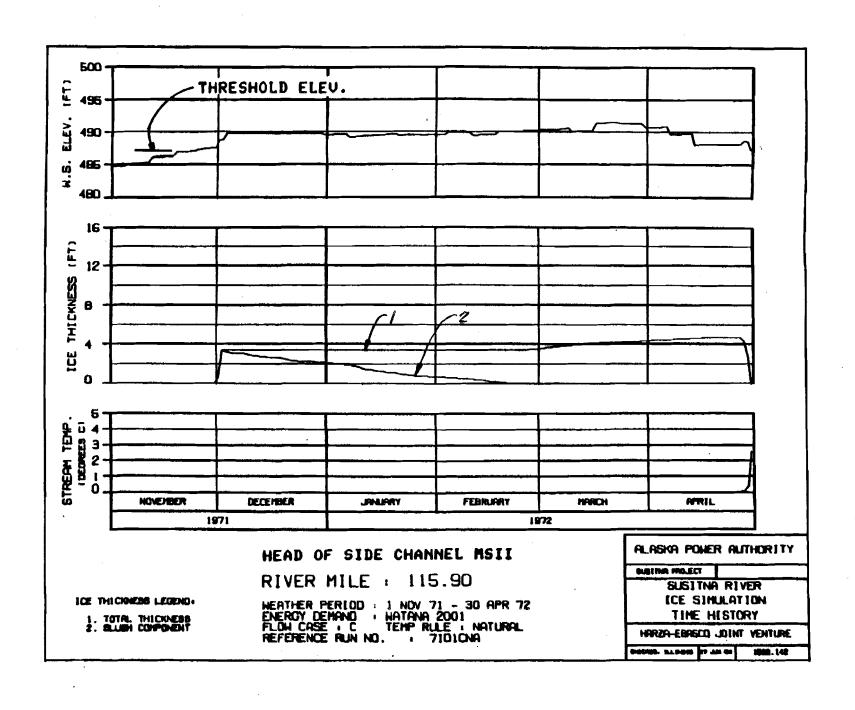


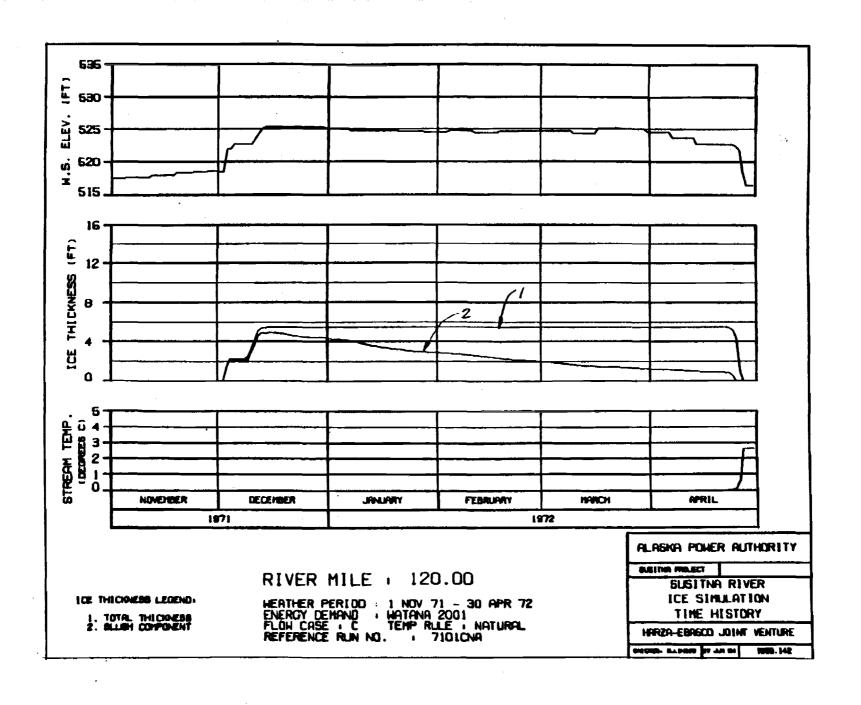


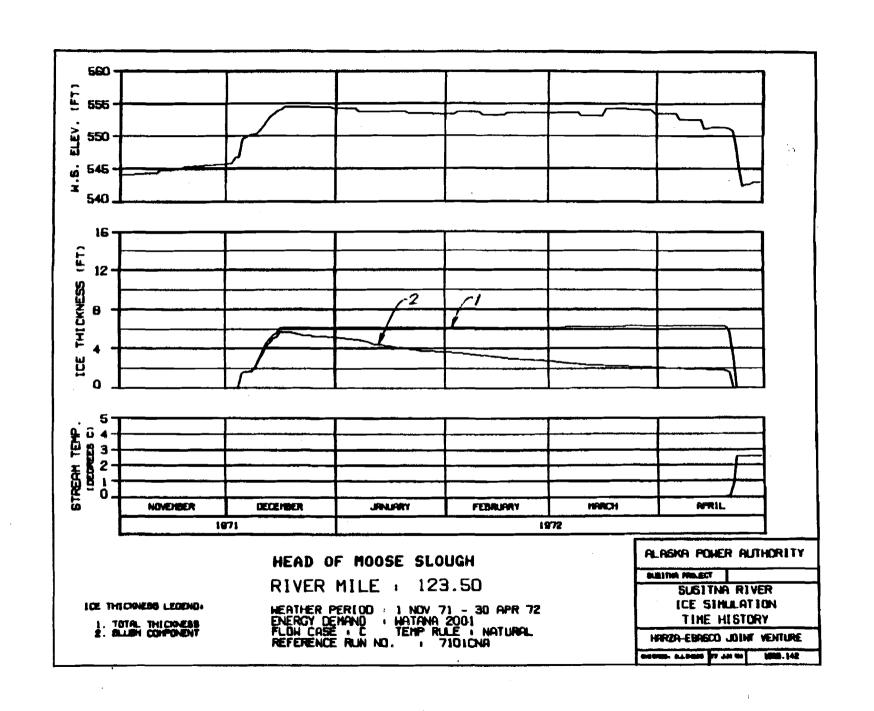


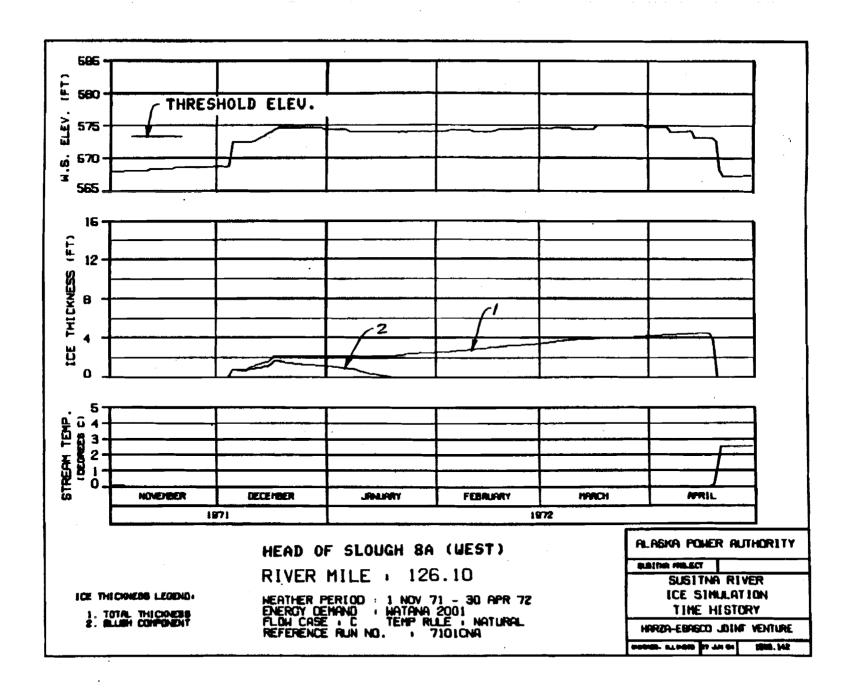
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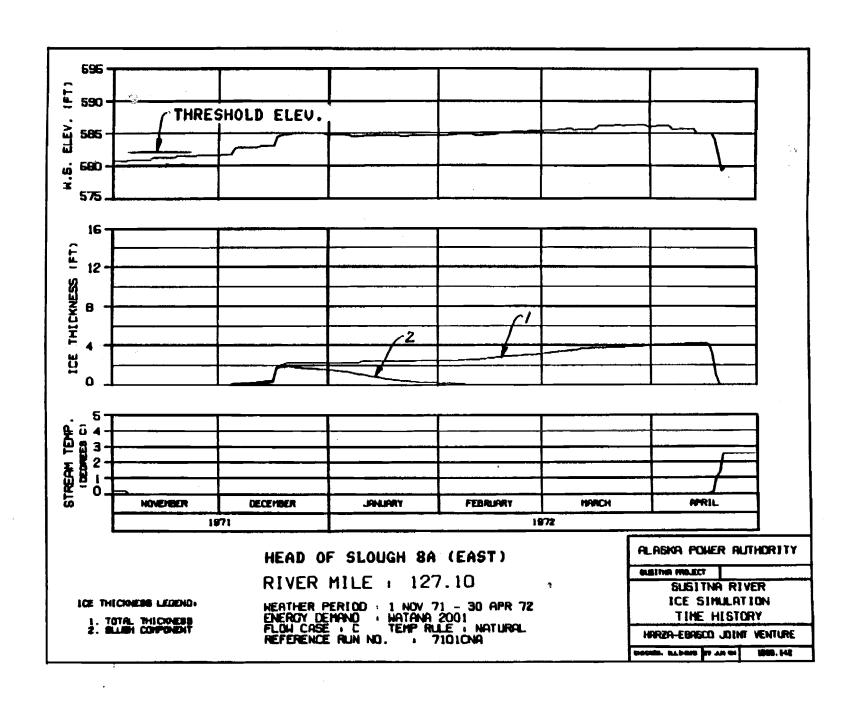


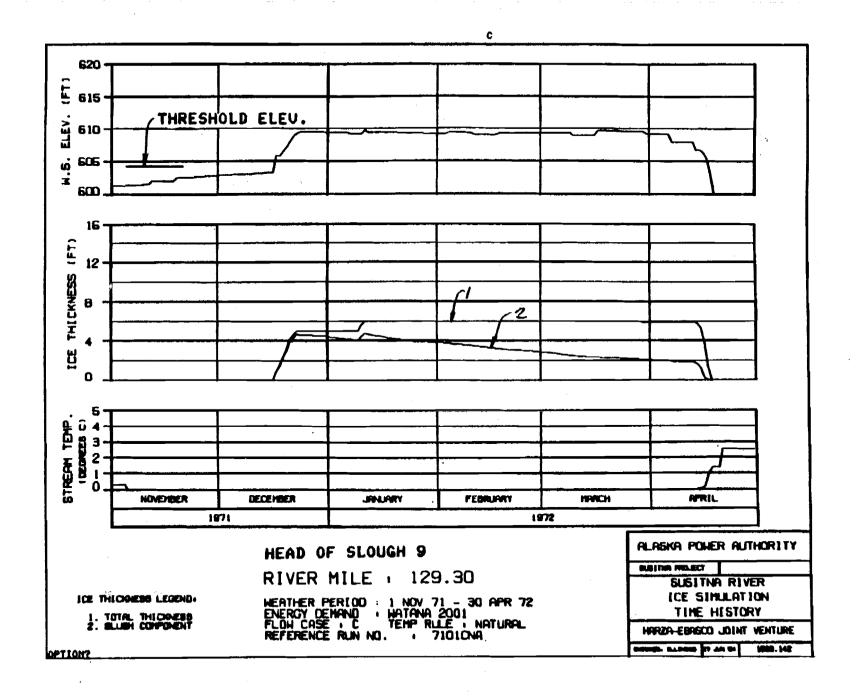


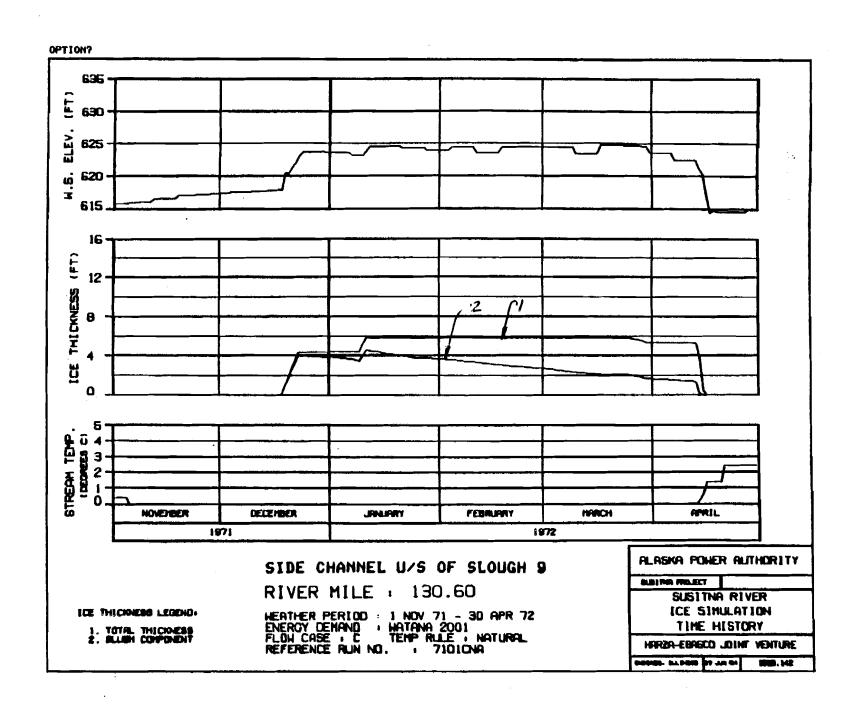






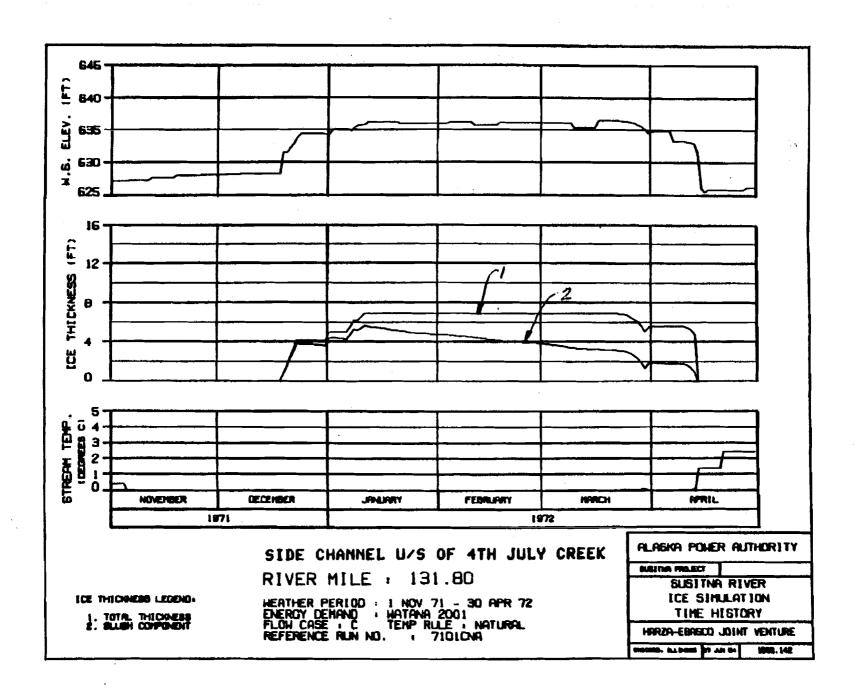


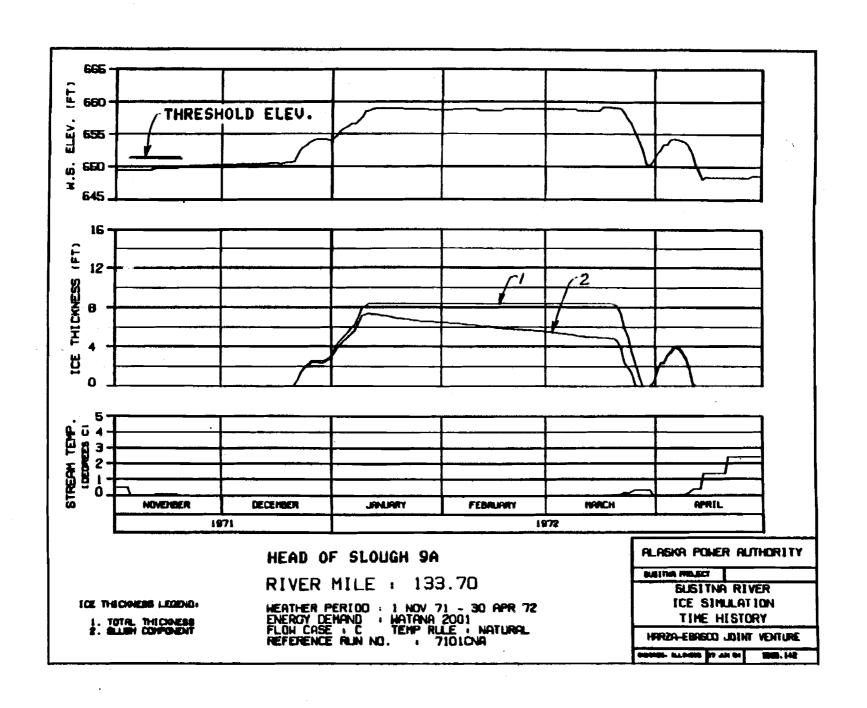


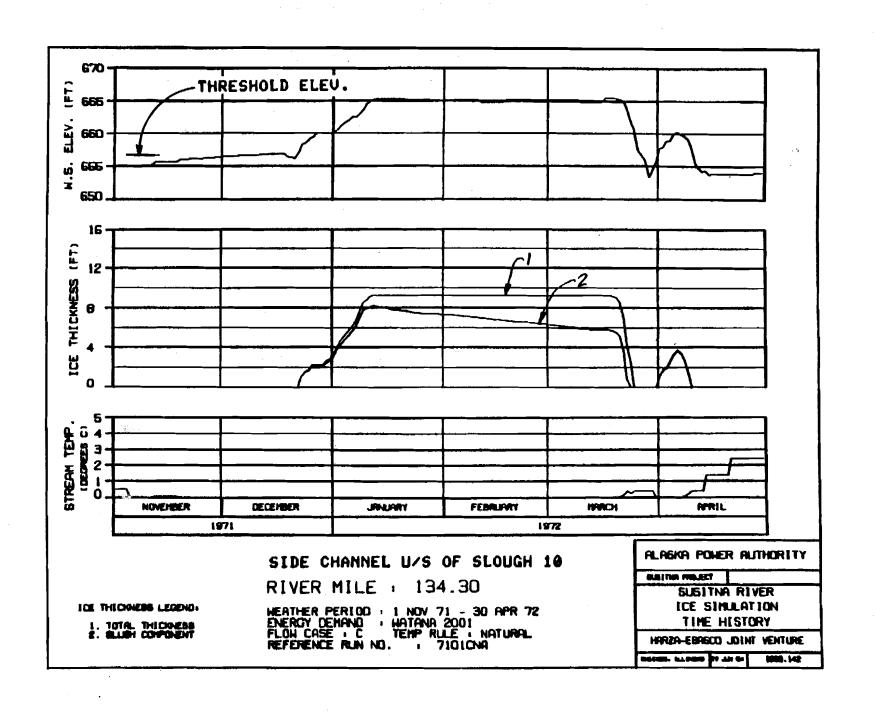


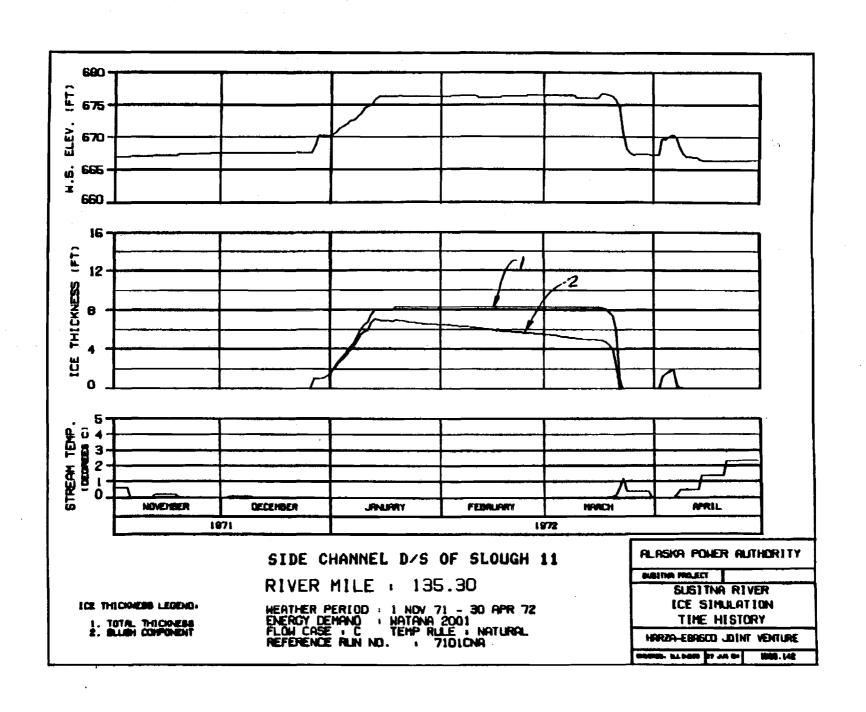
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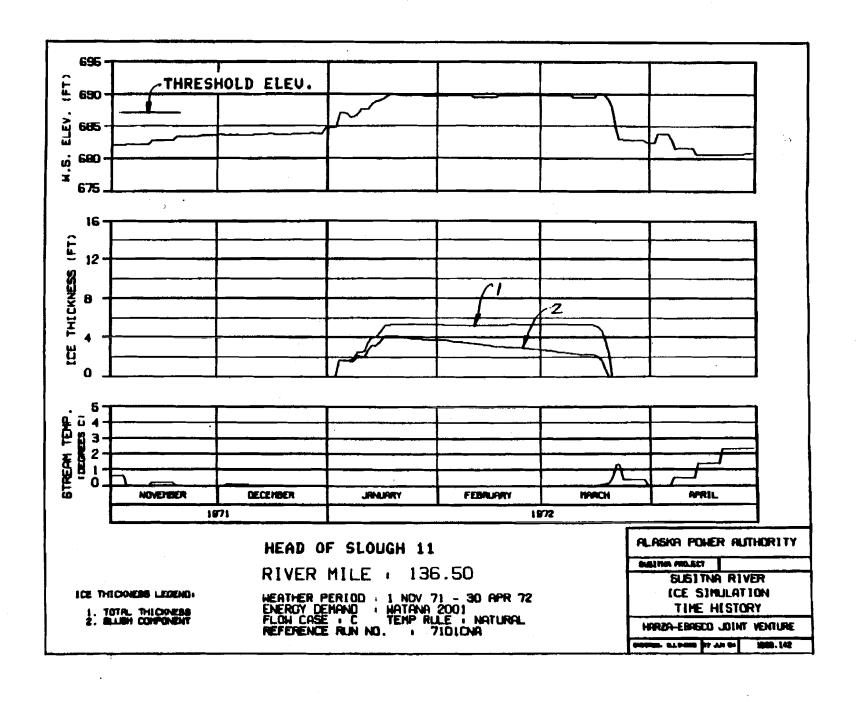


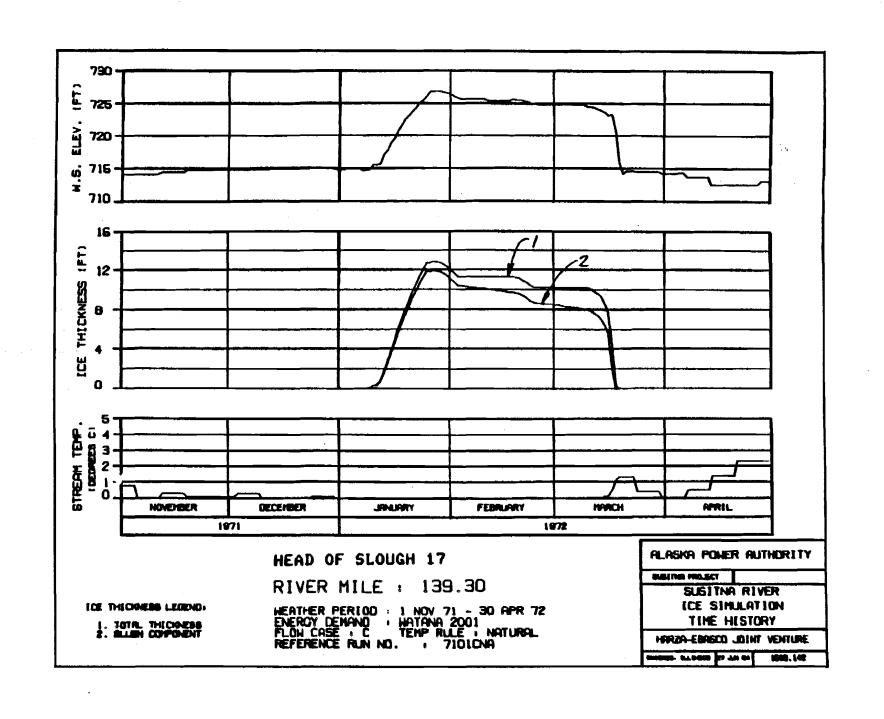


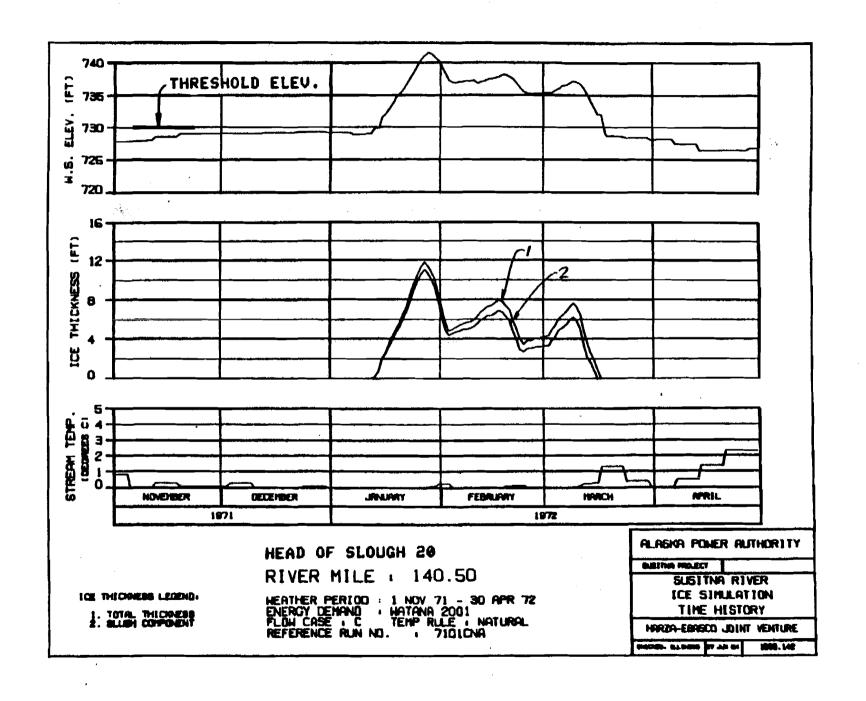


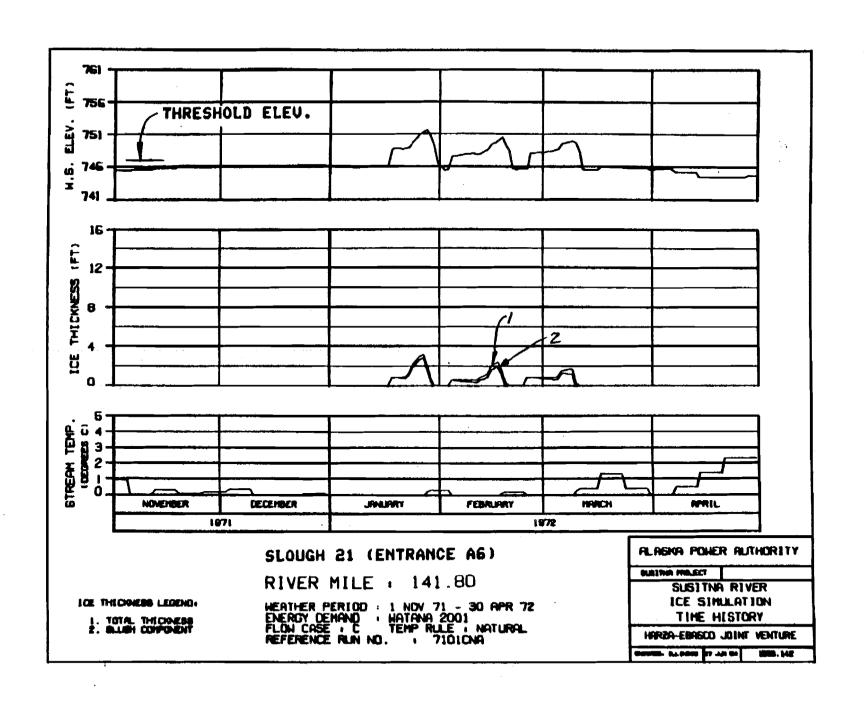


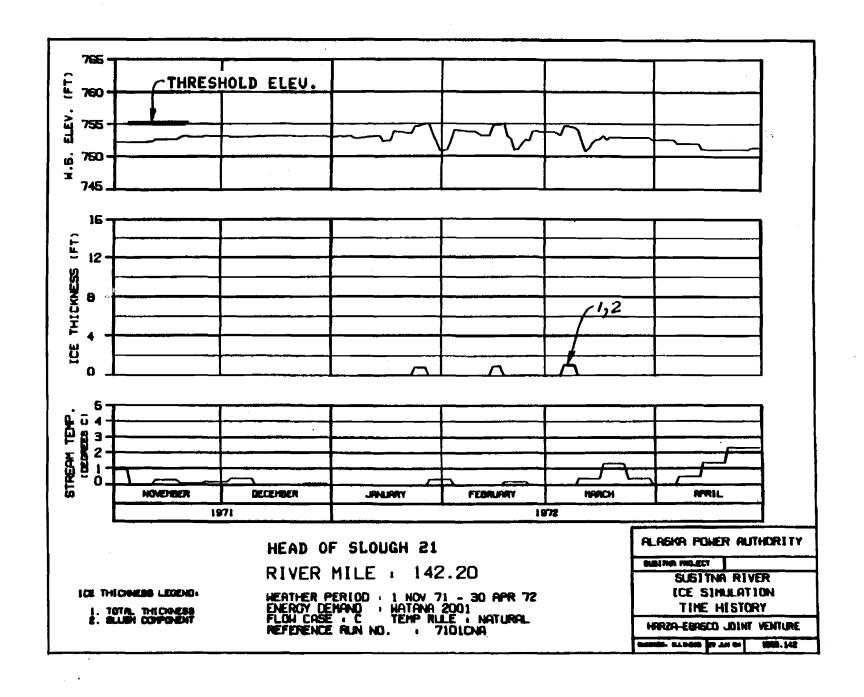
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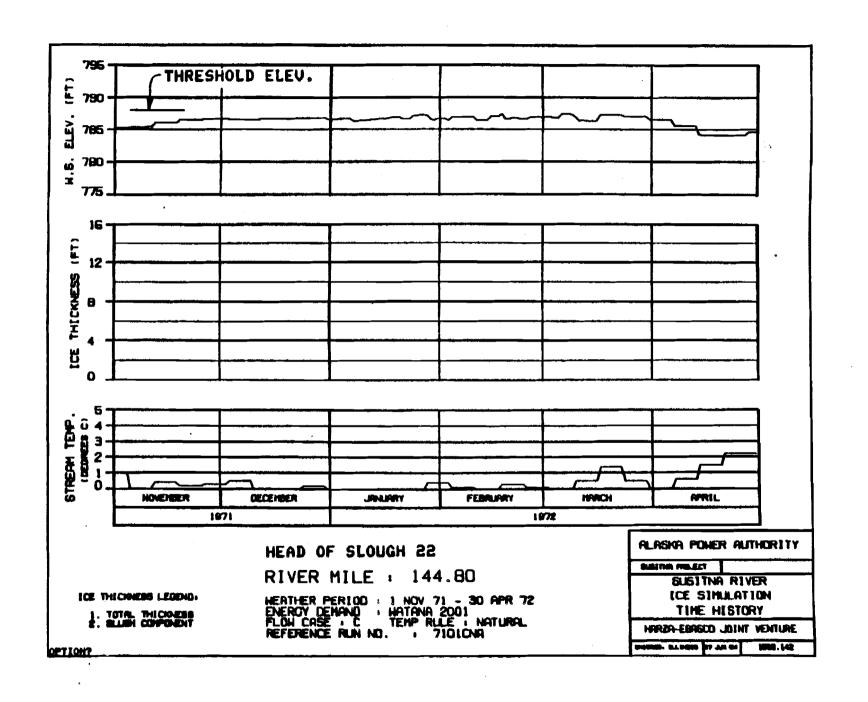




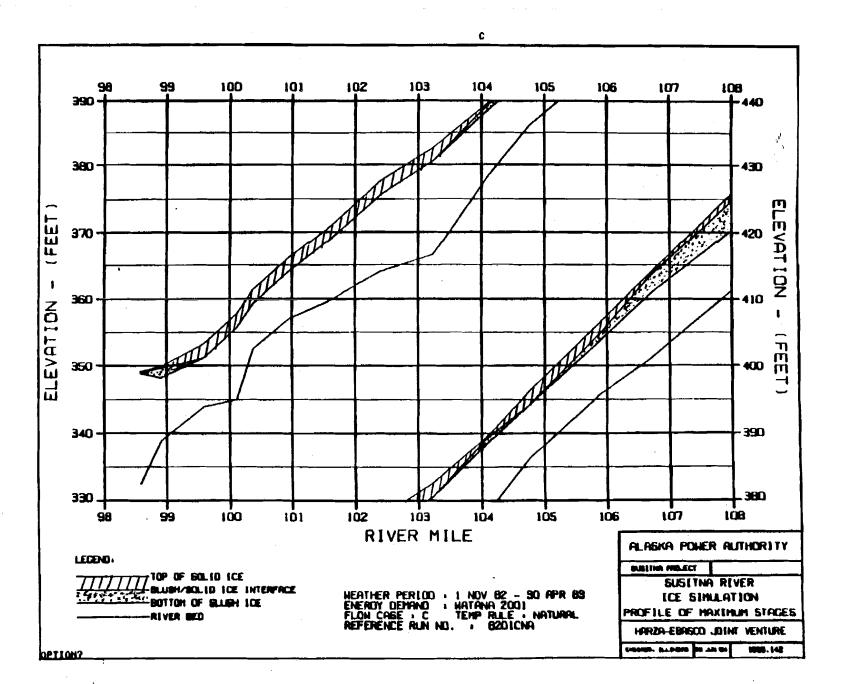




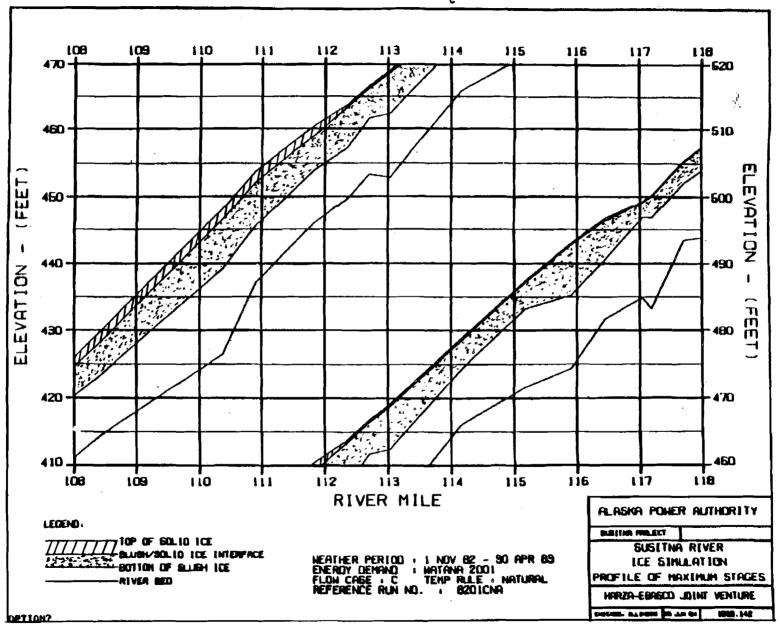




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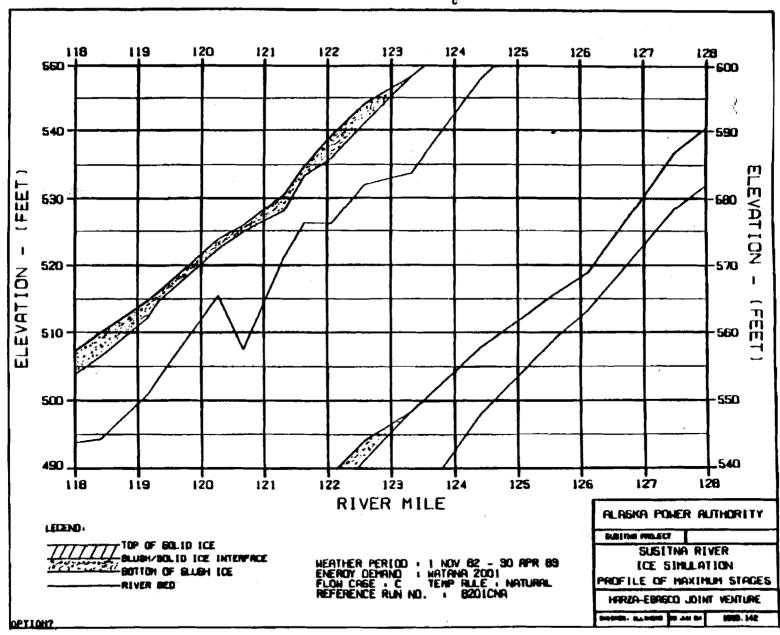




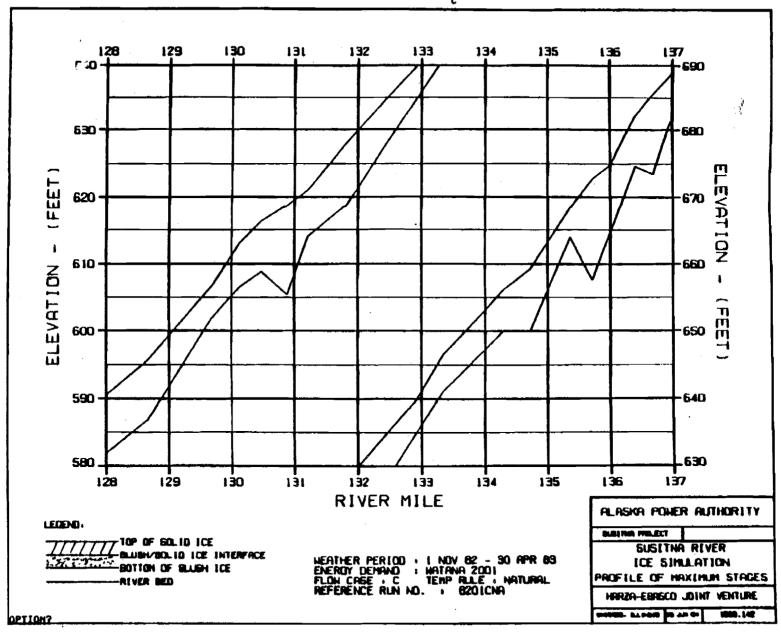


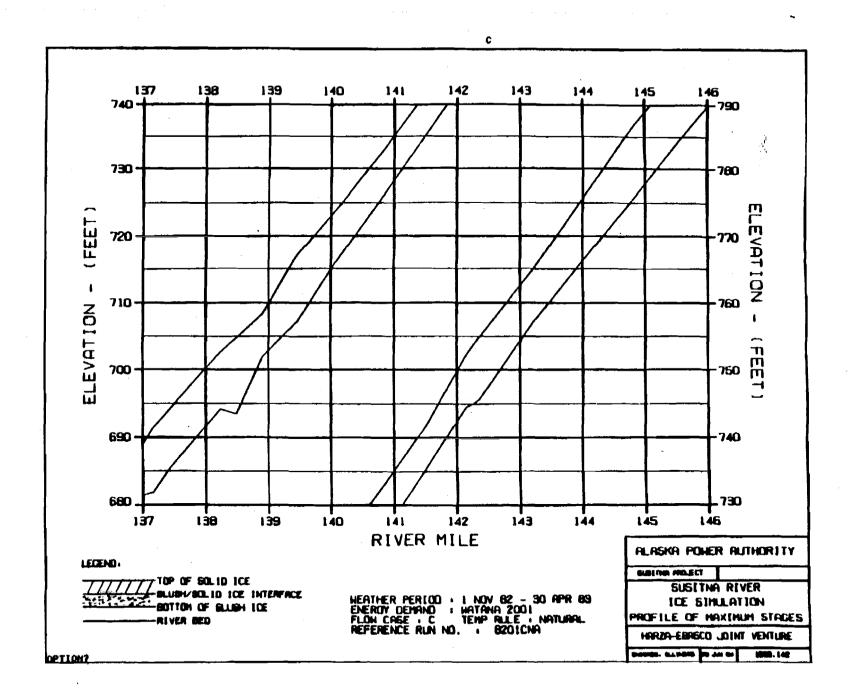
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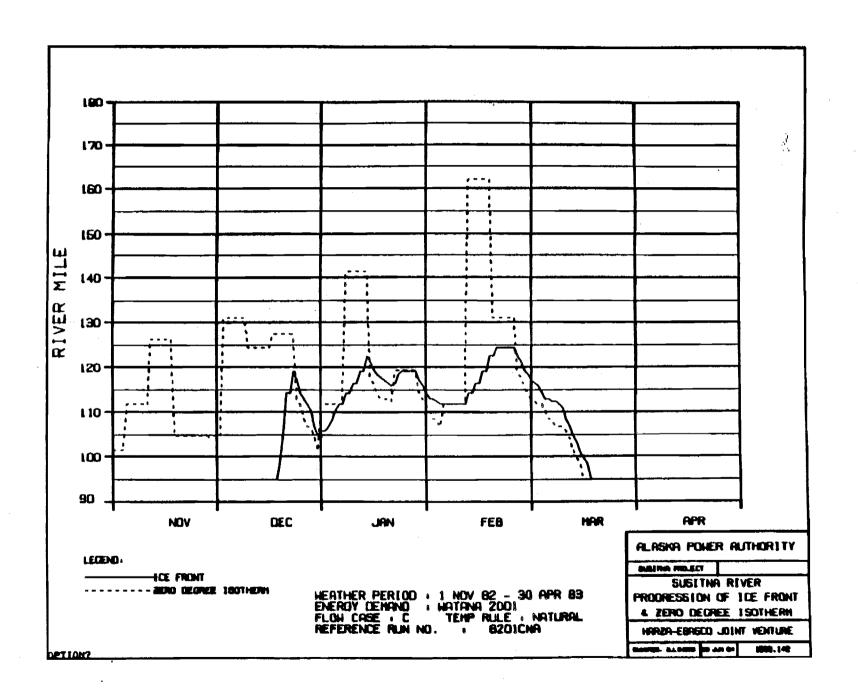




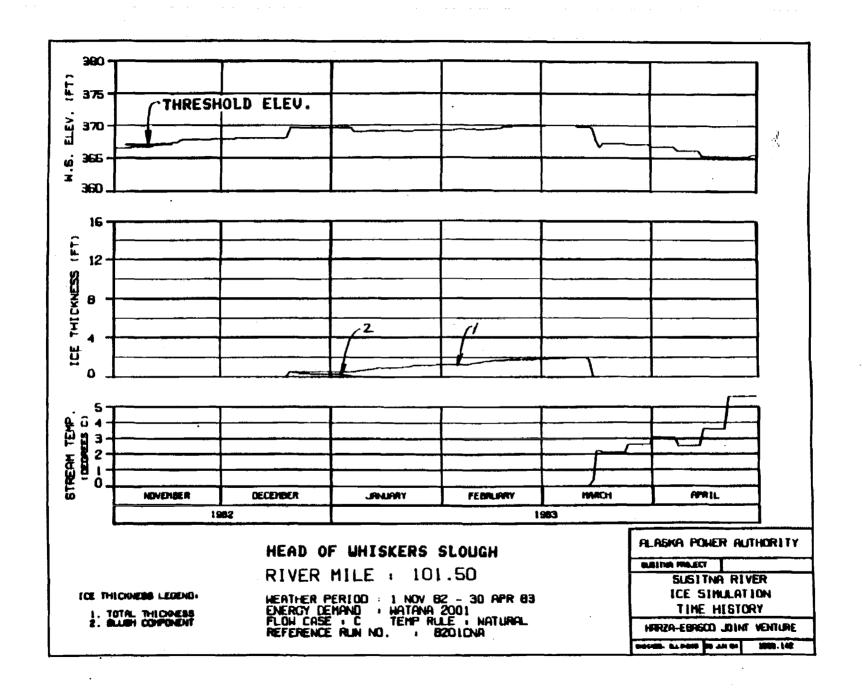


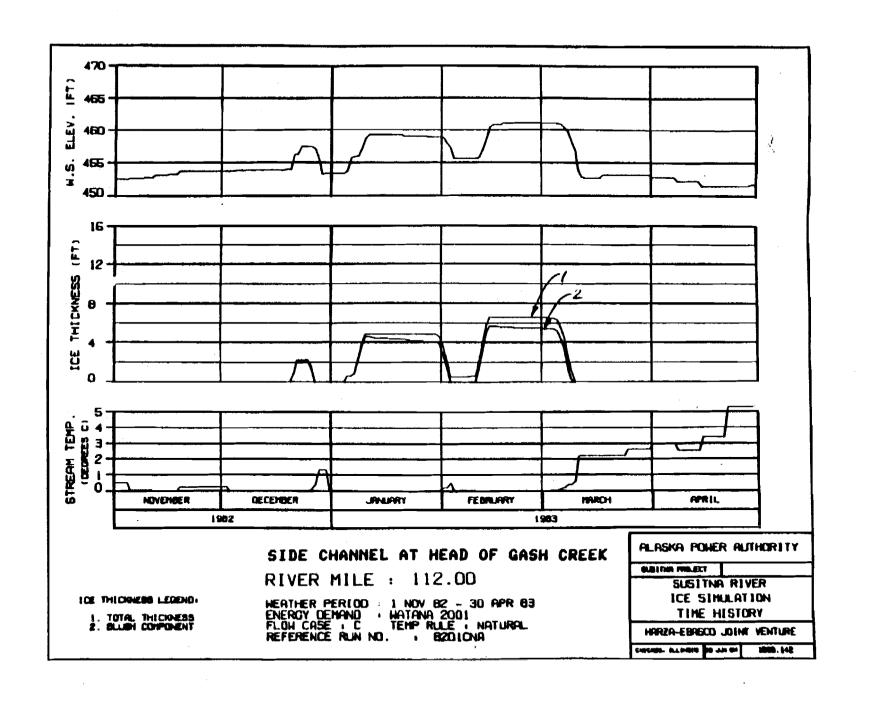


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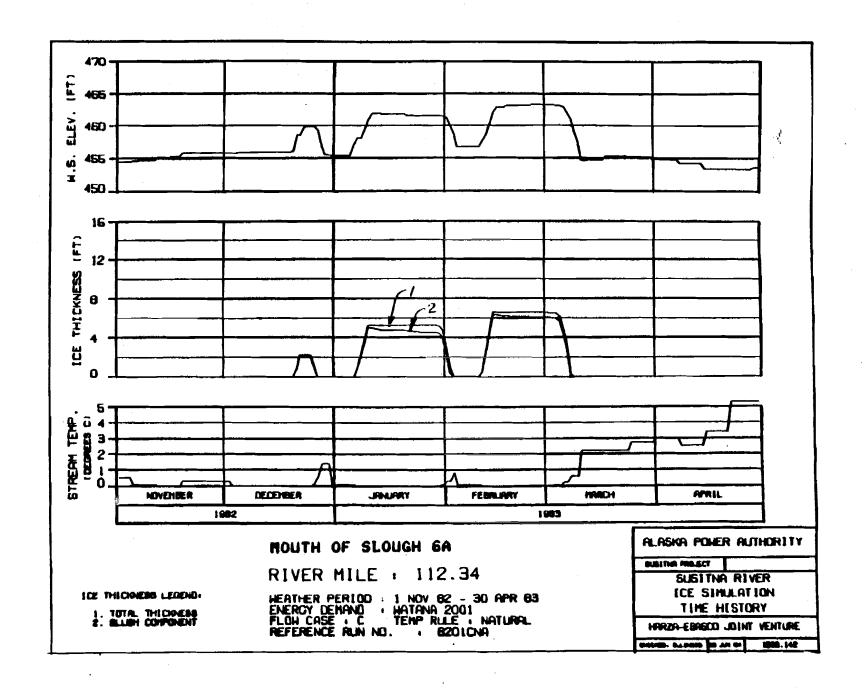


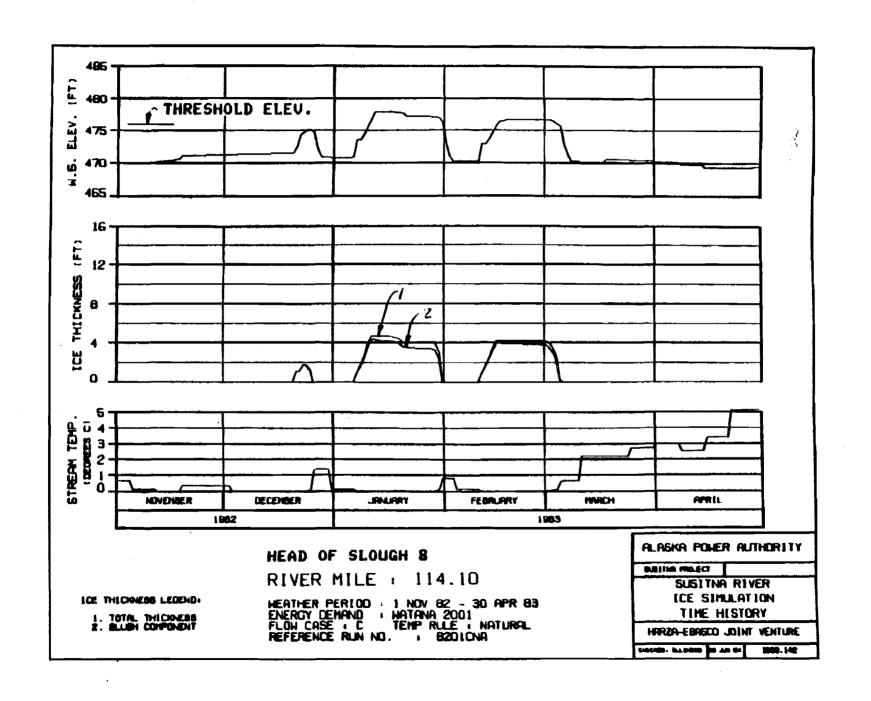
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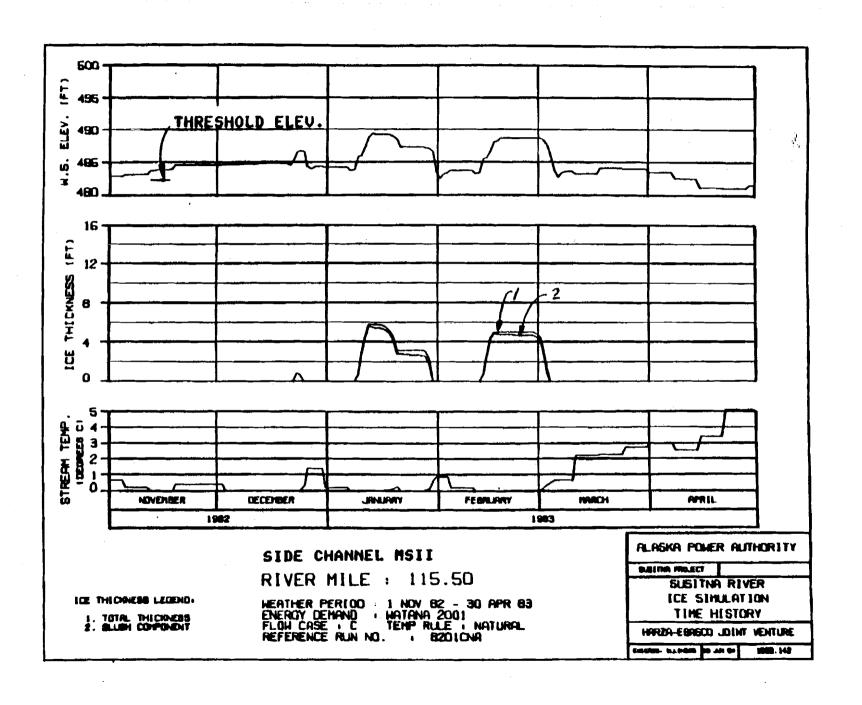


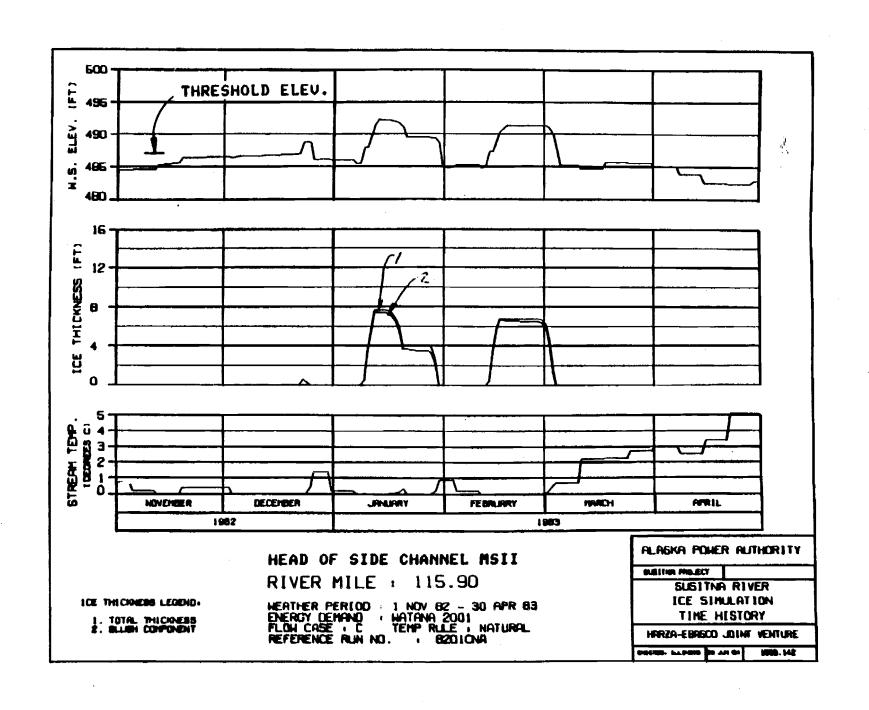
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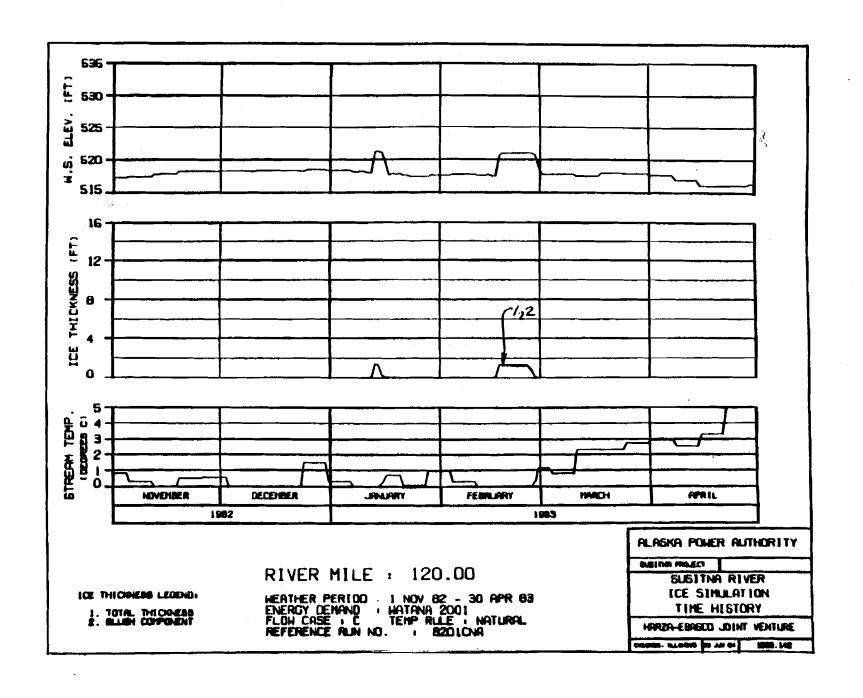


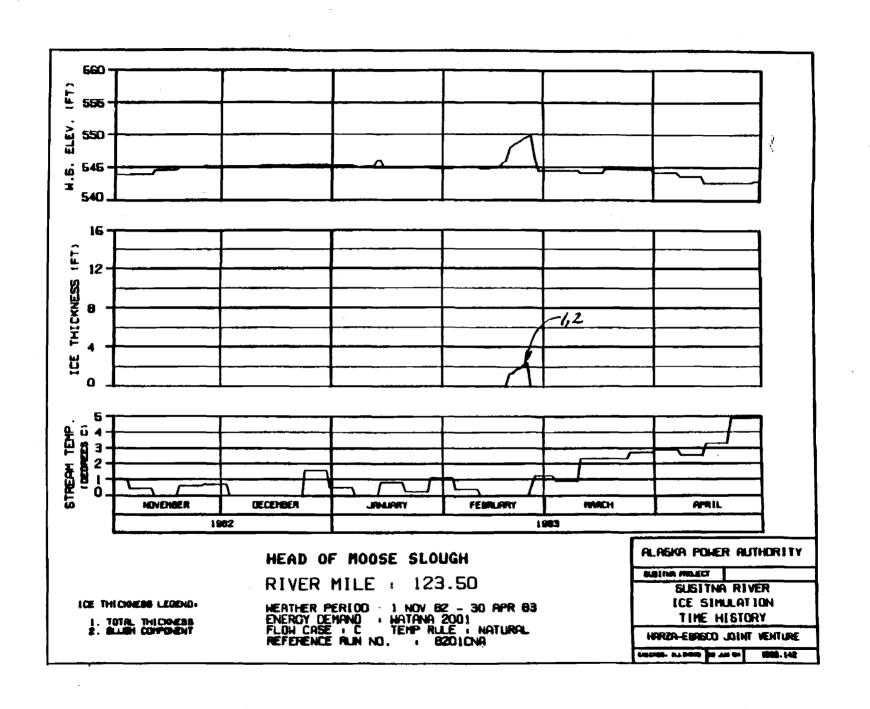


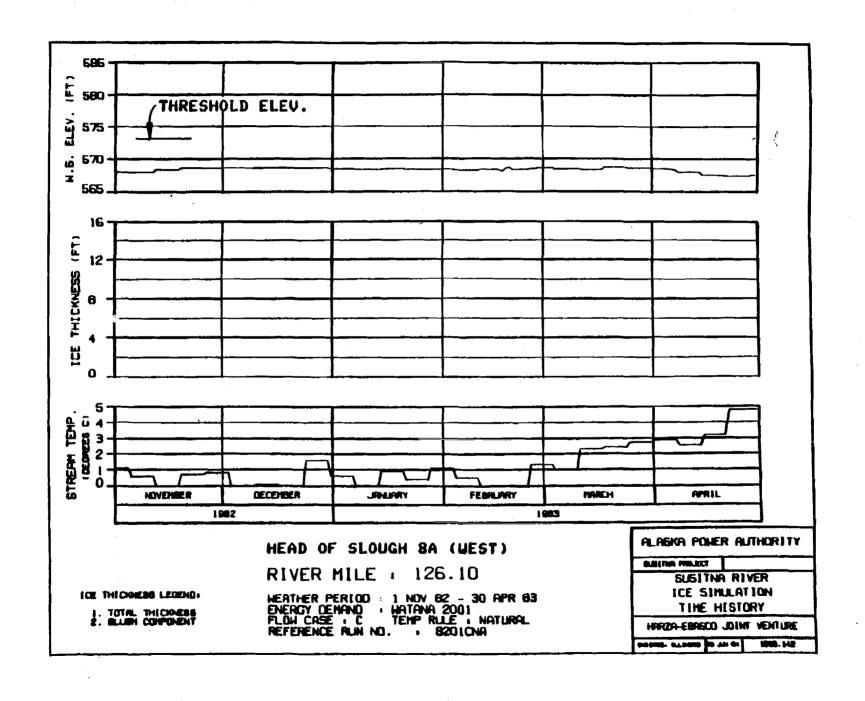
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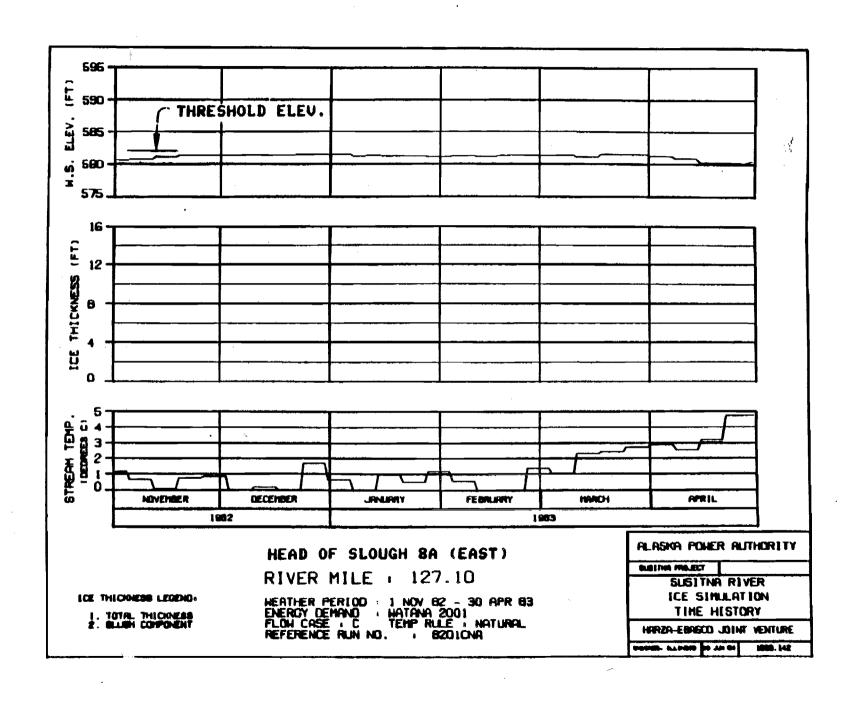




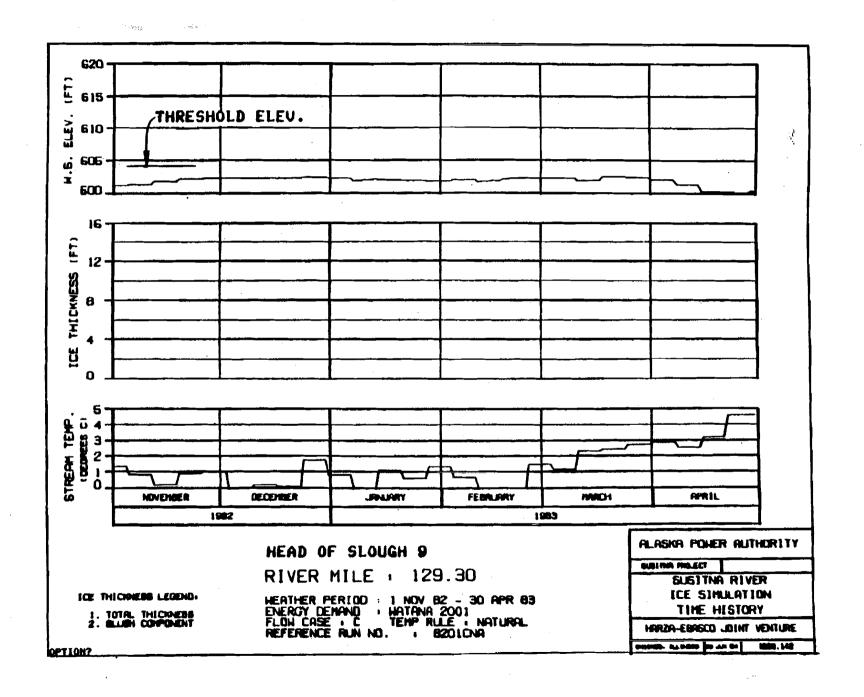
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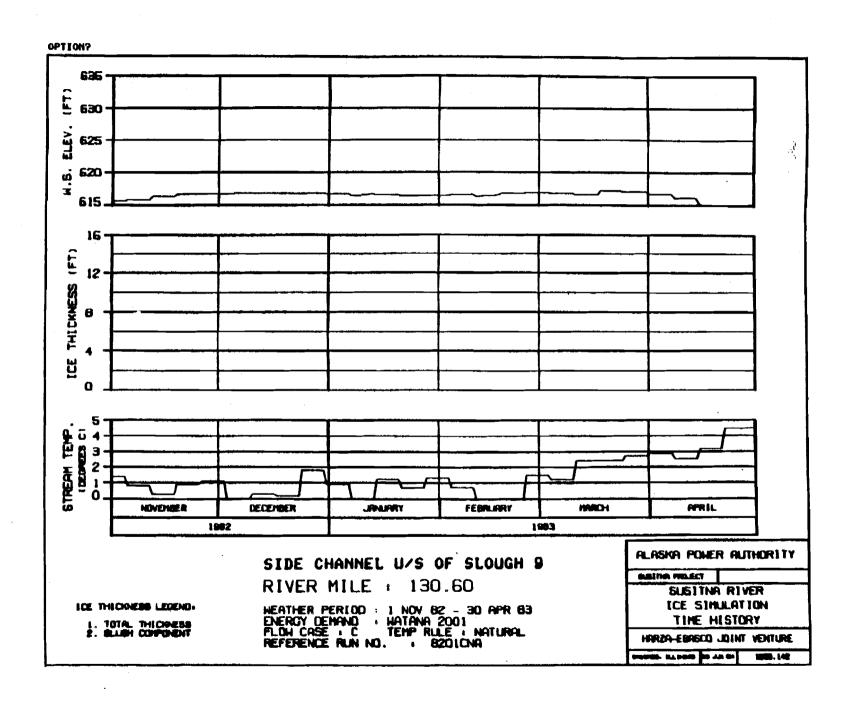




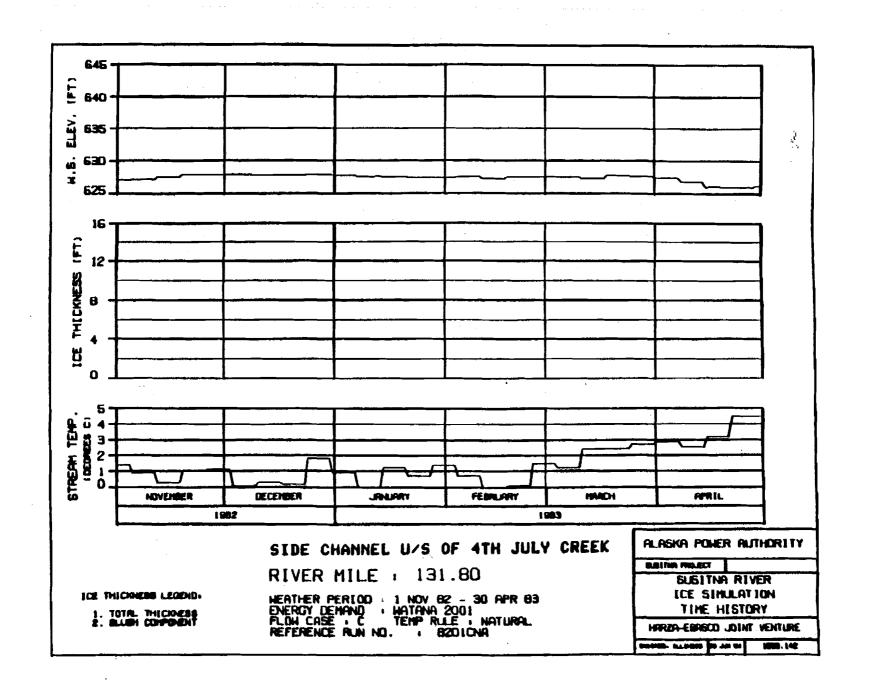


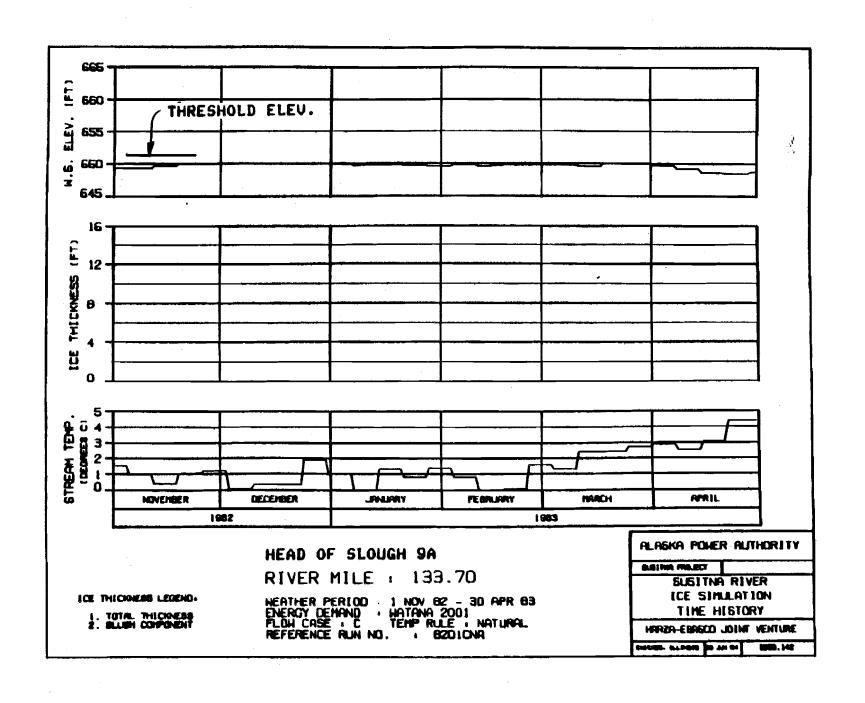
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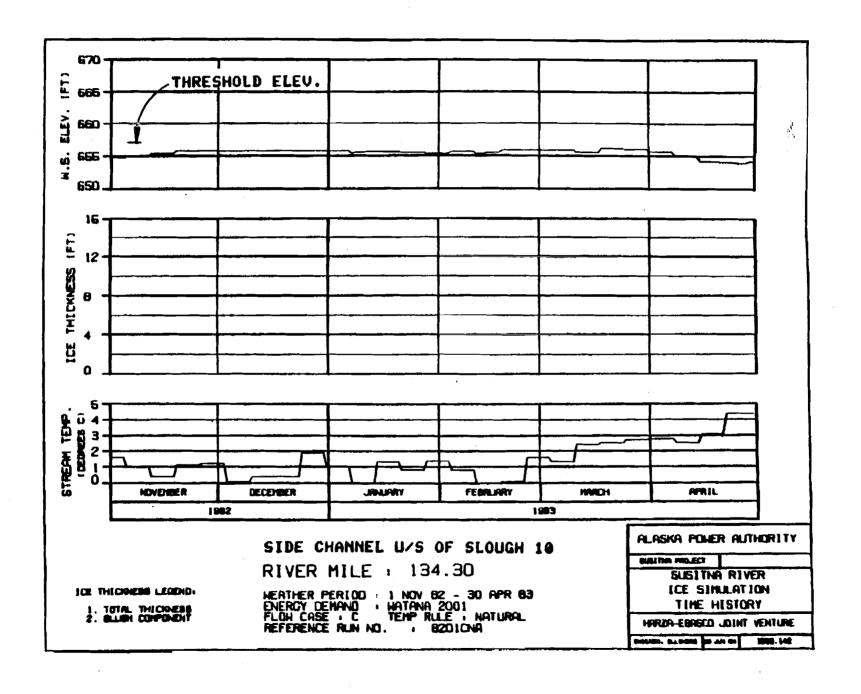


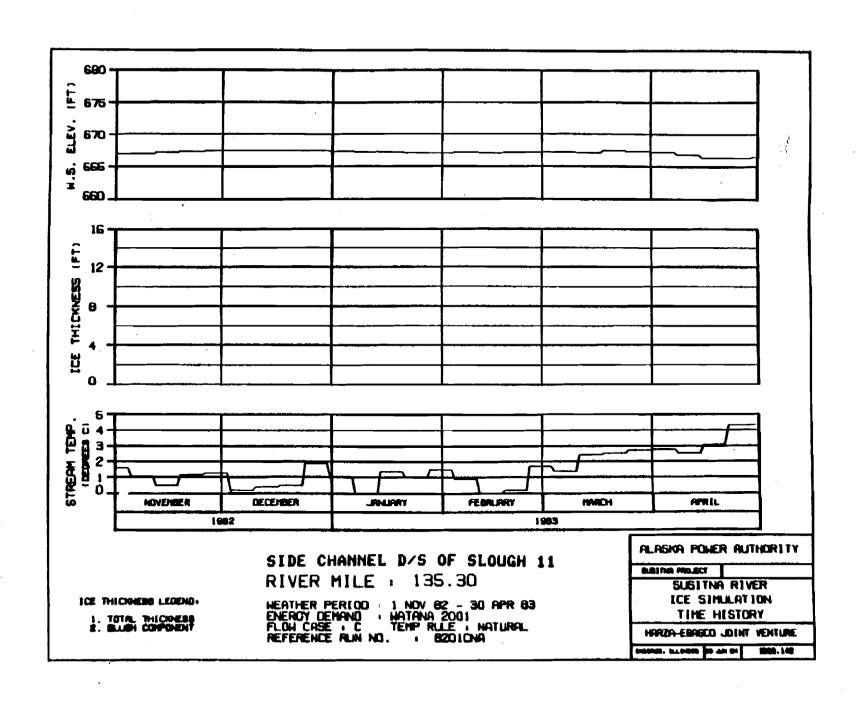


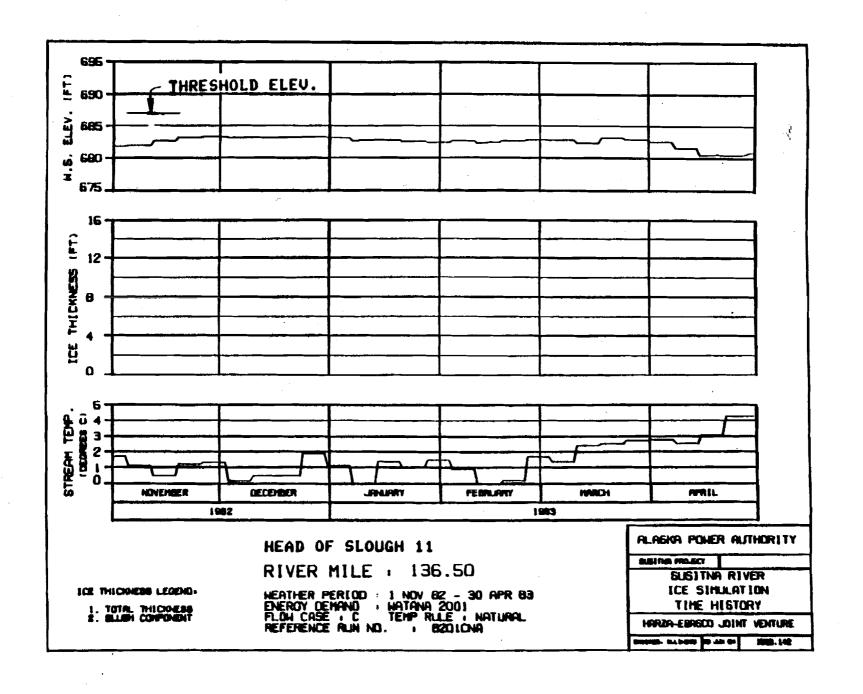
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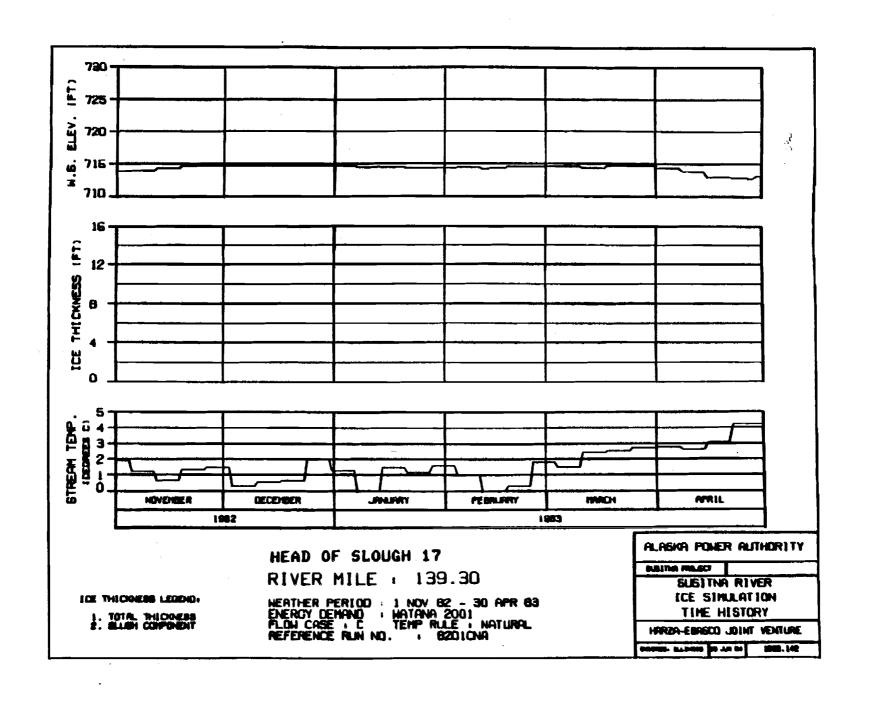


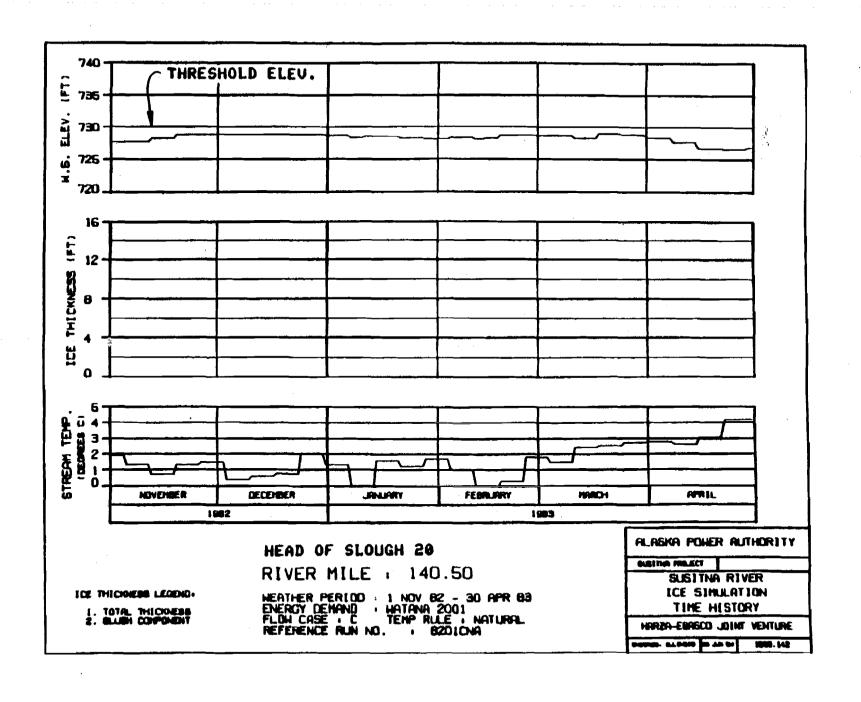


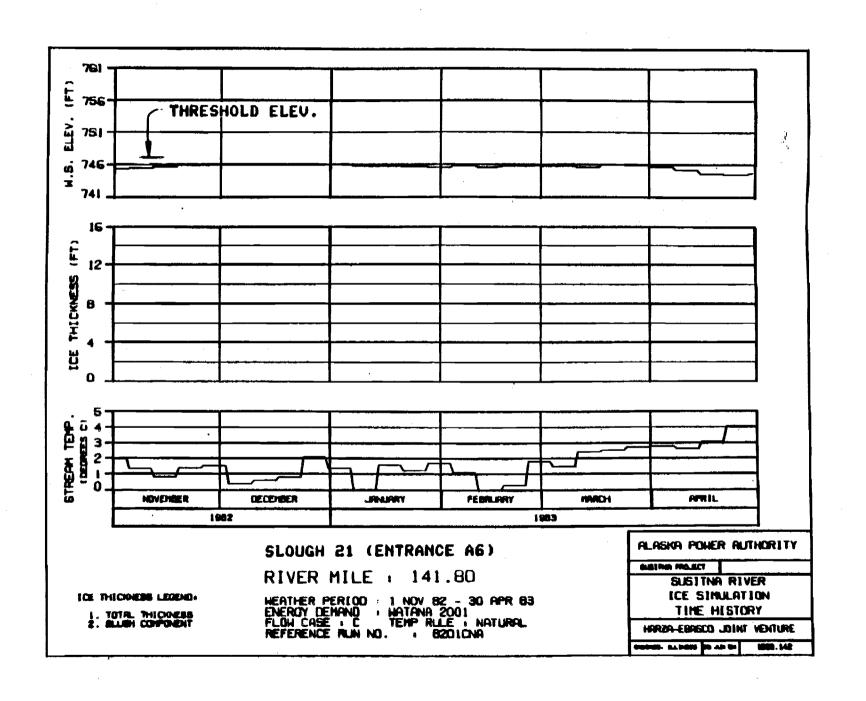


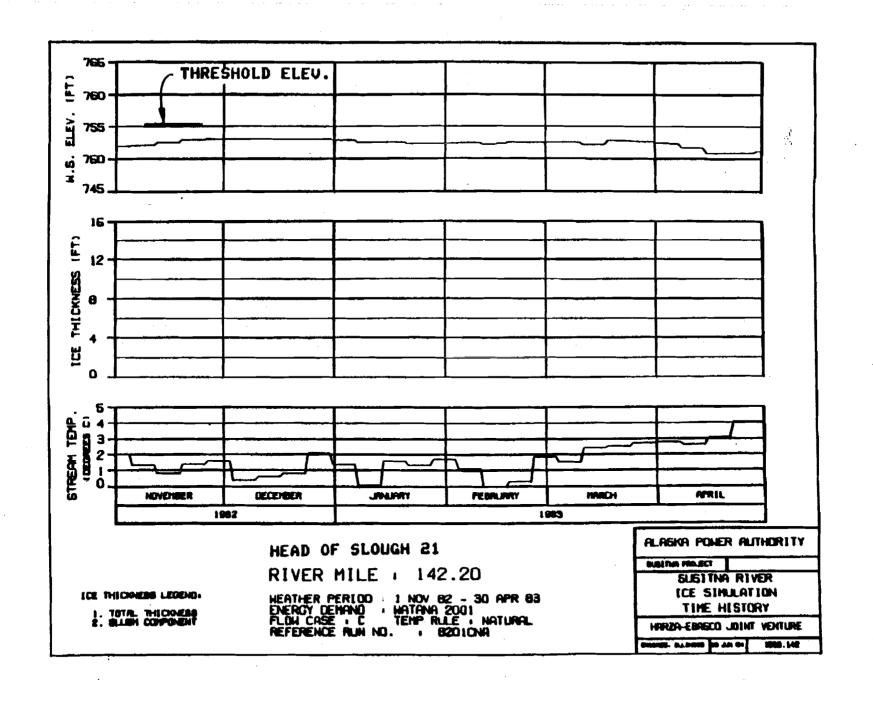












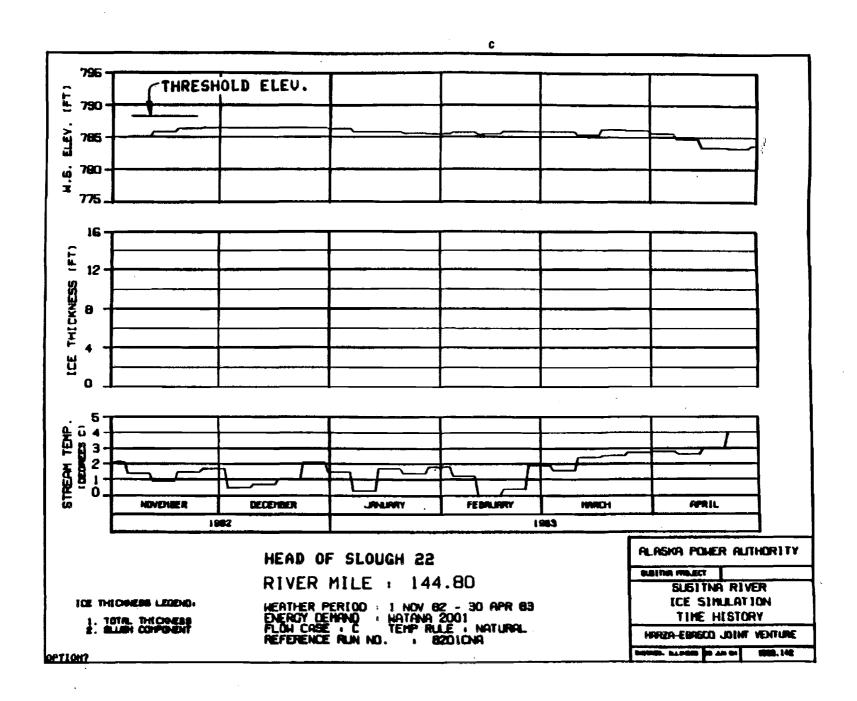
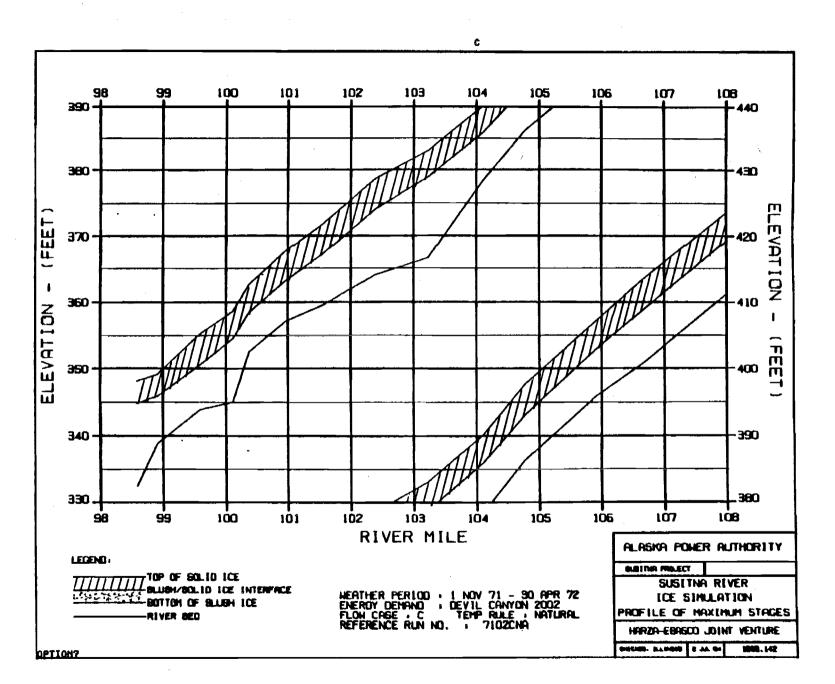
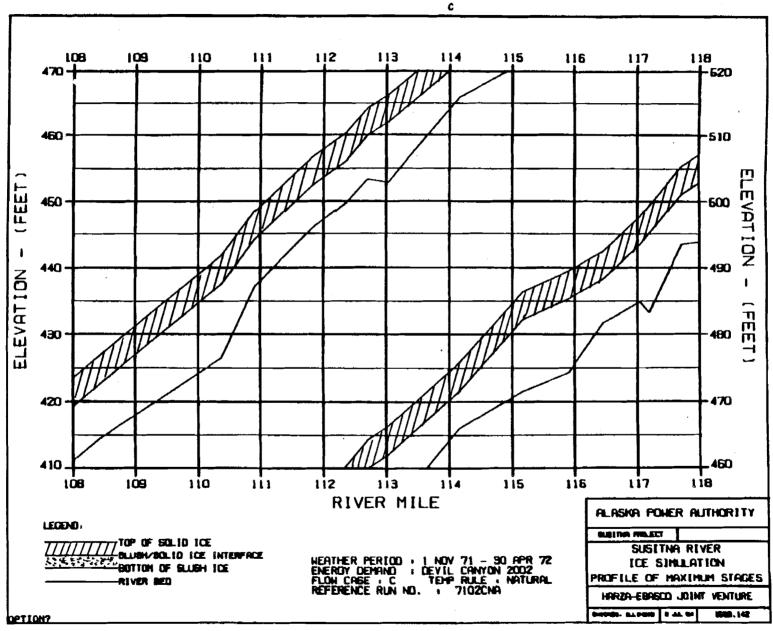
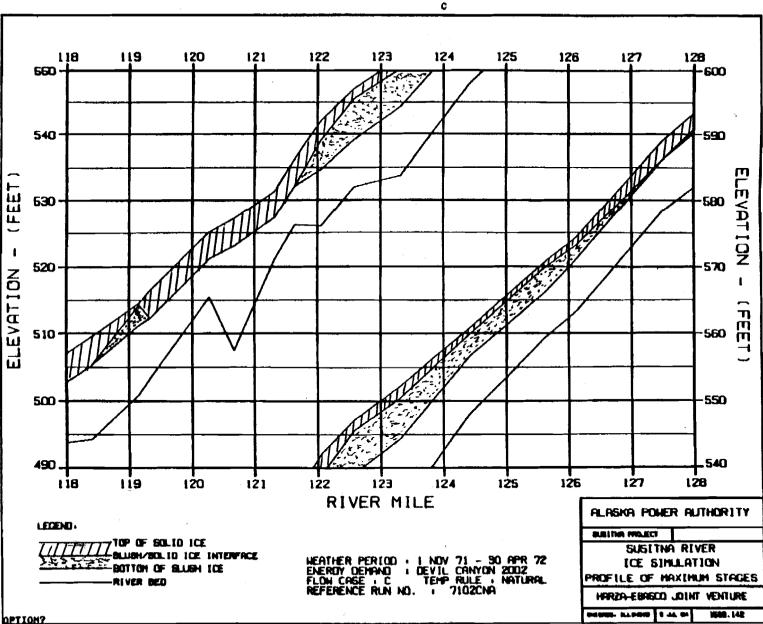


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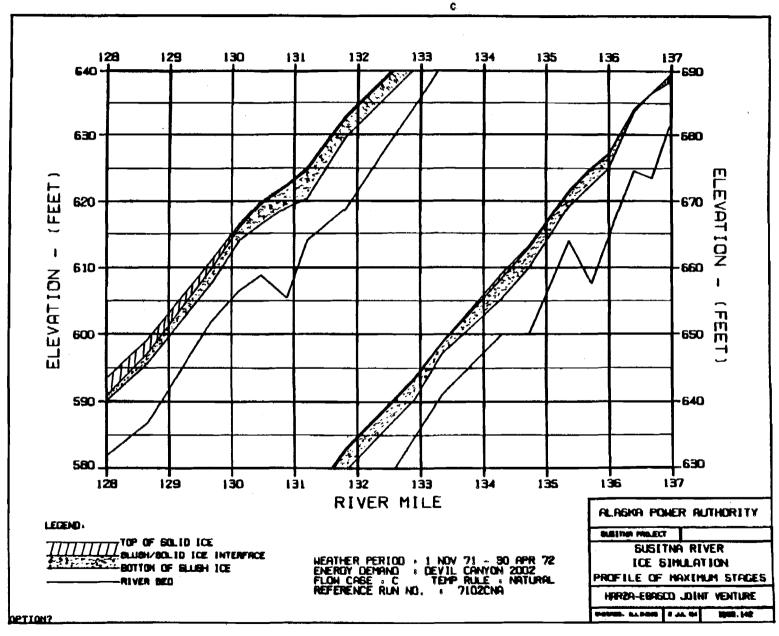




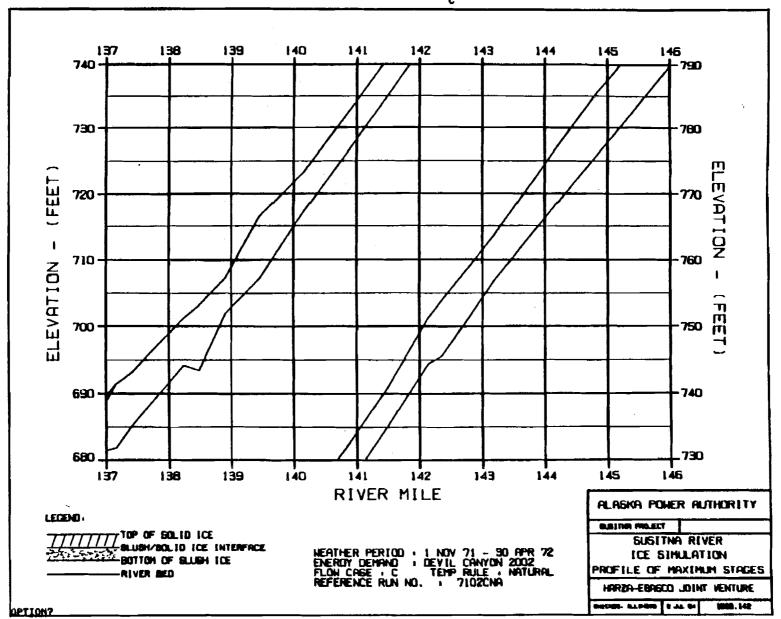


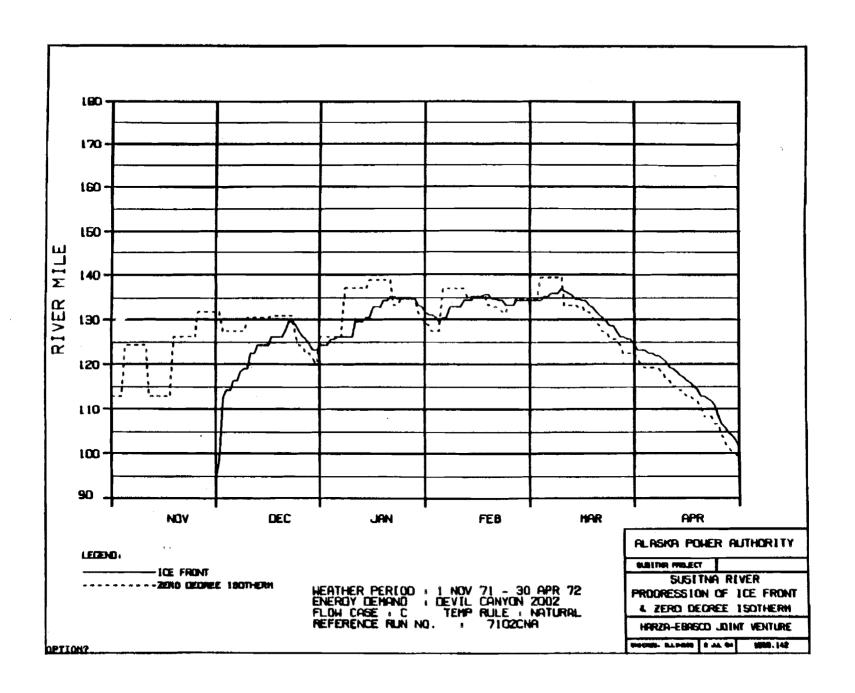


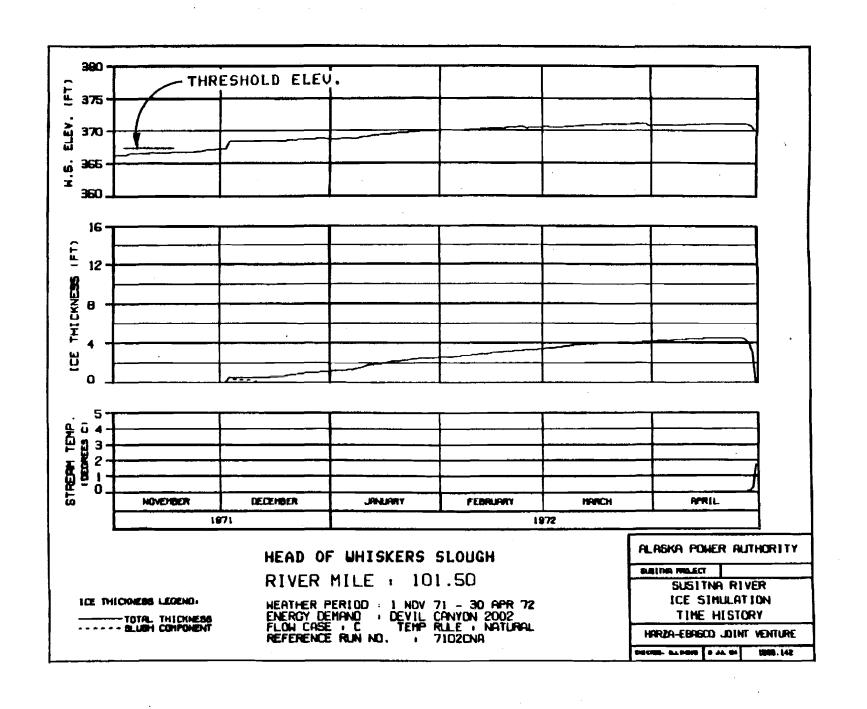


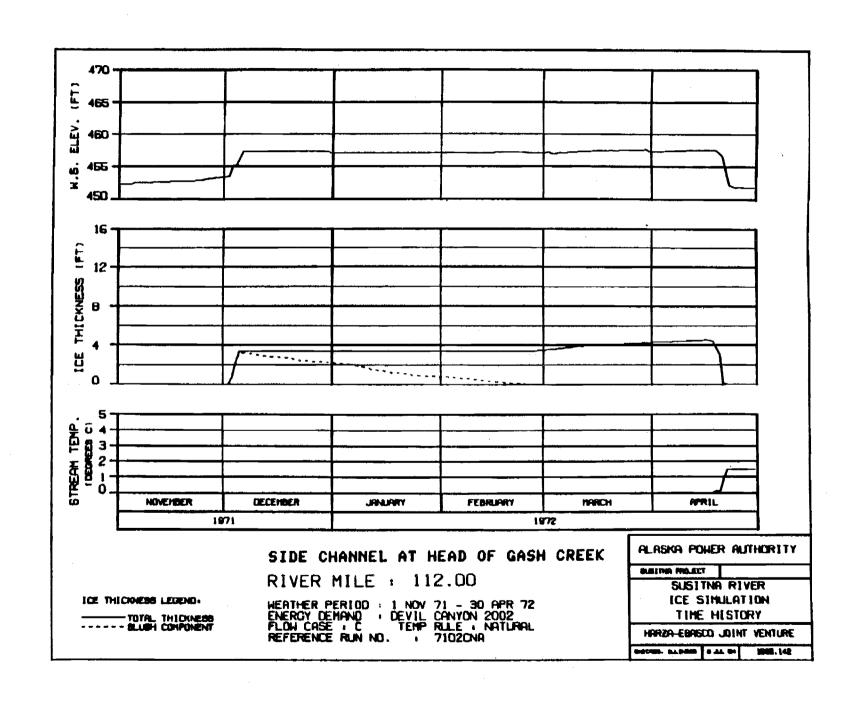


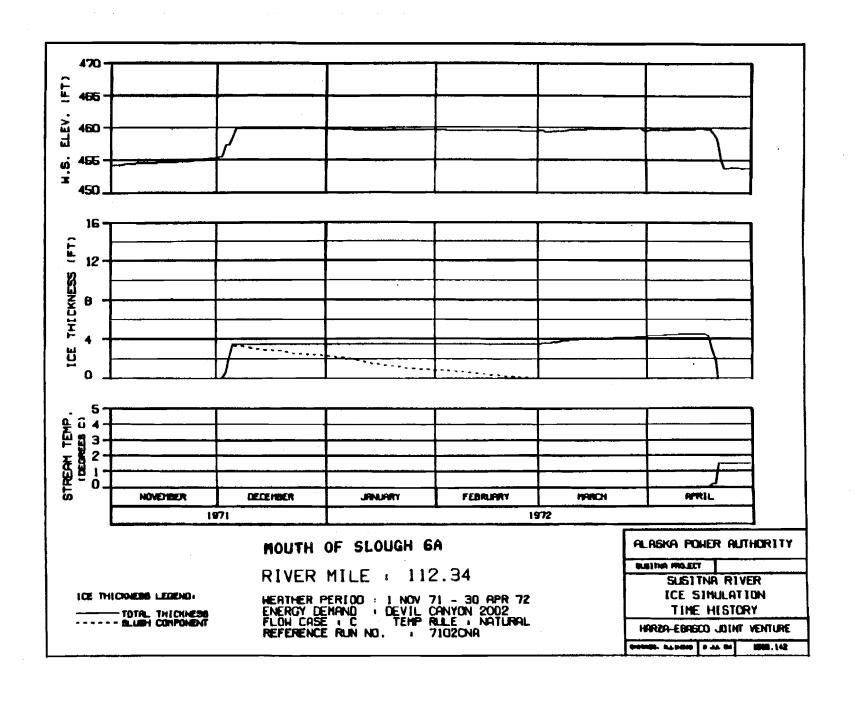
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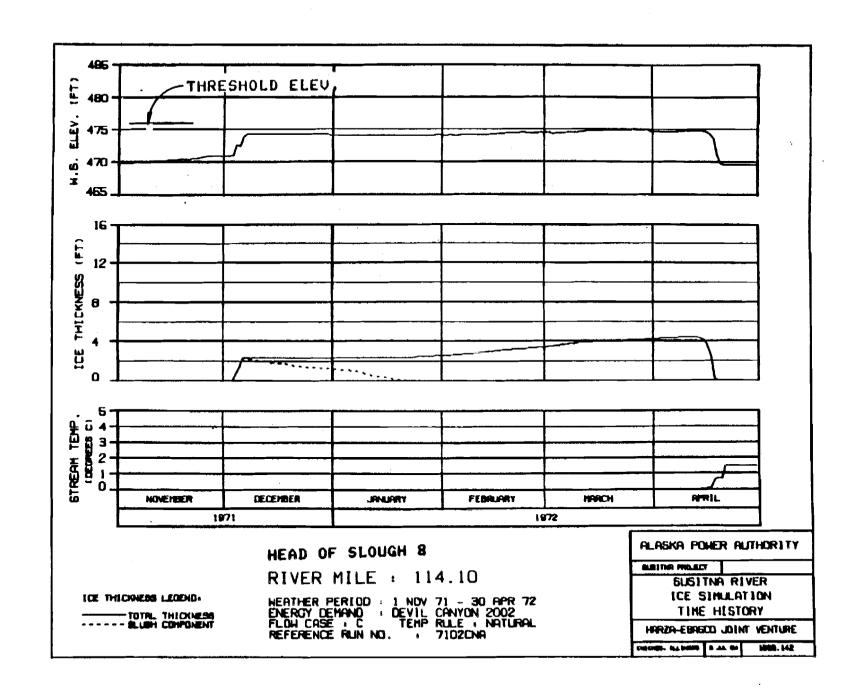




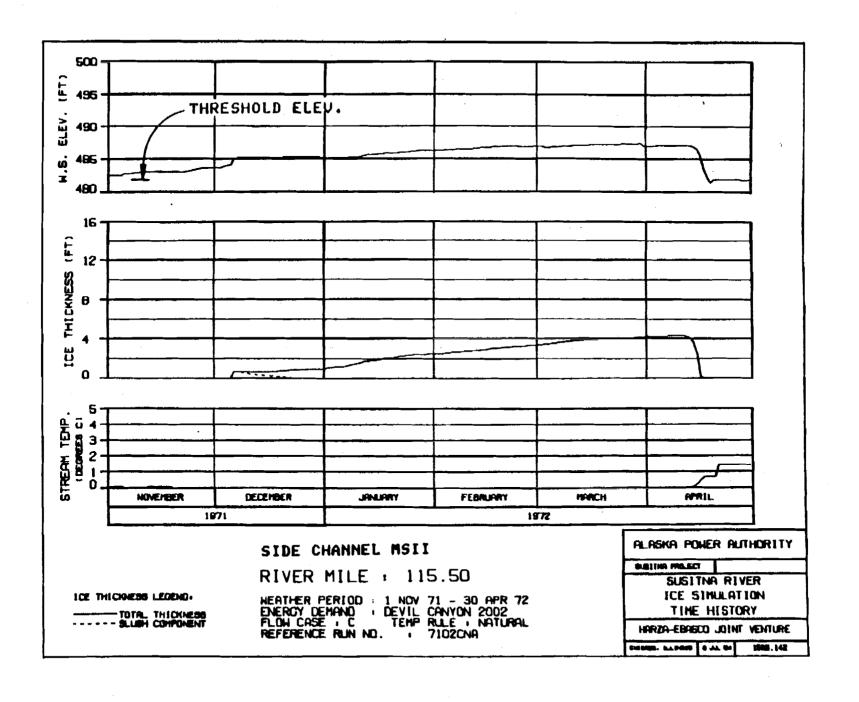


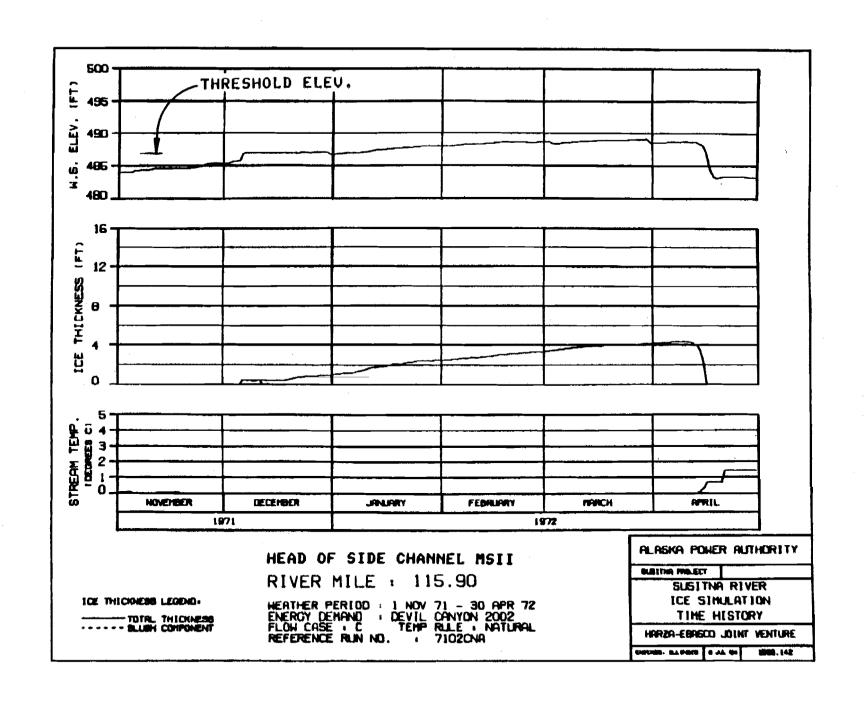


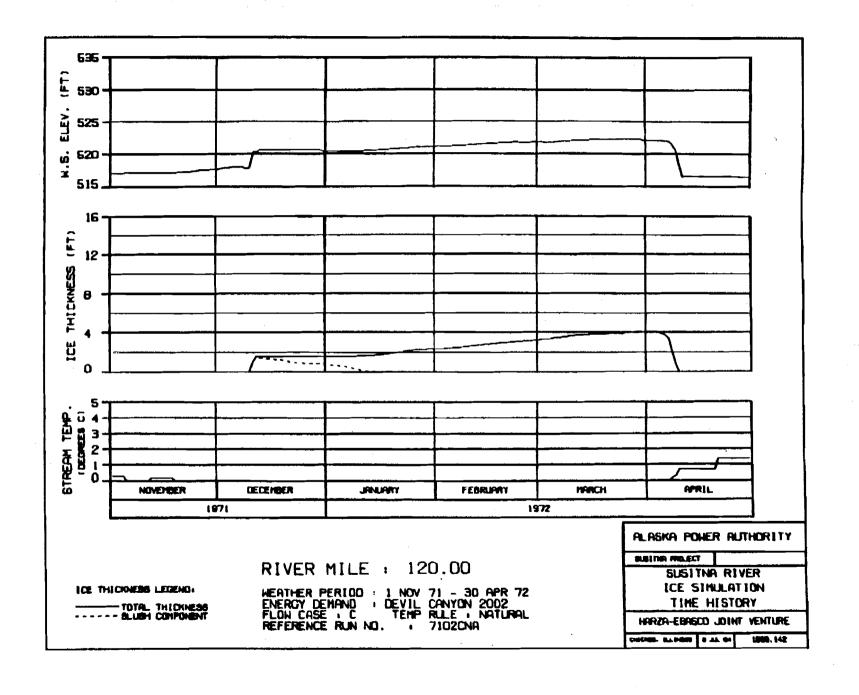


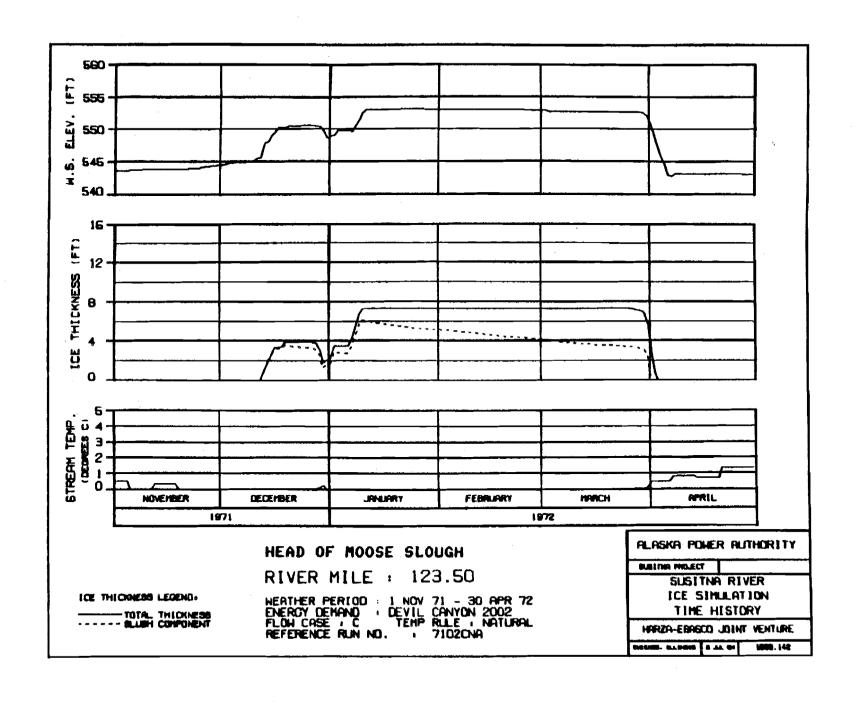


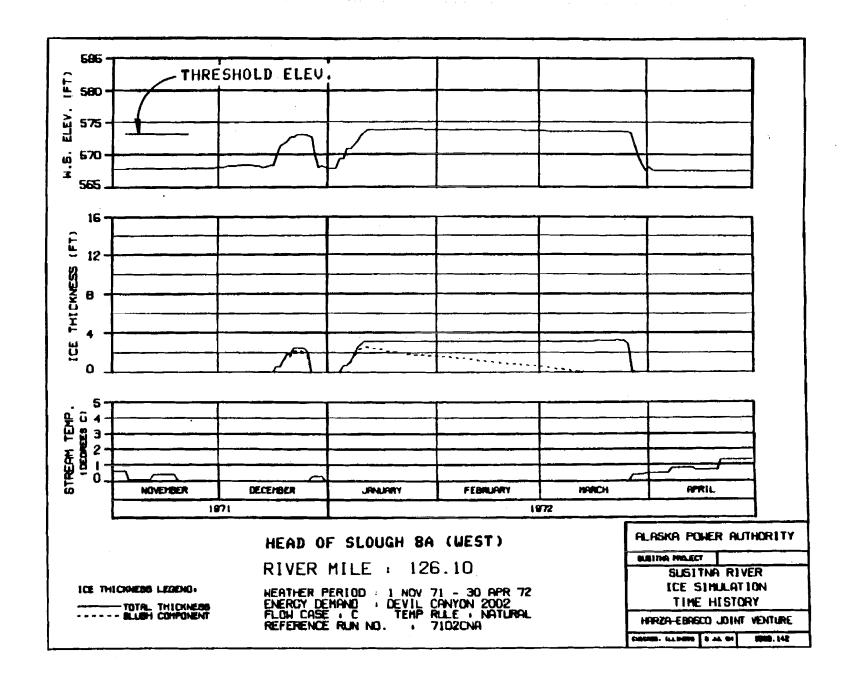
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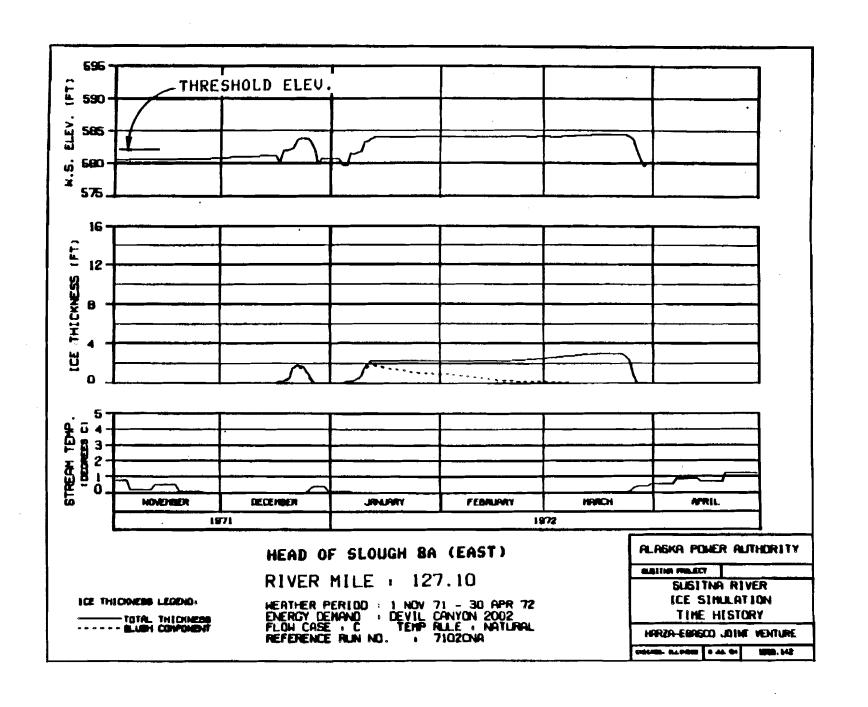


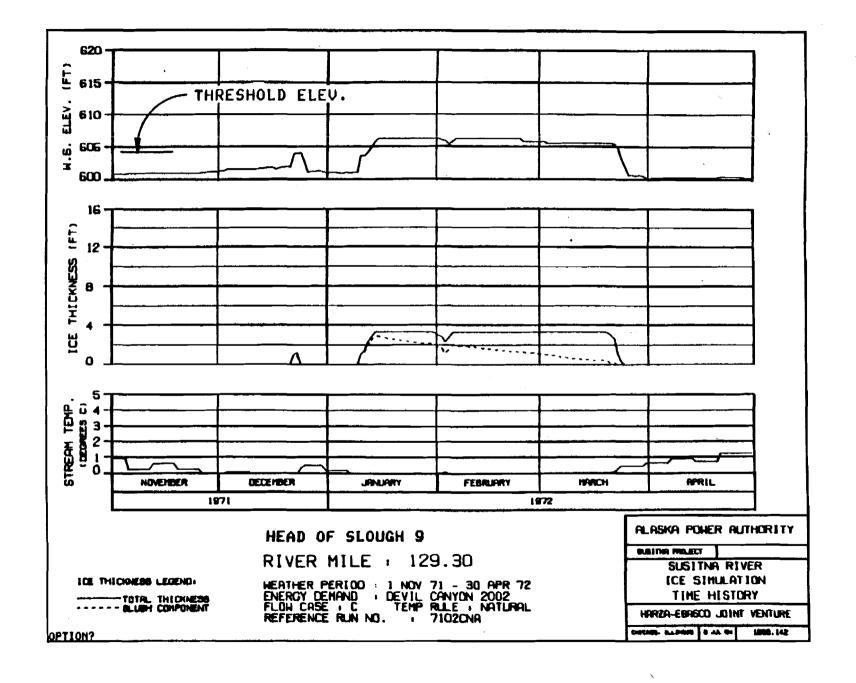


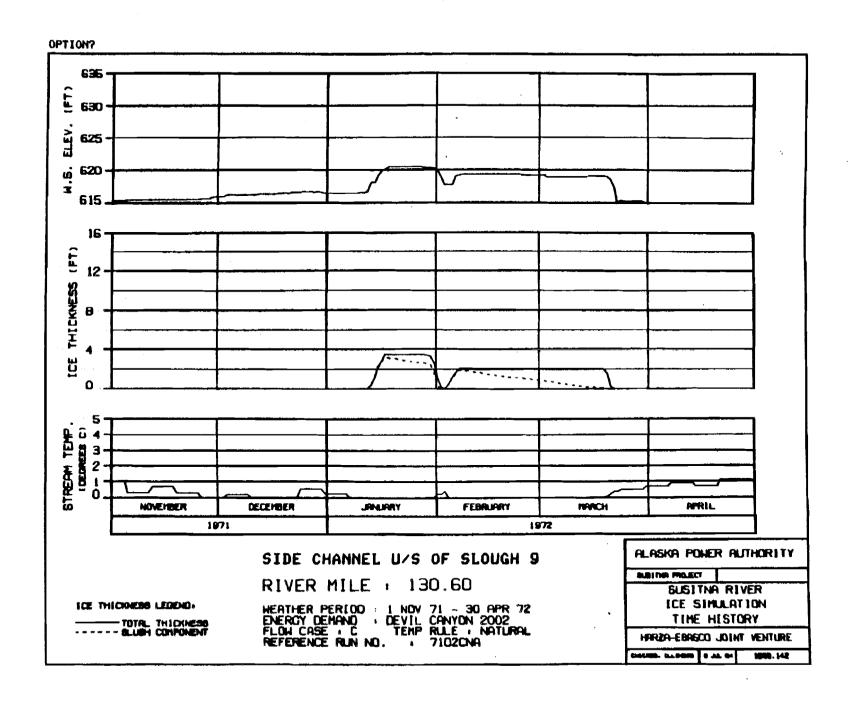
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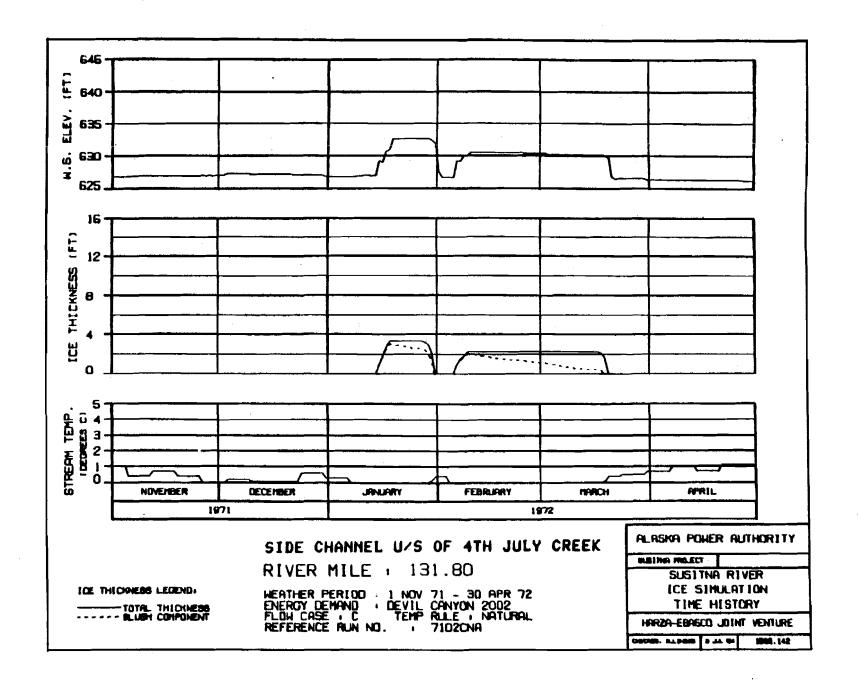


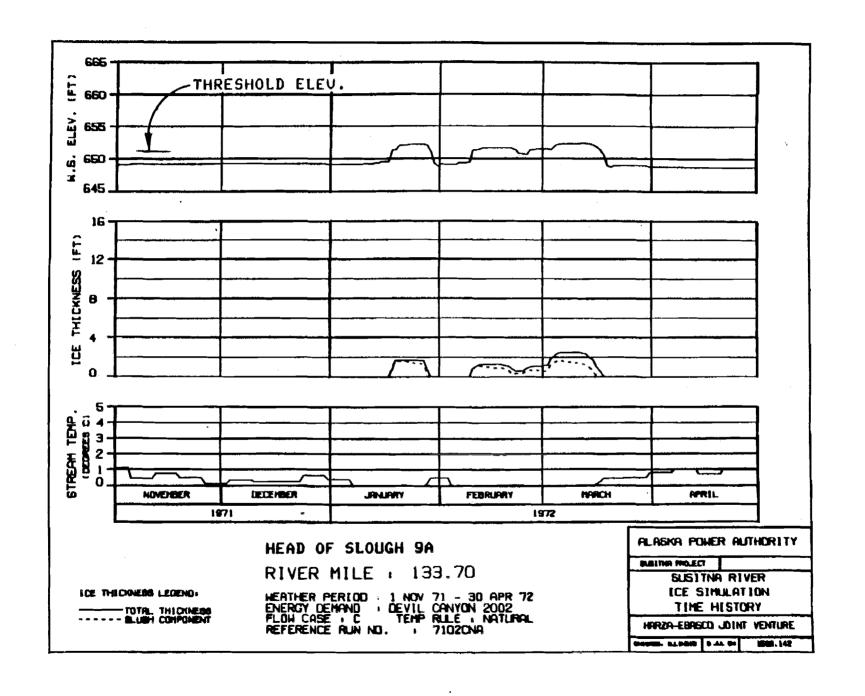




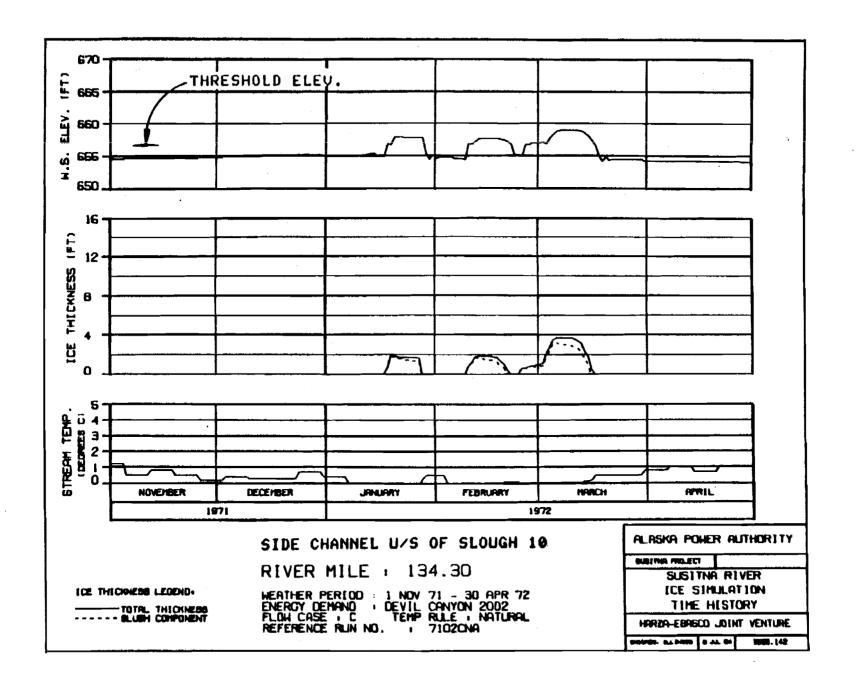


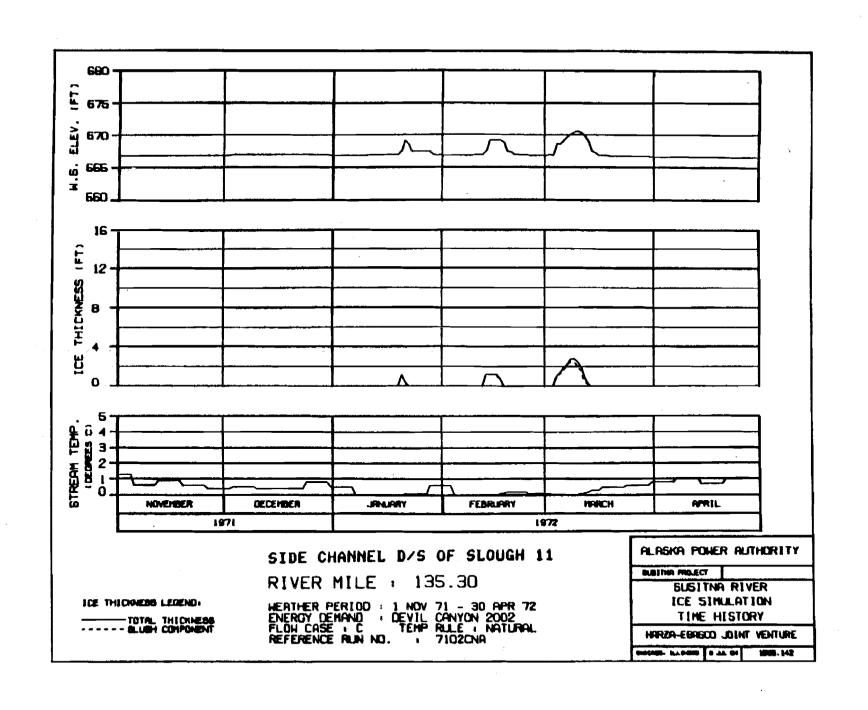


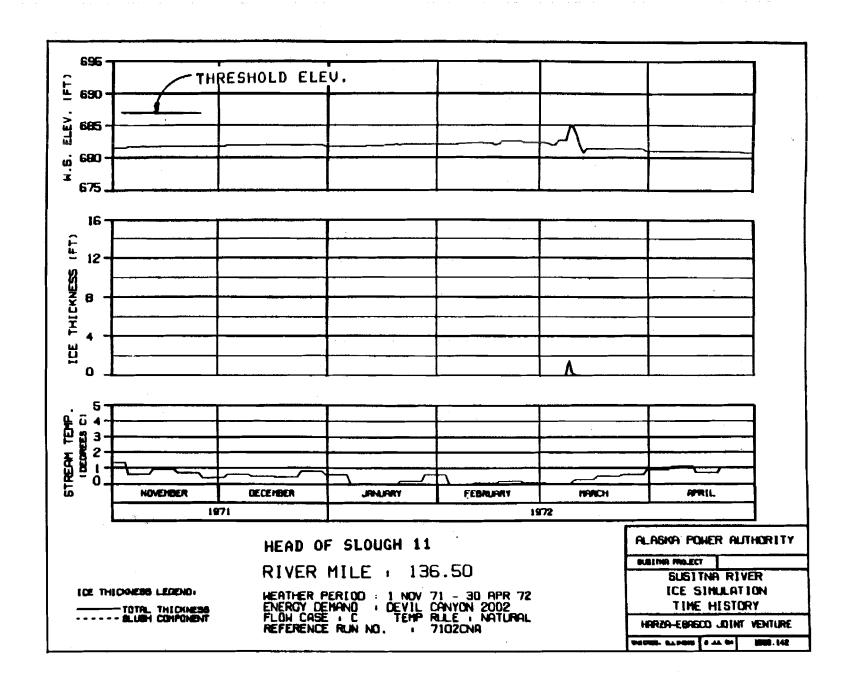


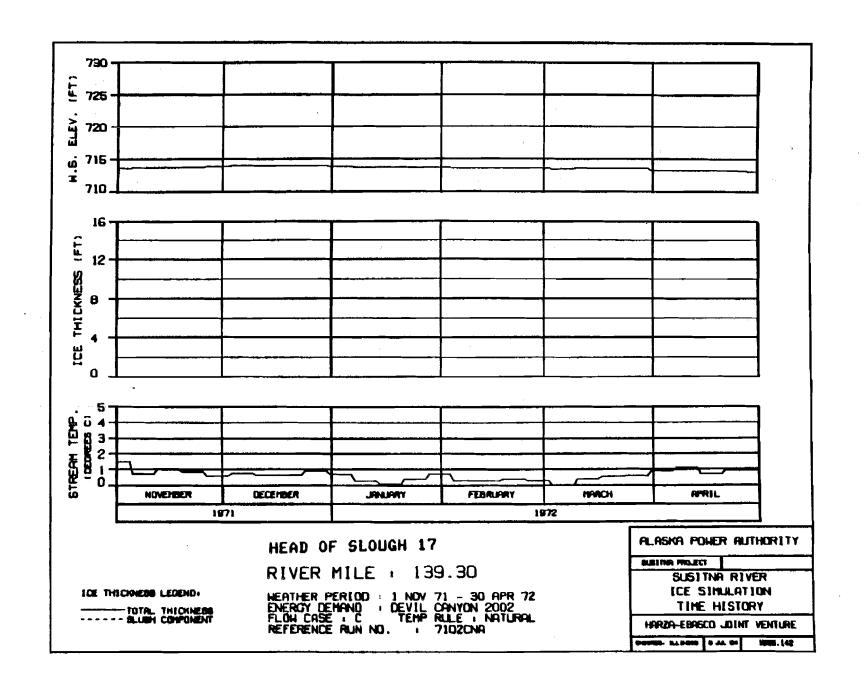


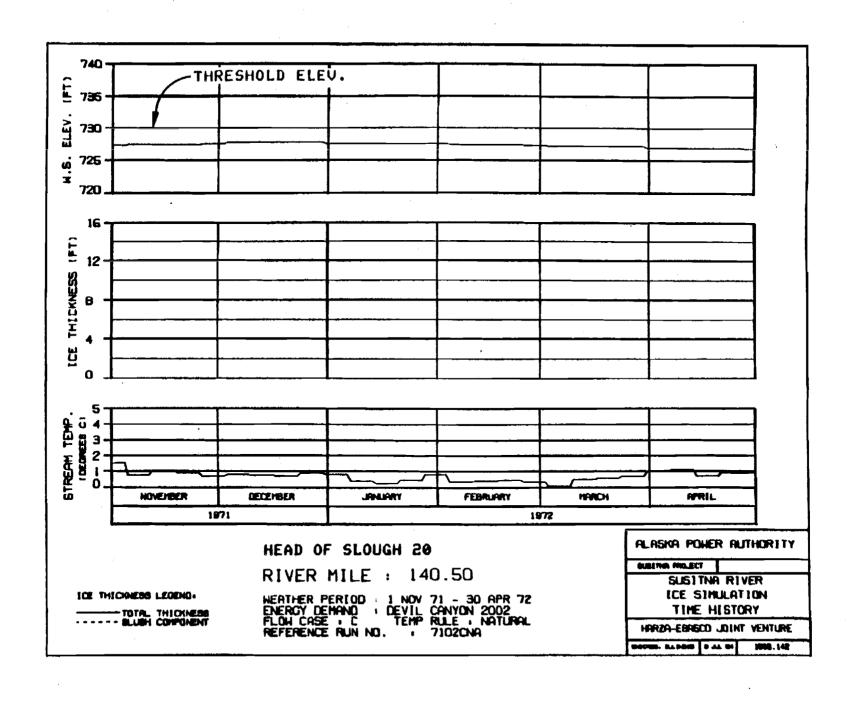
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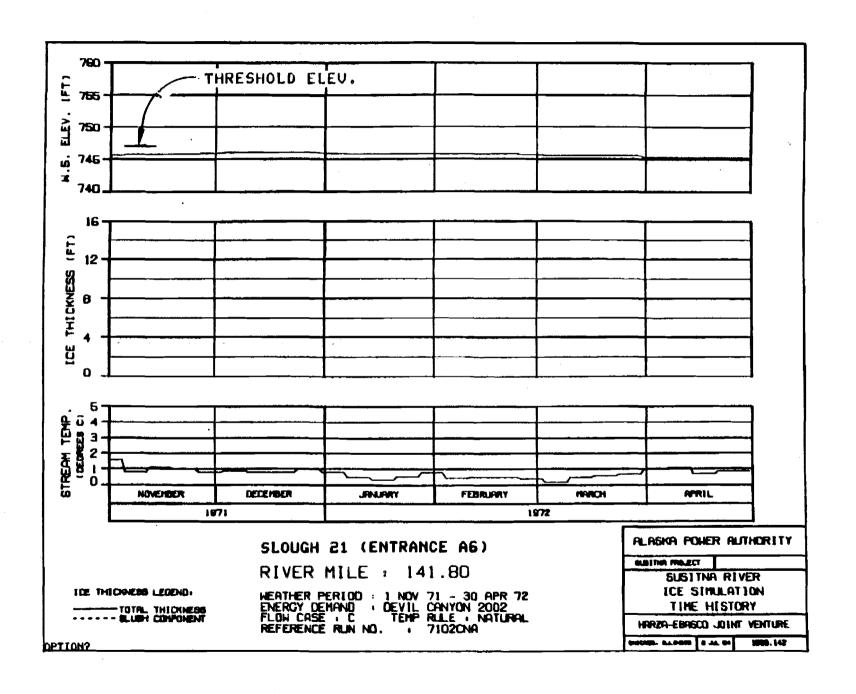


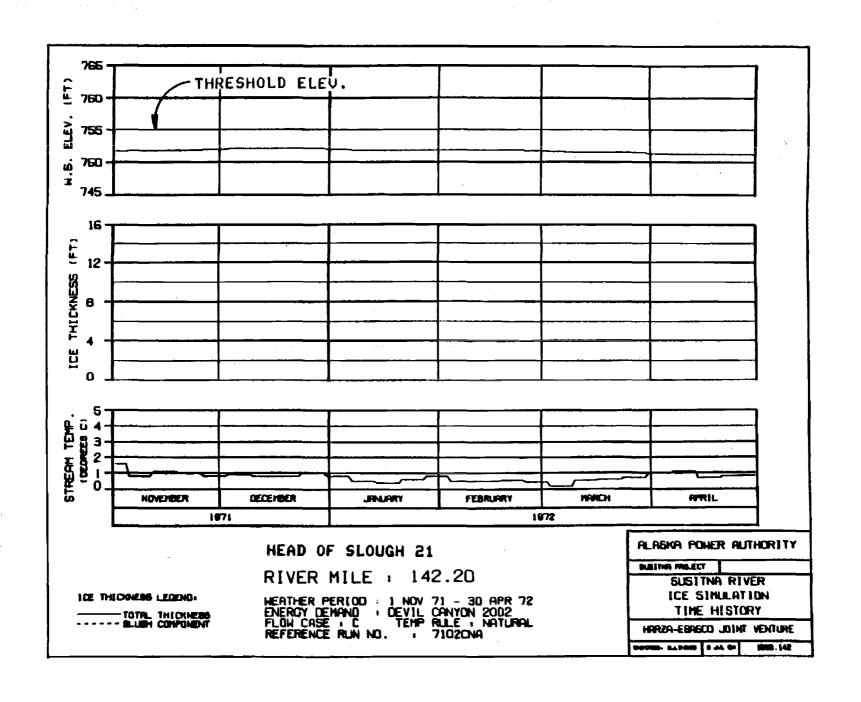


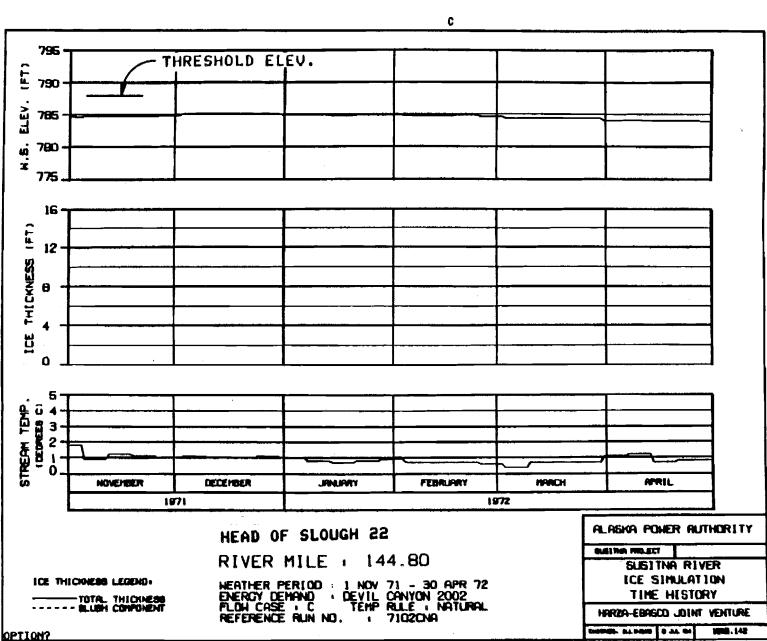




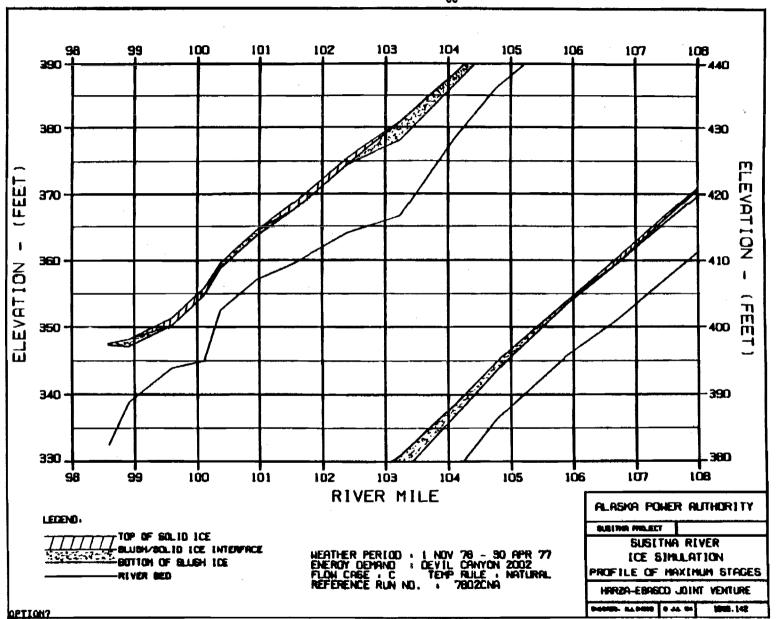


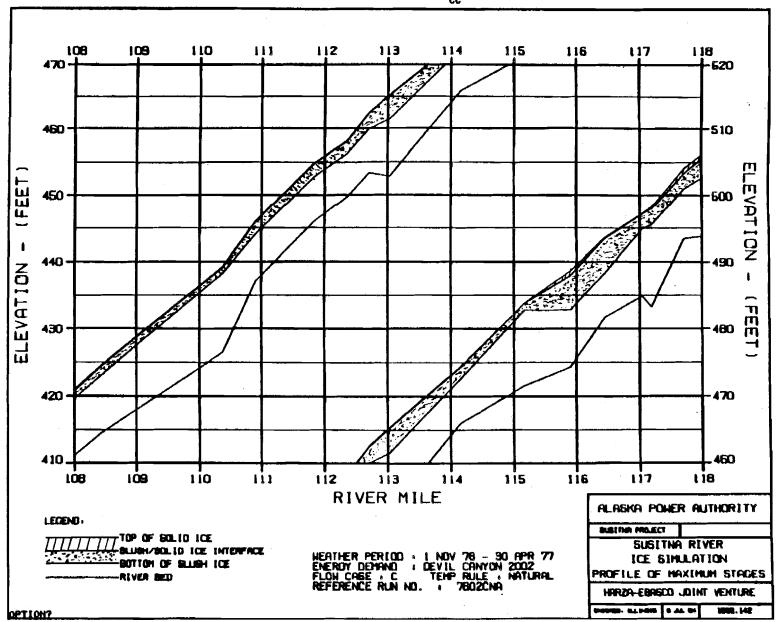


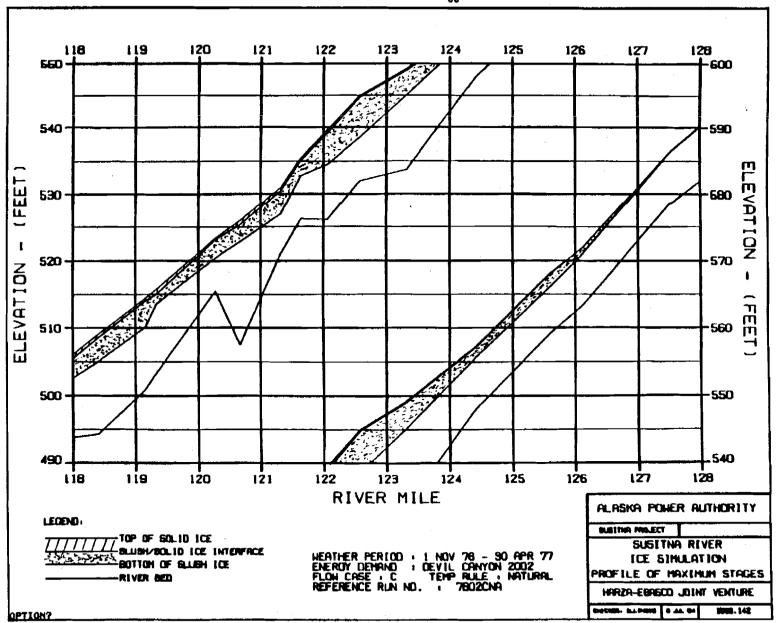


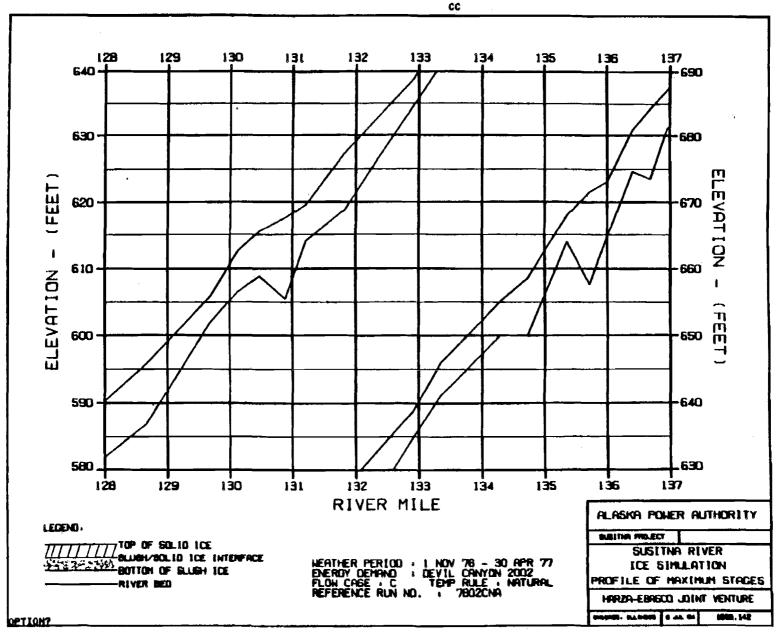


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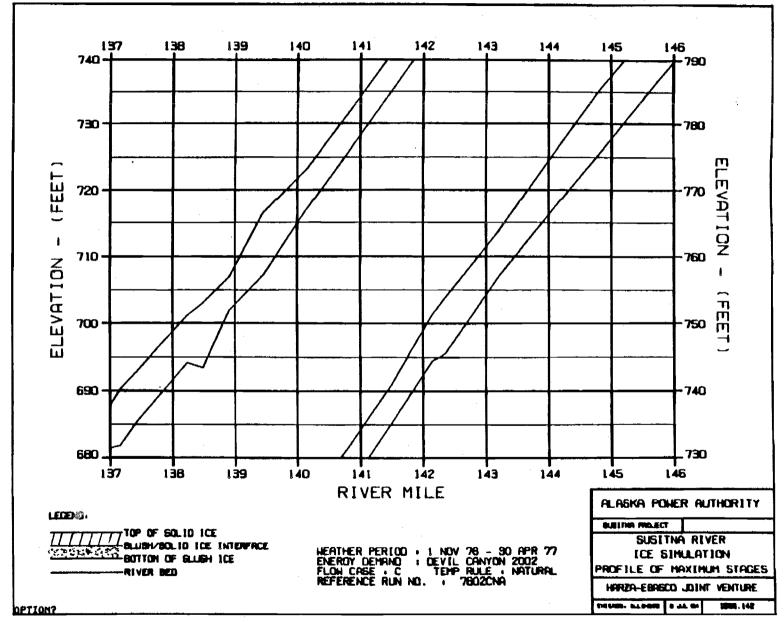


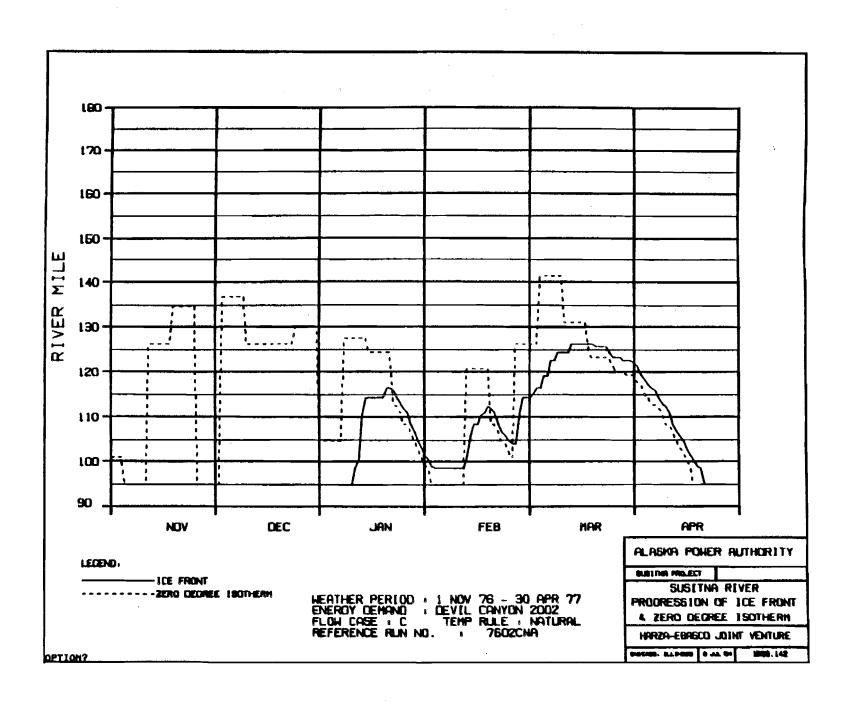




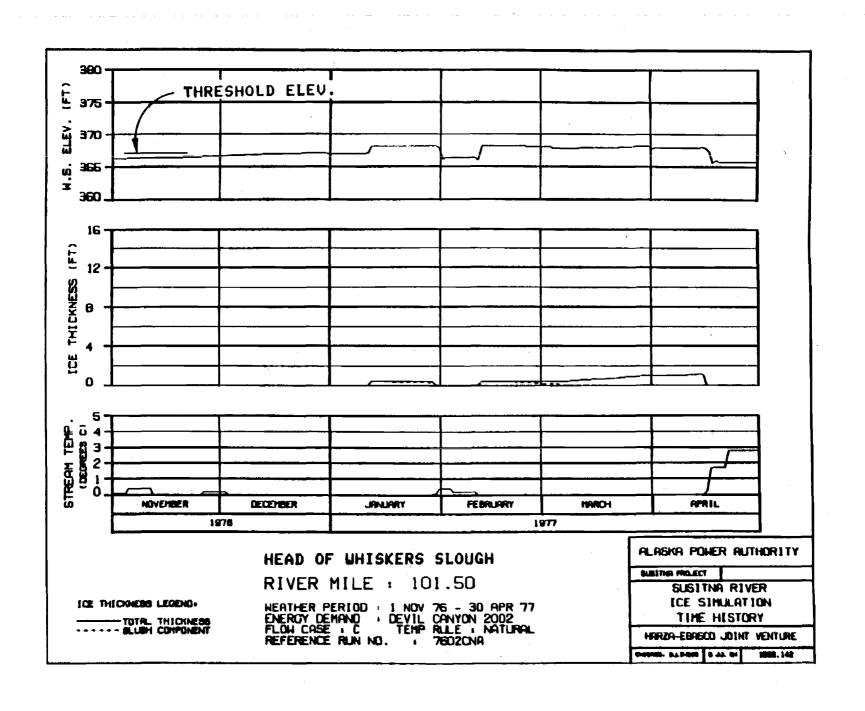


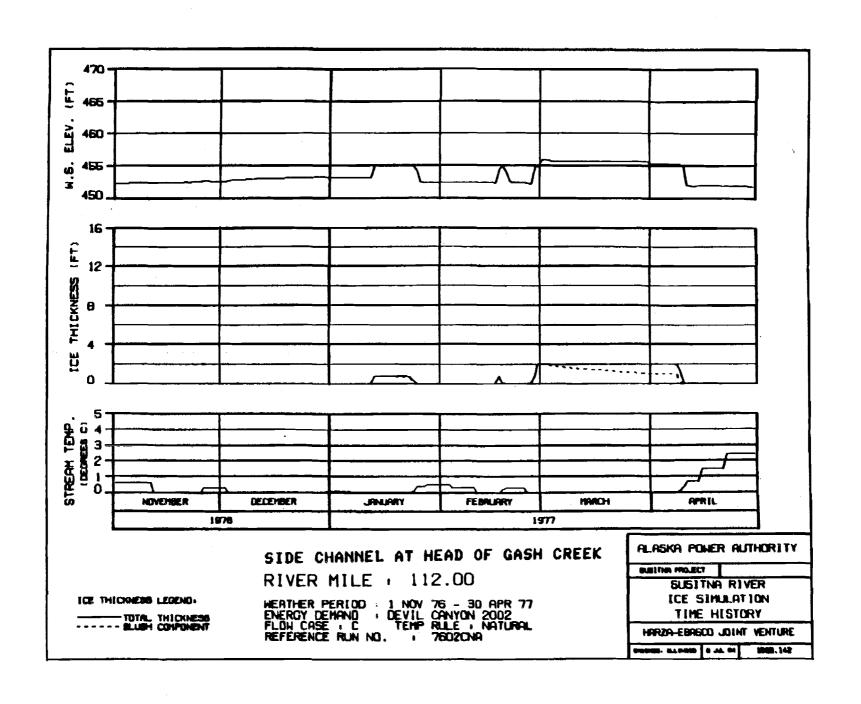
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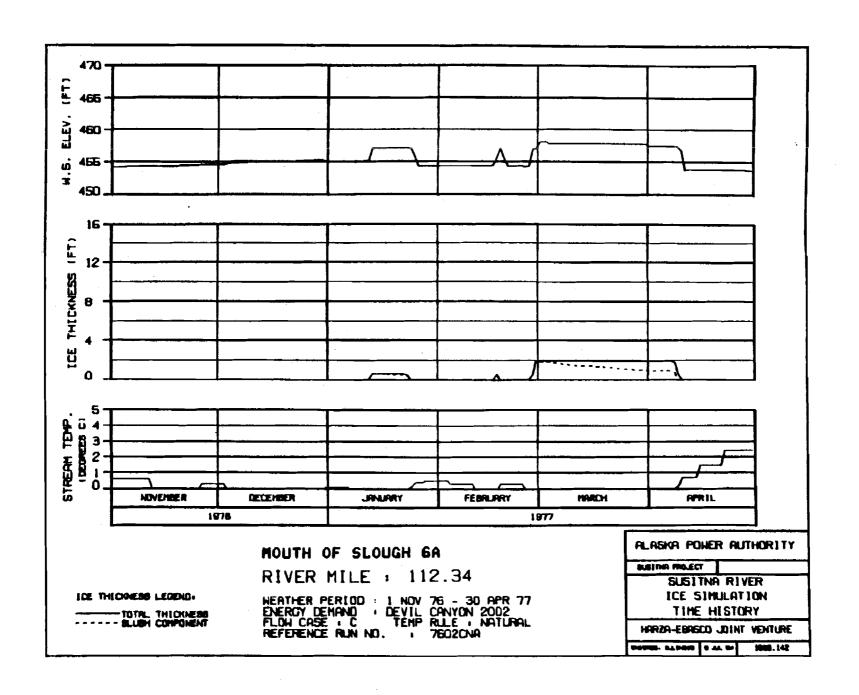


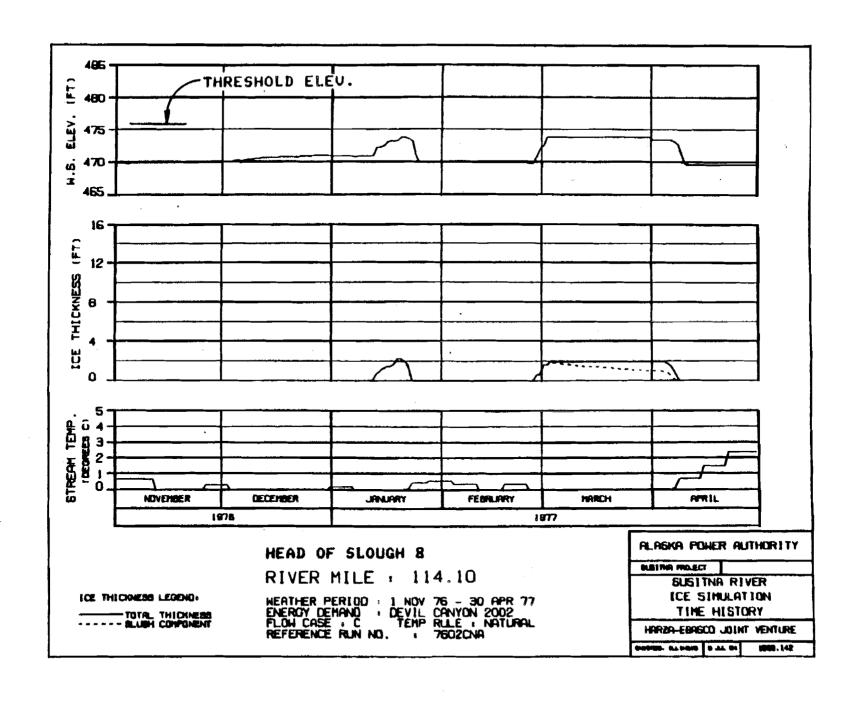
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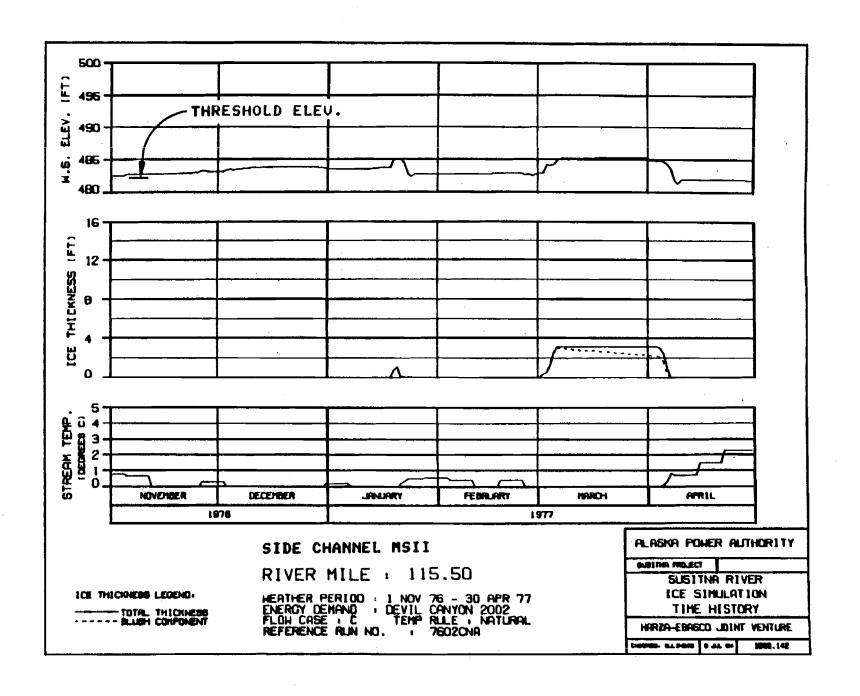


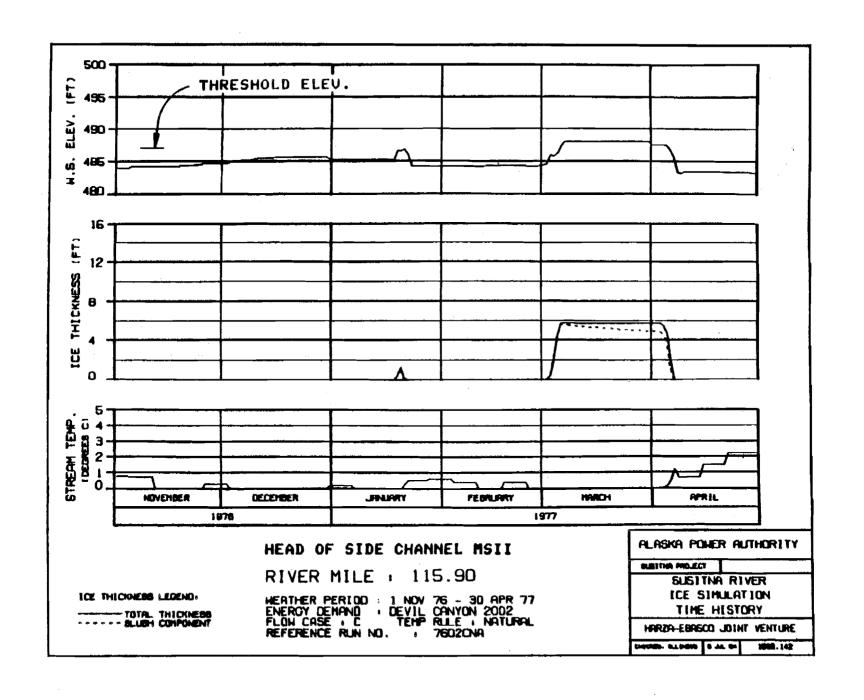


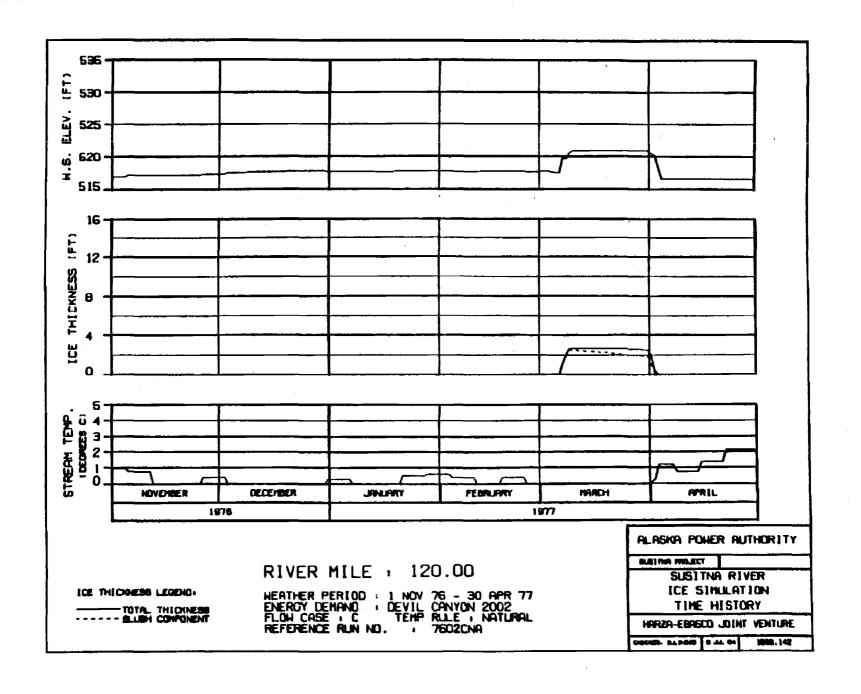
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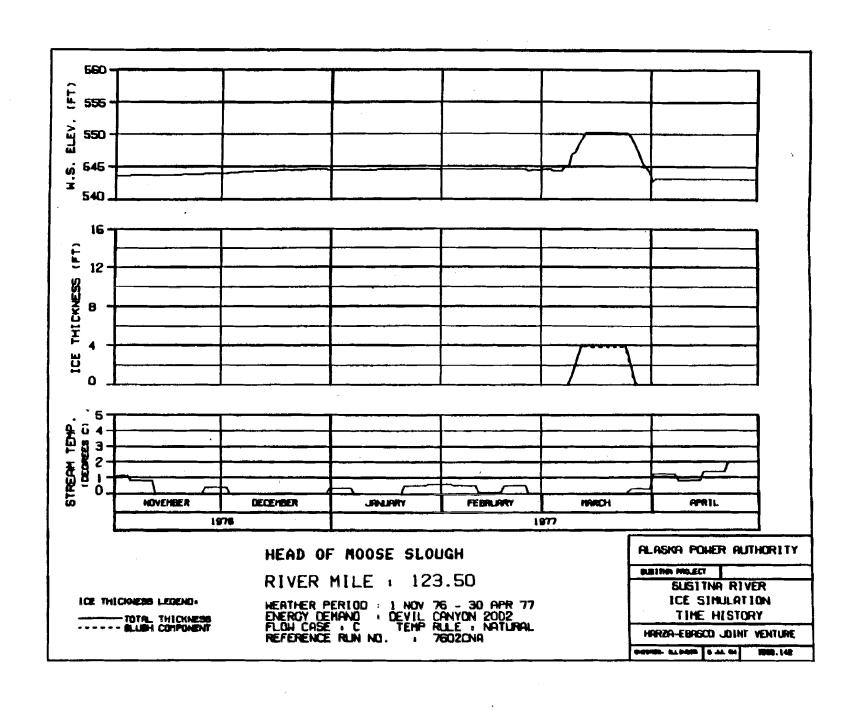


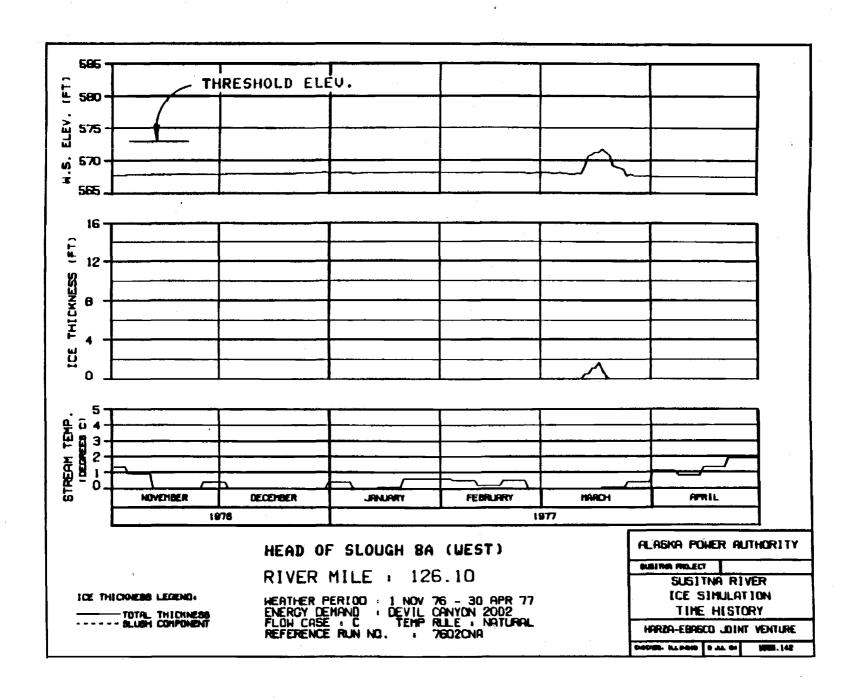


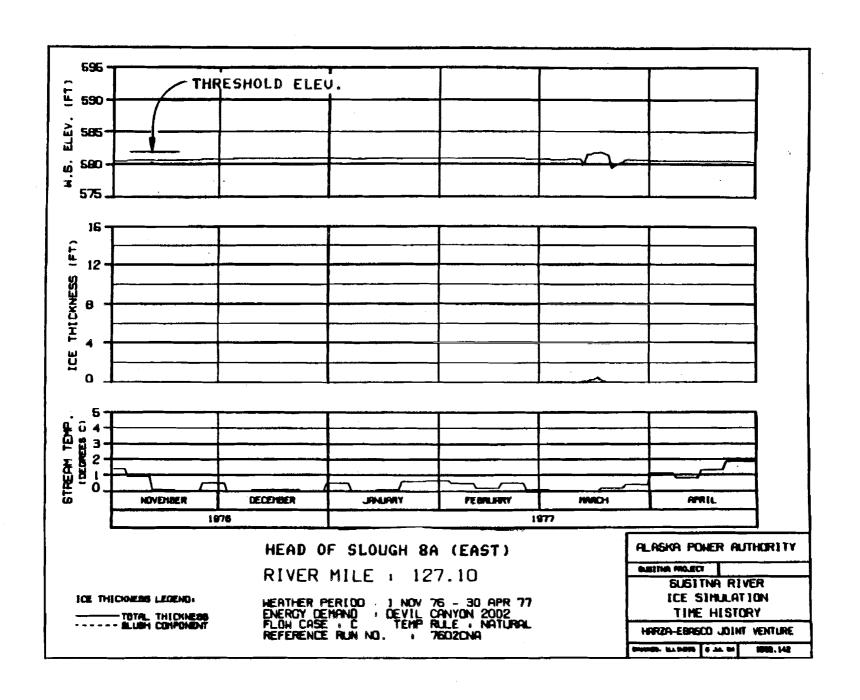


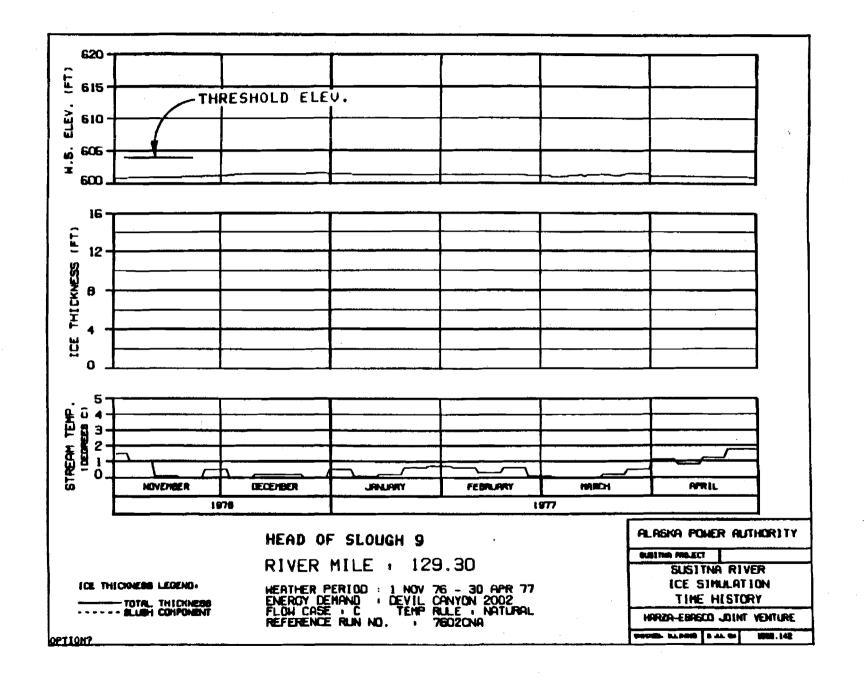


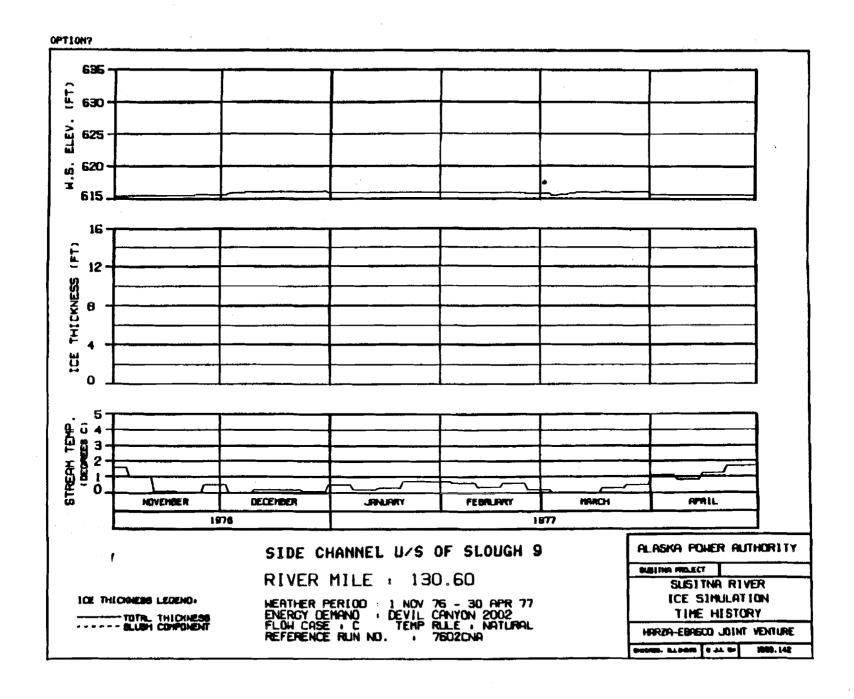


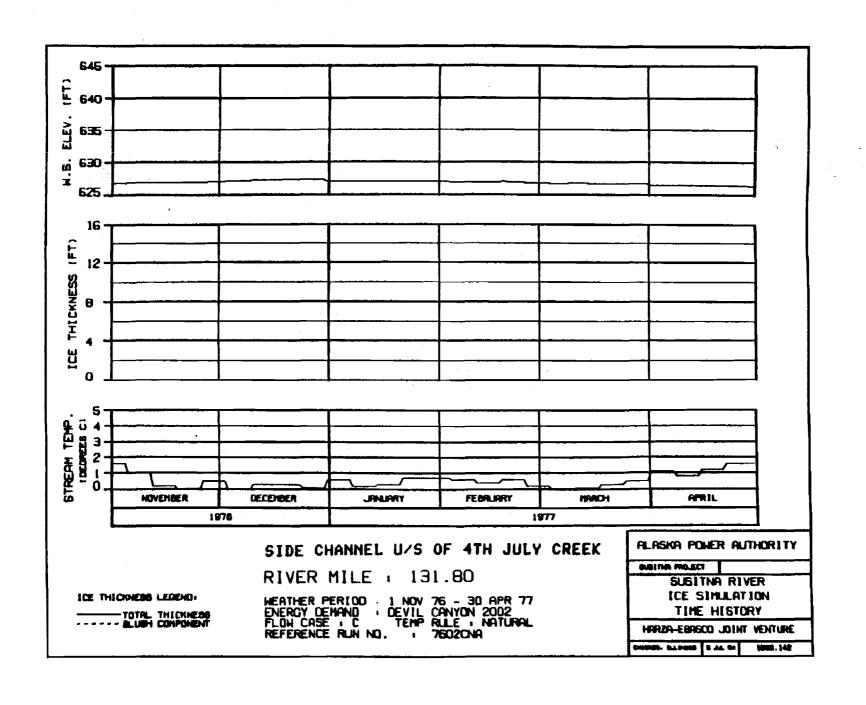


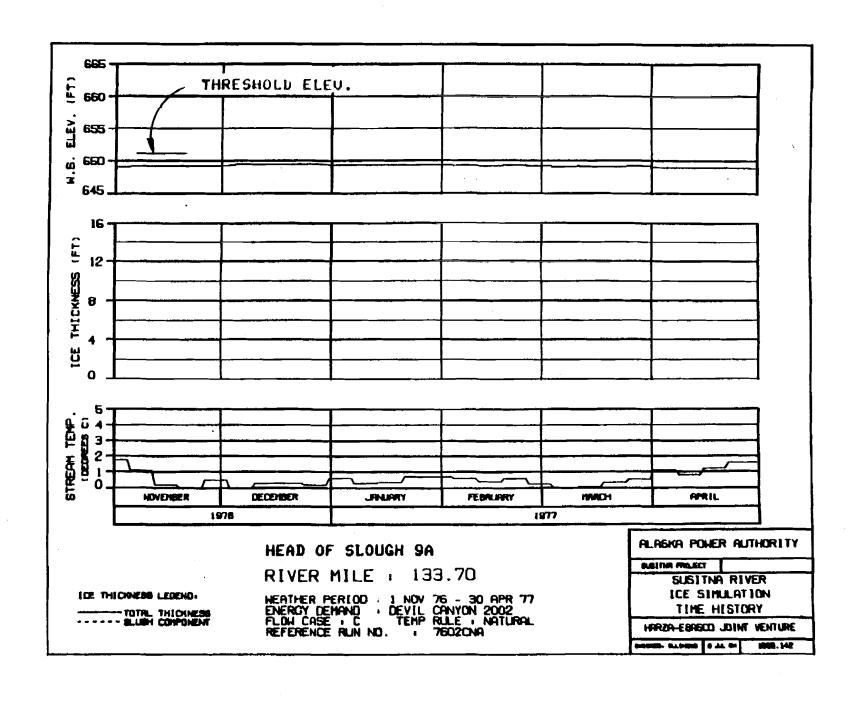




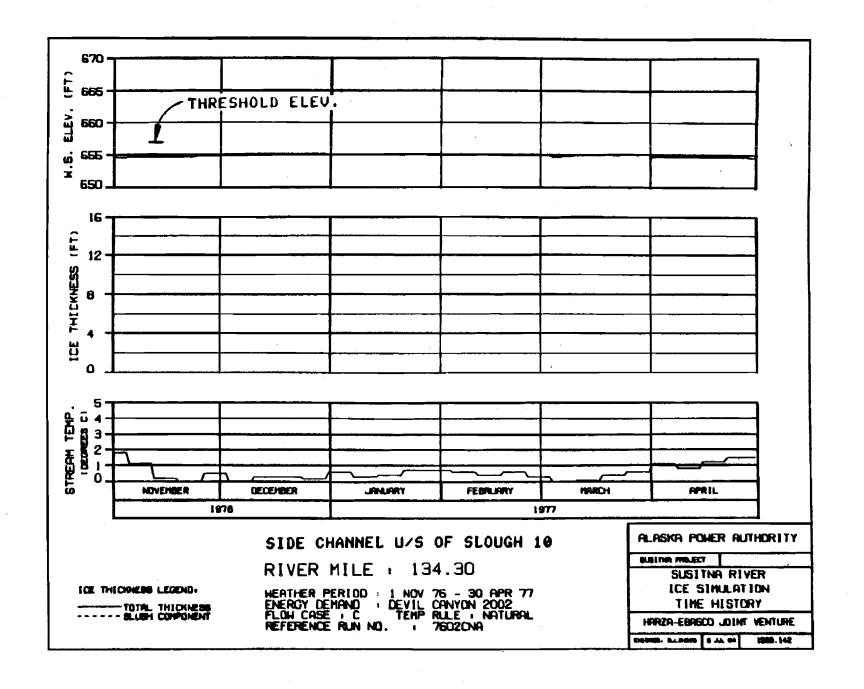


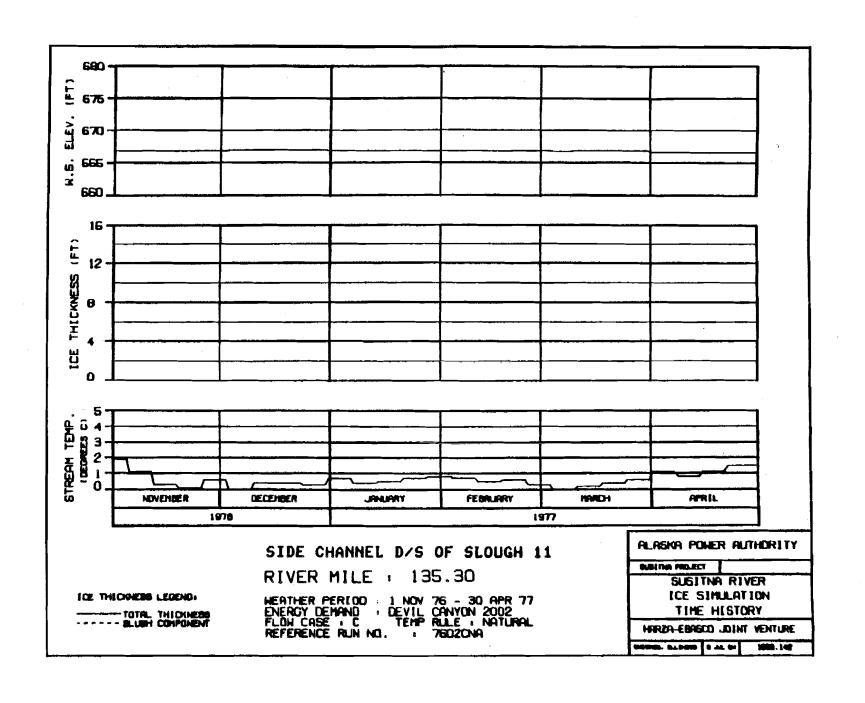


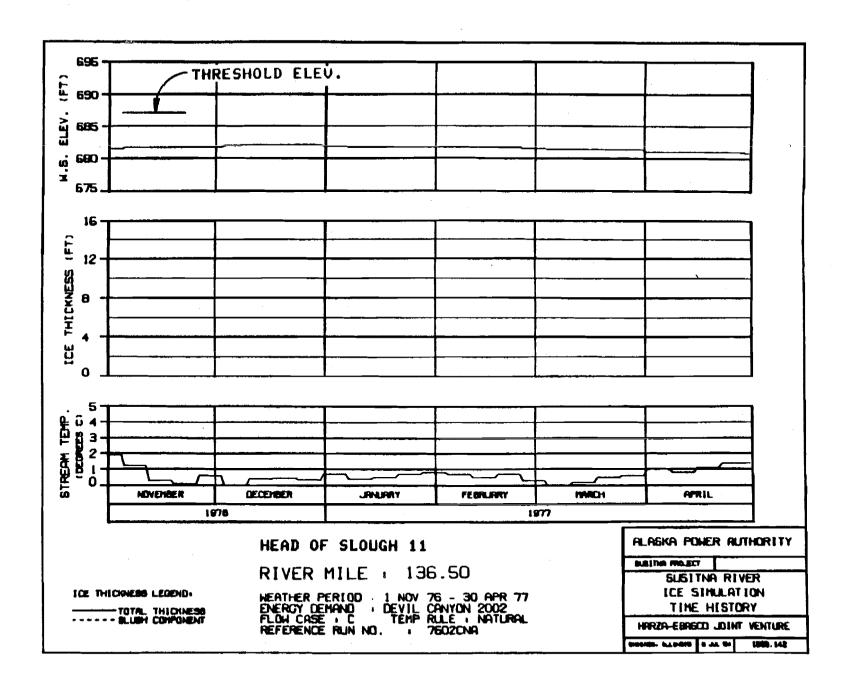


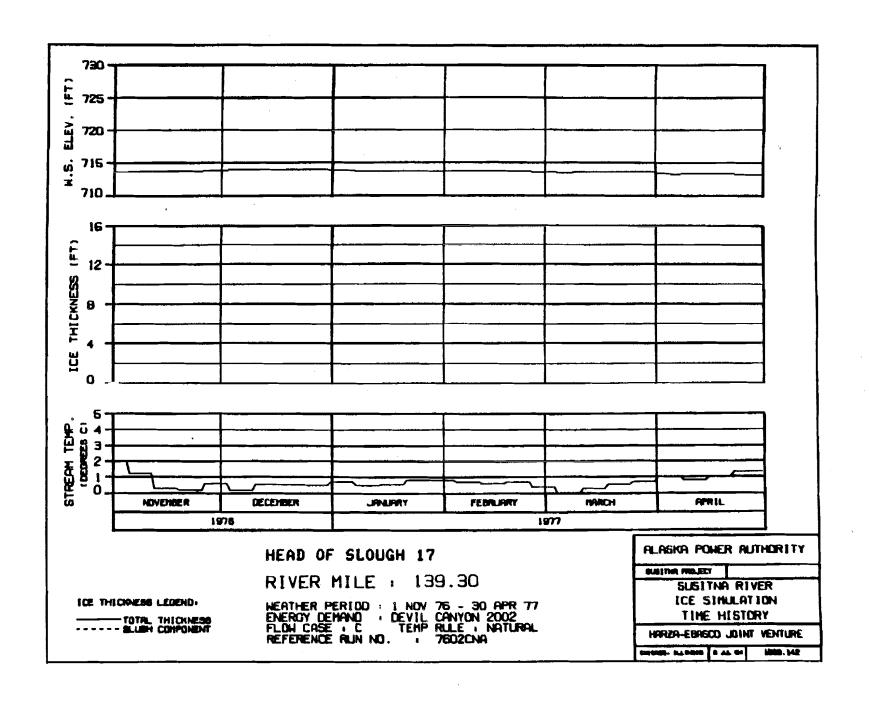


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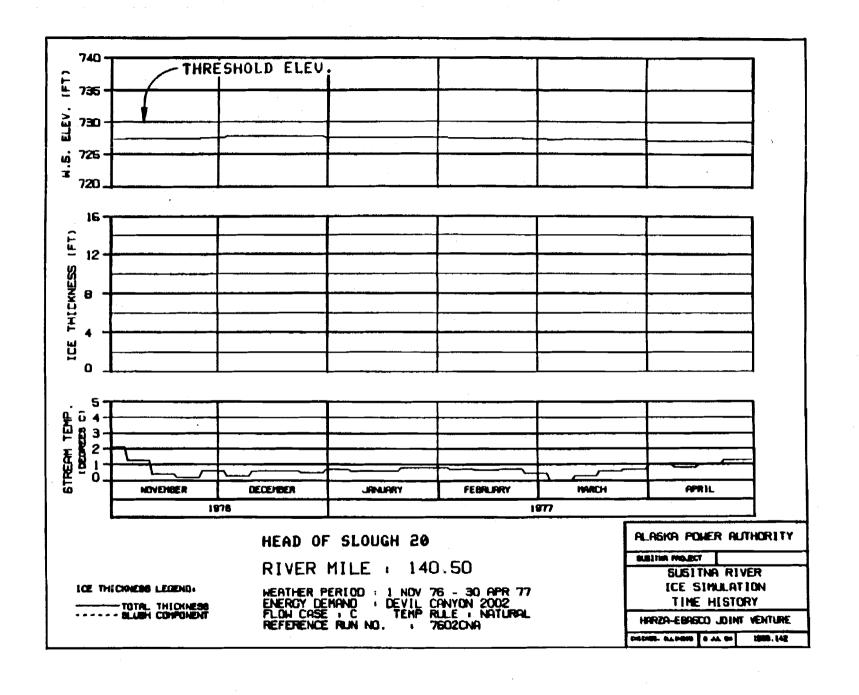


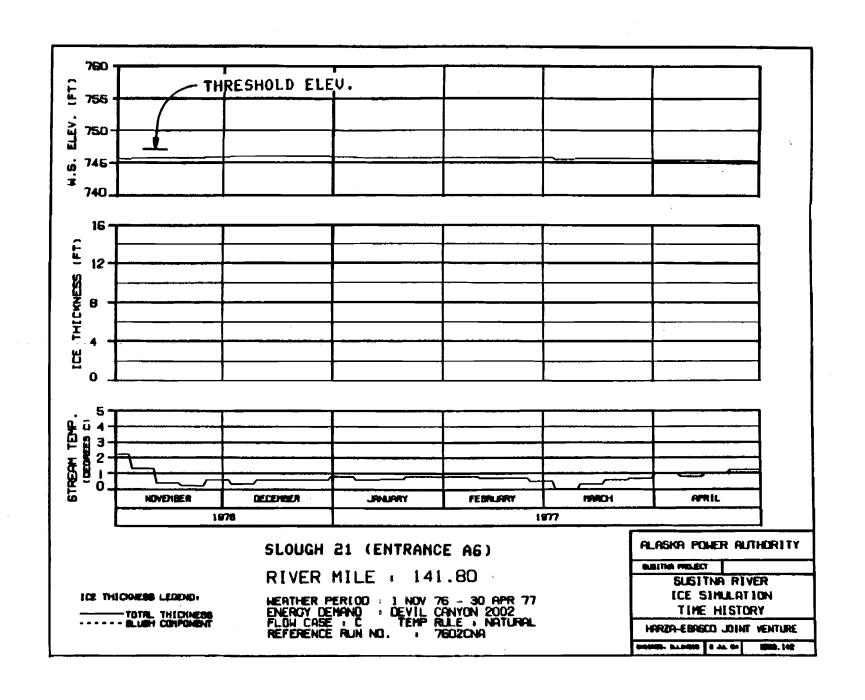


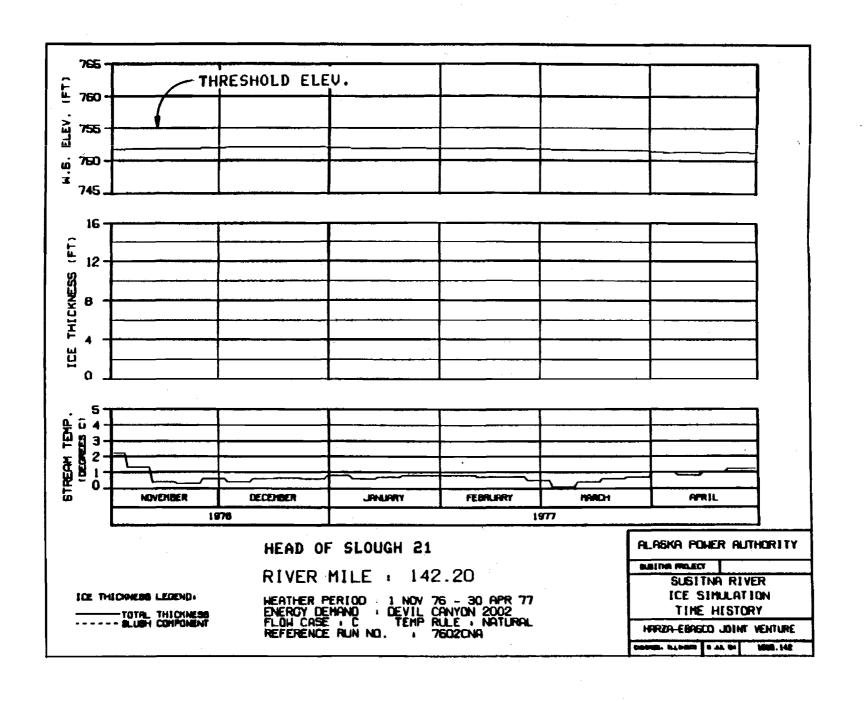


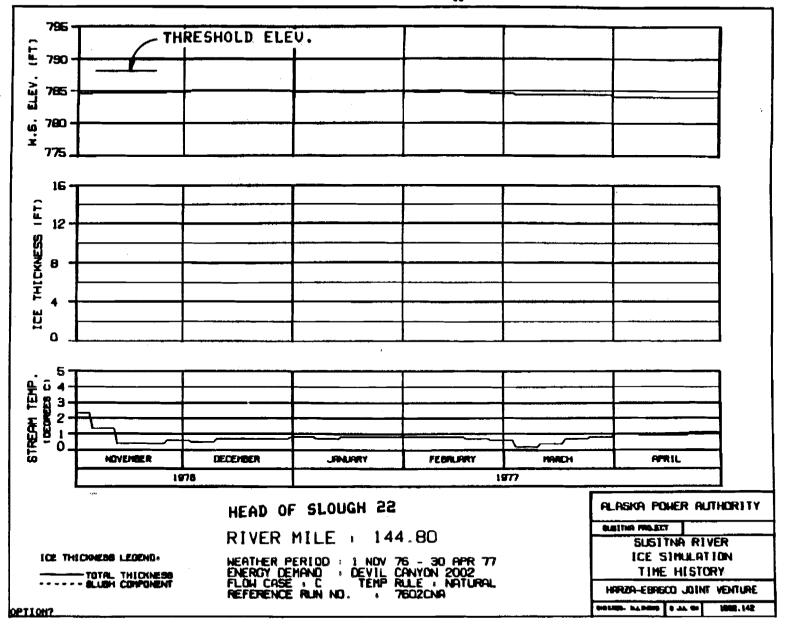


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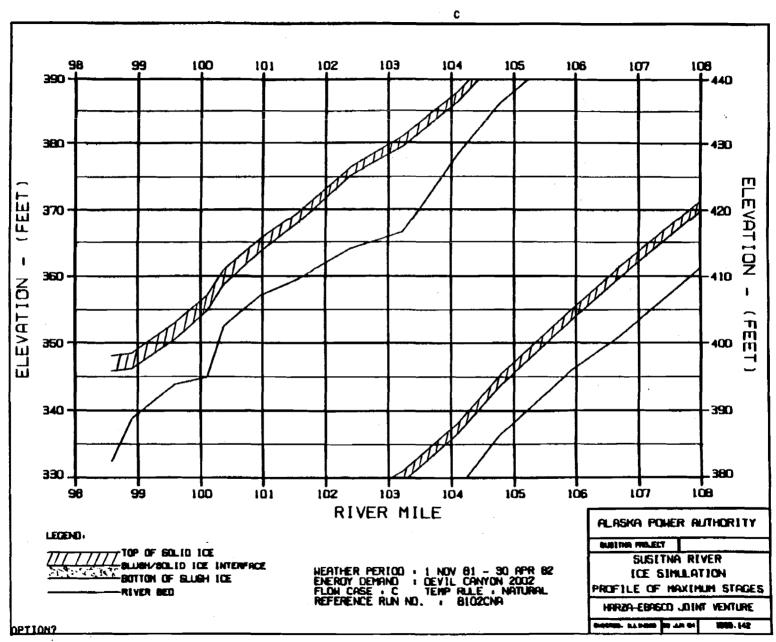






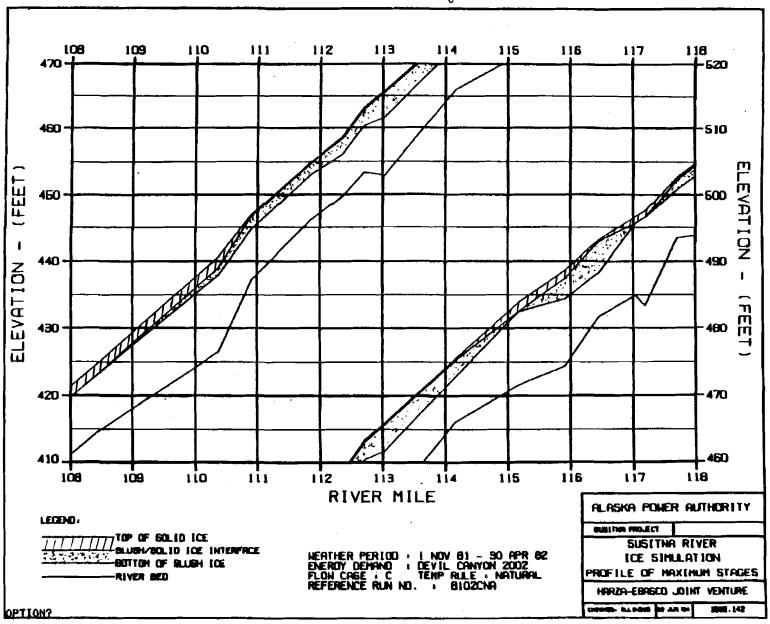
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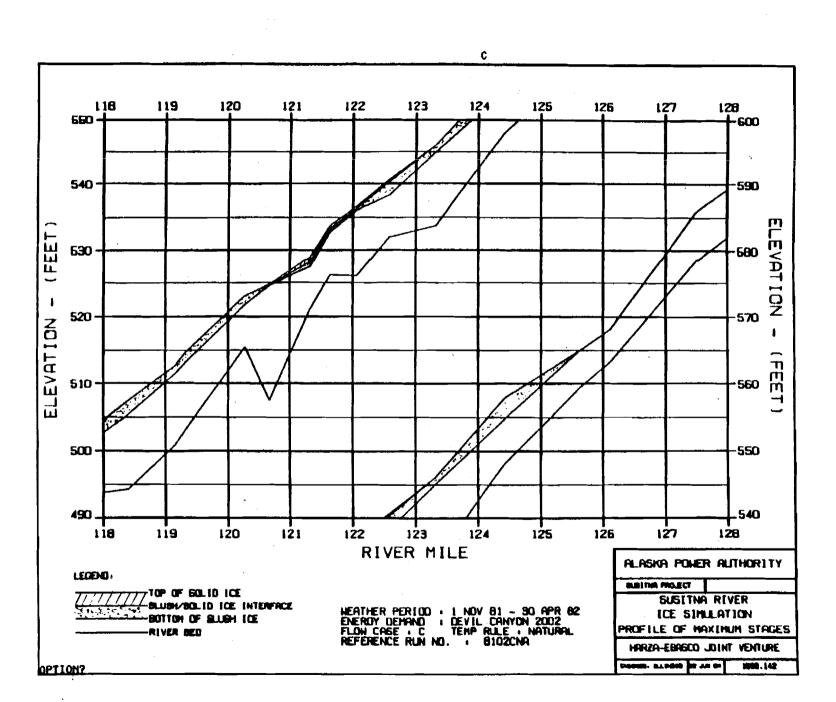
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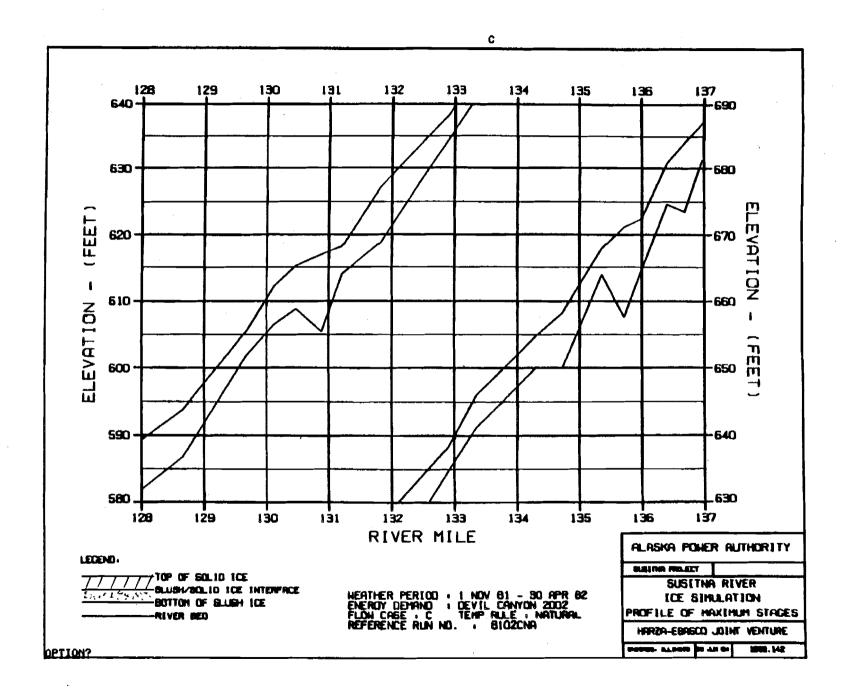


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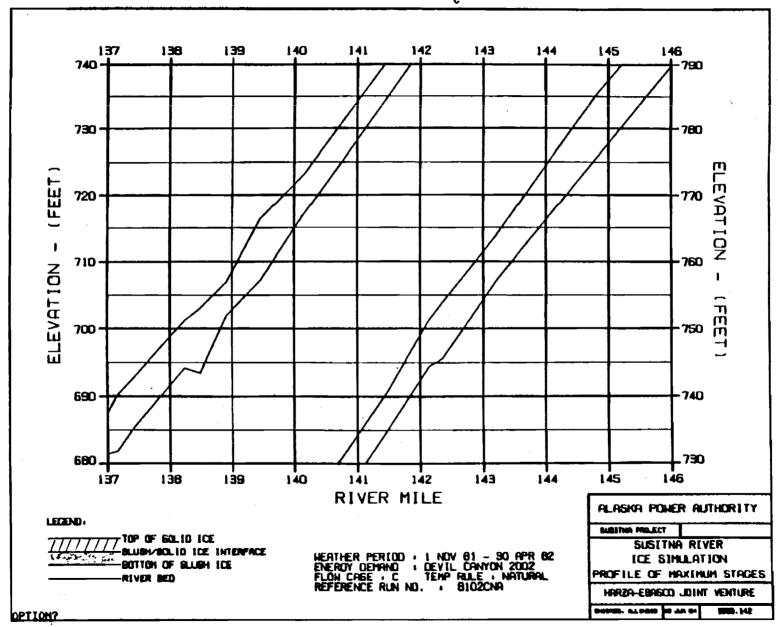


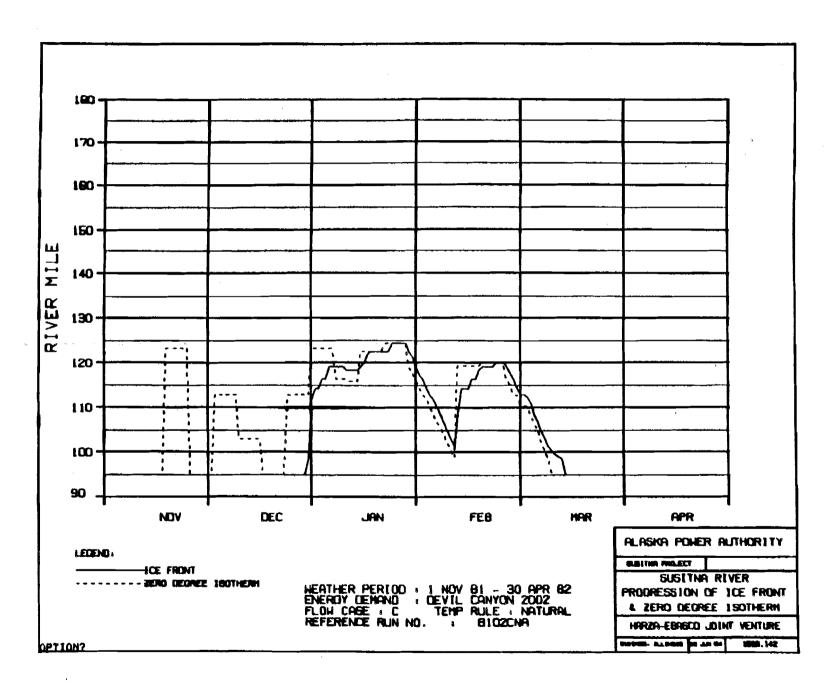




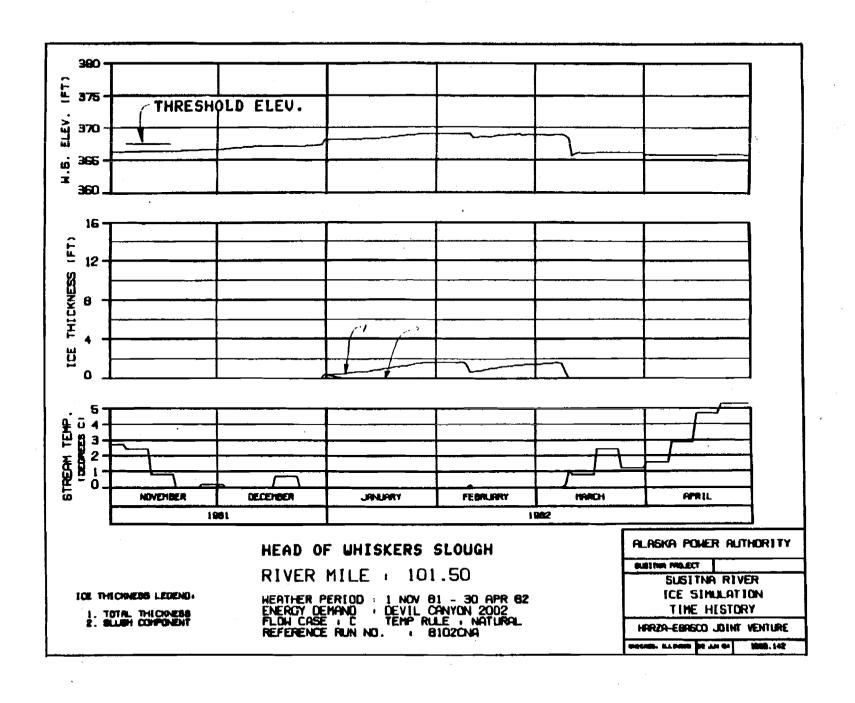
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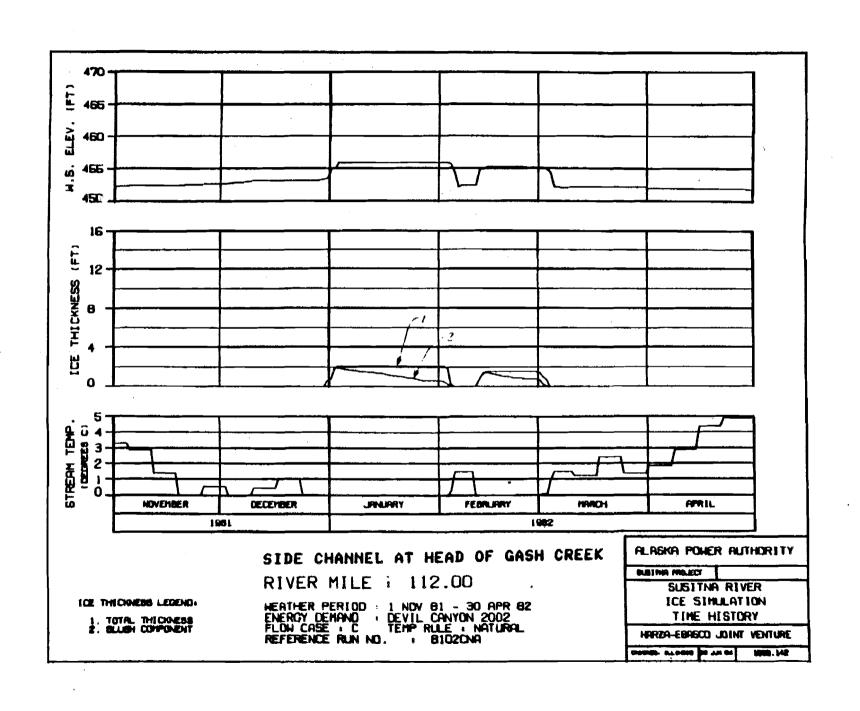






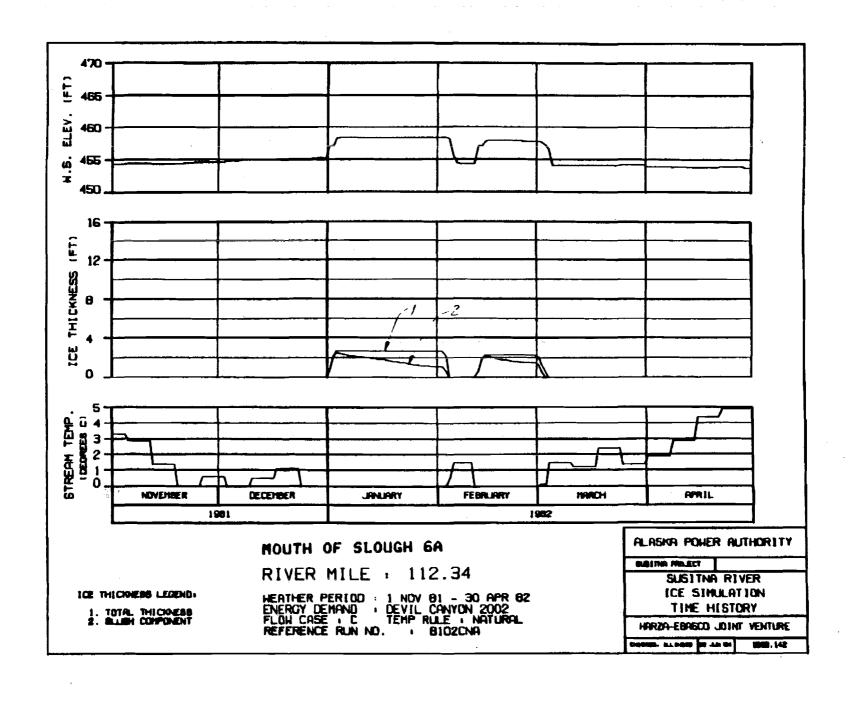
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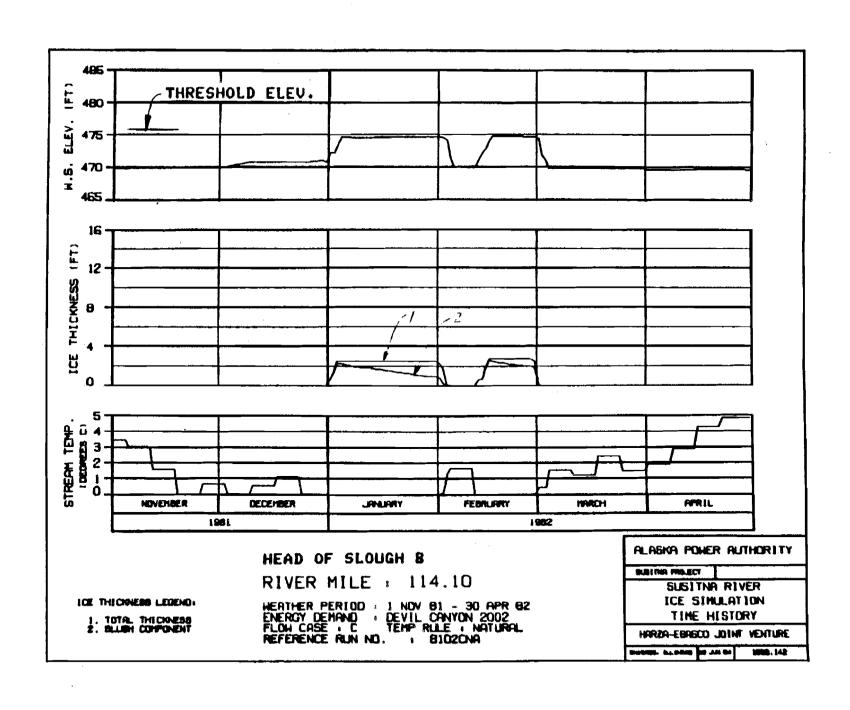


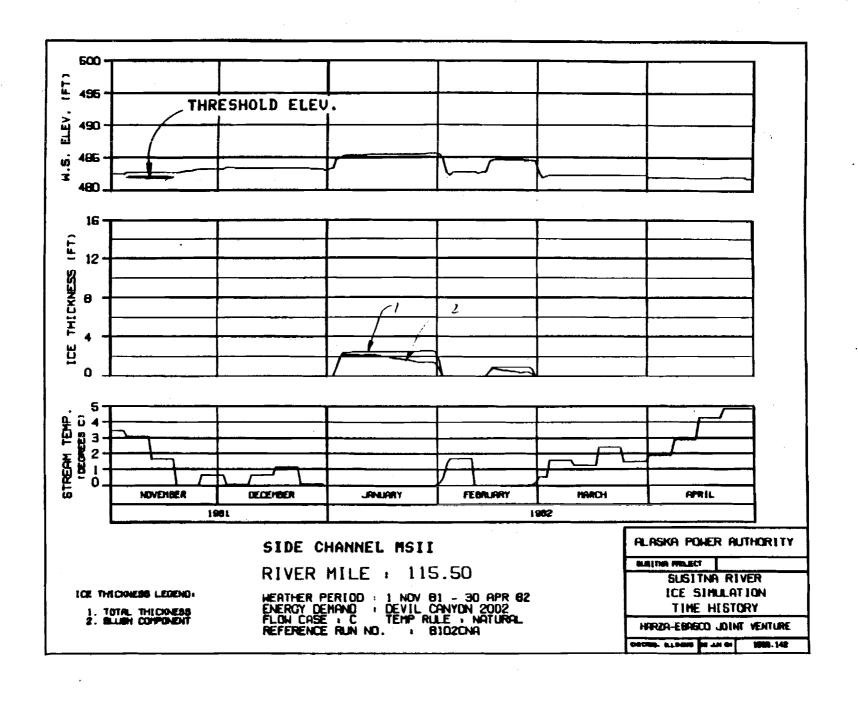


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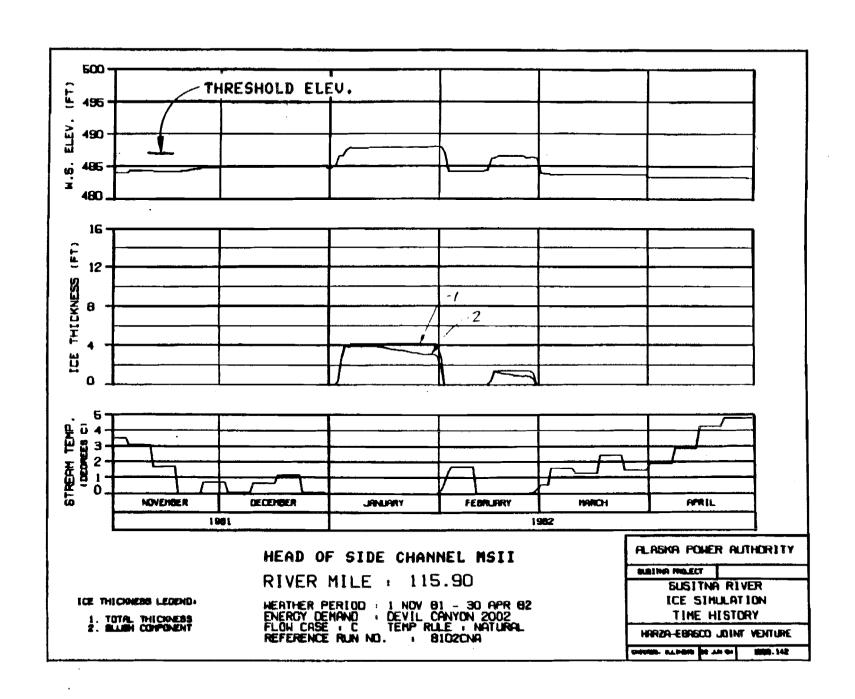
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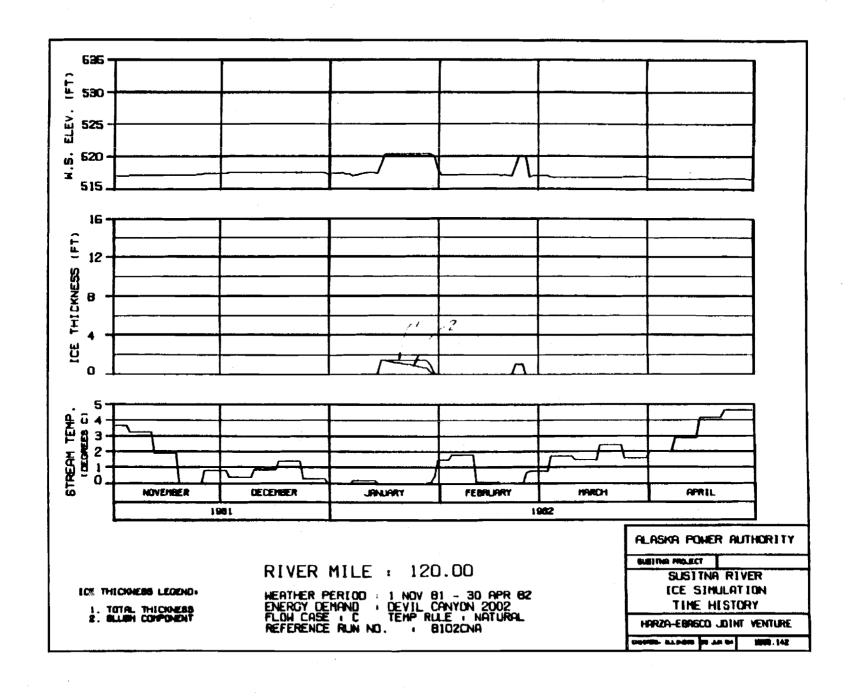


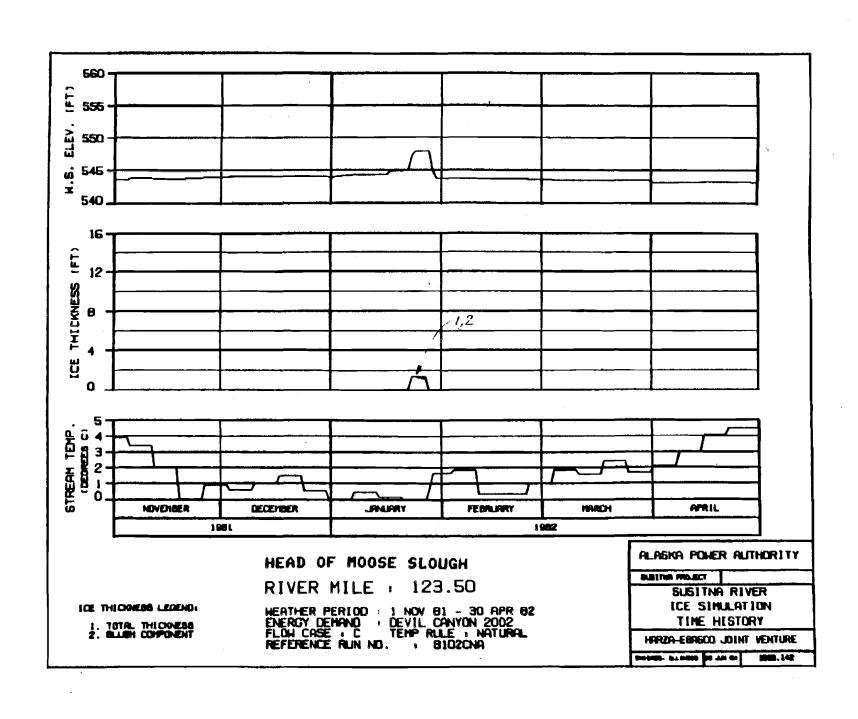




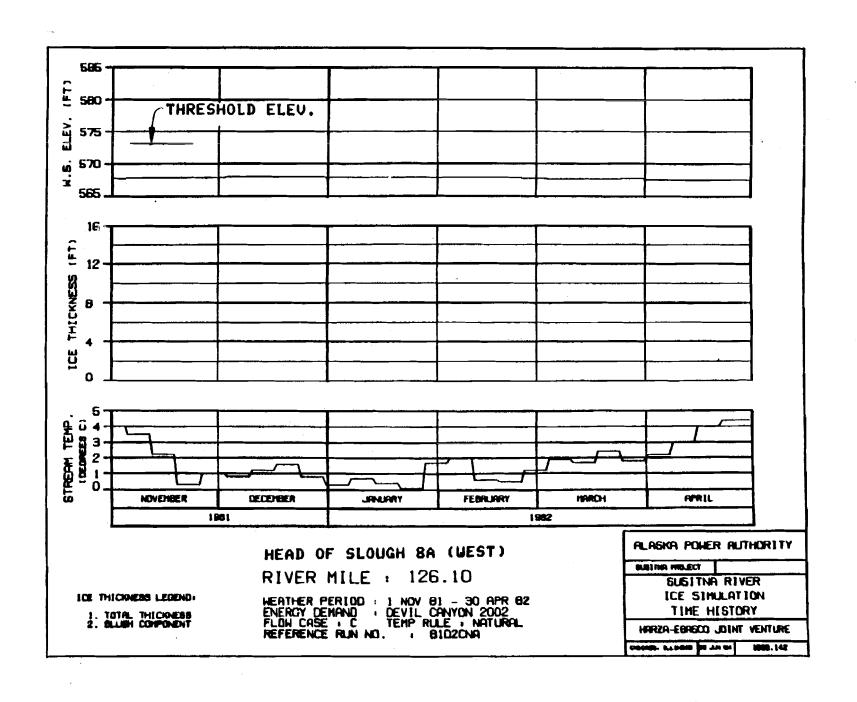


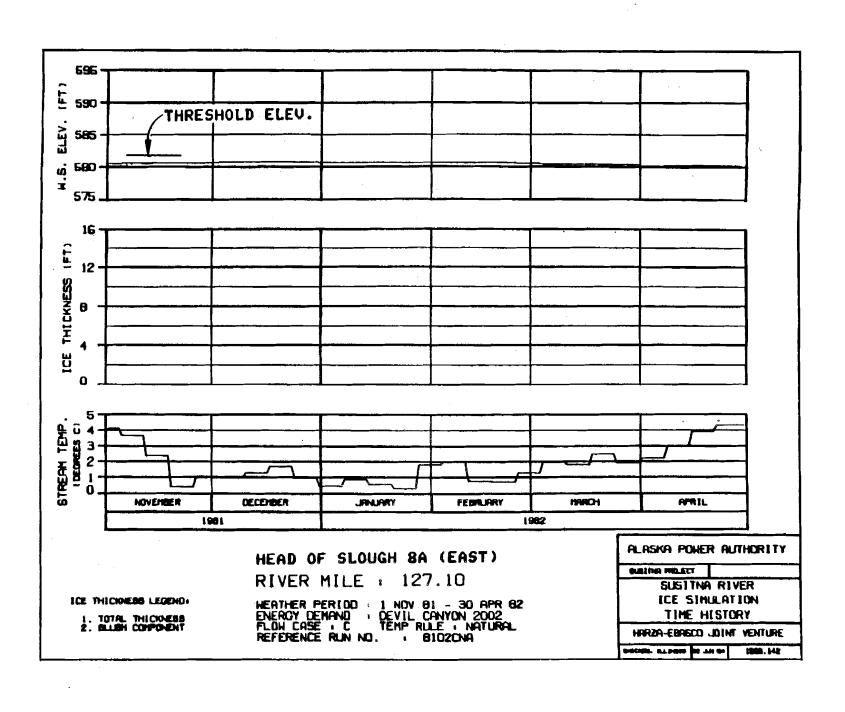




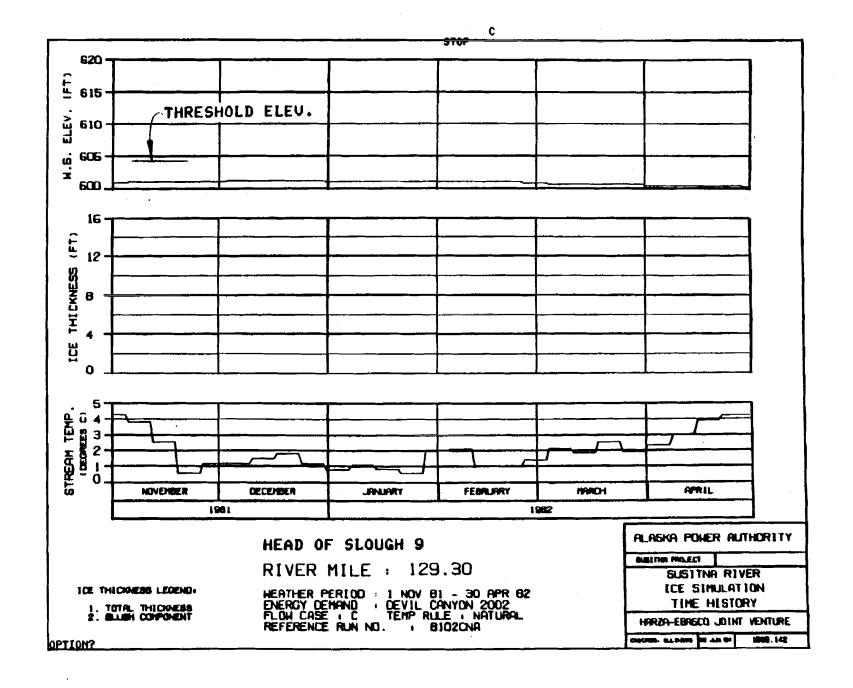


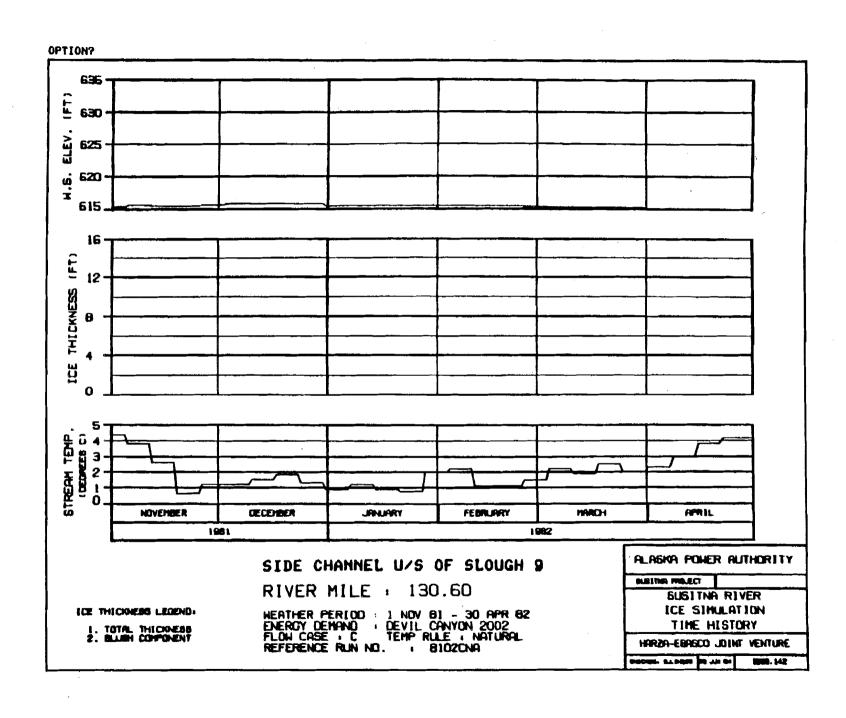
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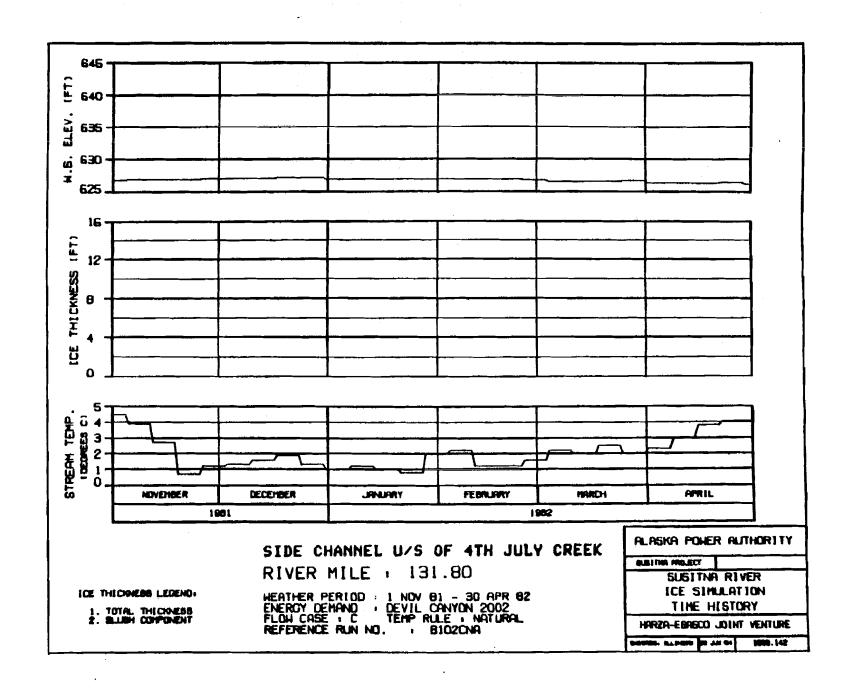


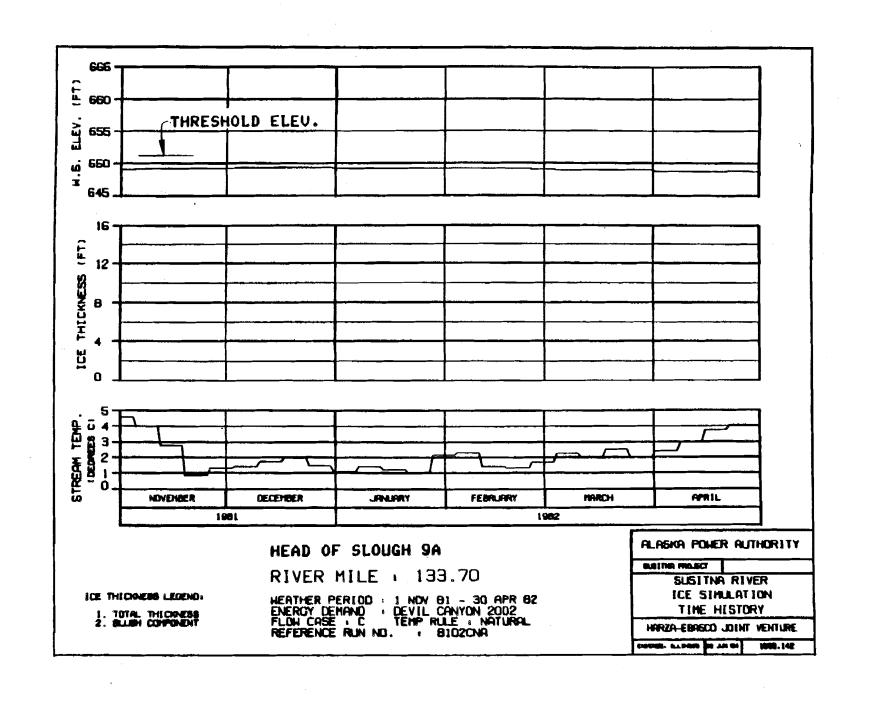
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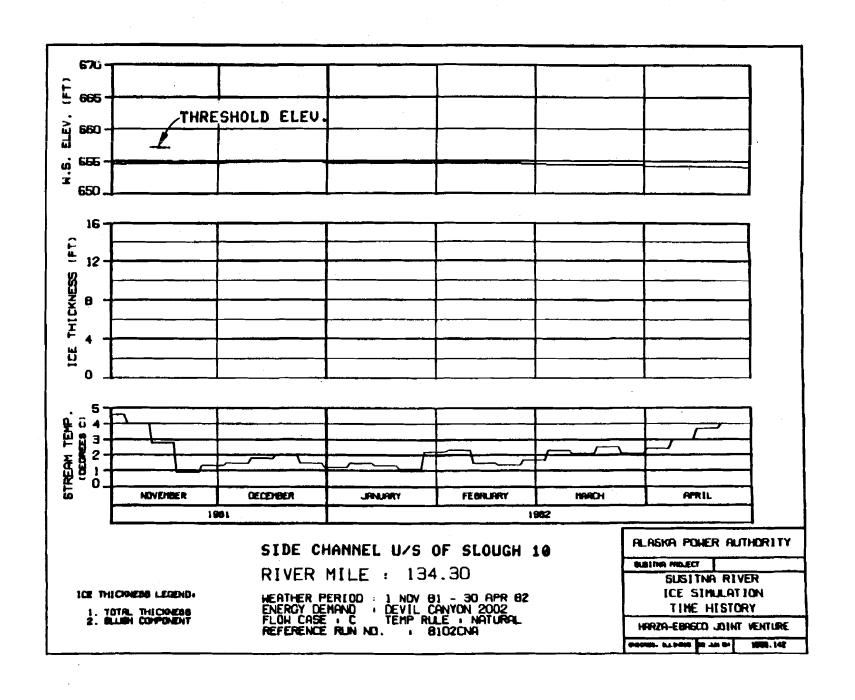


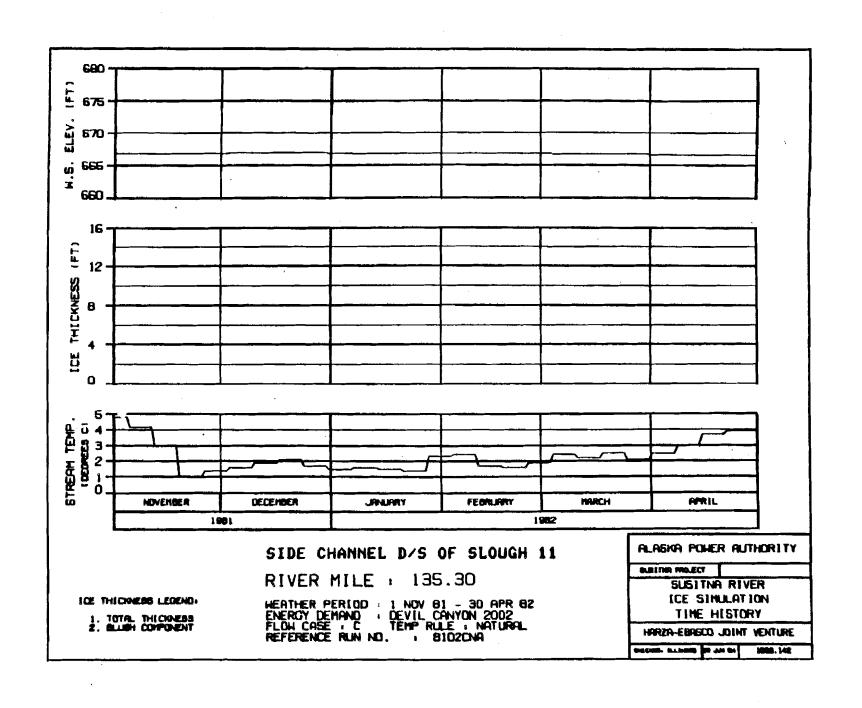
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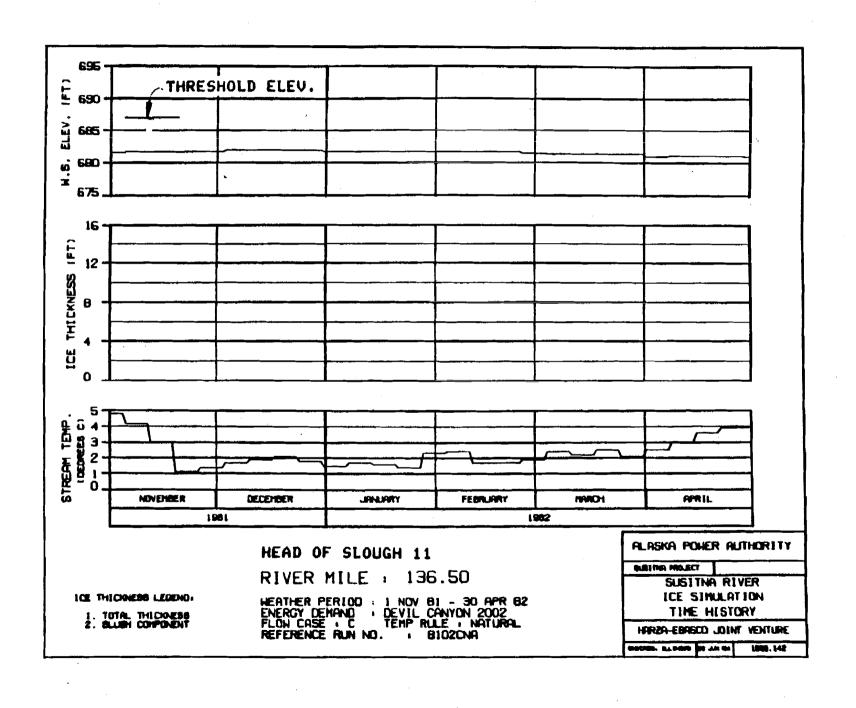
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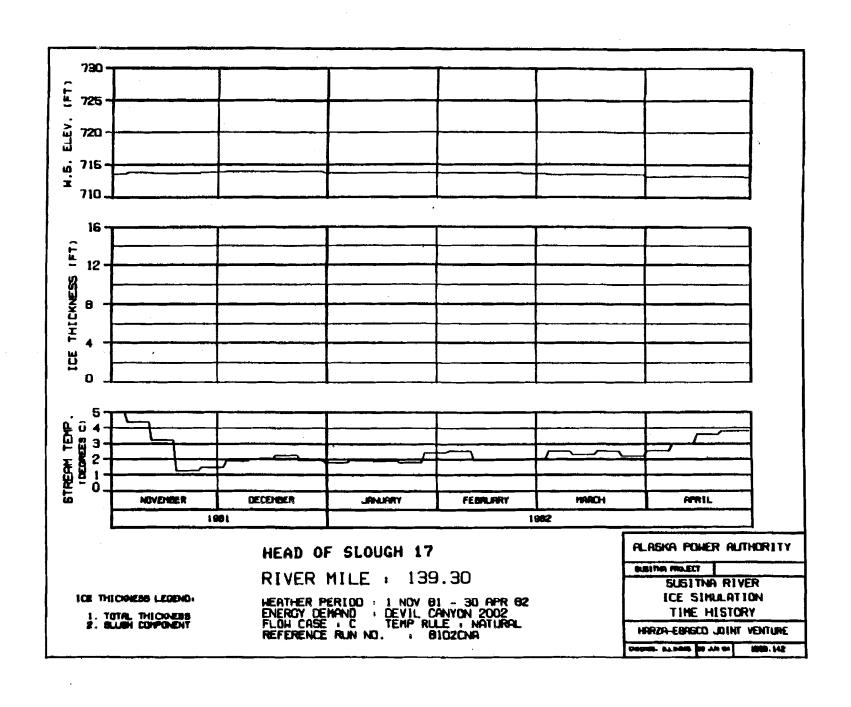


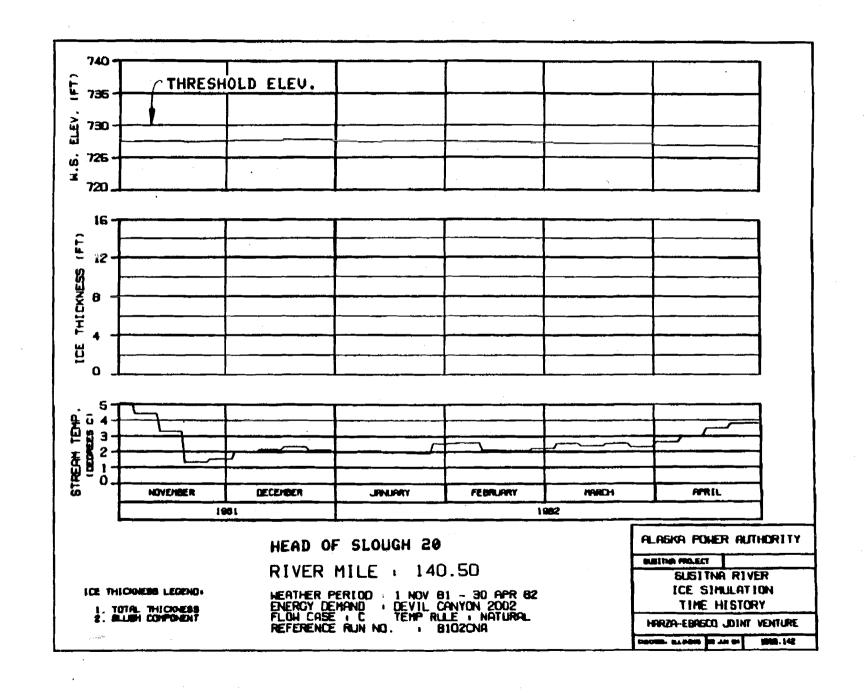


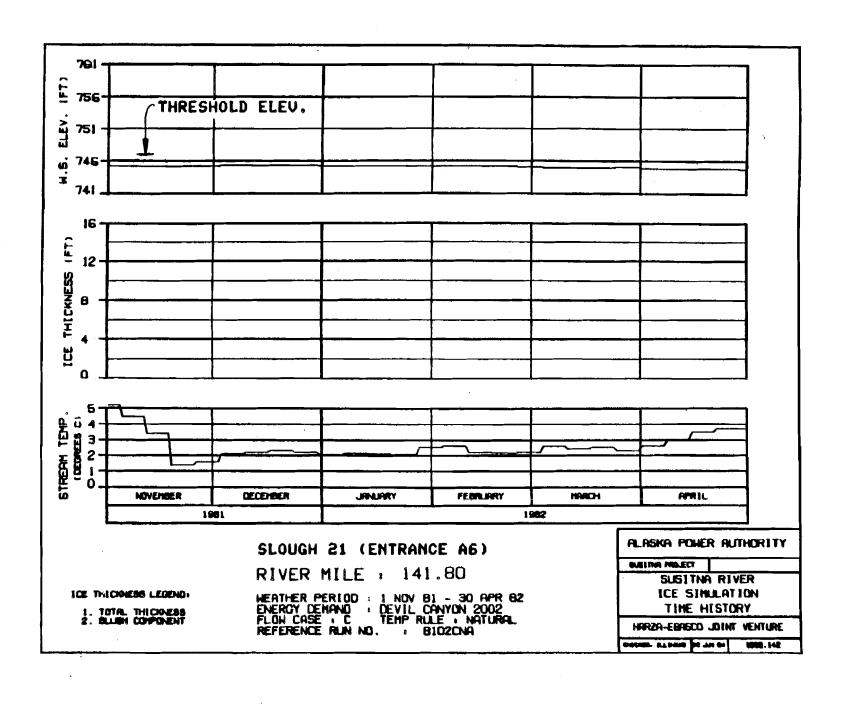
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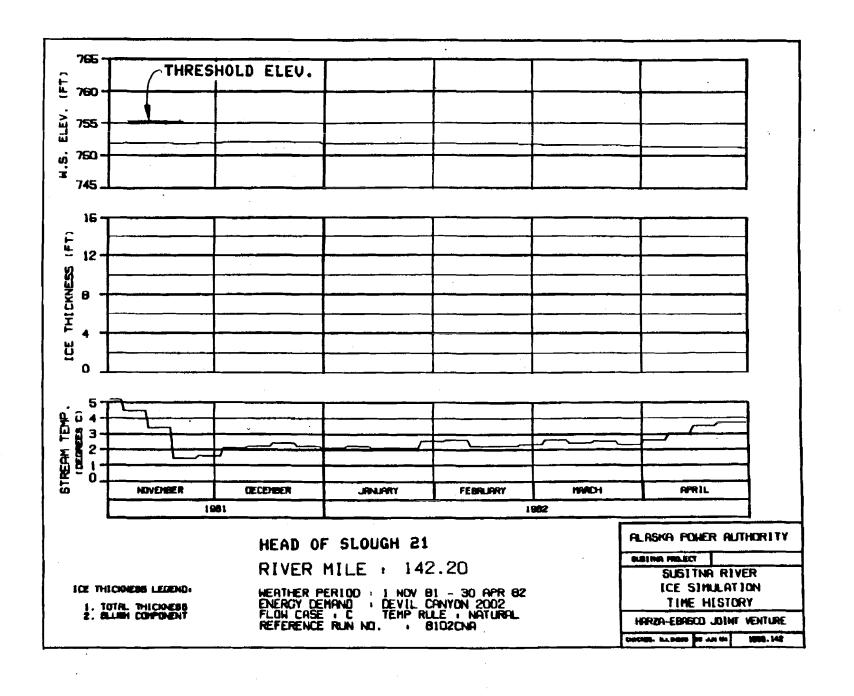
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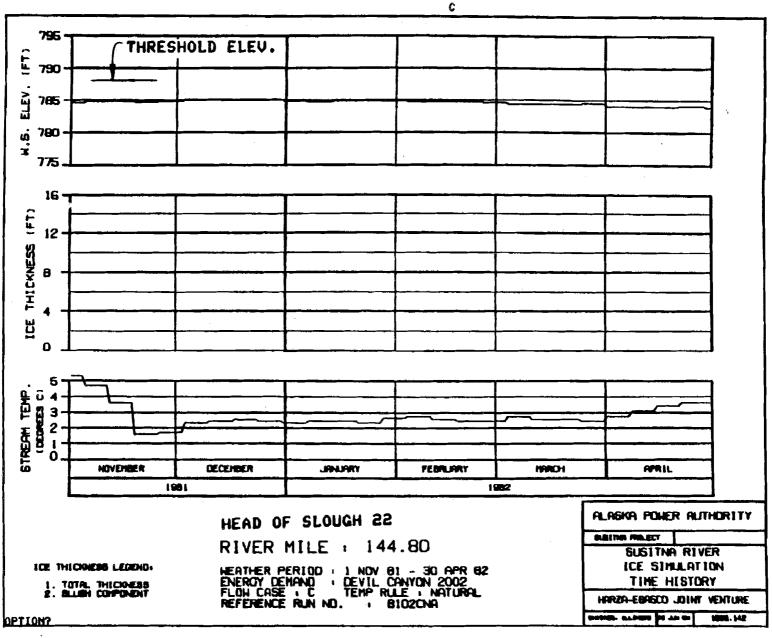
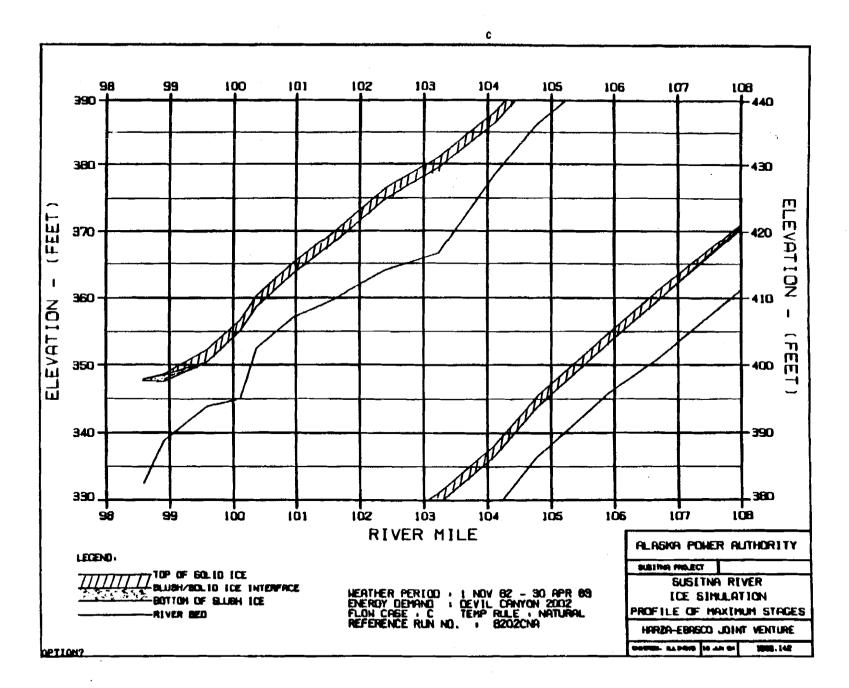
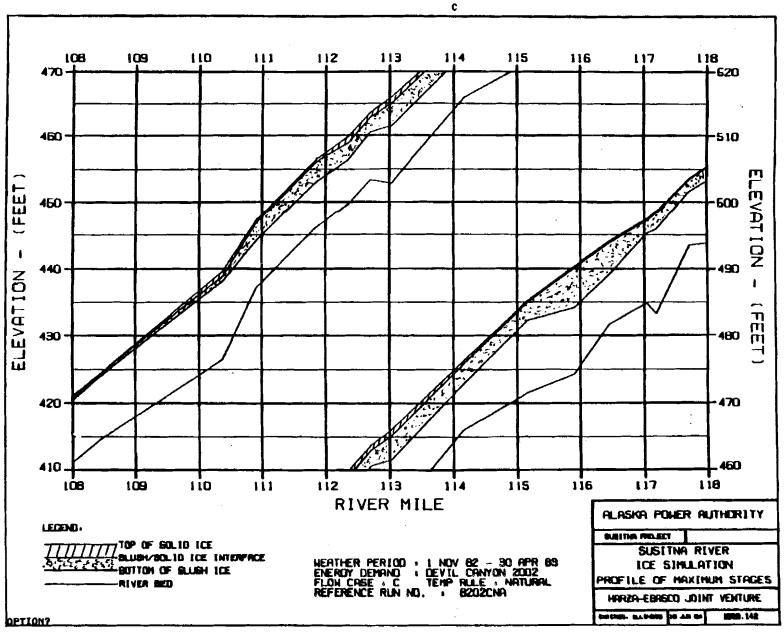


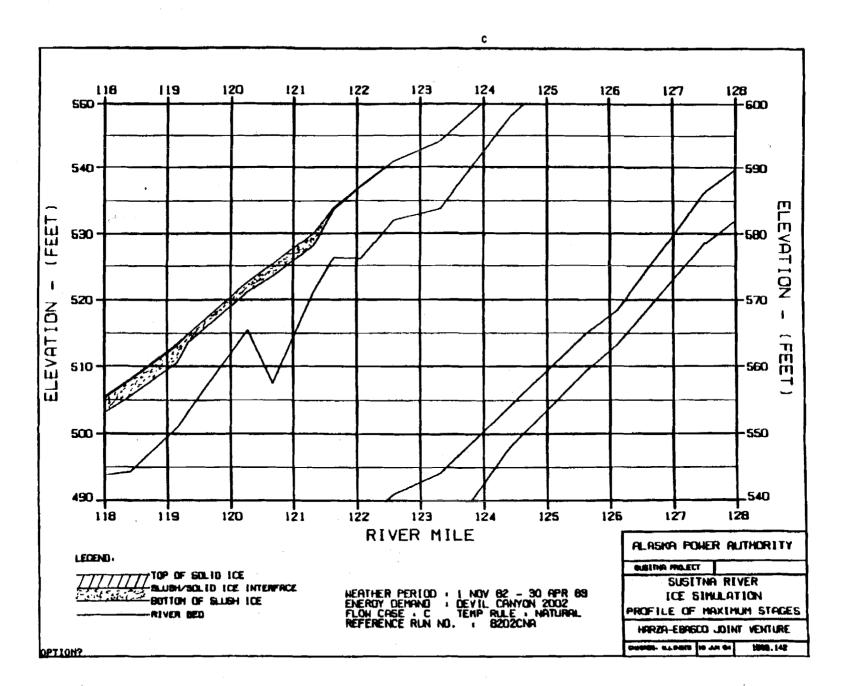
EXHIBIT P



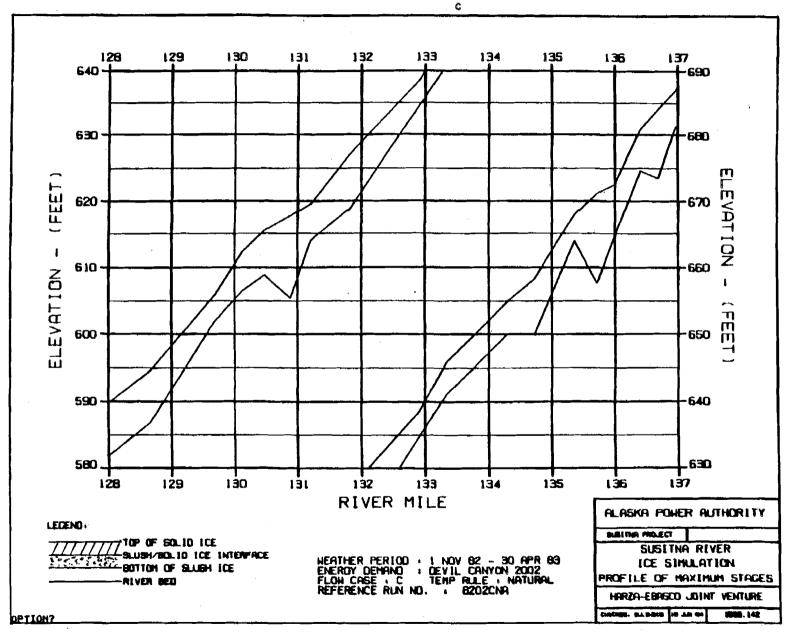




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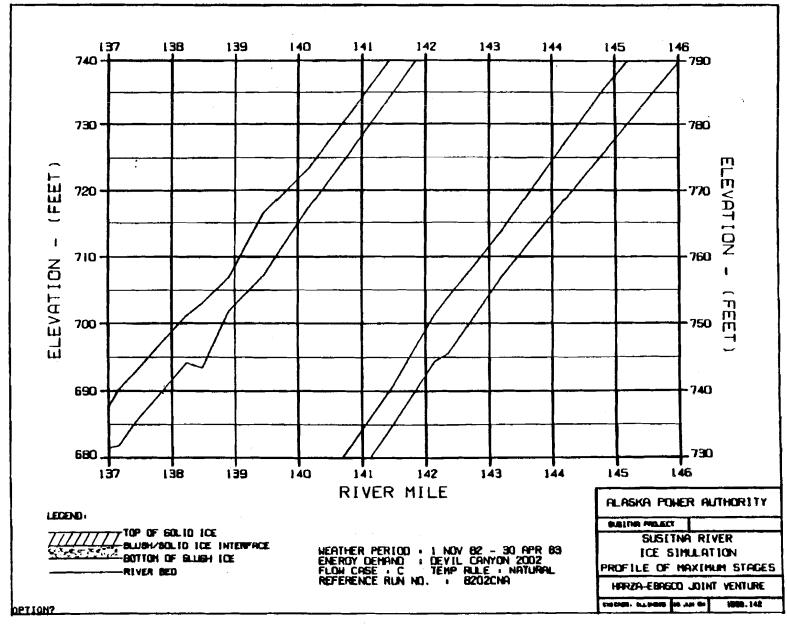


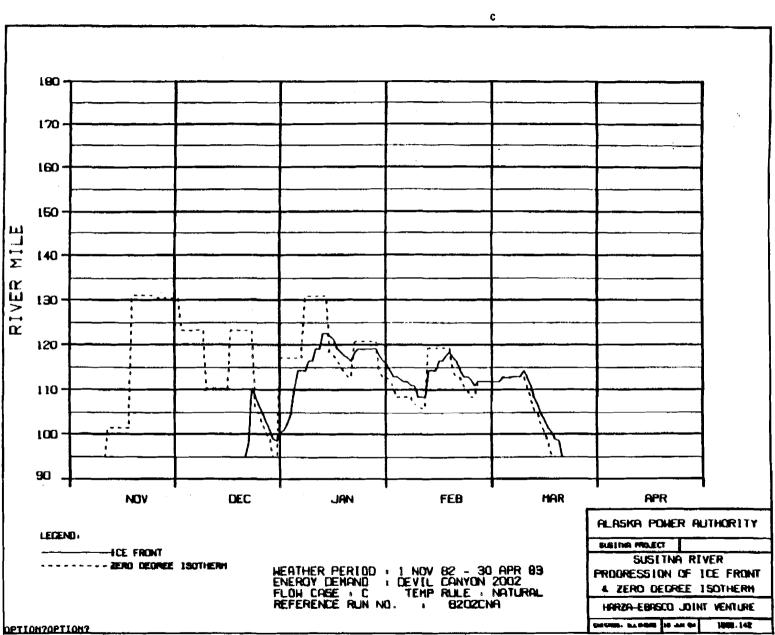


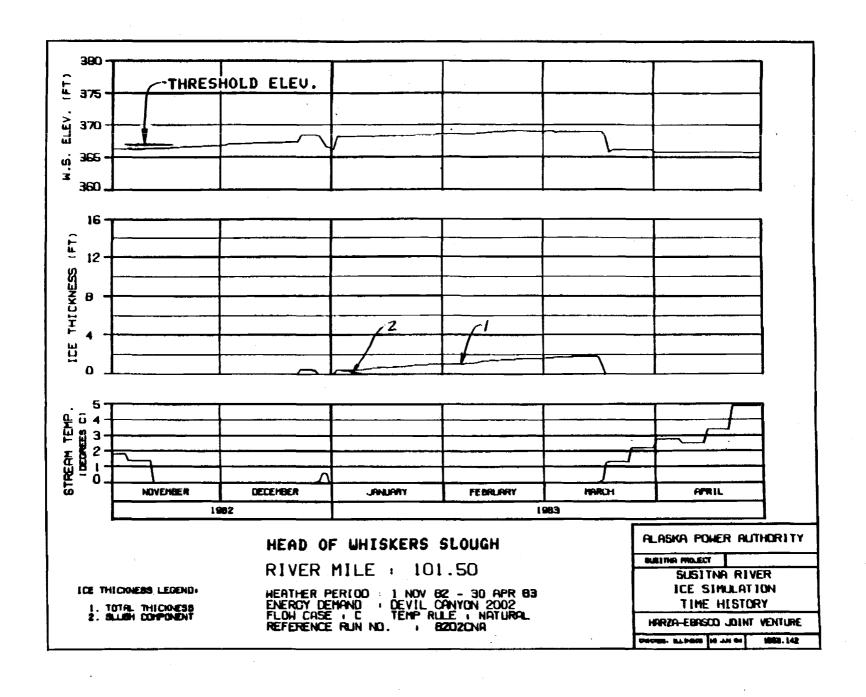


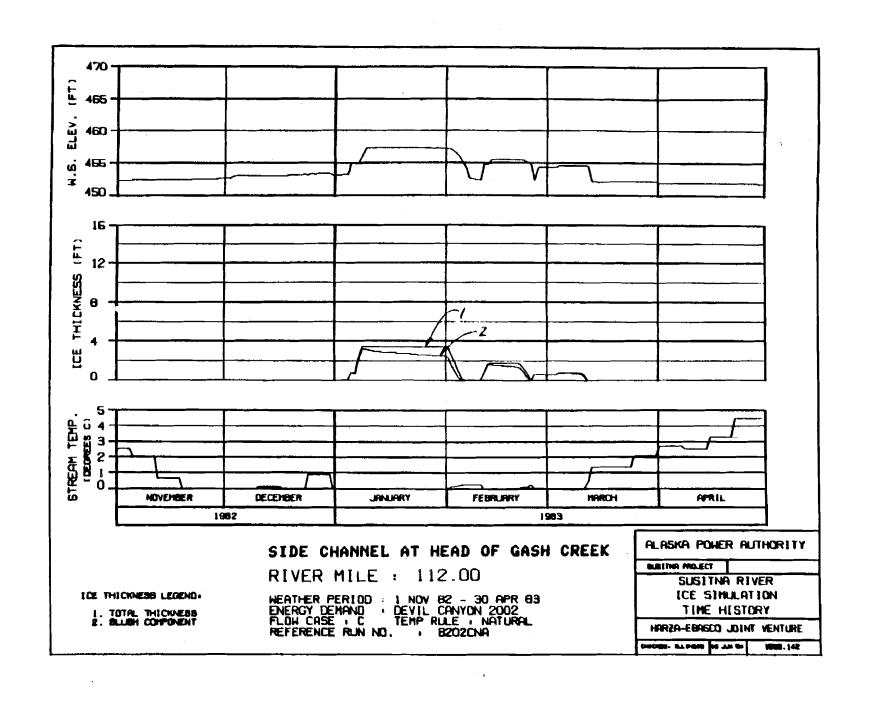
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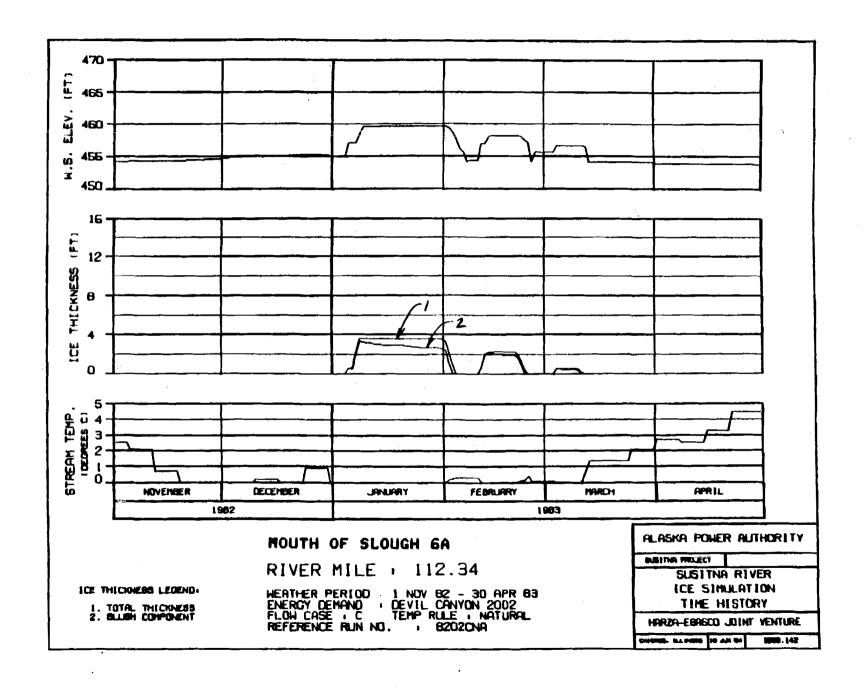


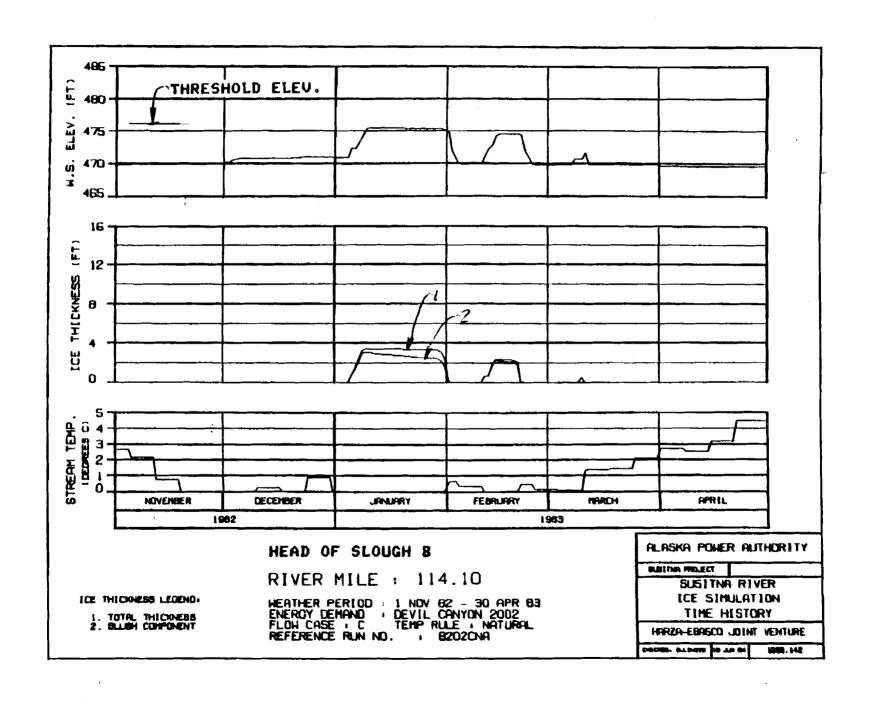


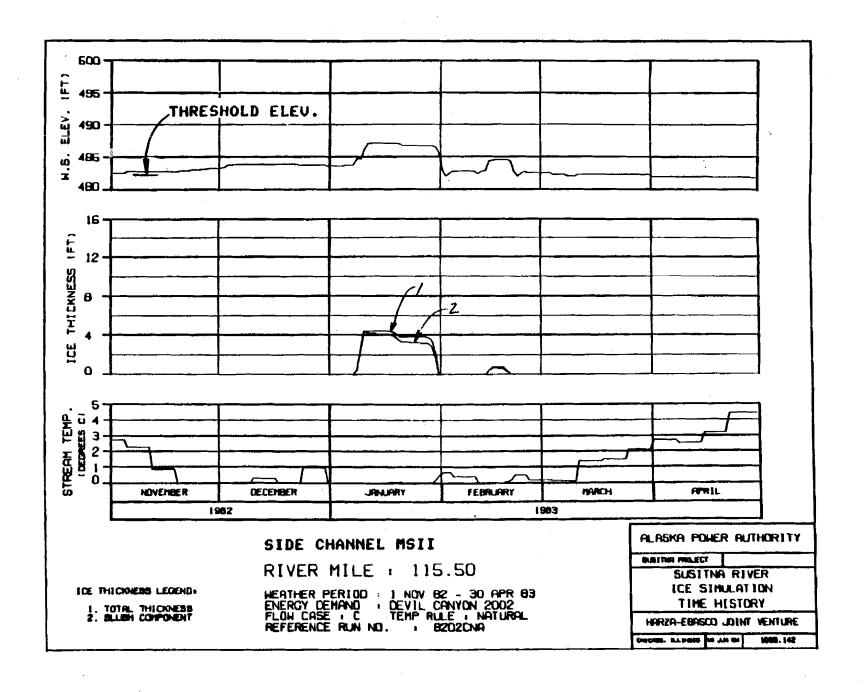


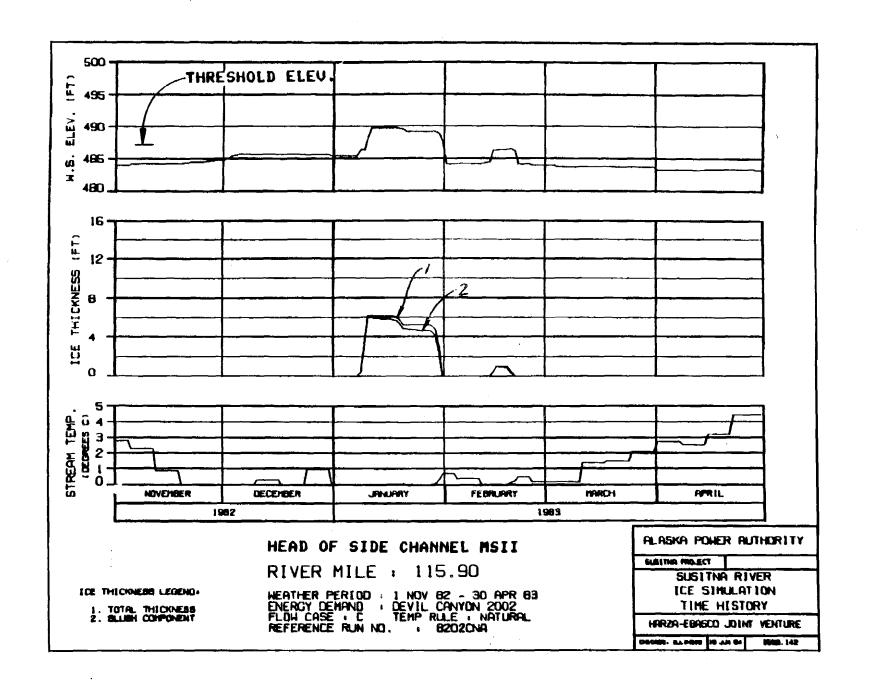


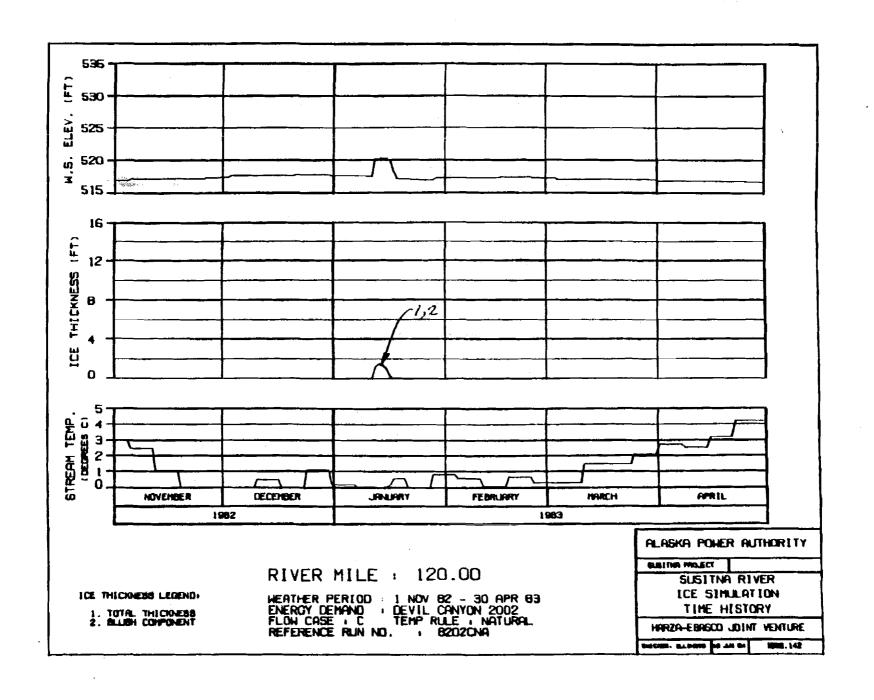


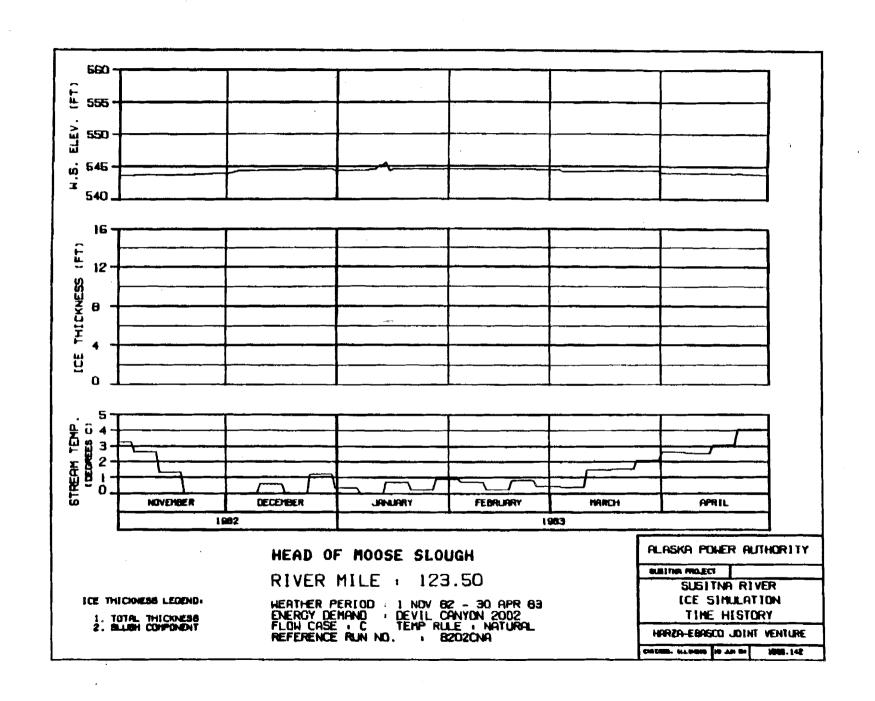




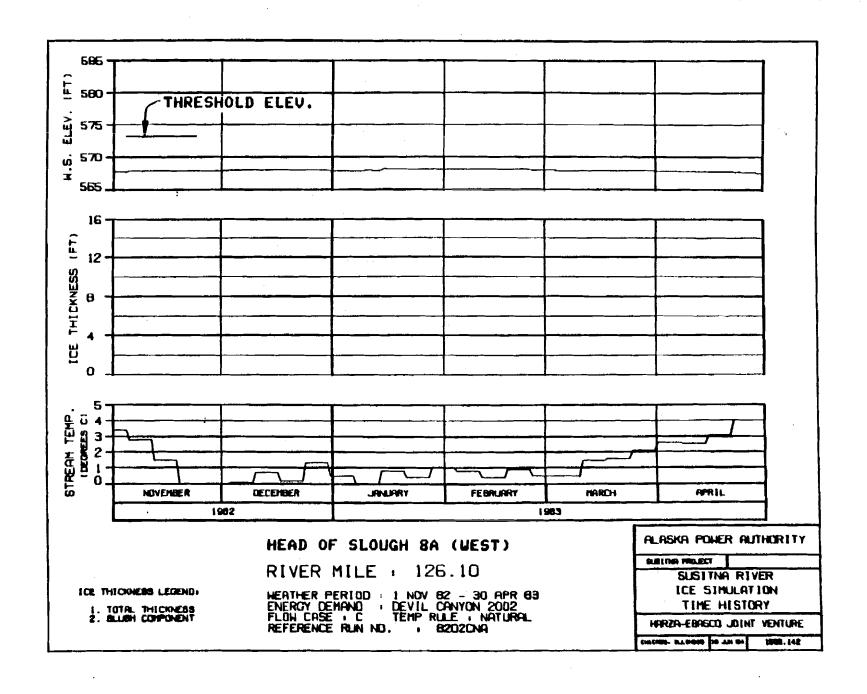


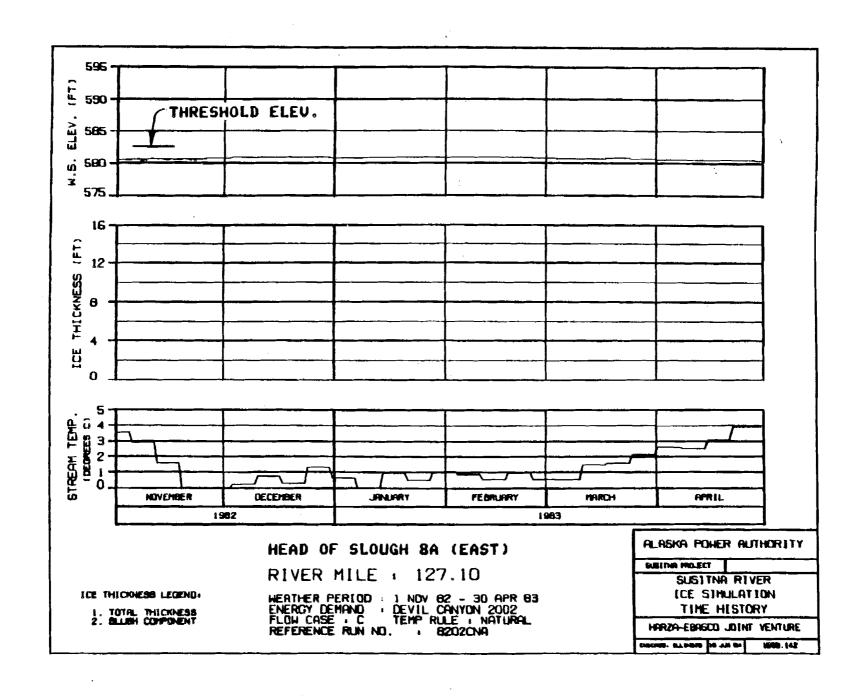




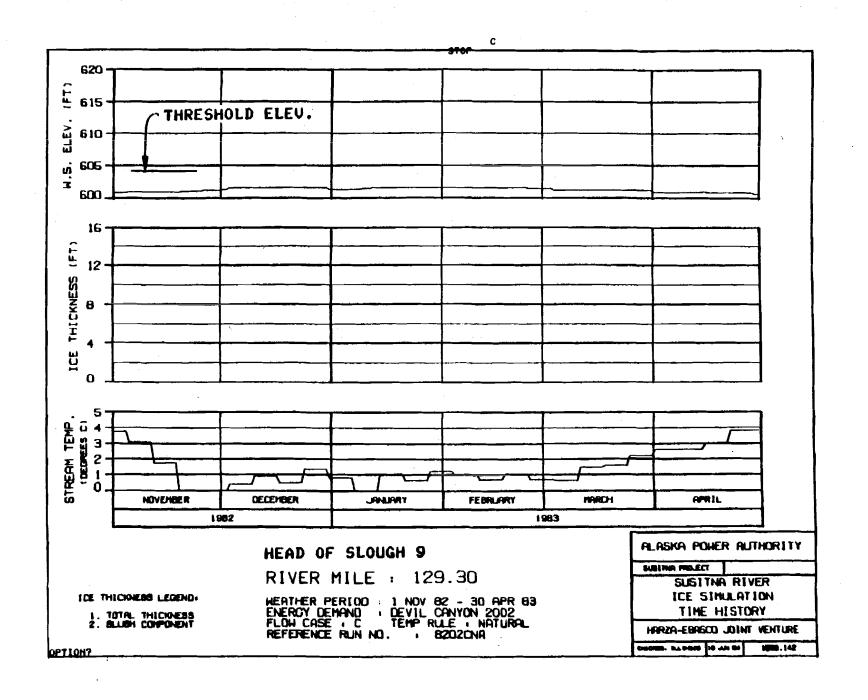


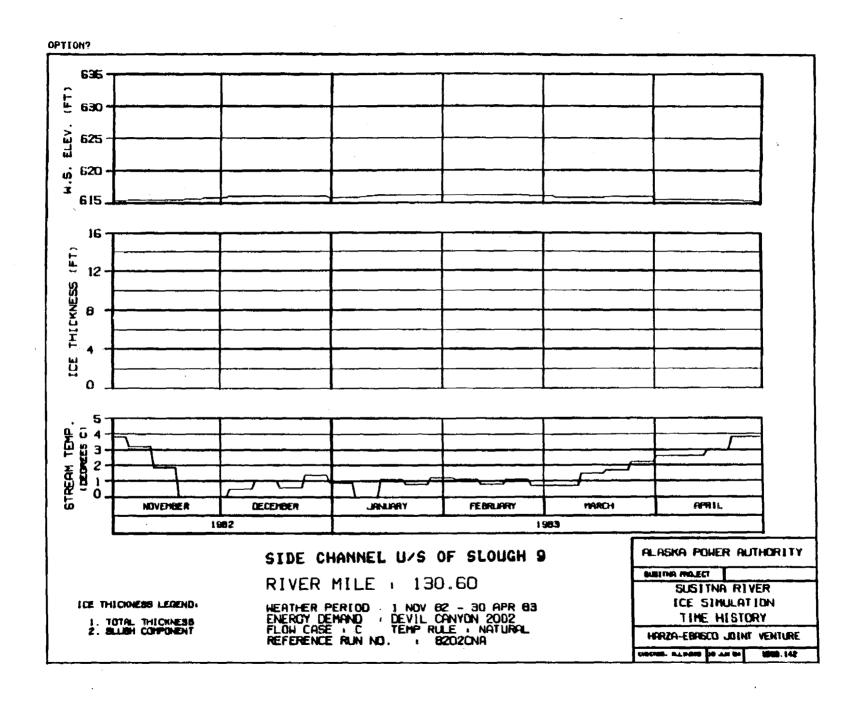
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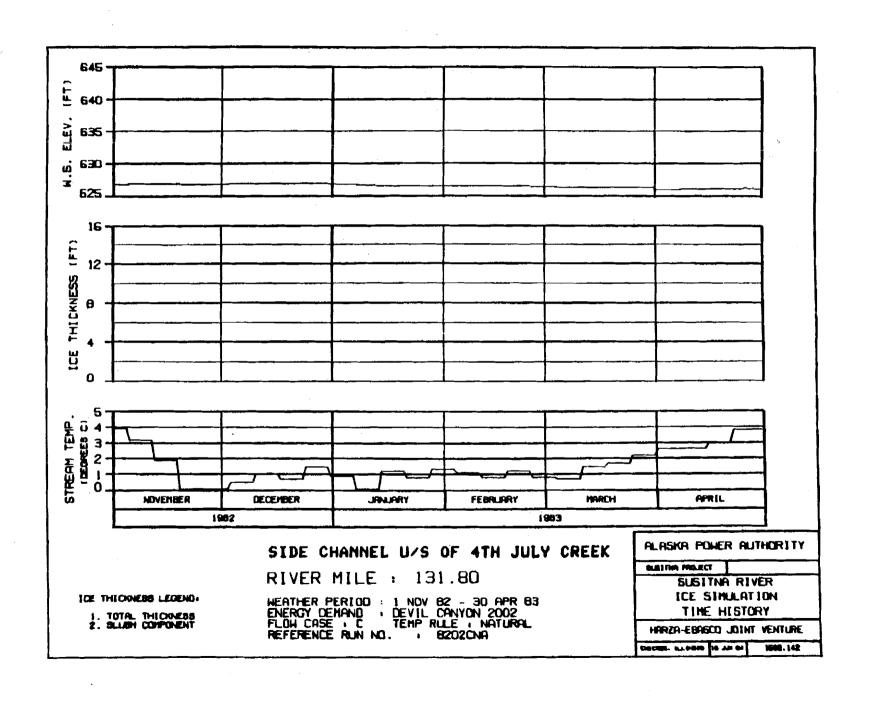


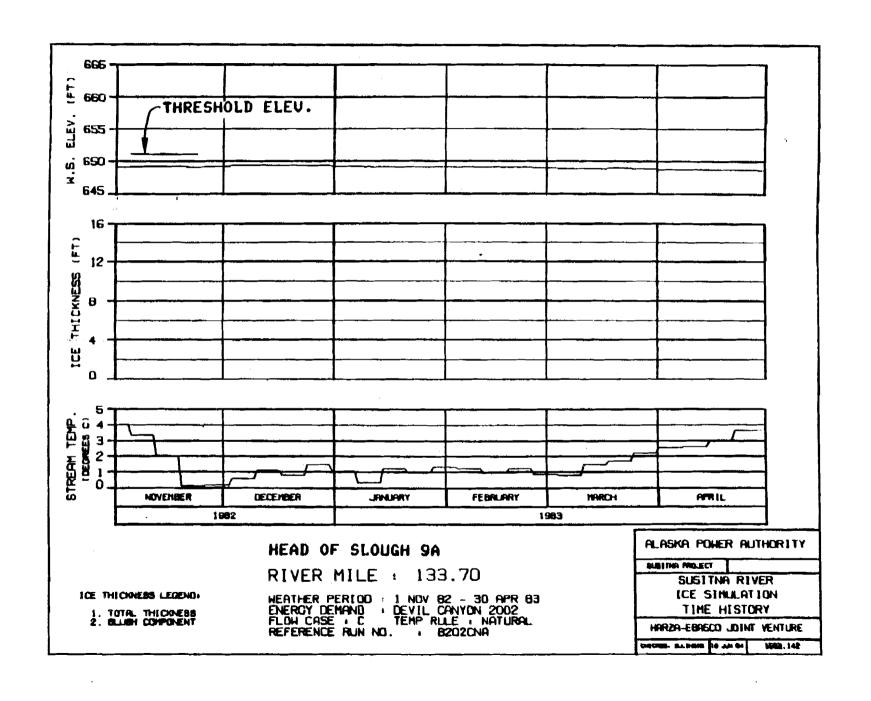
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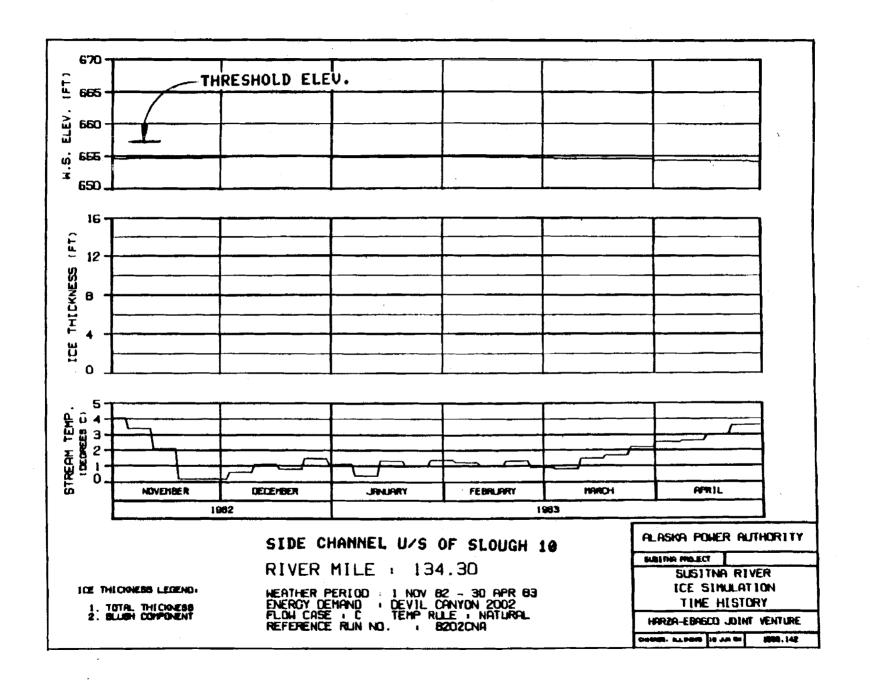


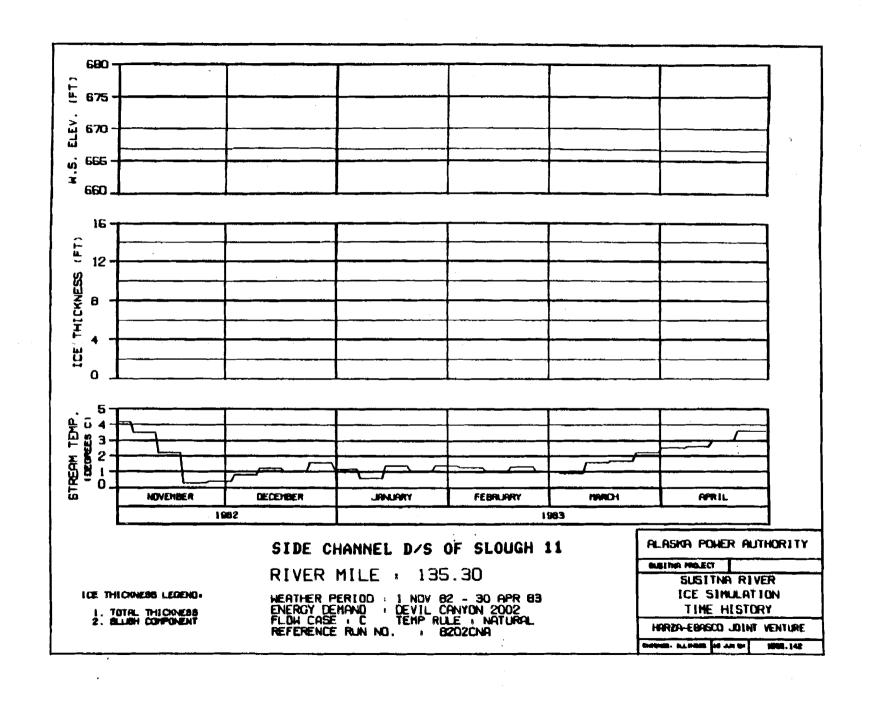
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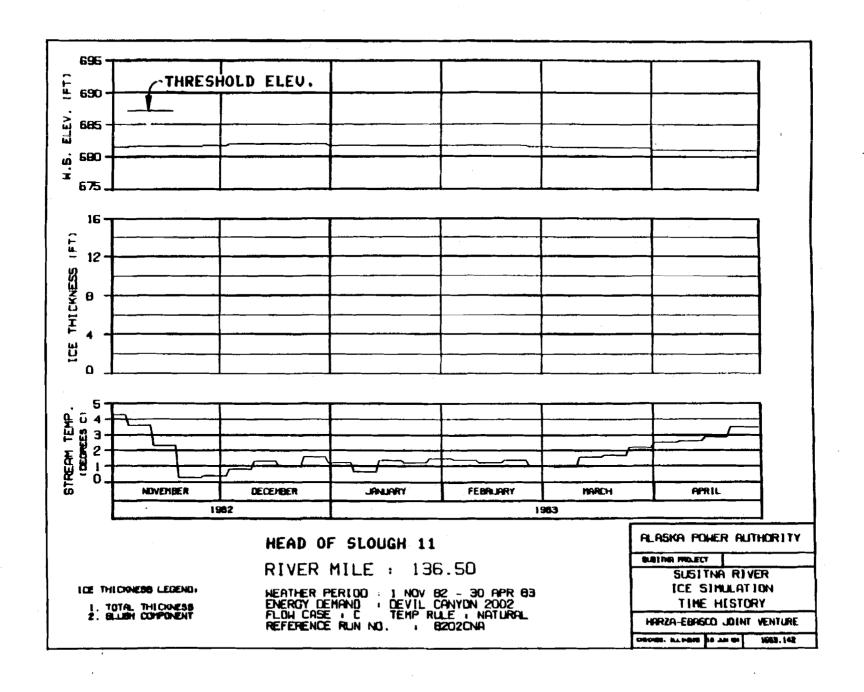


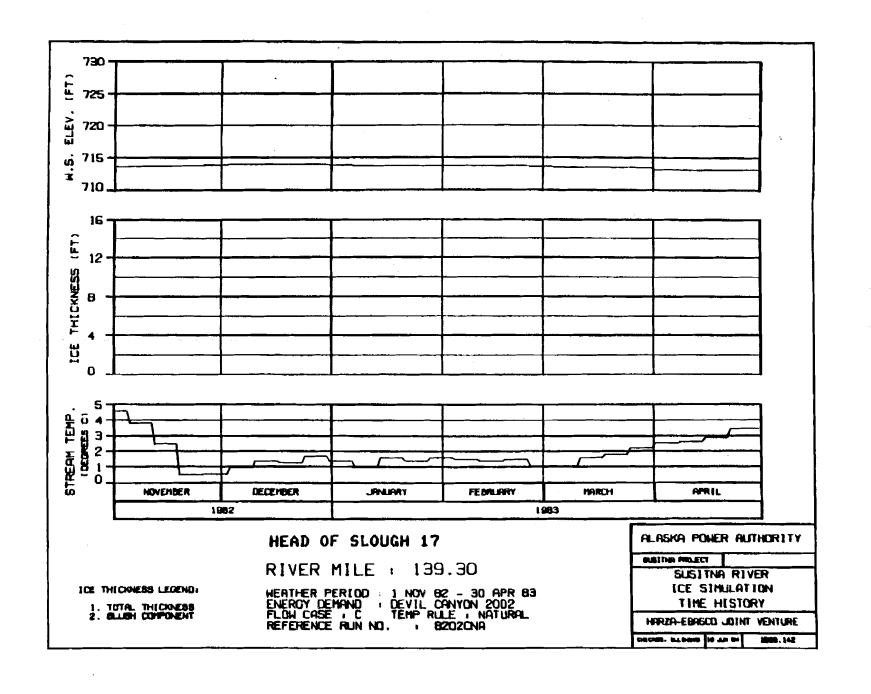


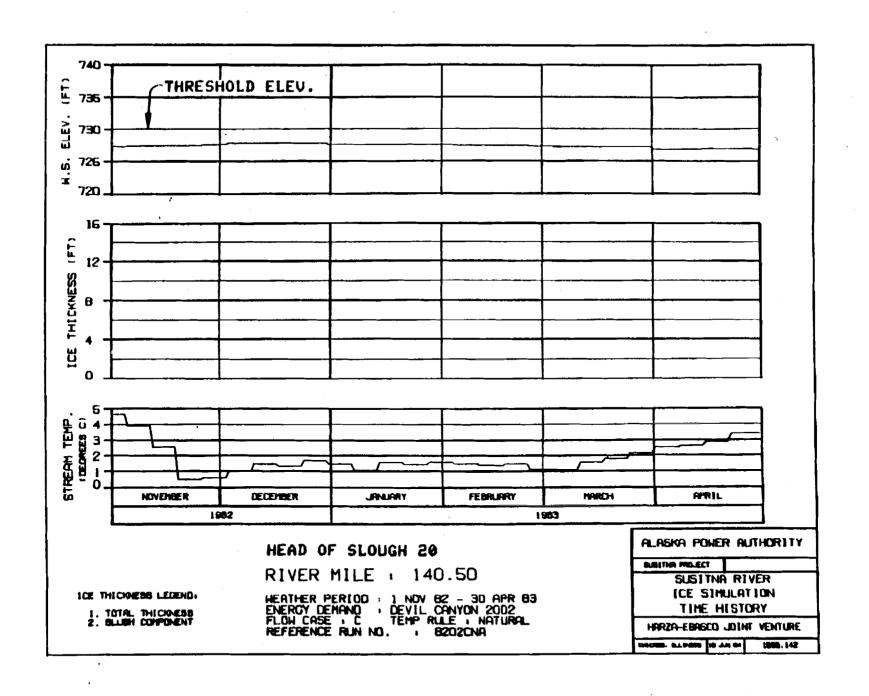
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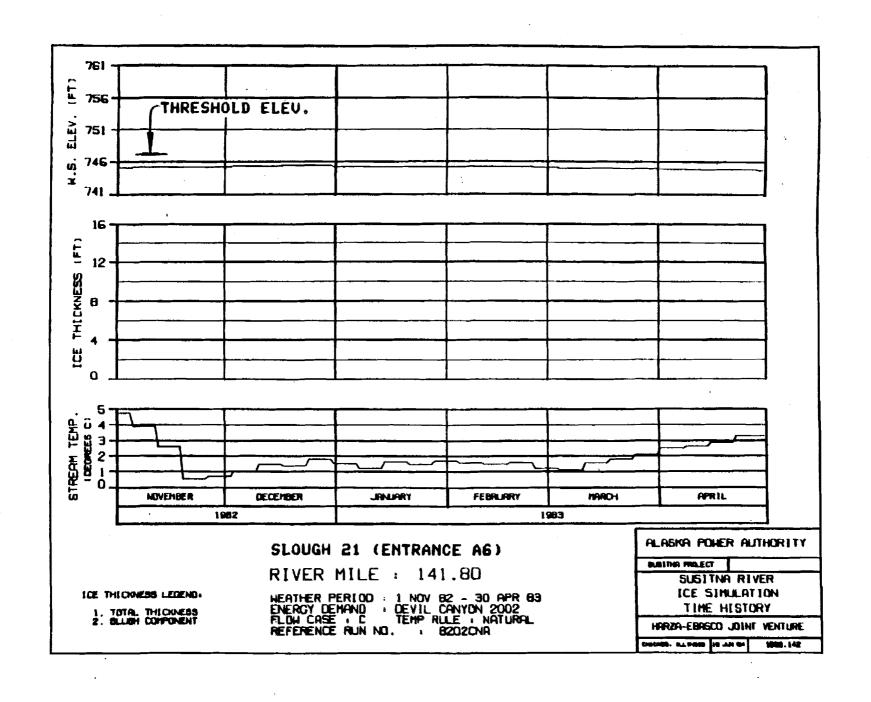


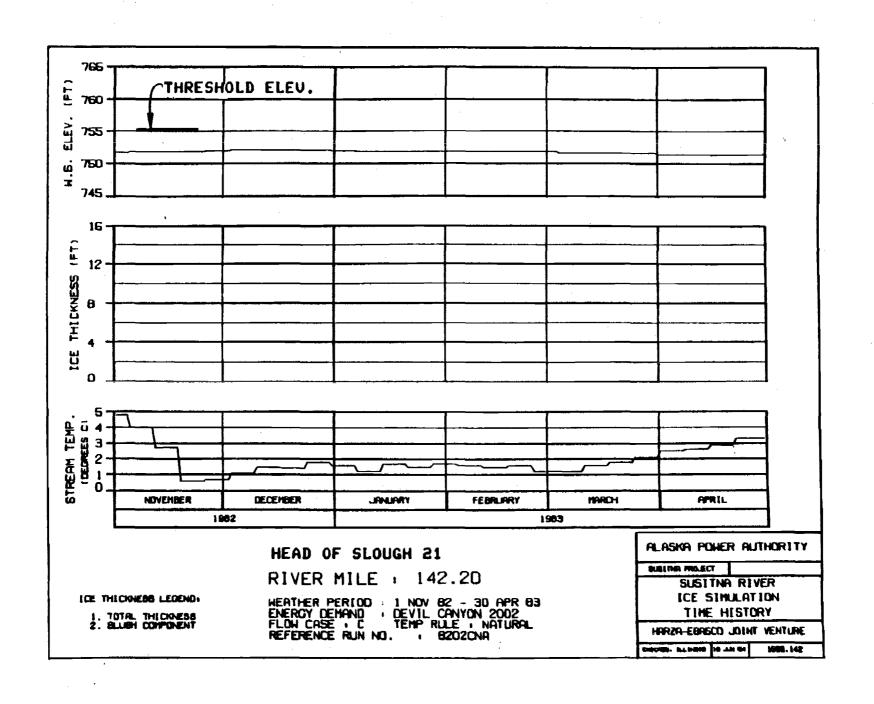


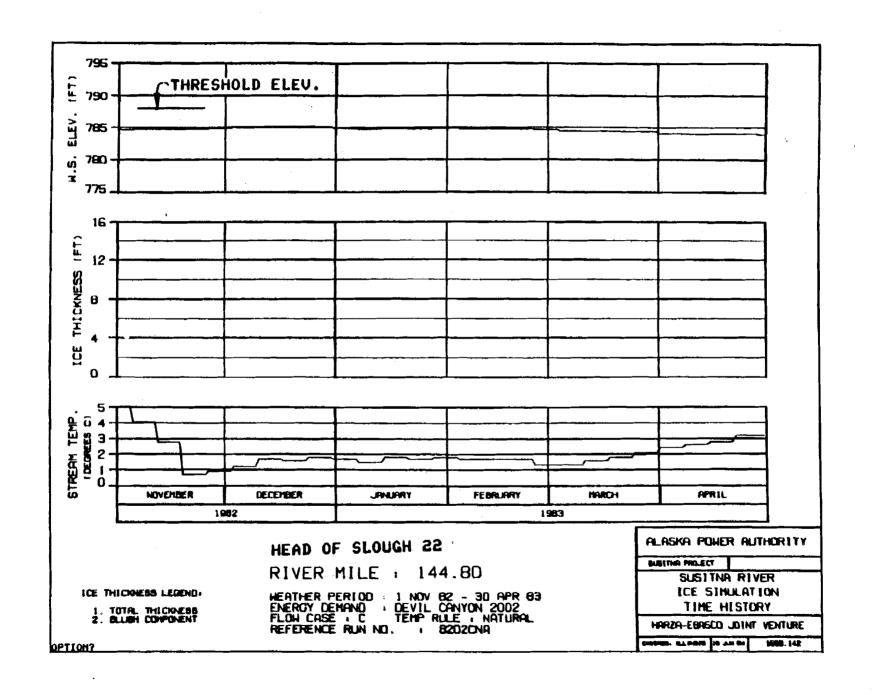






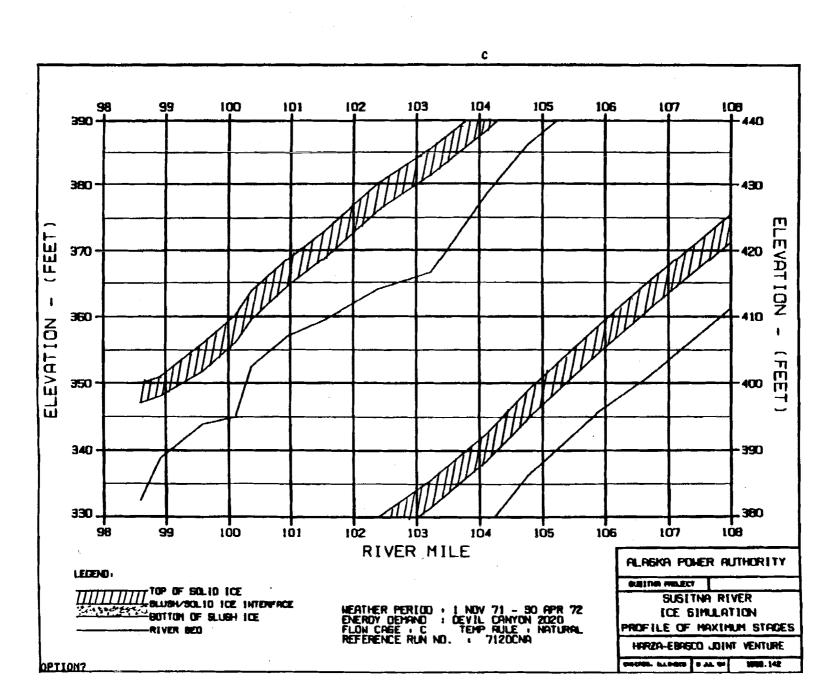




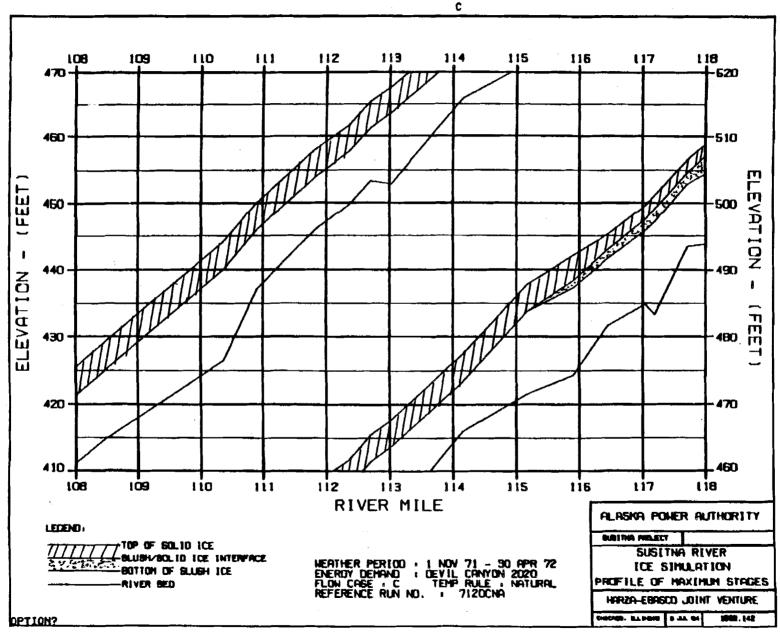


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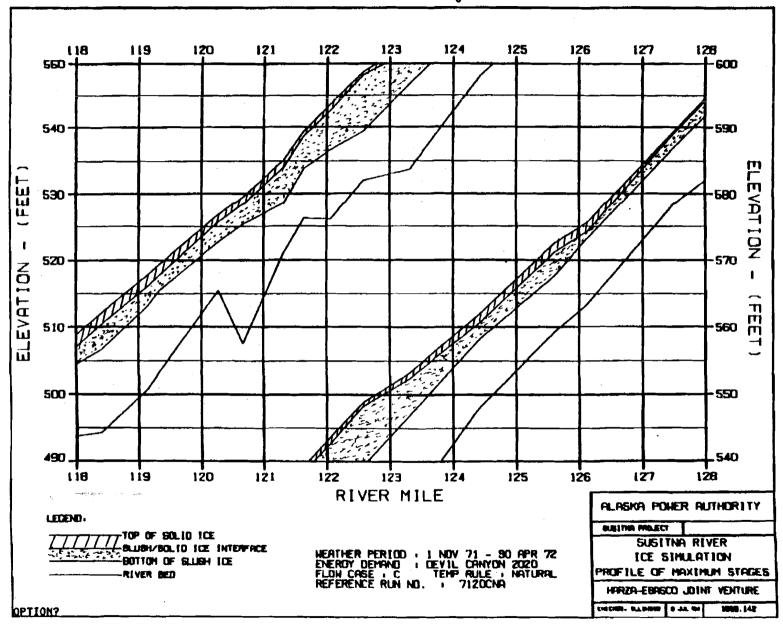
EXHIBIT Q



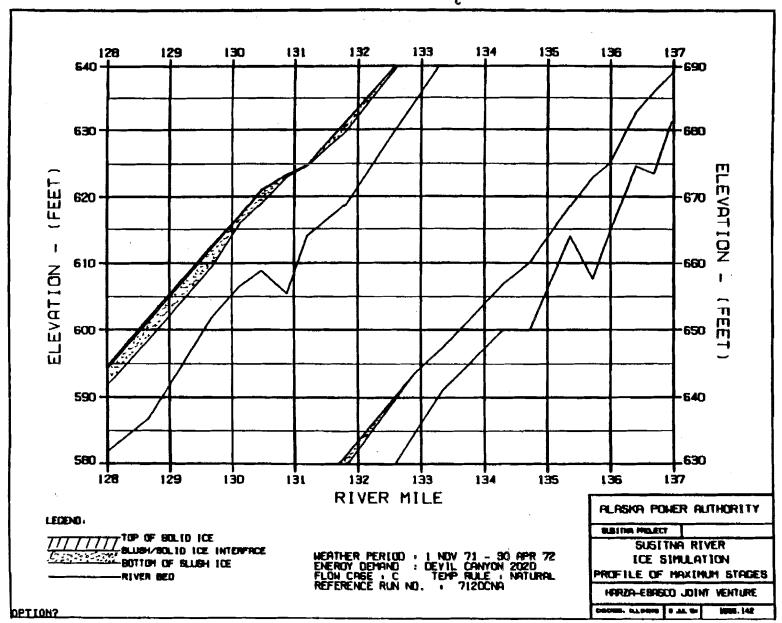




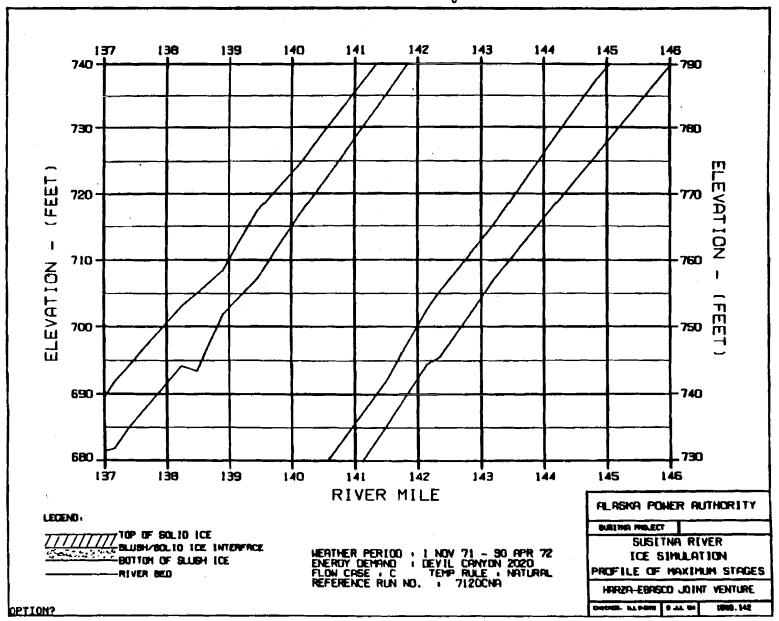




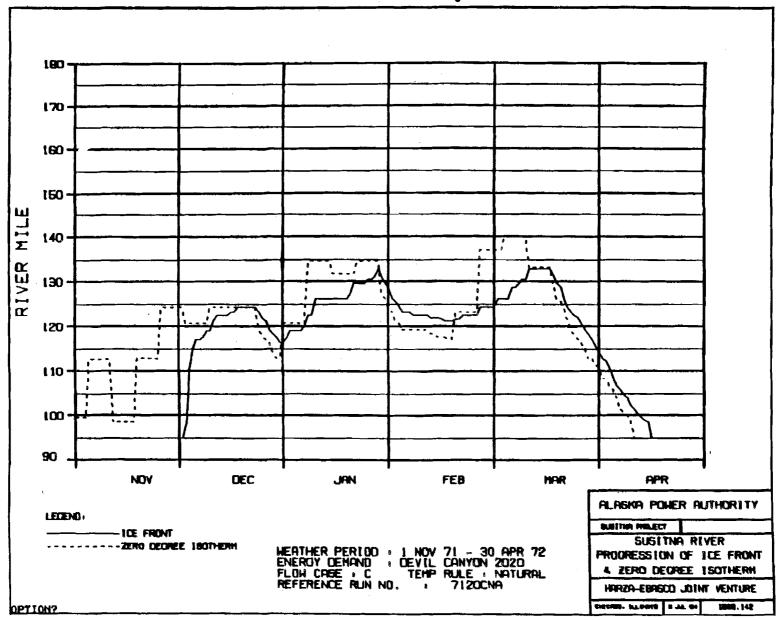
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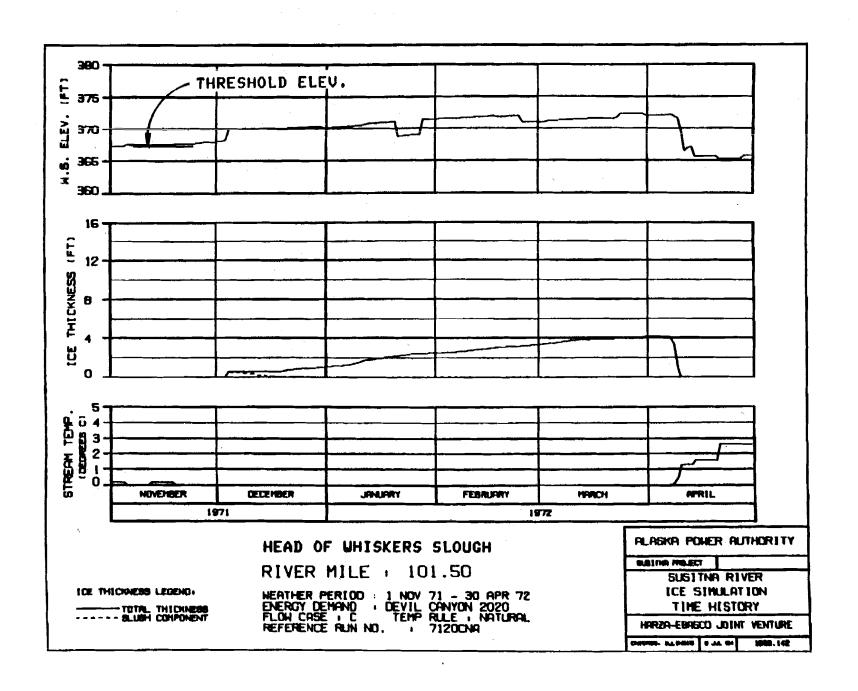


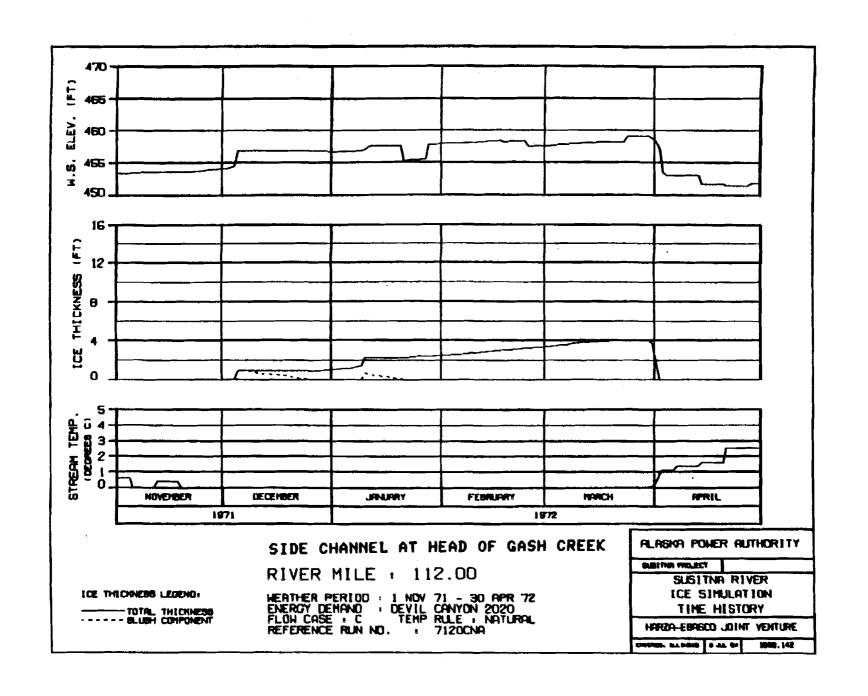




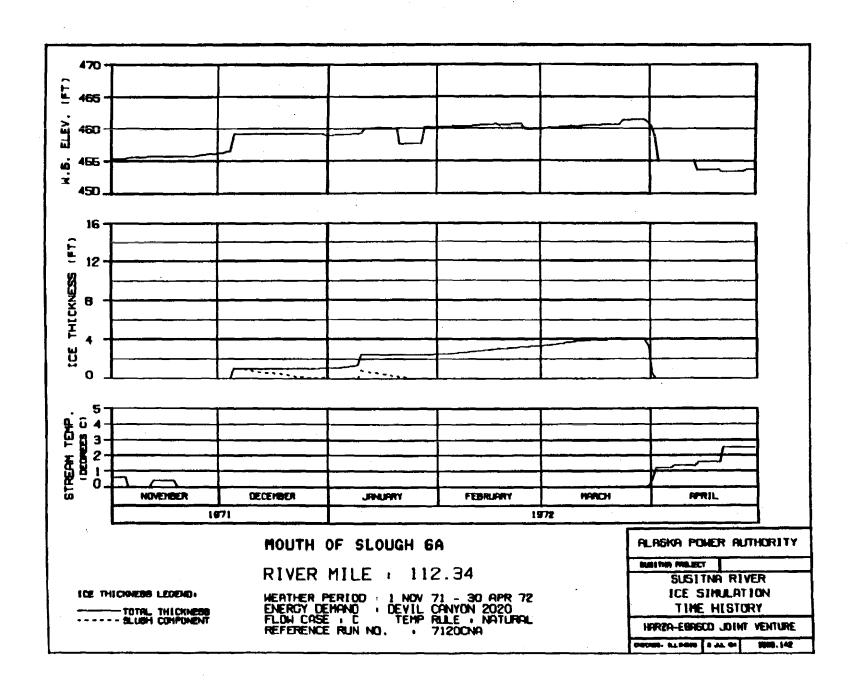


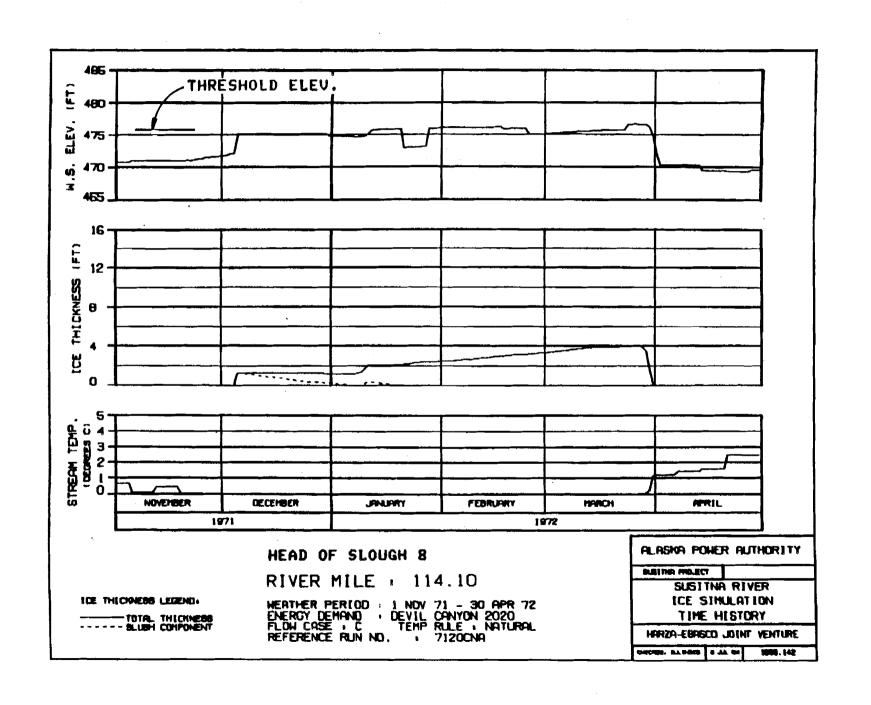




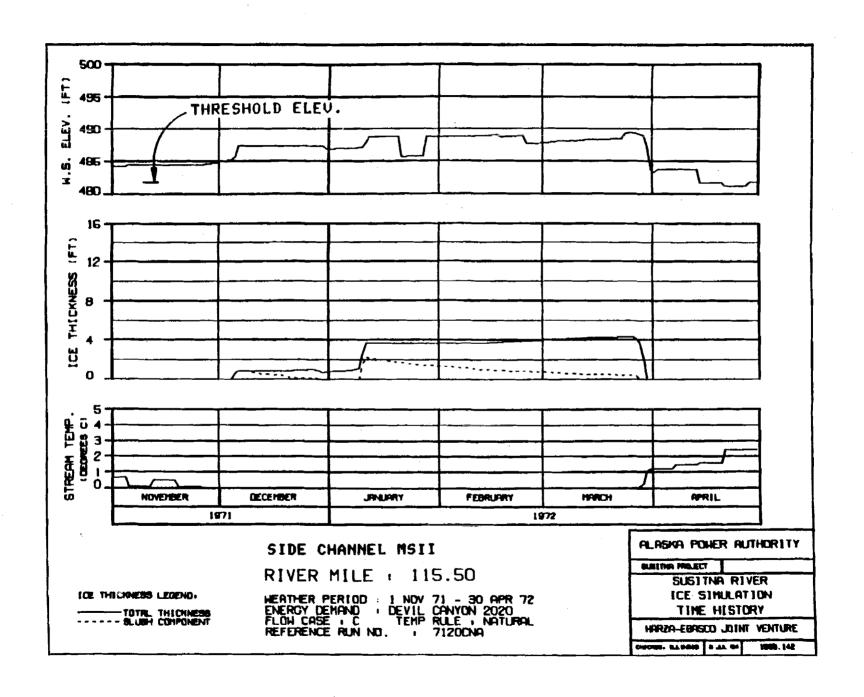


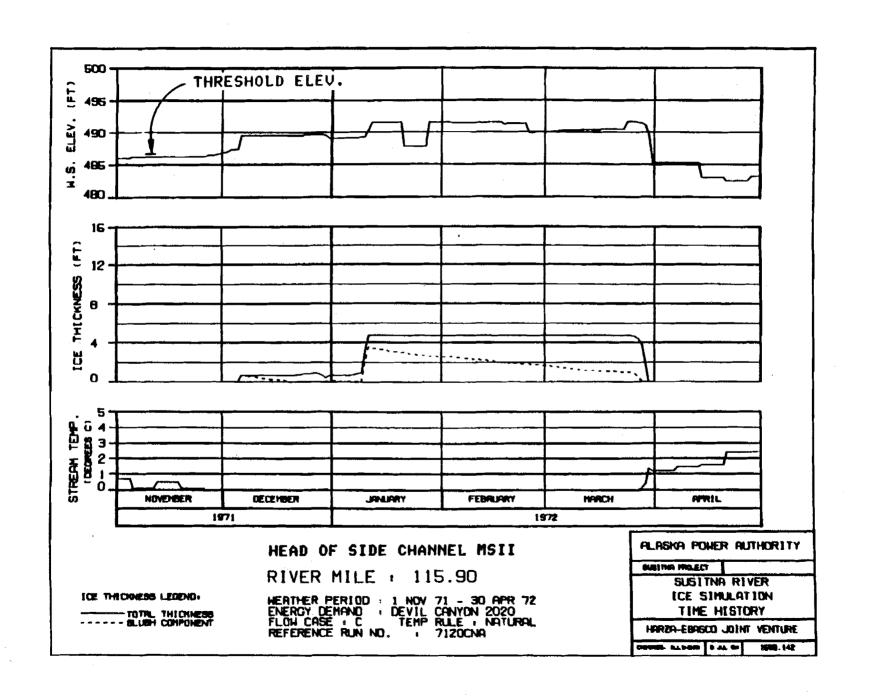
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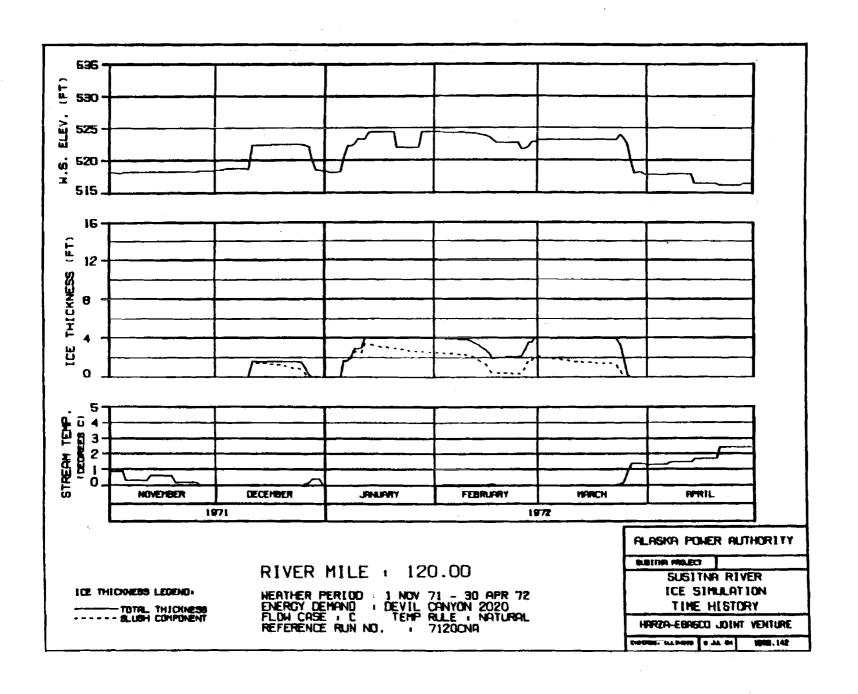


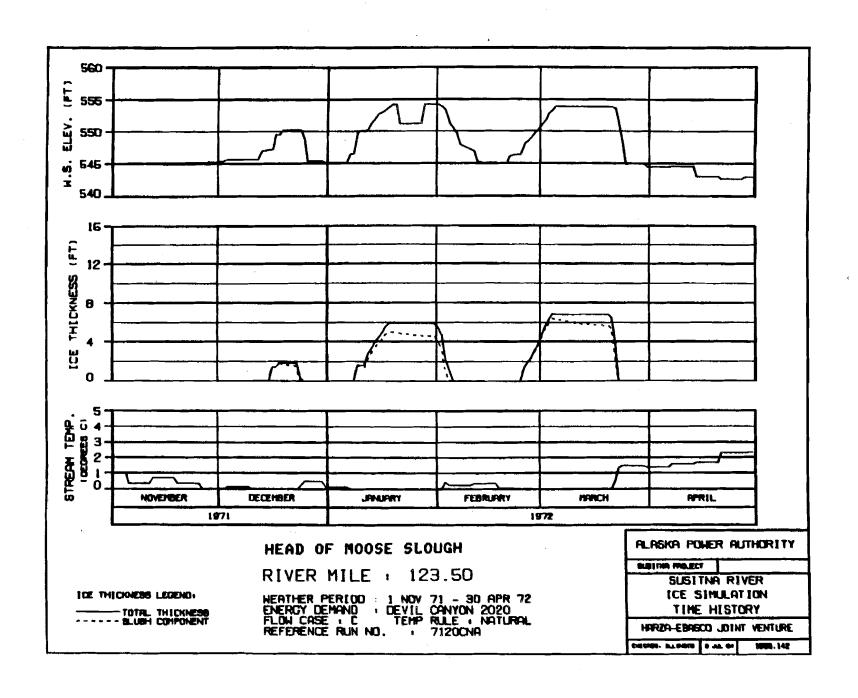


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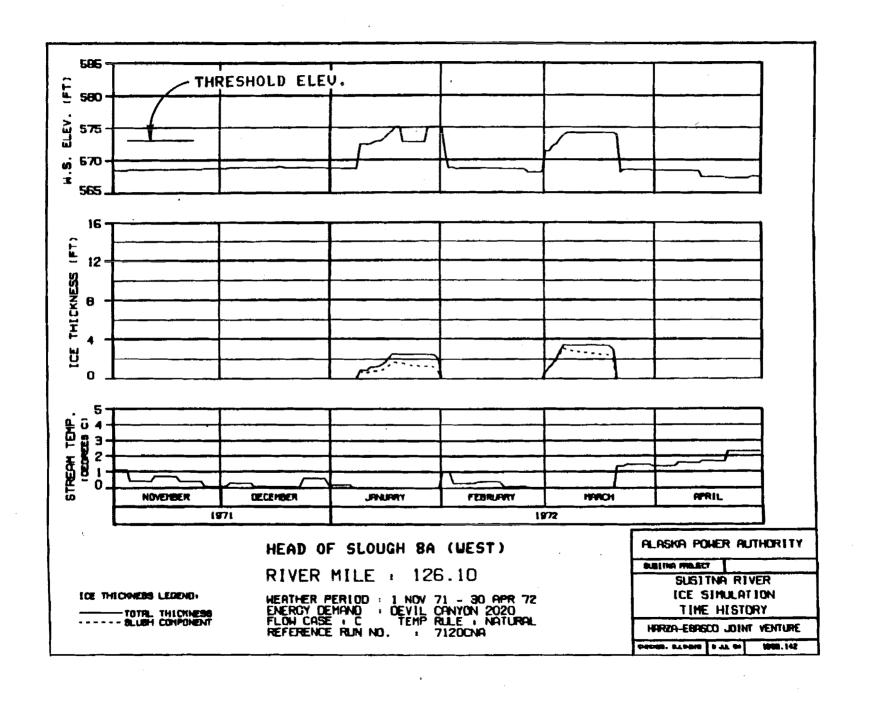


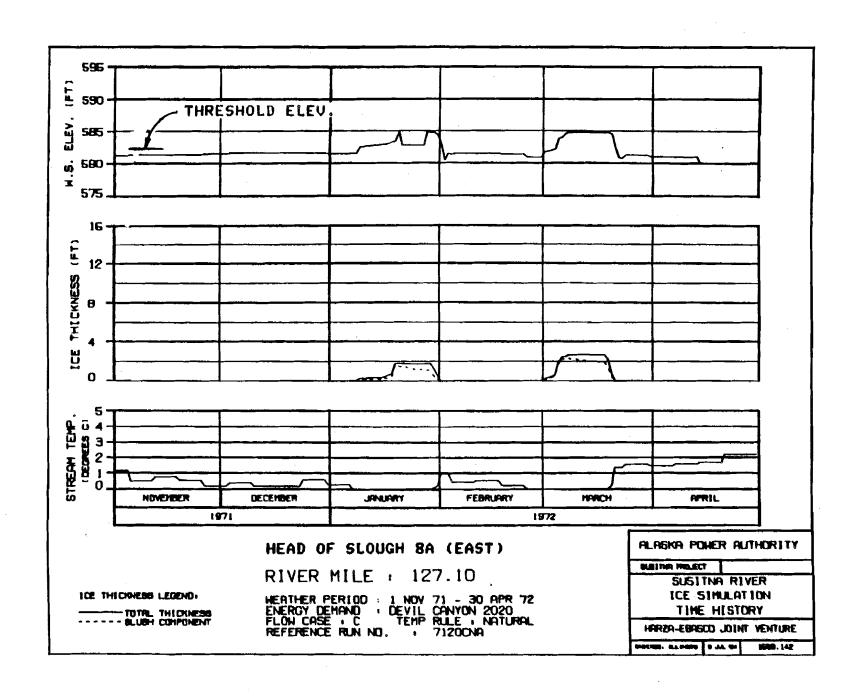




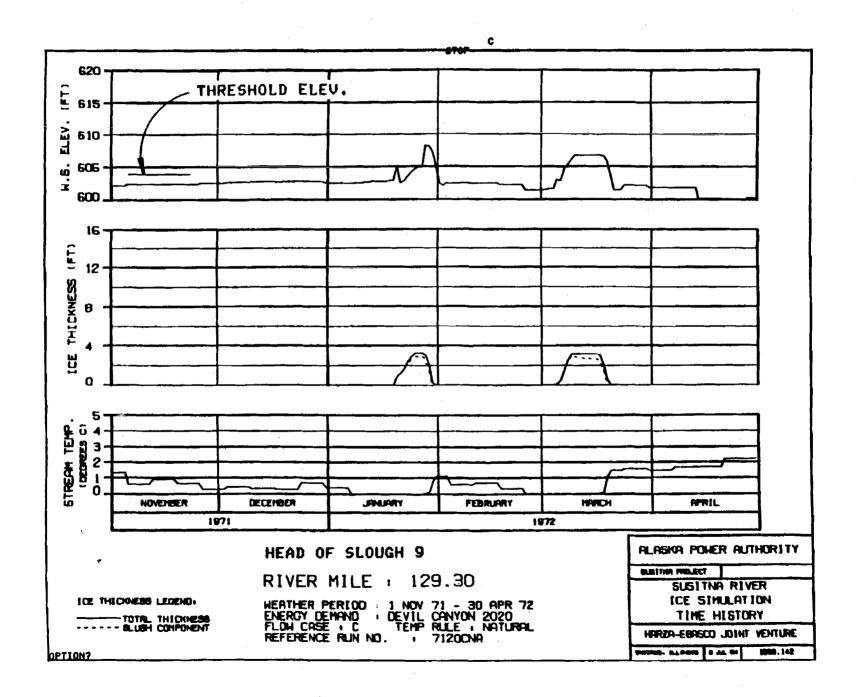


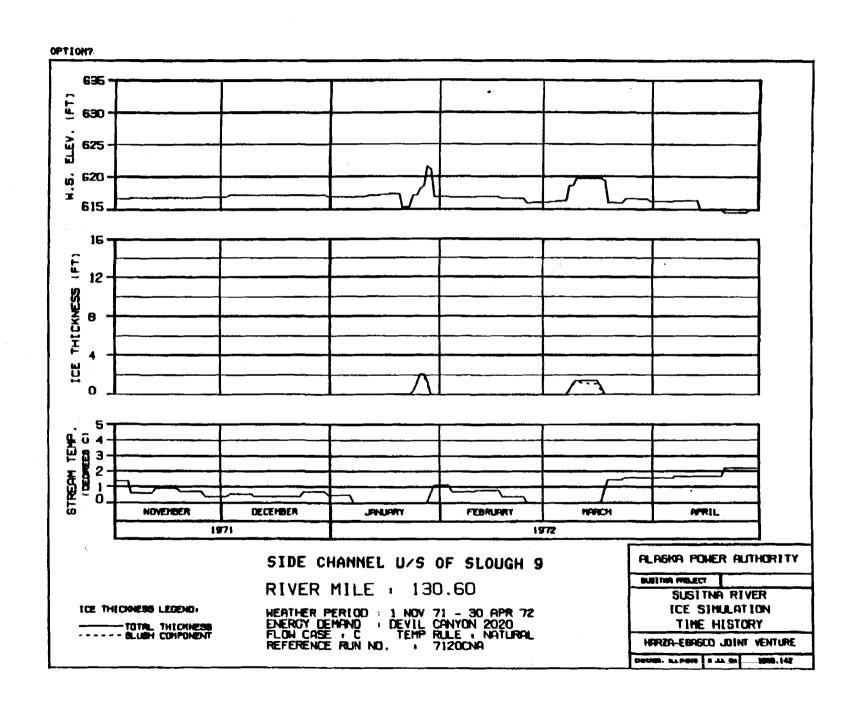
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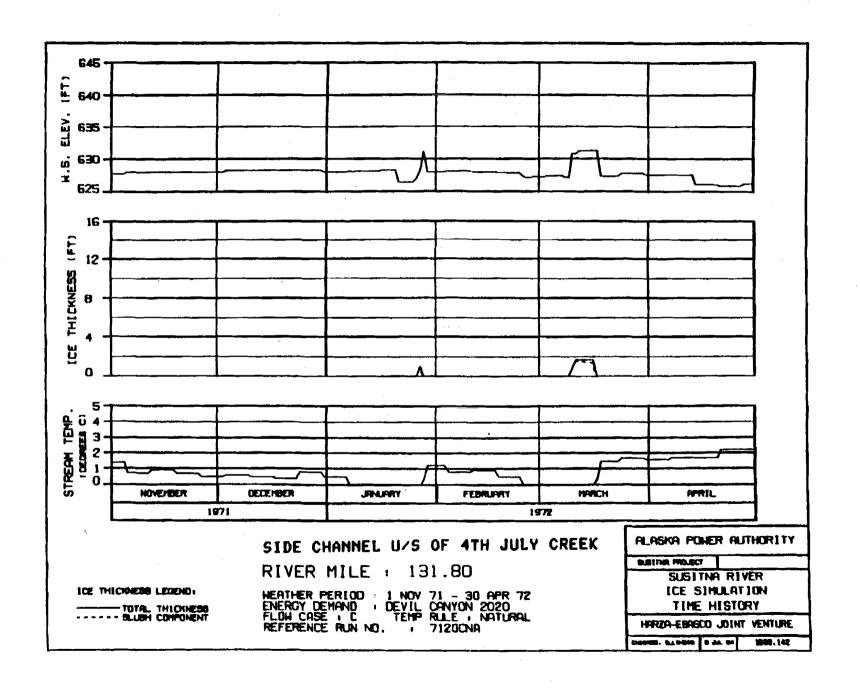


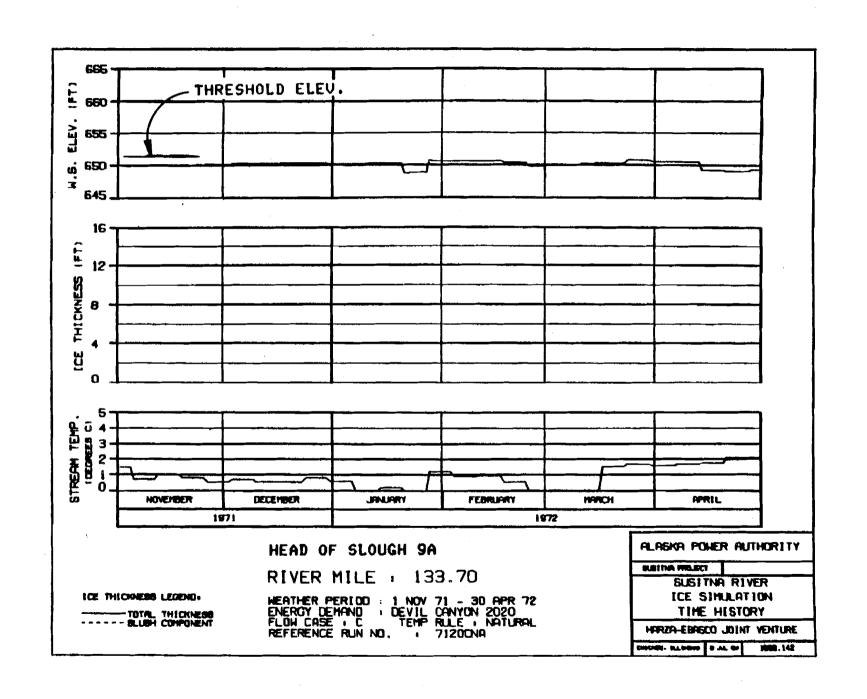


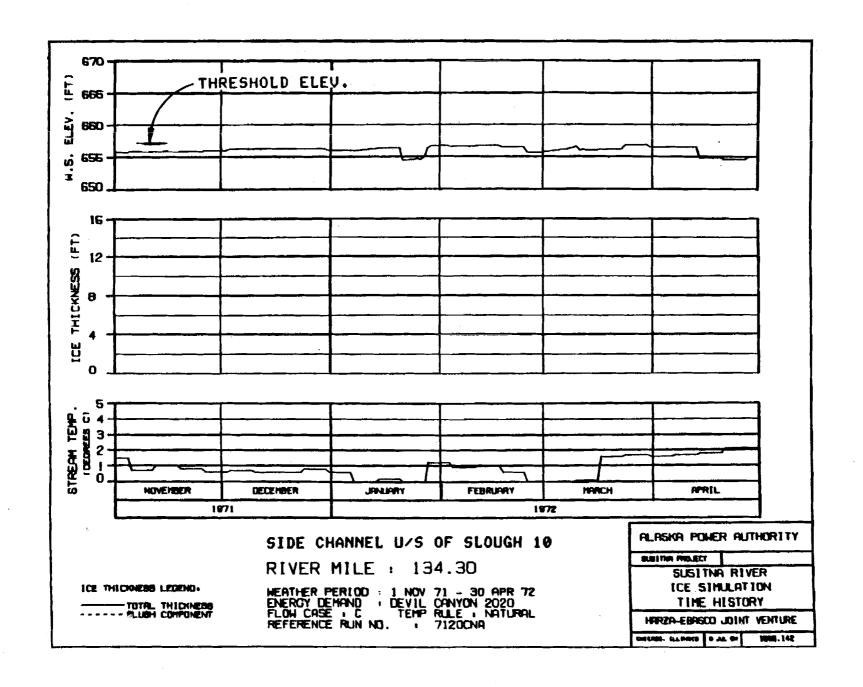
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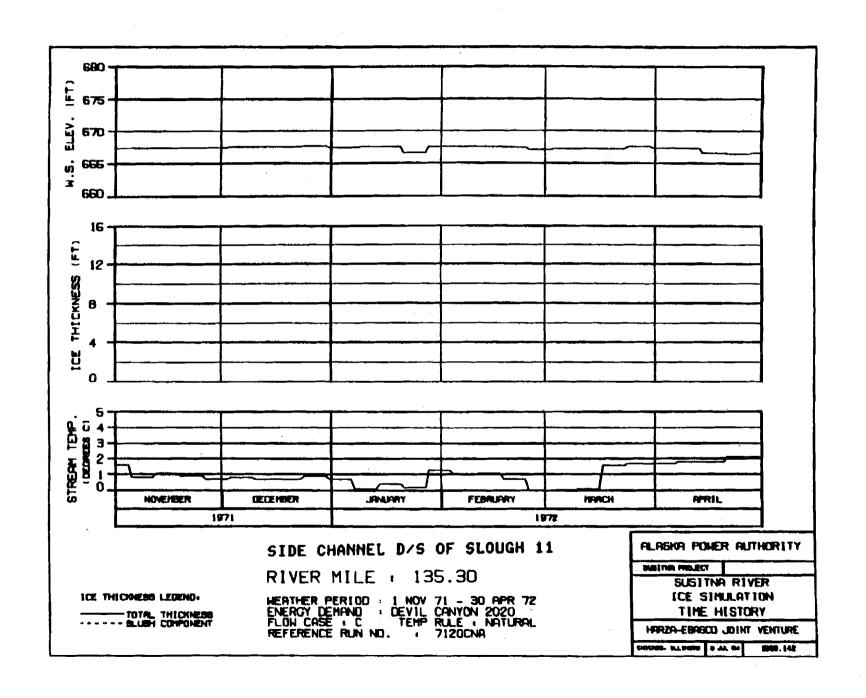


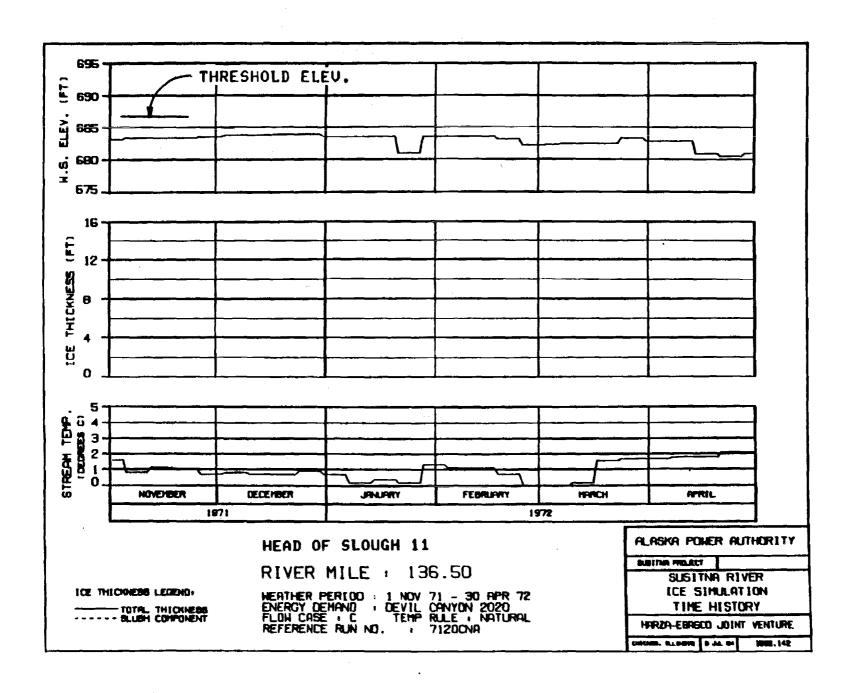


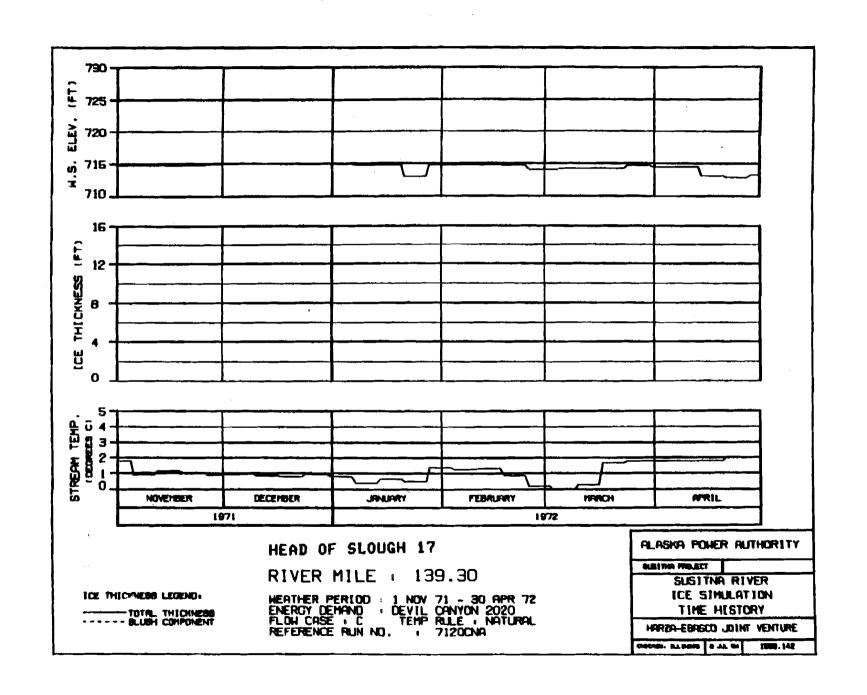


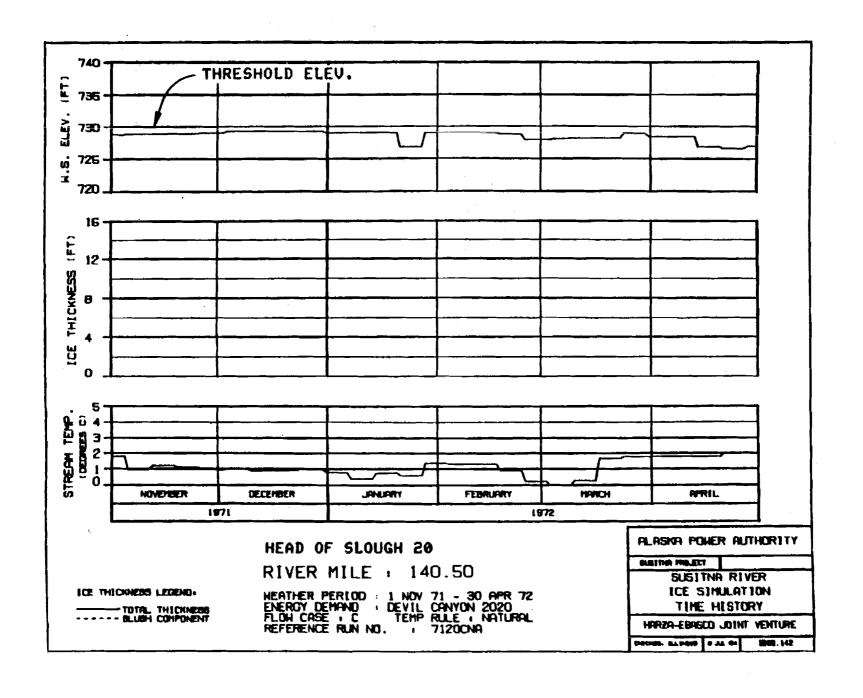


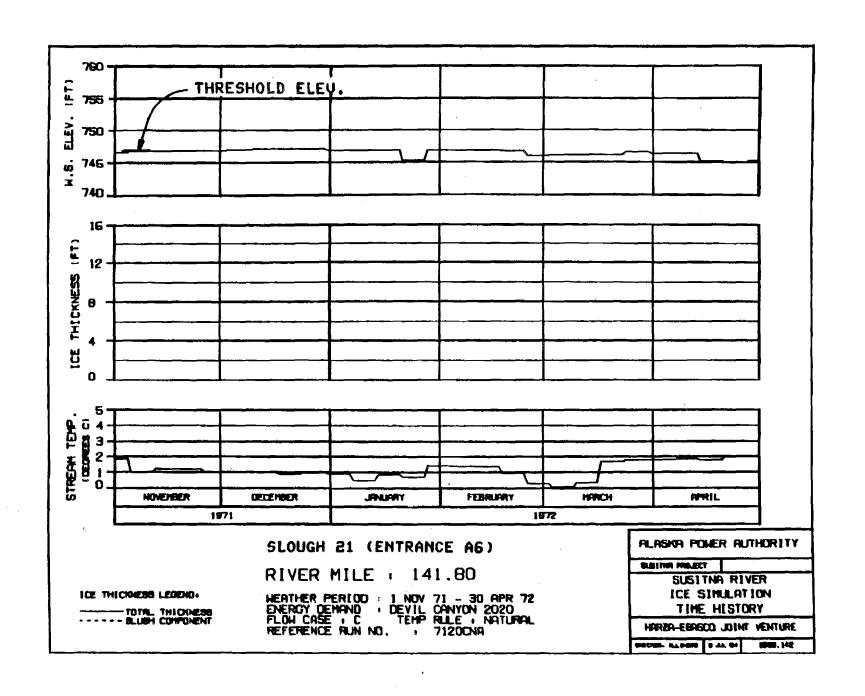




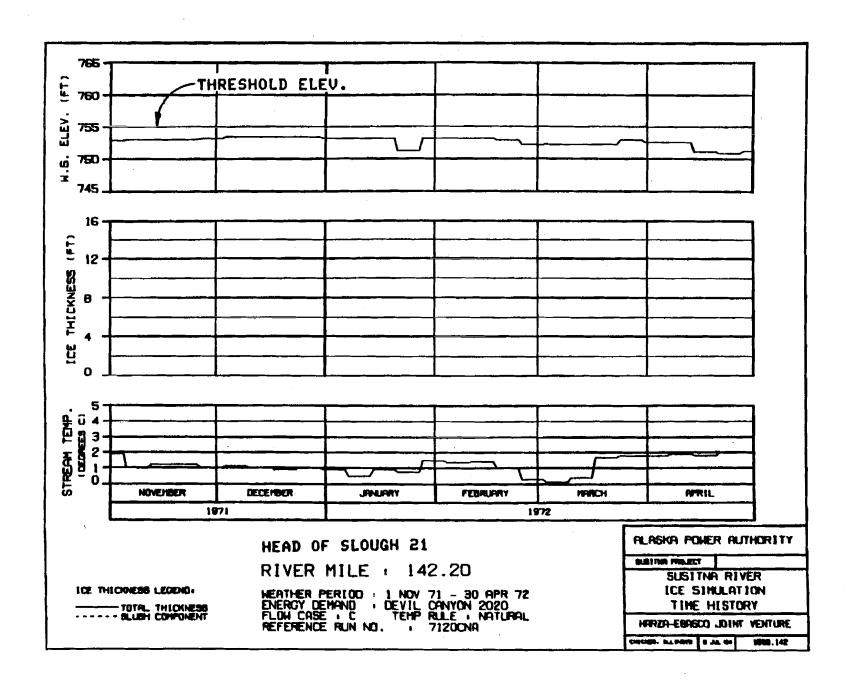


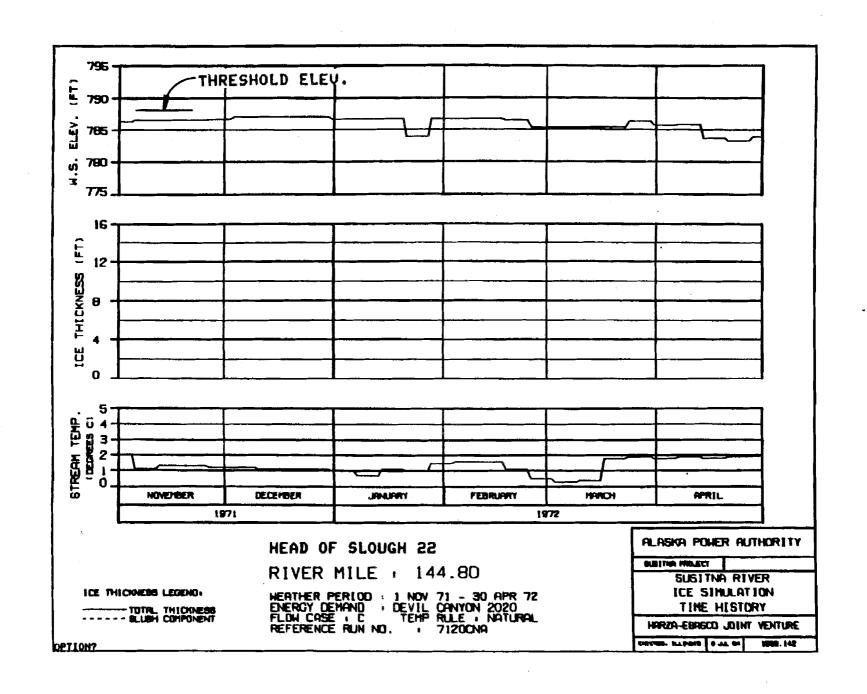






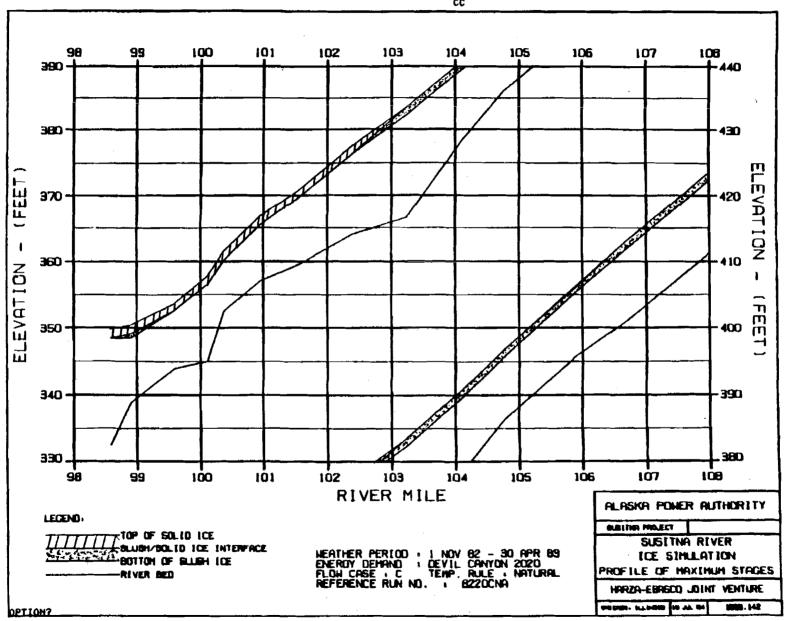
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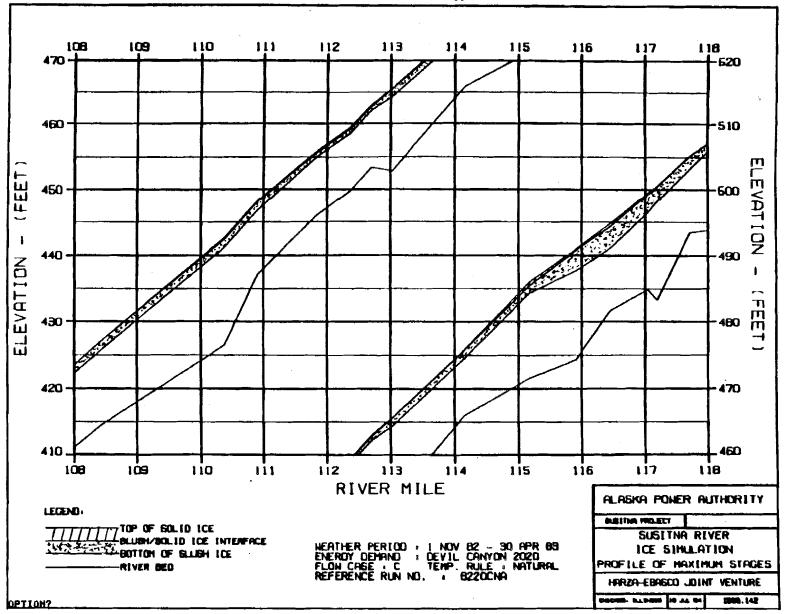




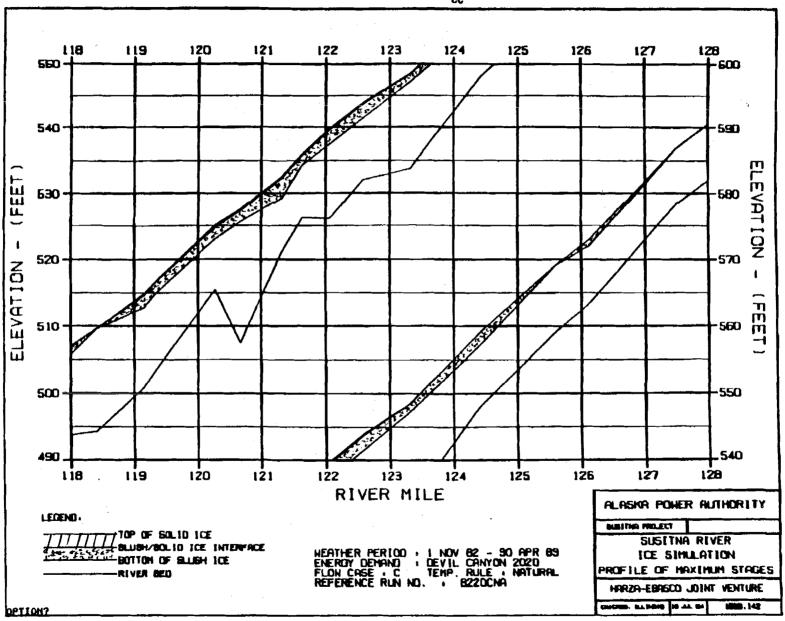
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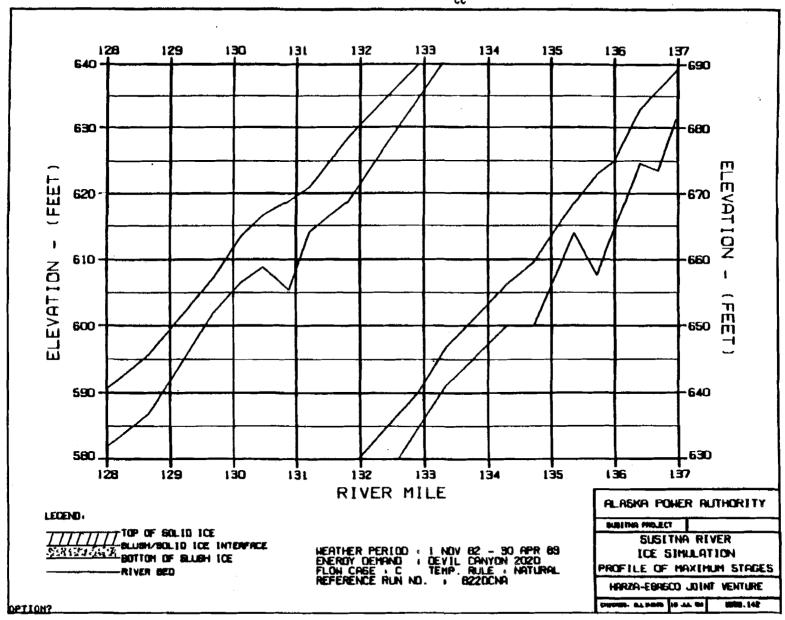
EXHIBIT R

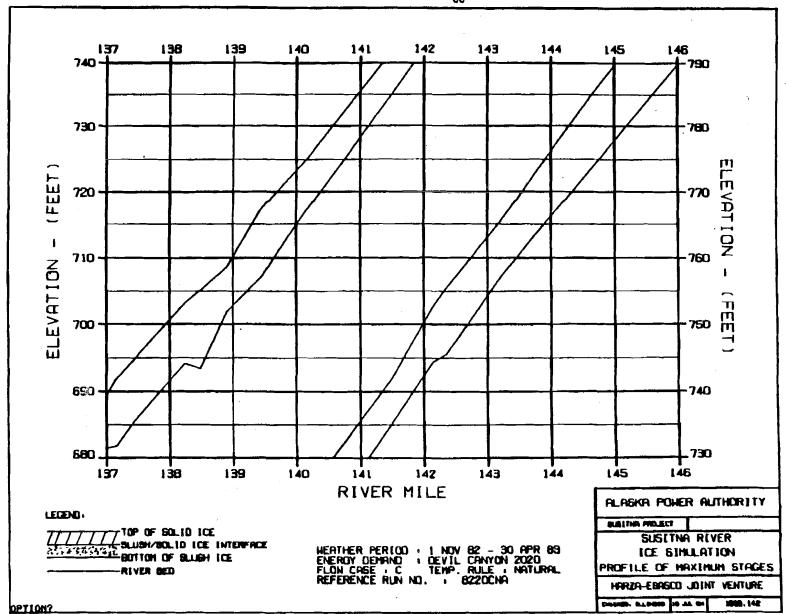


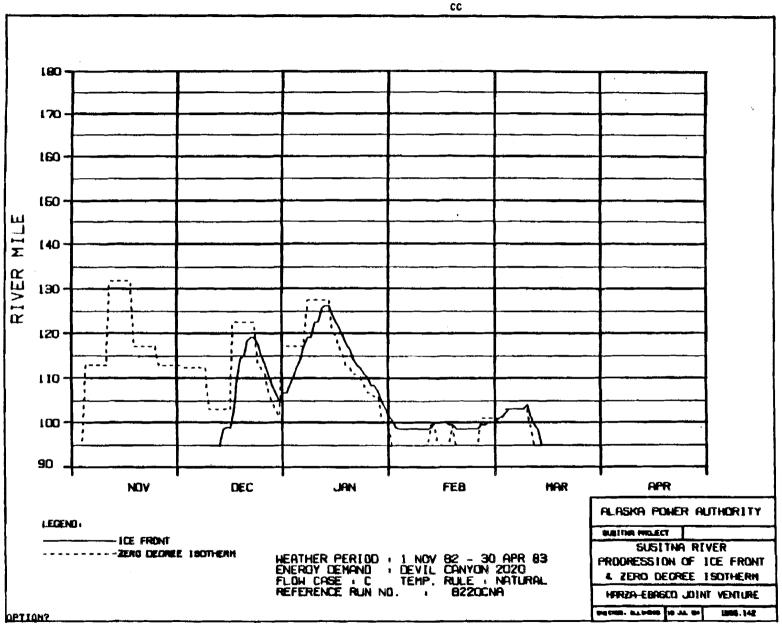


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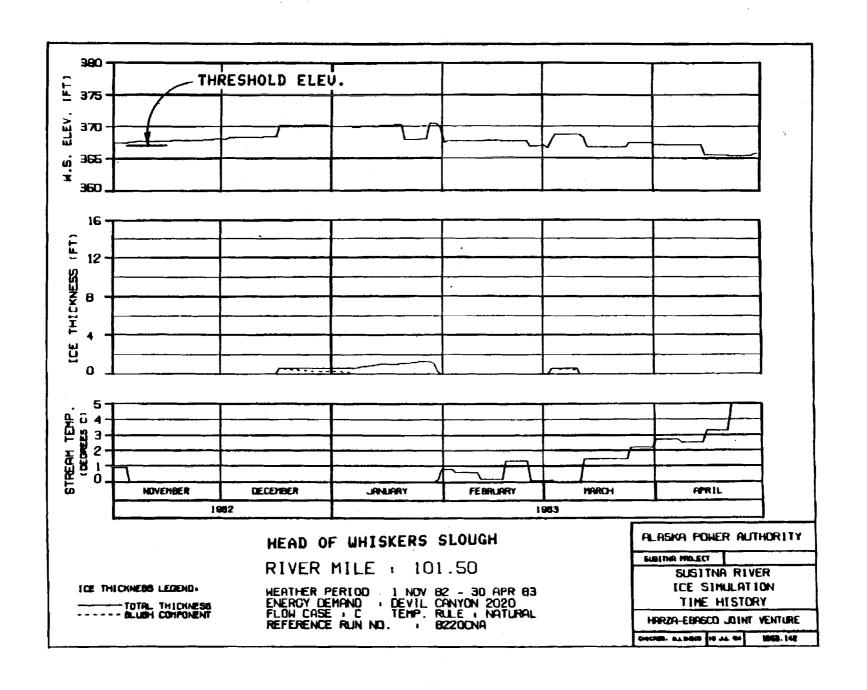


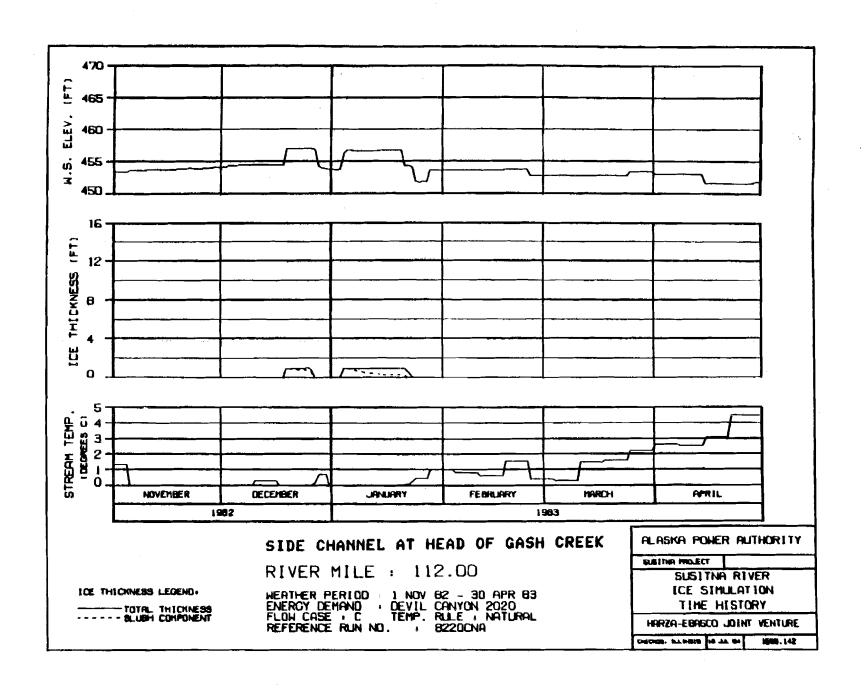


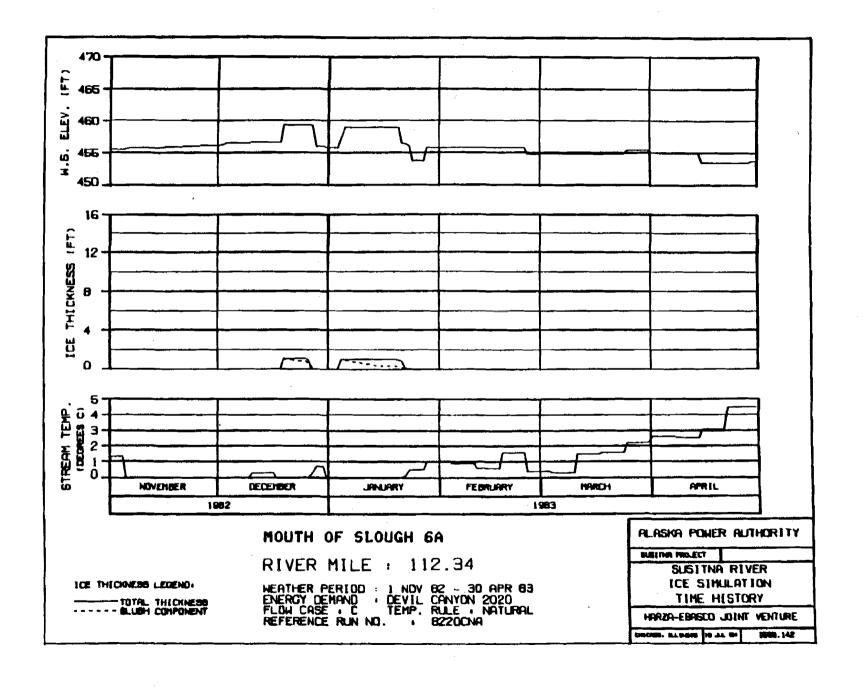
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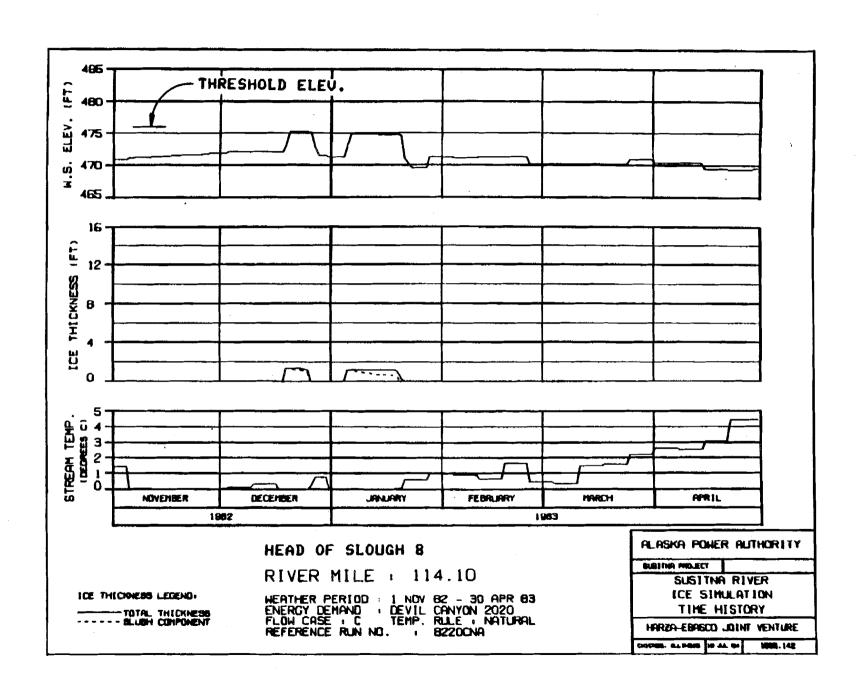


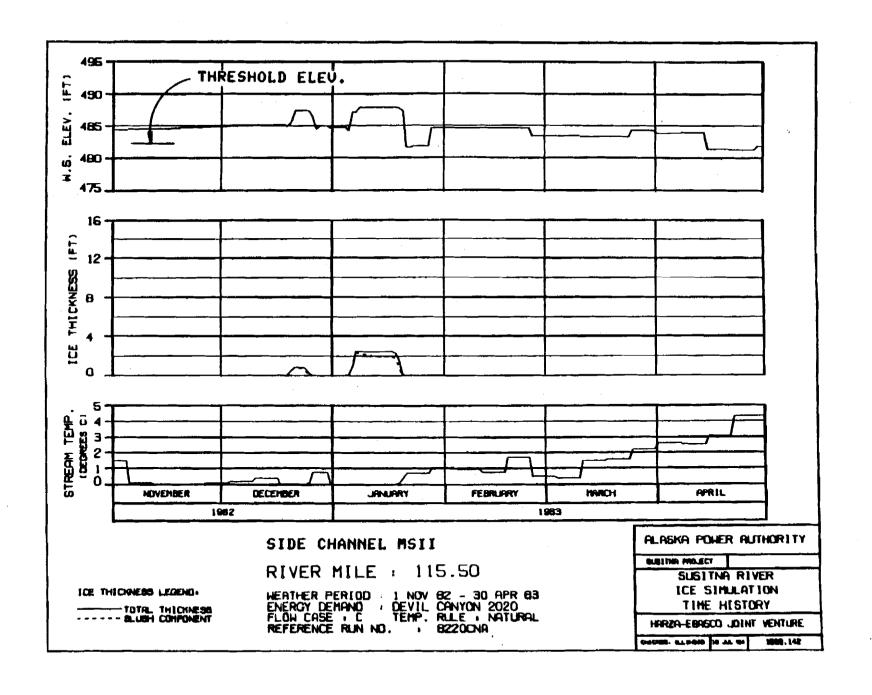
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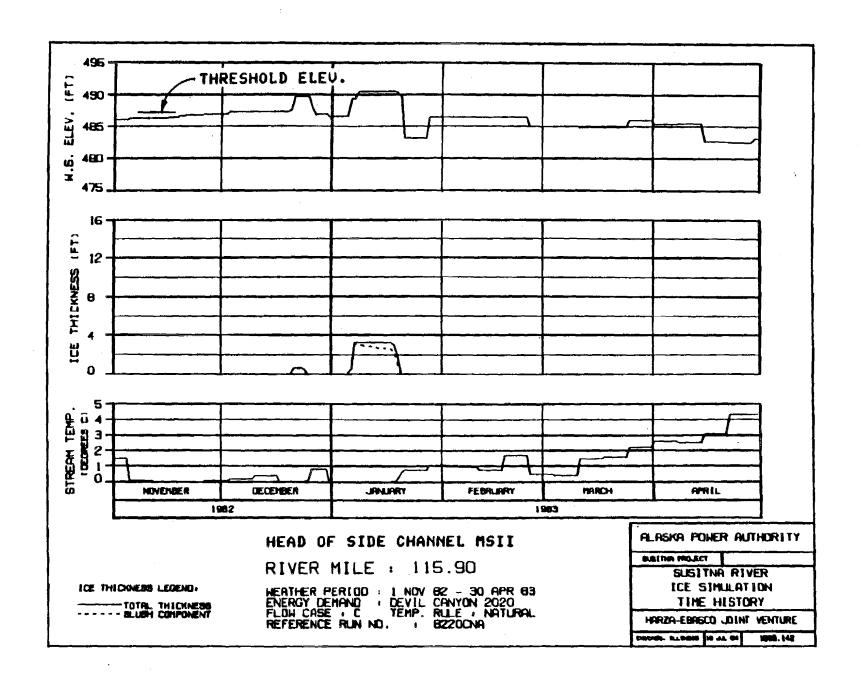


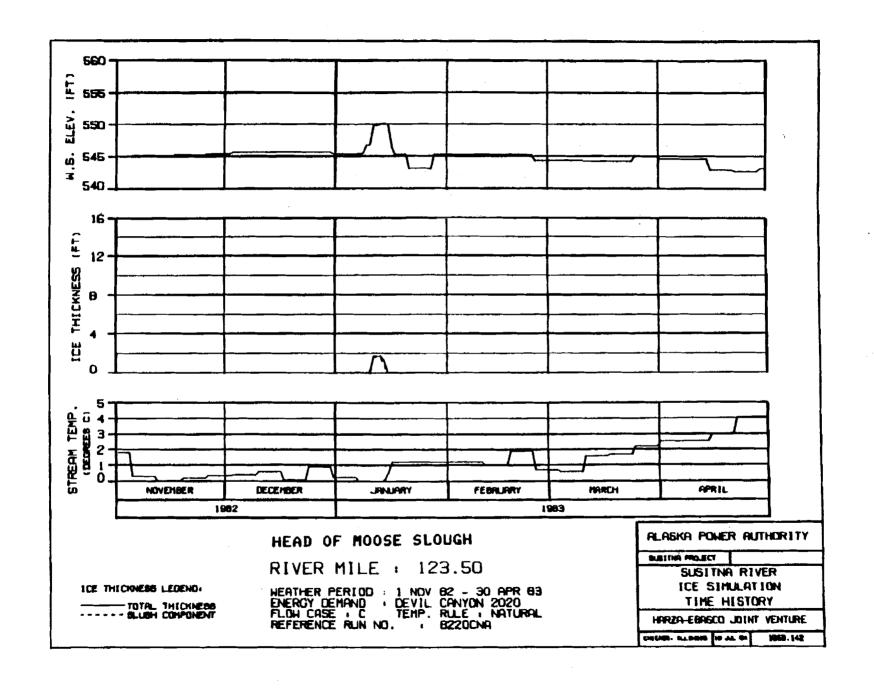


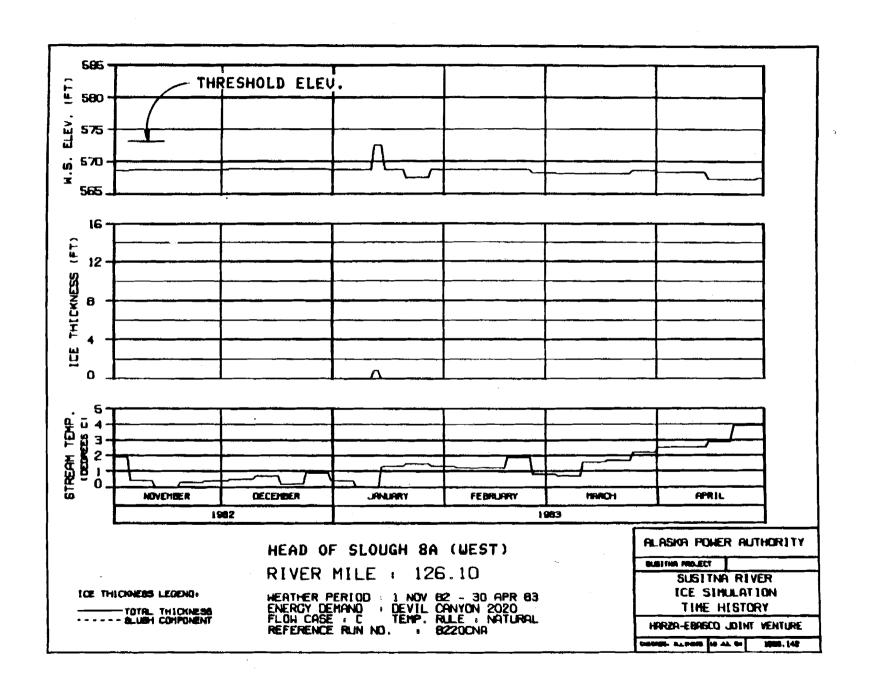


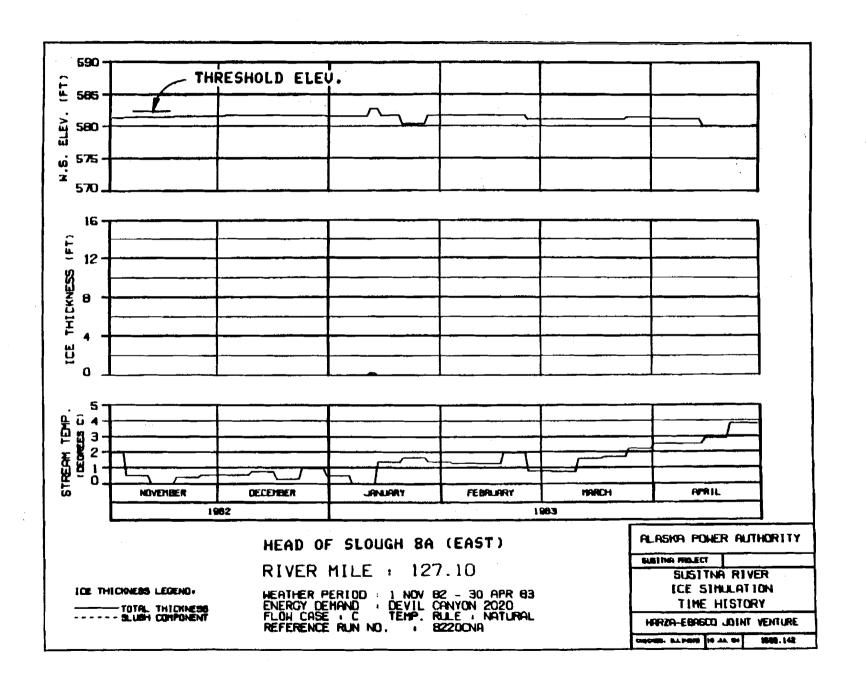


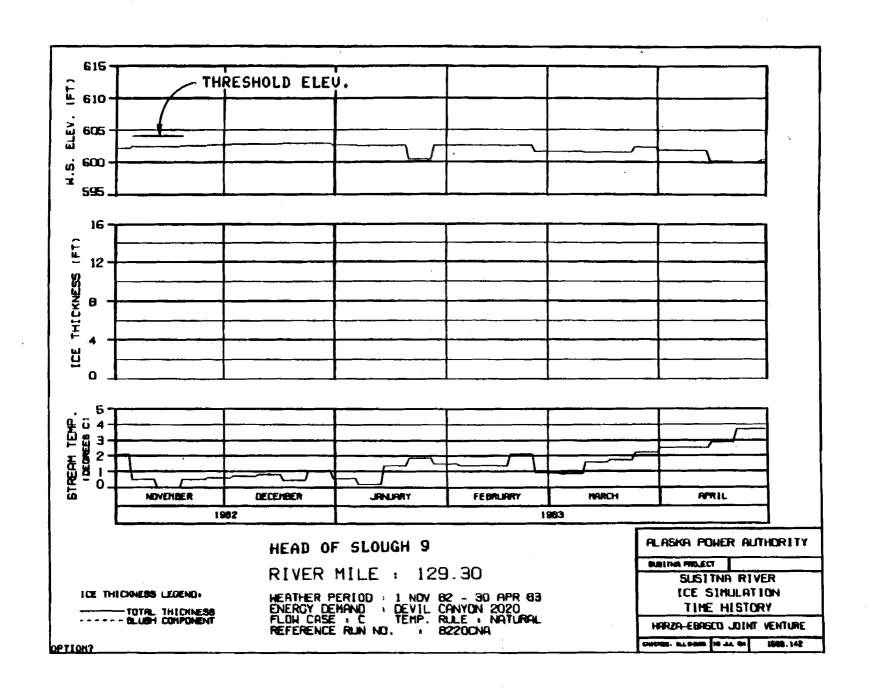


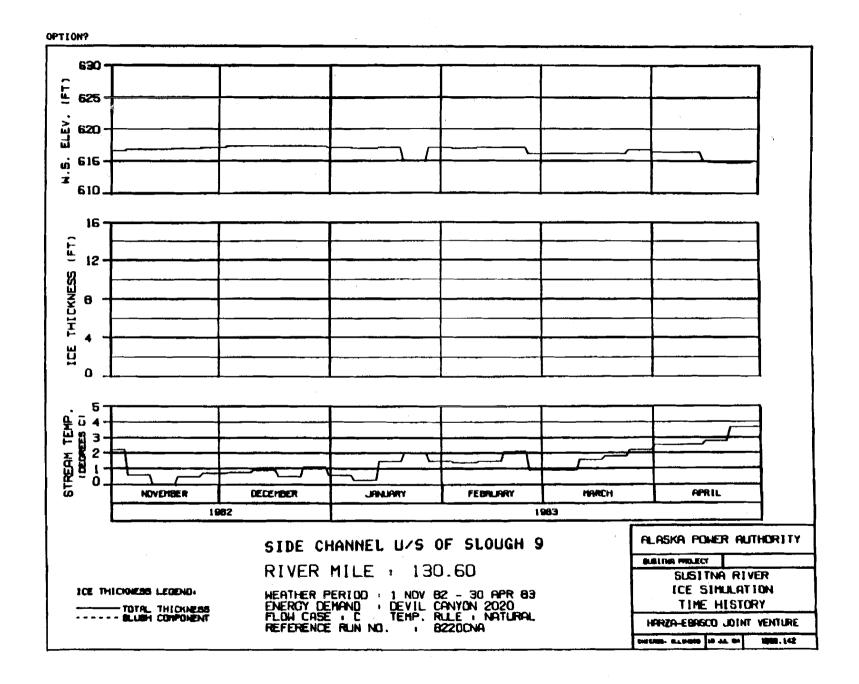


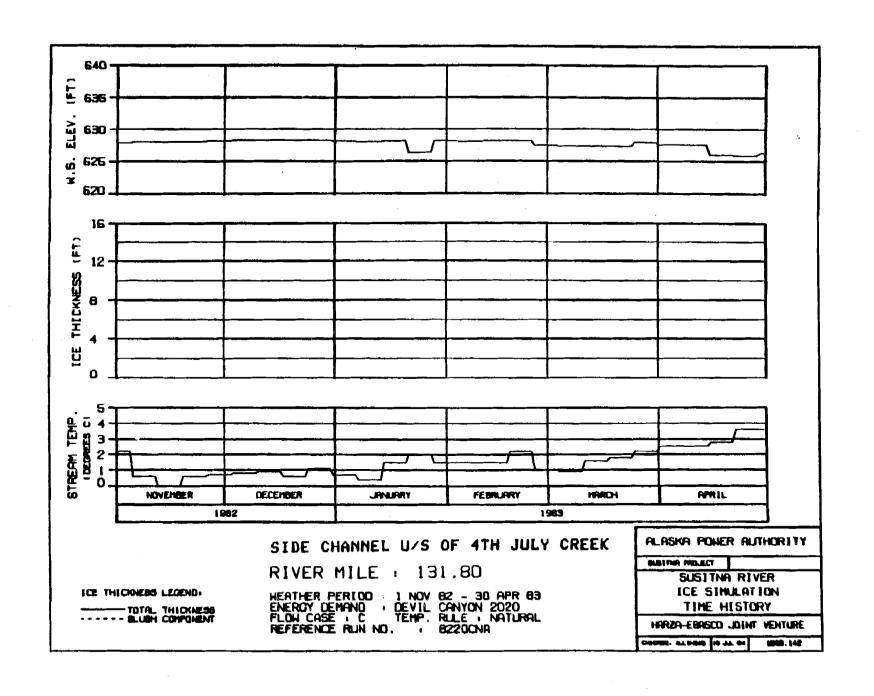


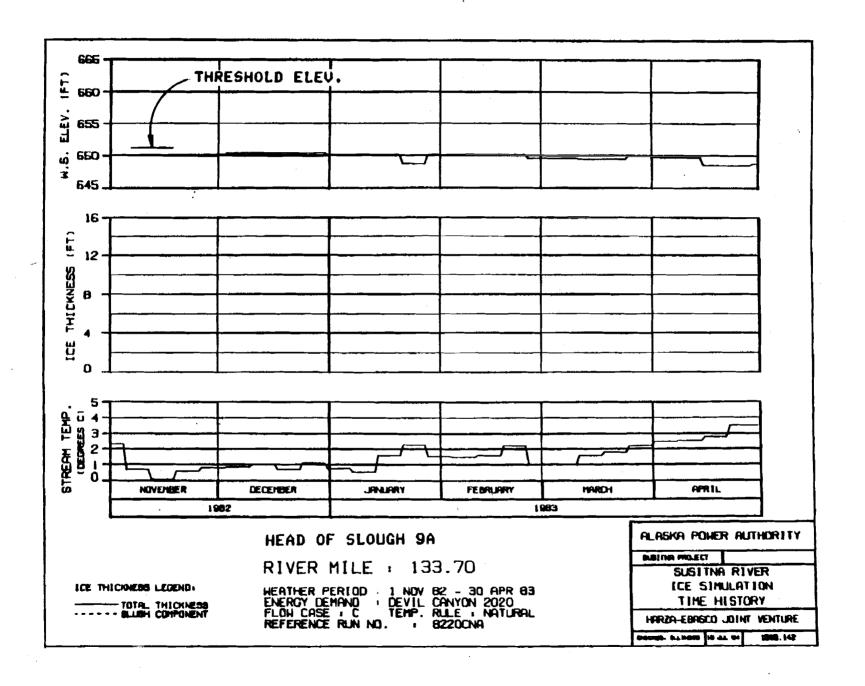


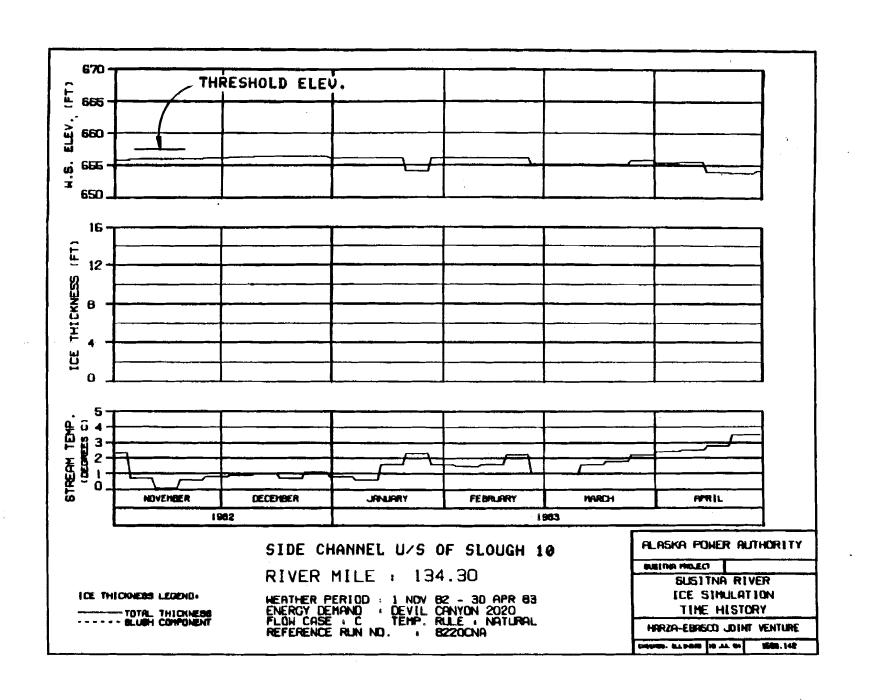


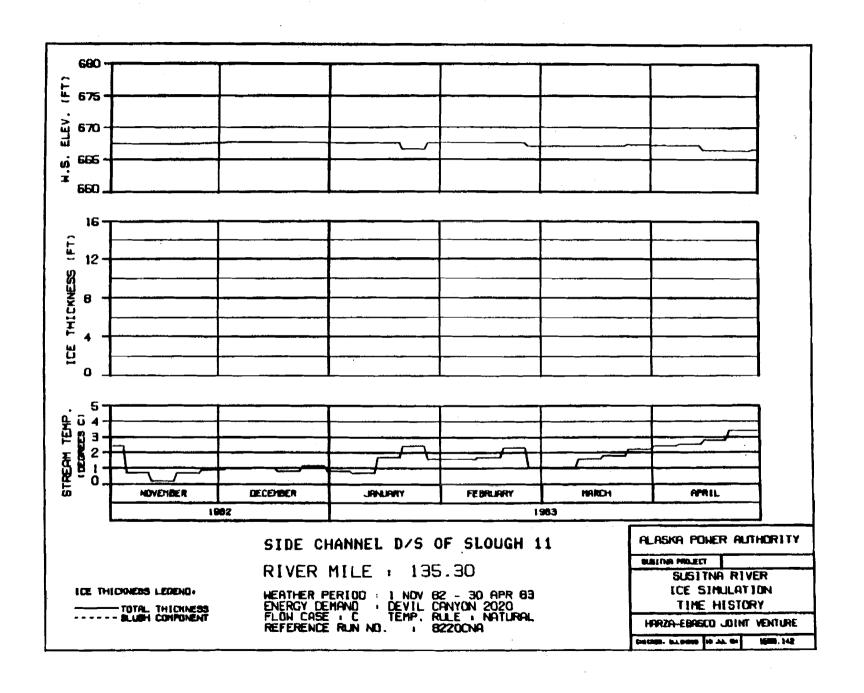


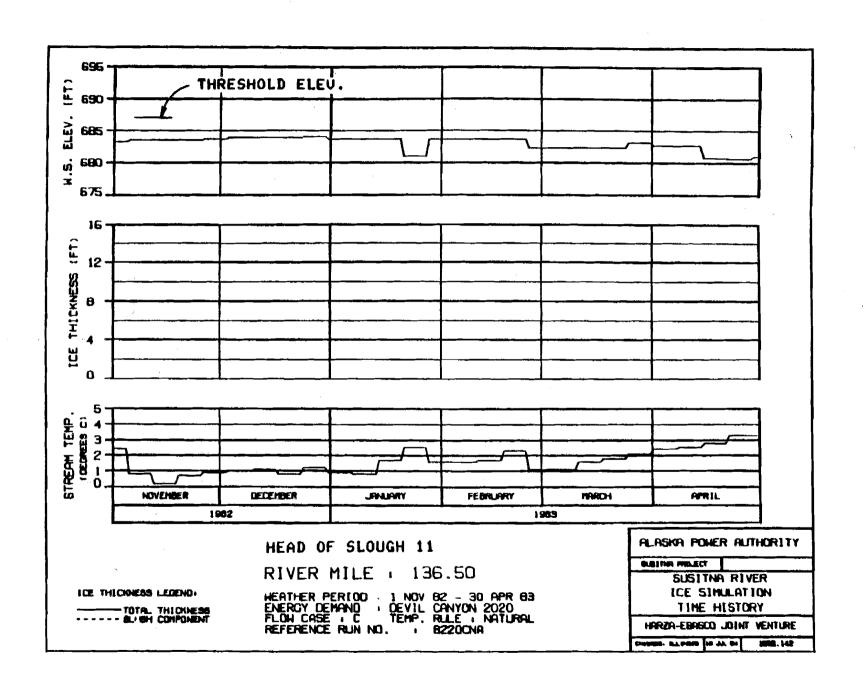


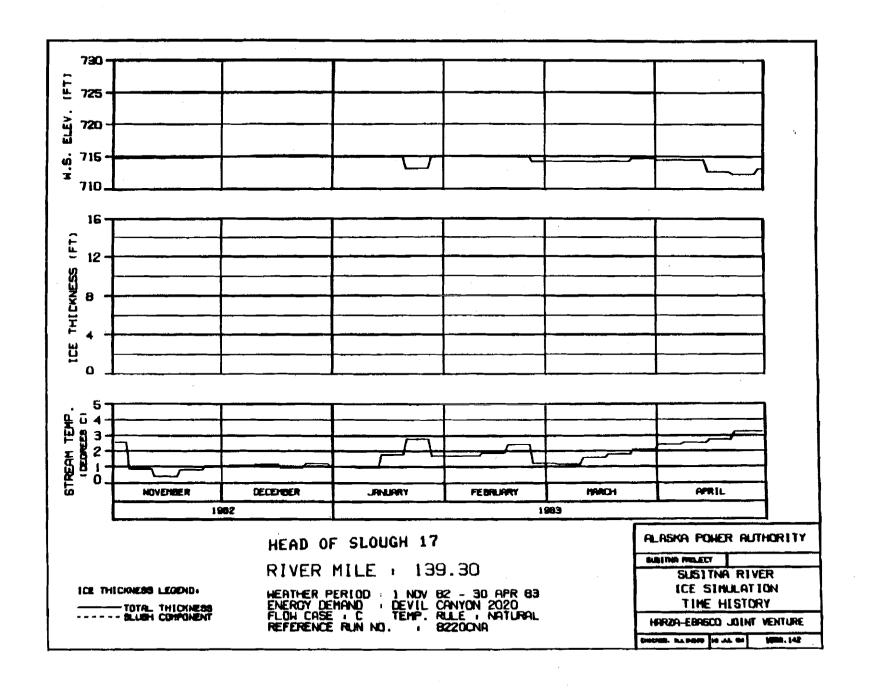


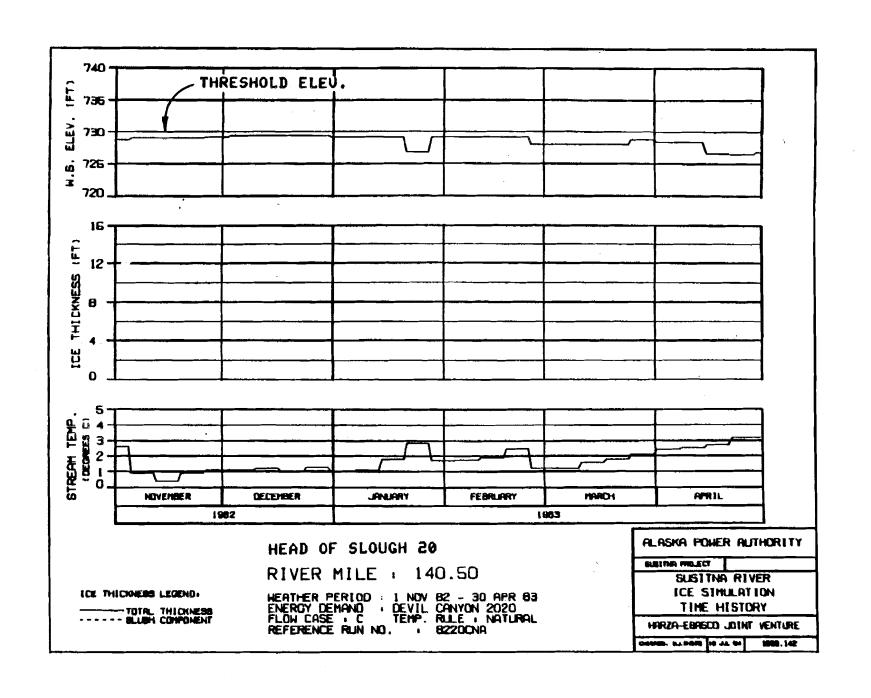


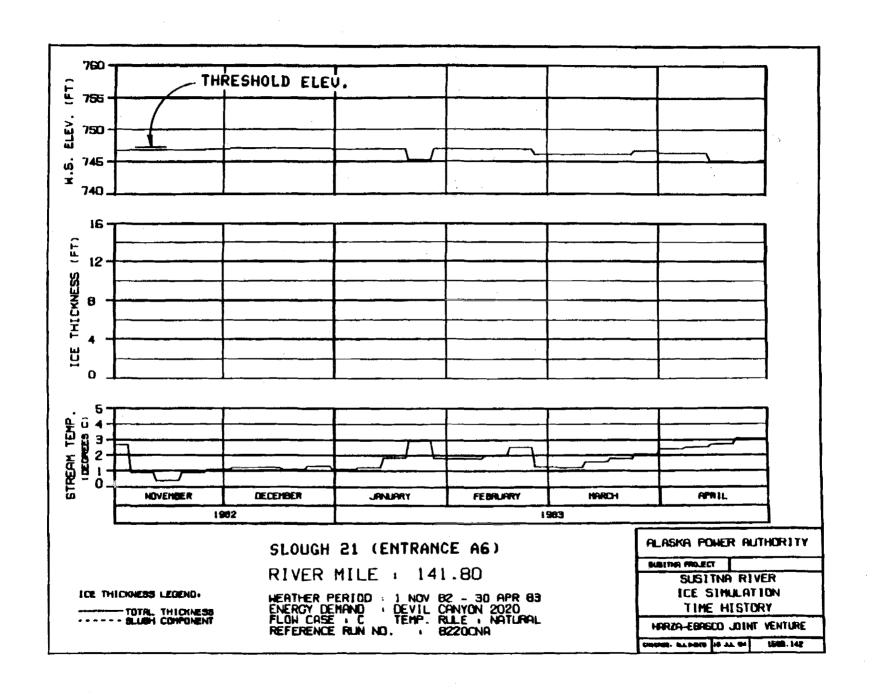


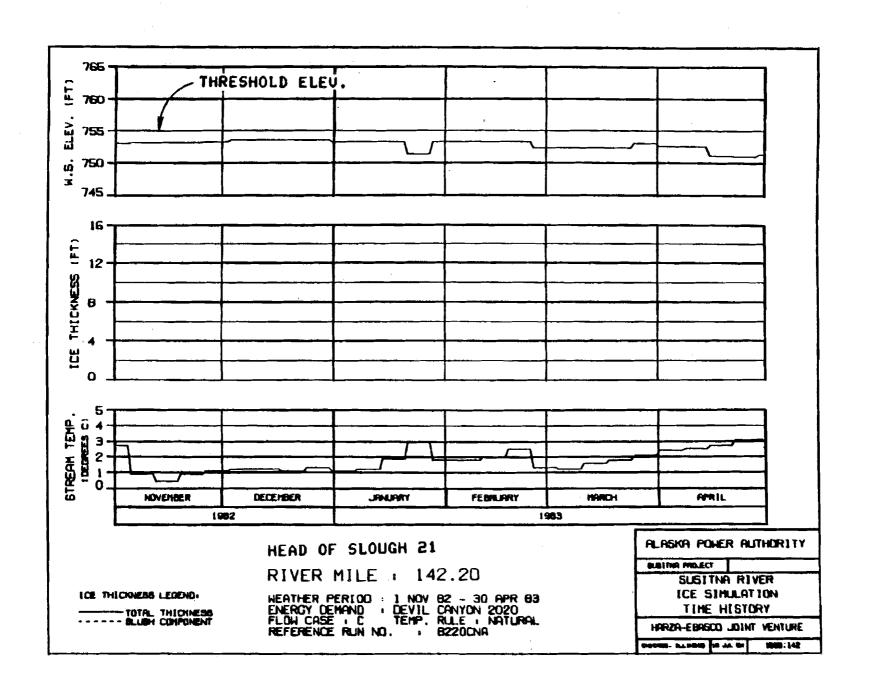












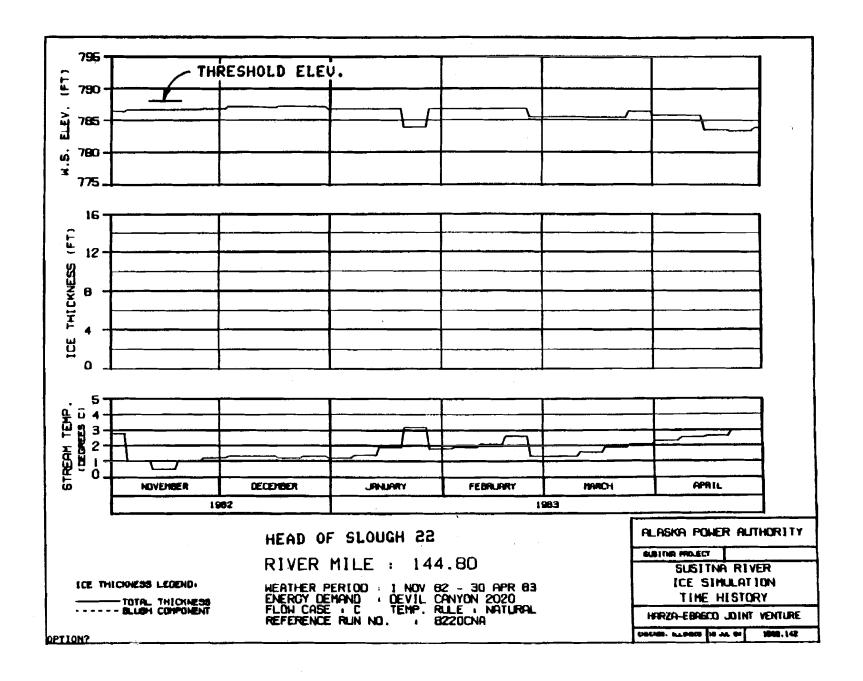
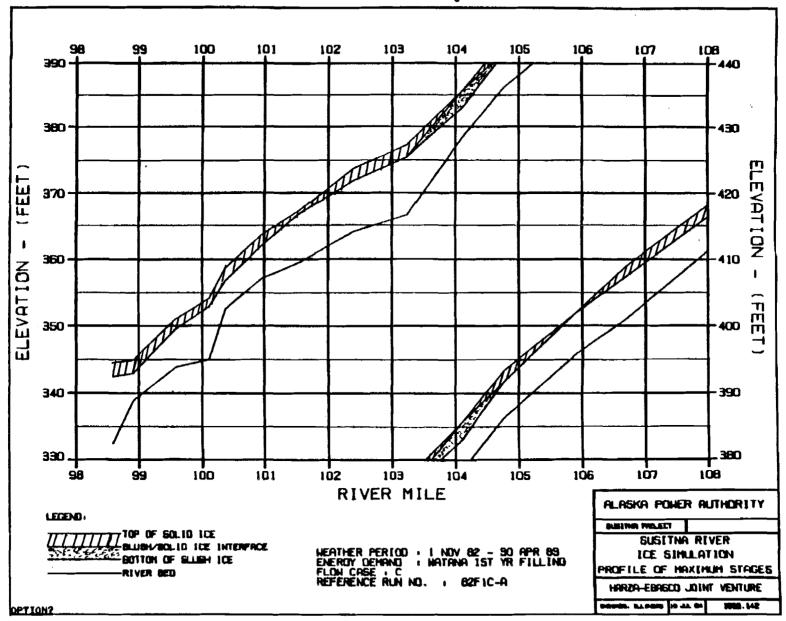
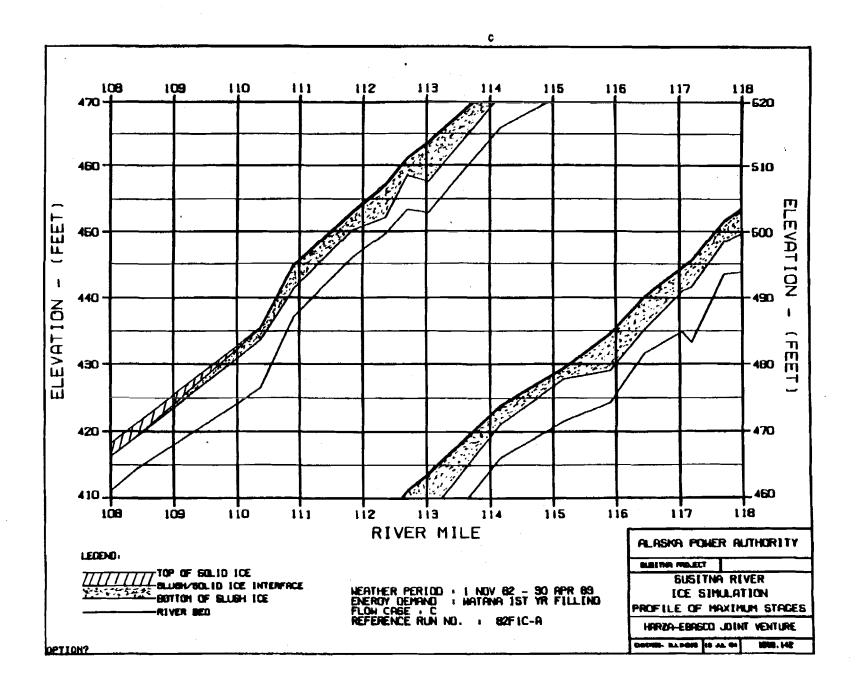


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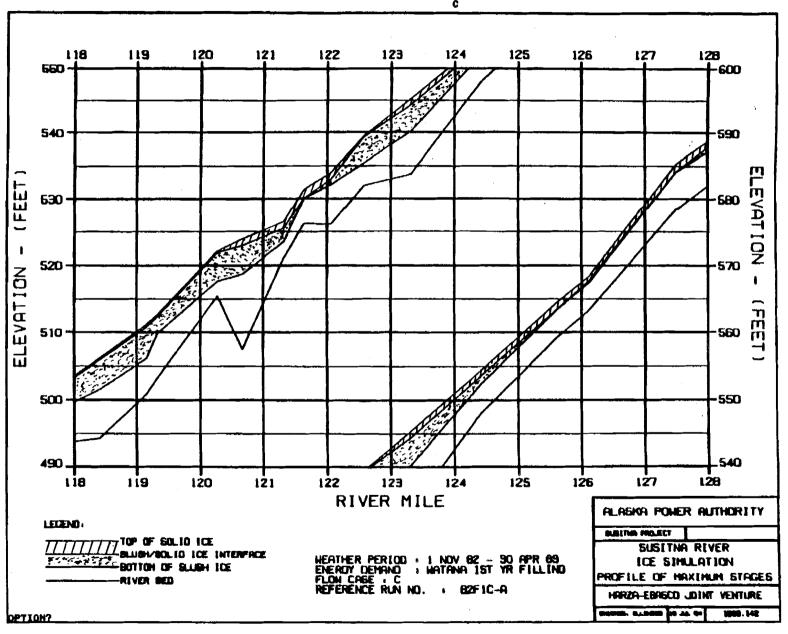
The following study, entitled "Watana-First Year Filling" corresponds to the winter of 1991-92, as depicted in Exhibit E.2.138 of the License Application. The weather used corresponds to the winter of 1982-83, which is a mild winter. Releases from Watana under these conditions would be made thru the low-level outlet.





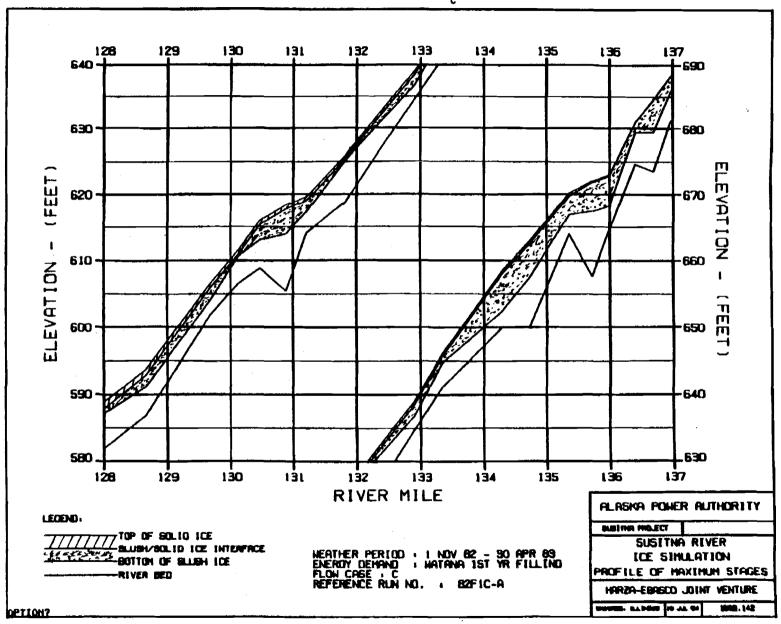




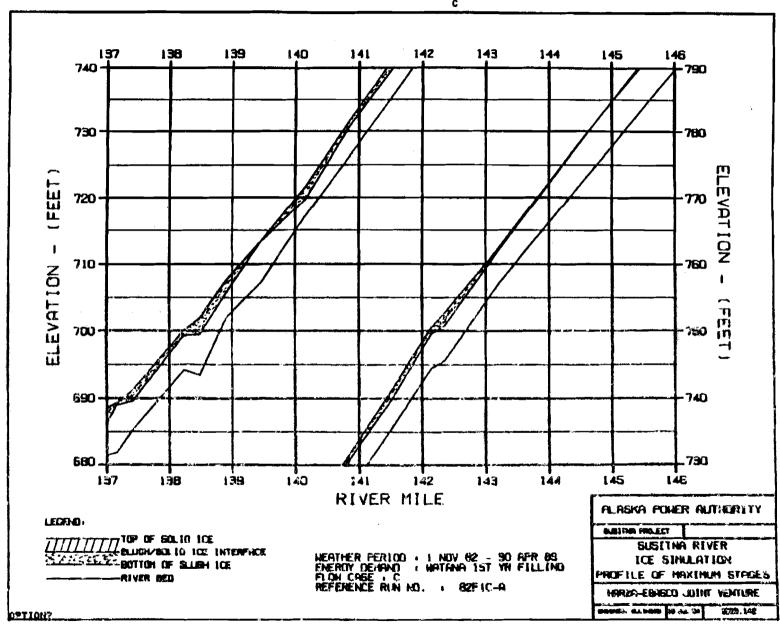


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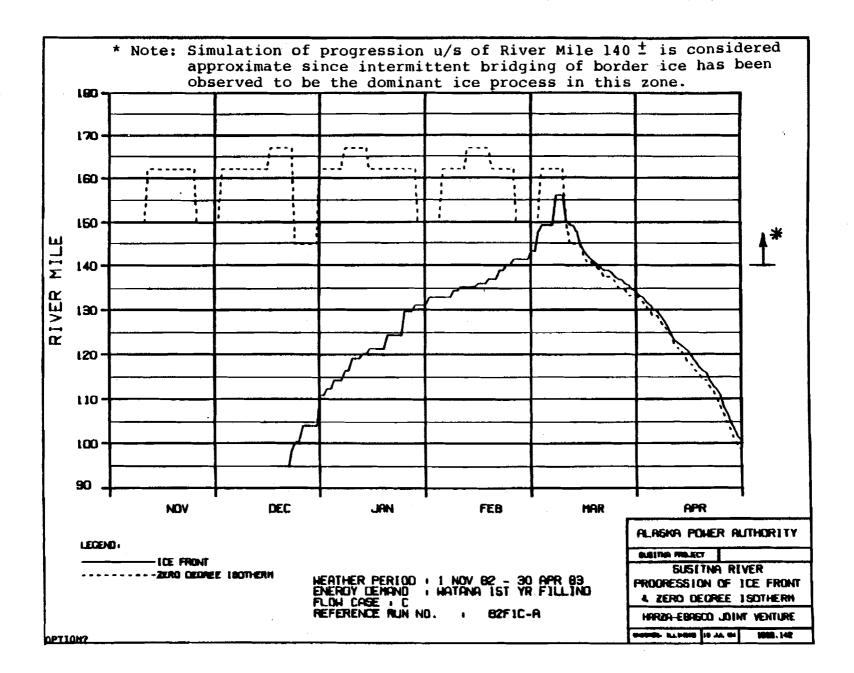


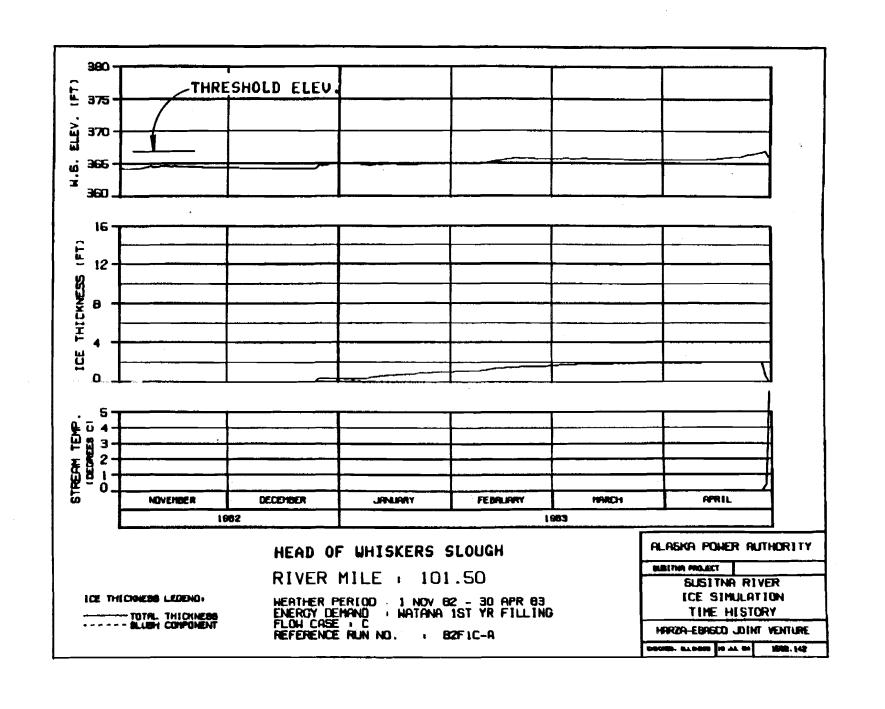


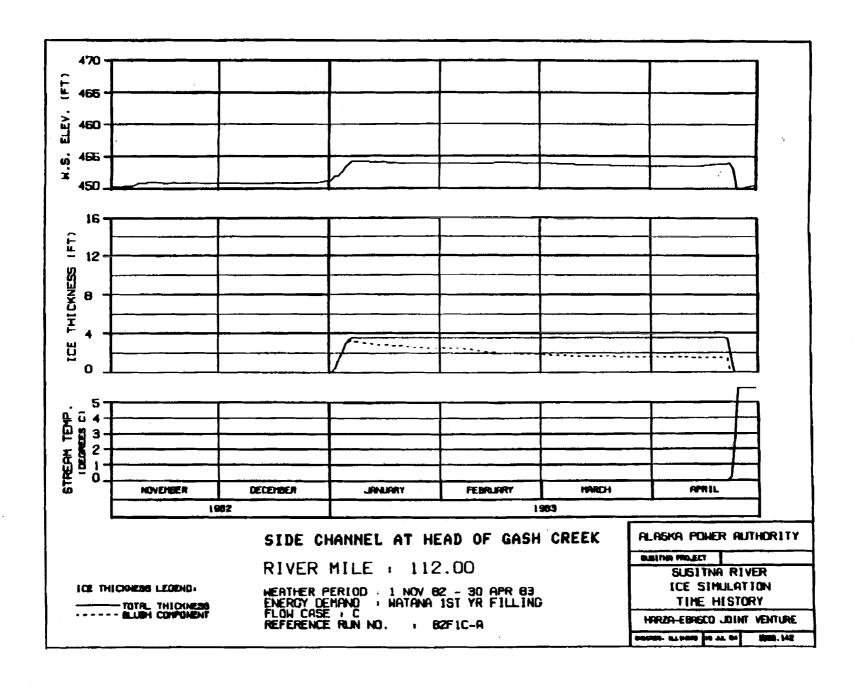


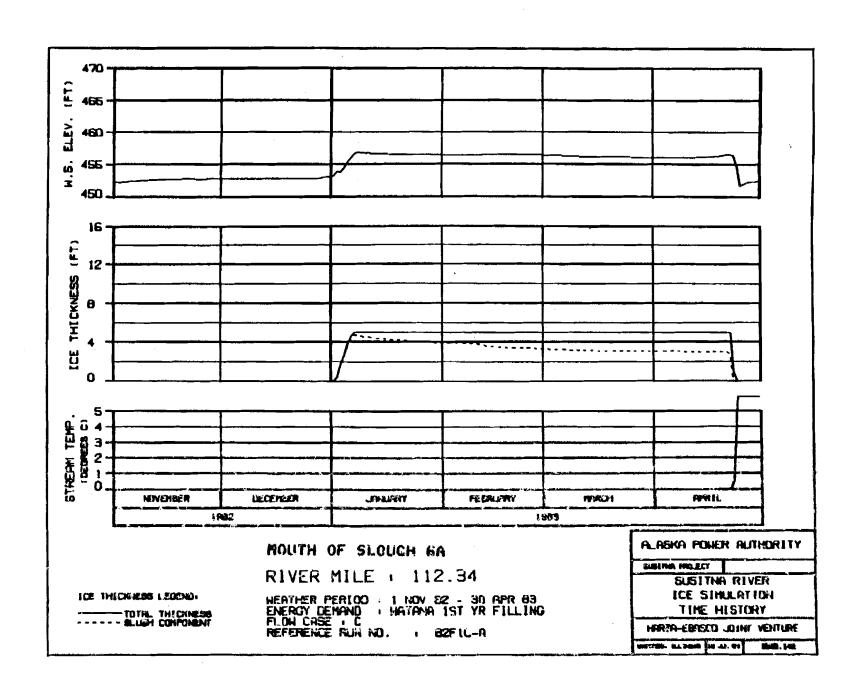


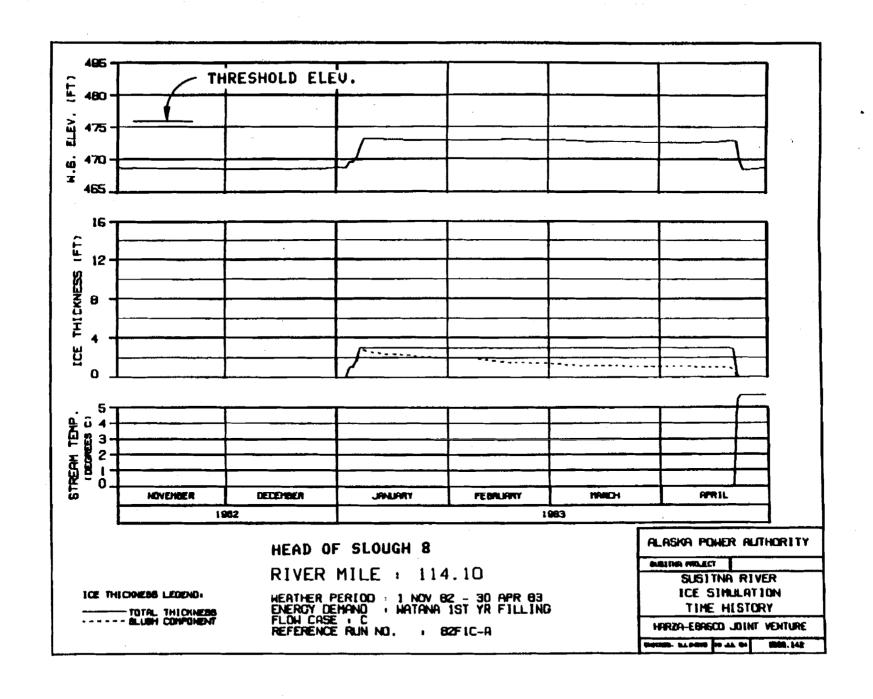
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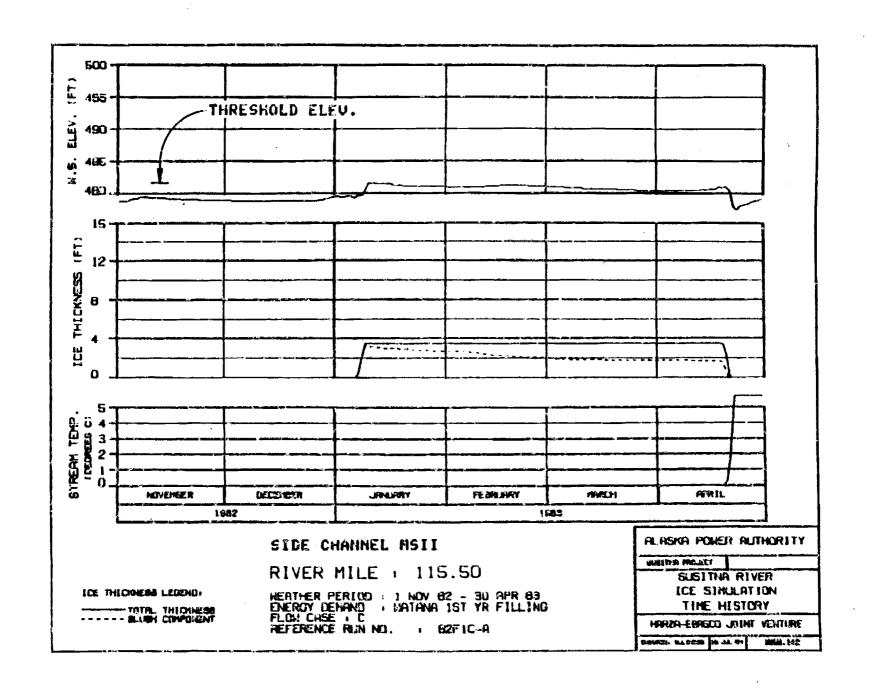




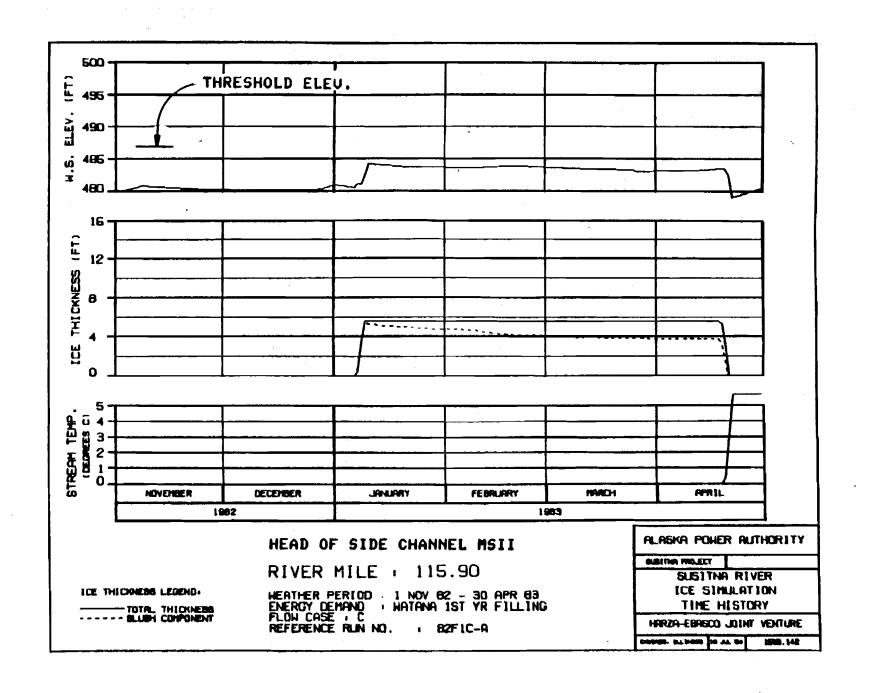




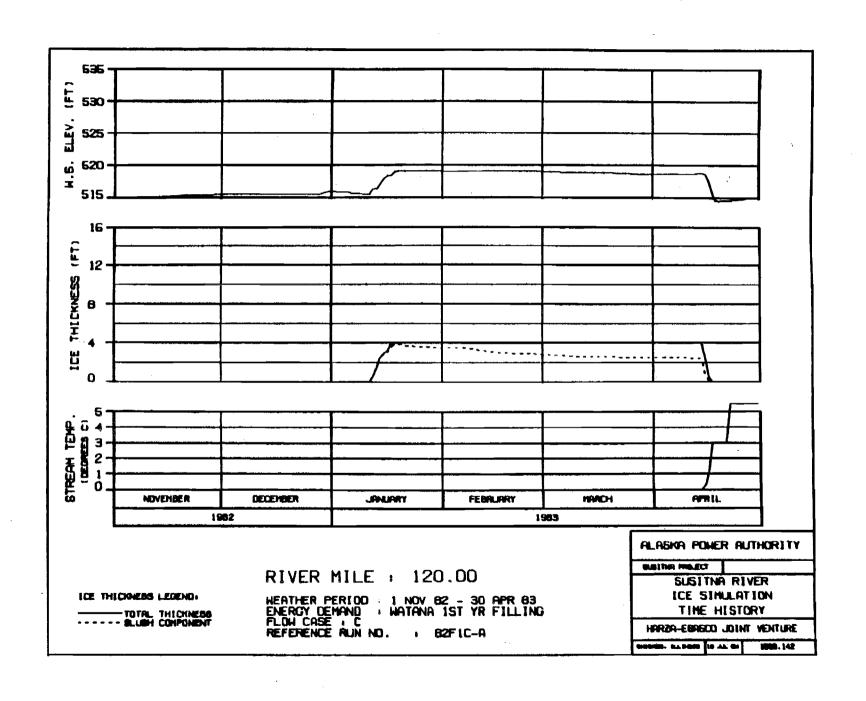
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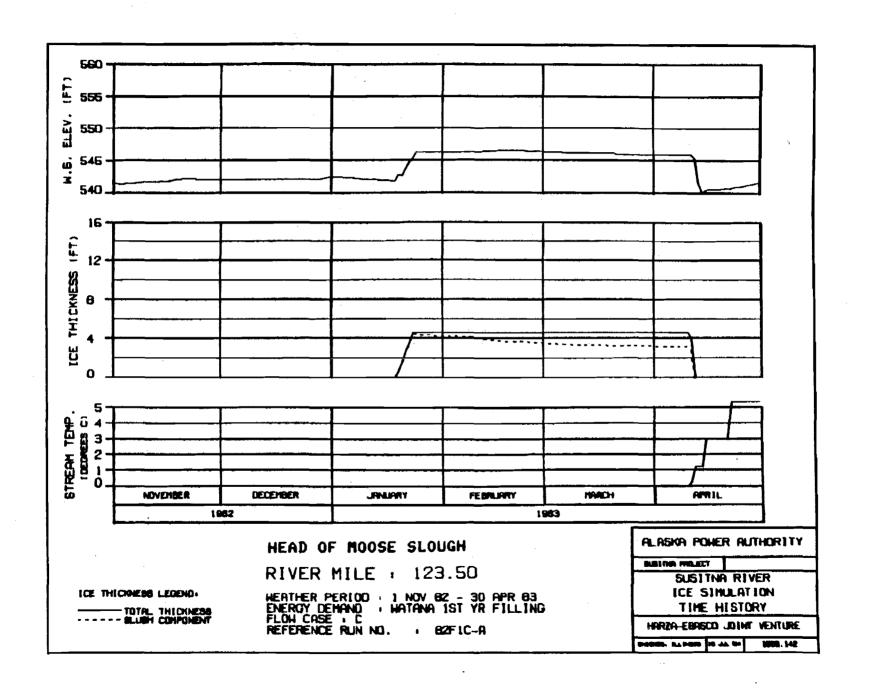
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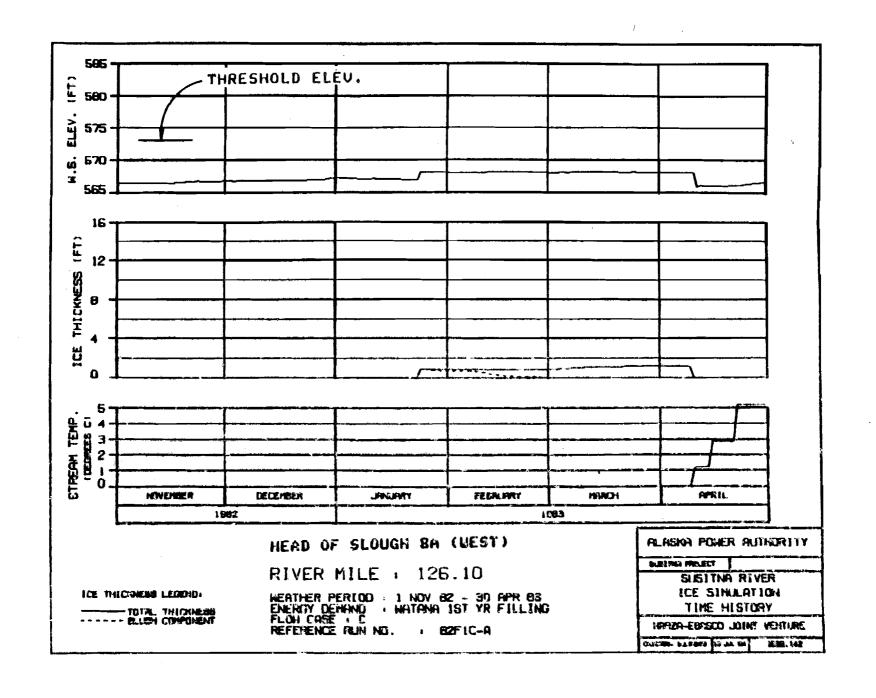


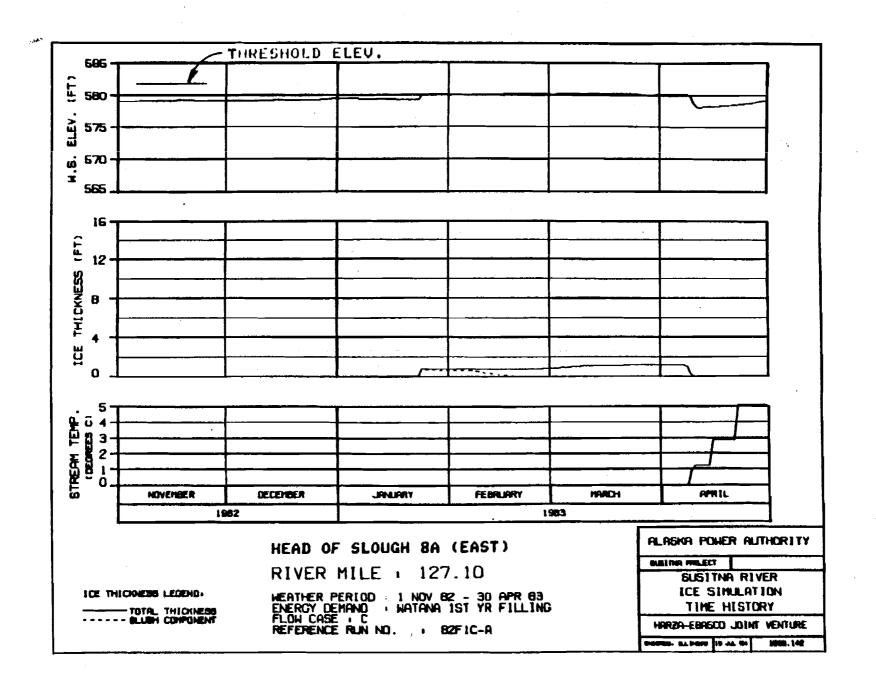
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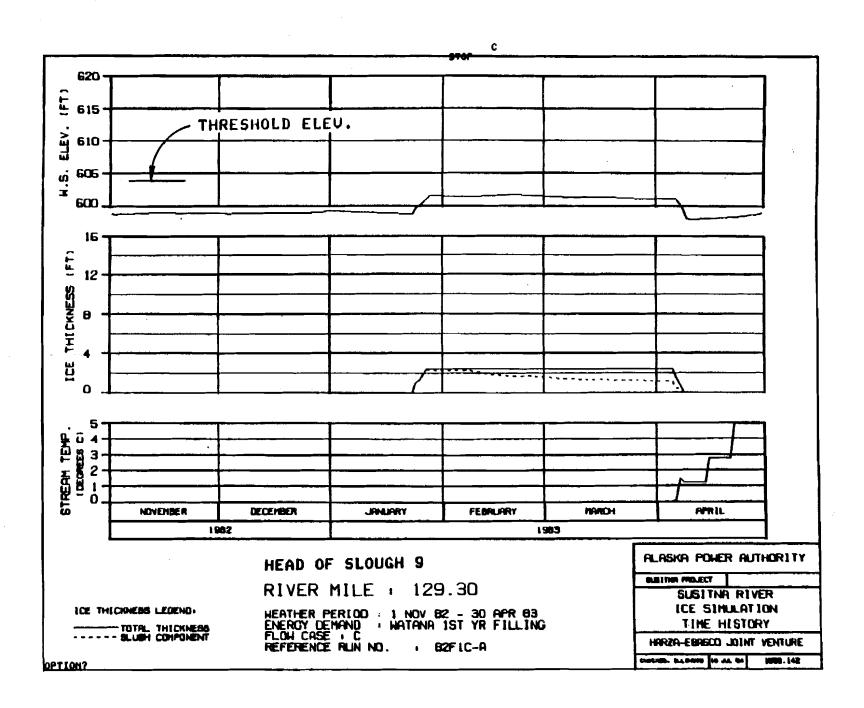


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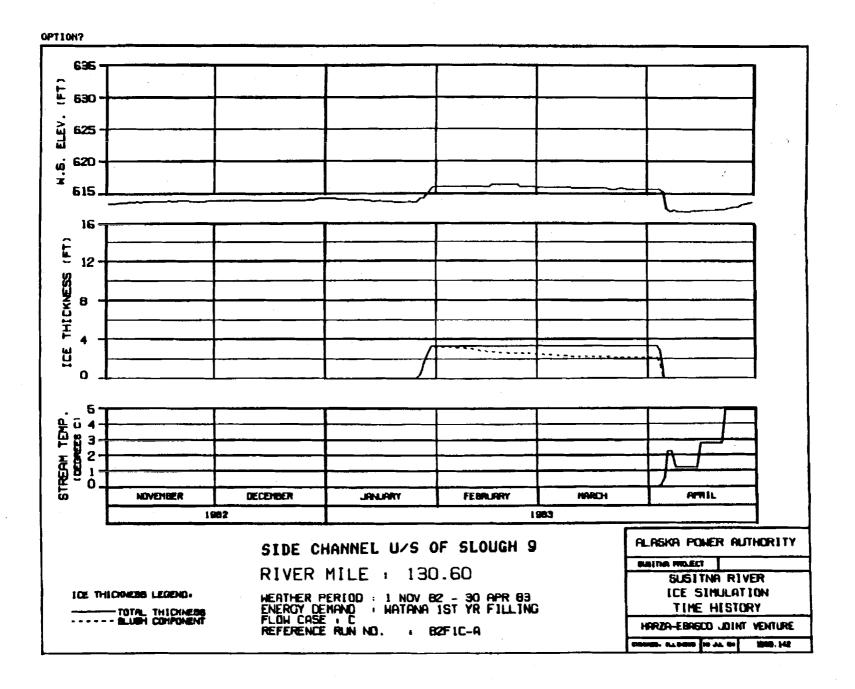




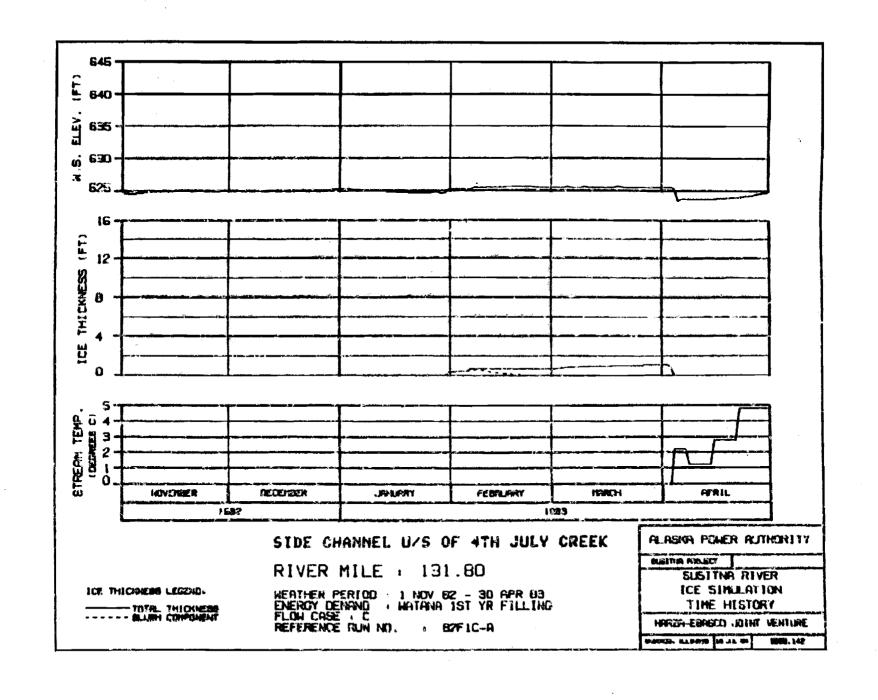




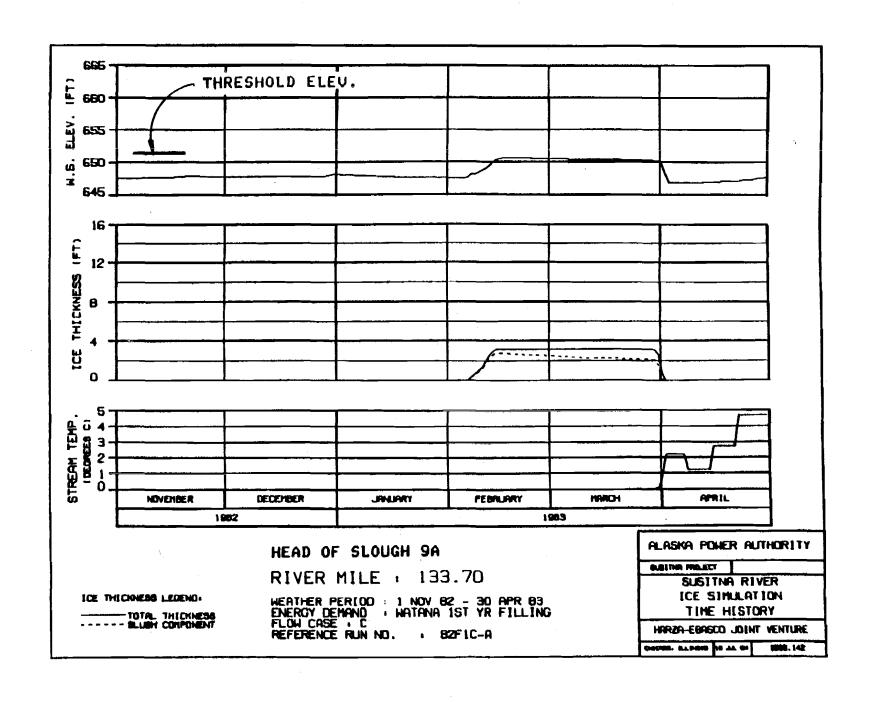
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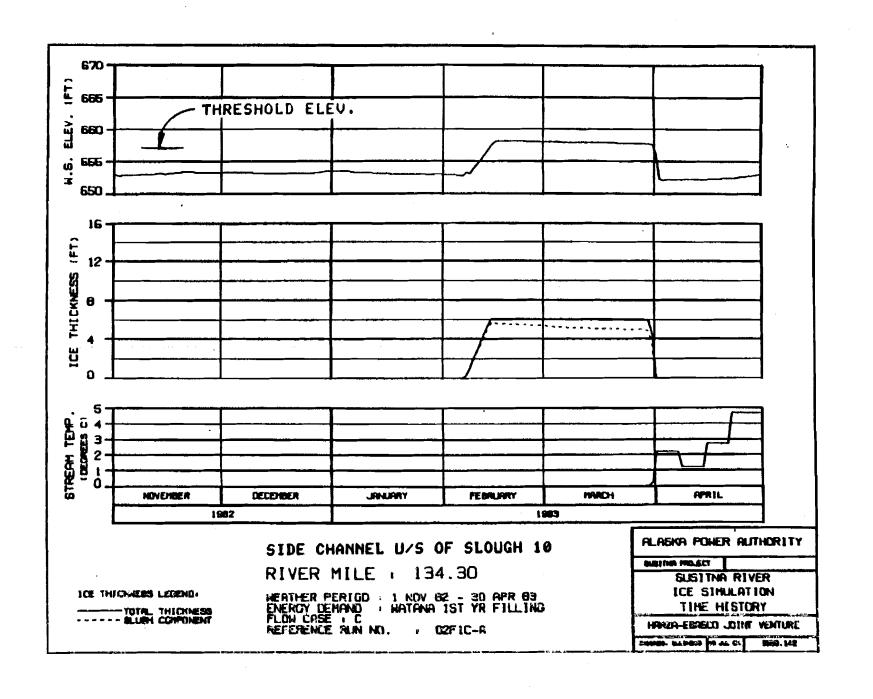
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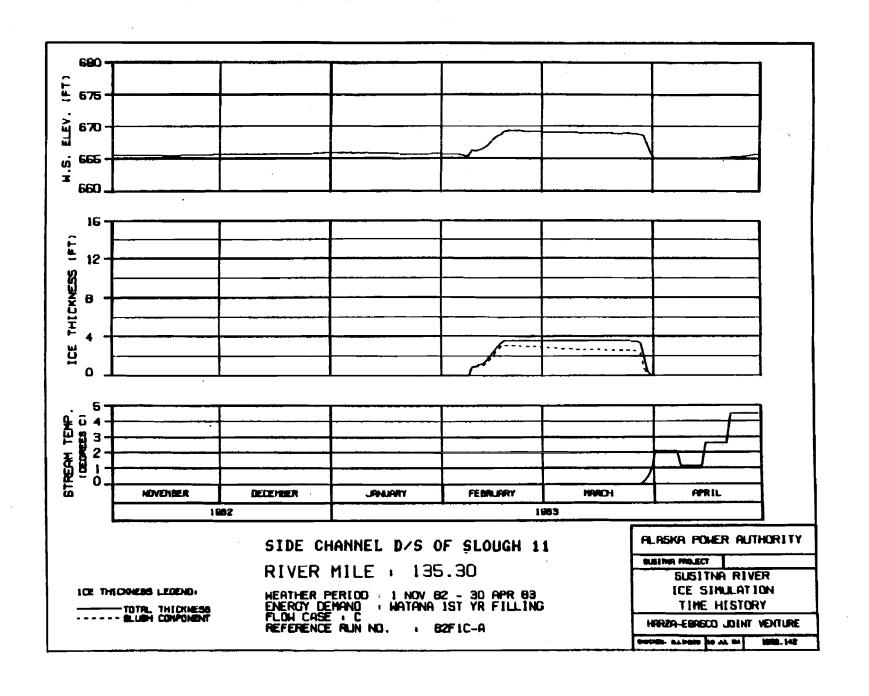


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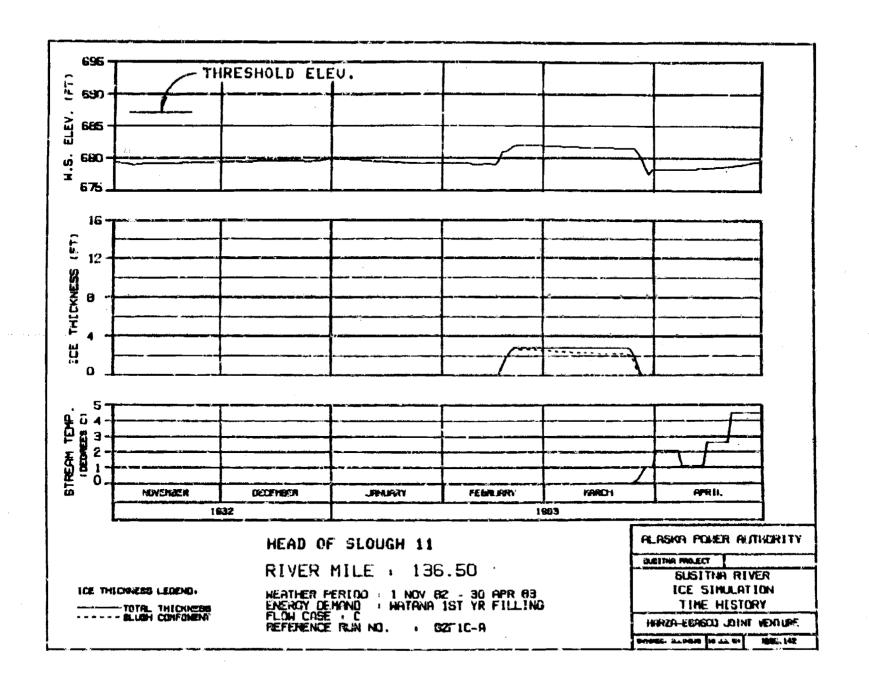


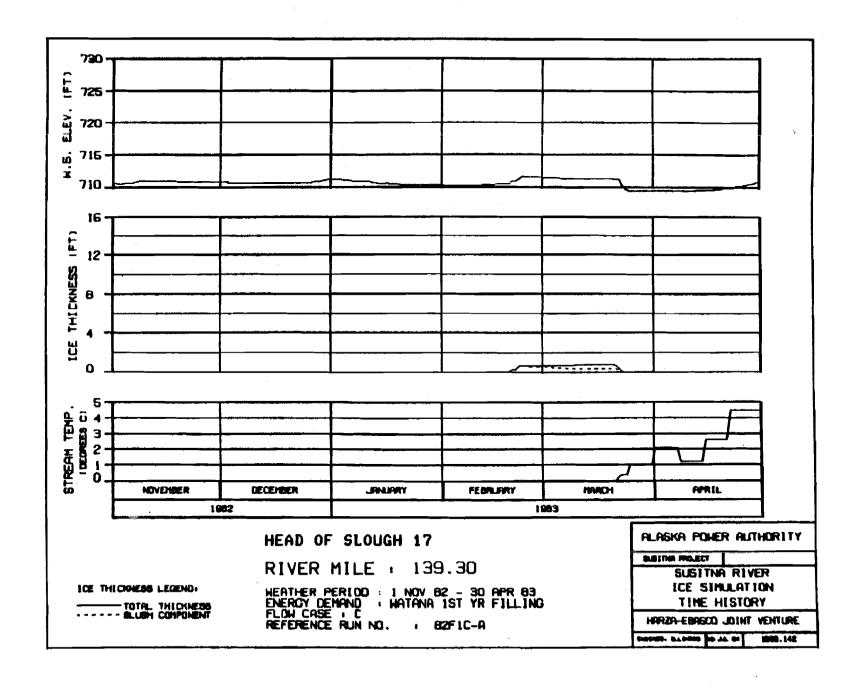
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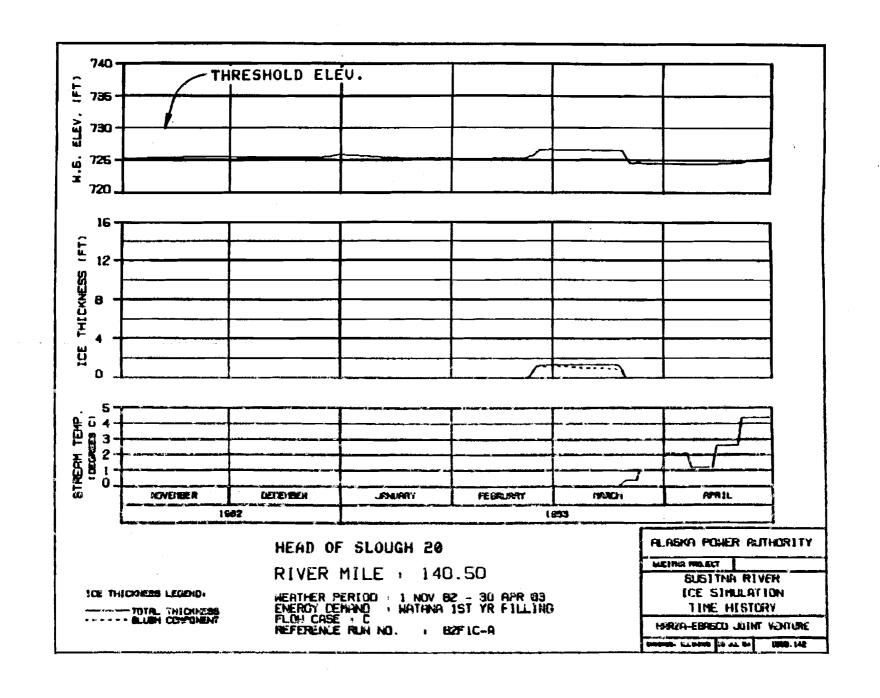




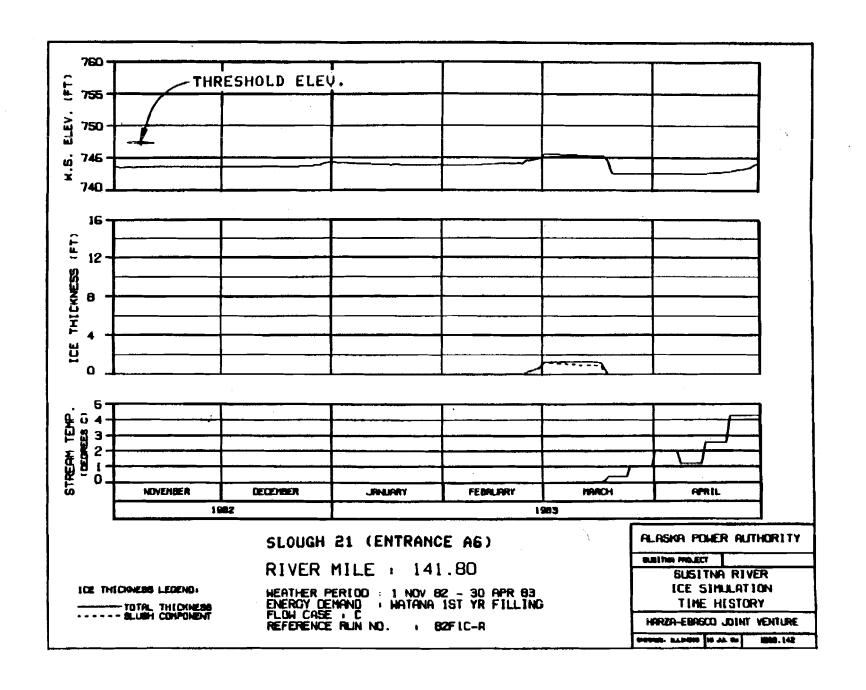
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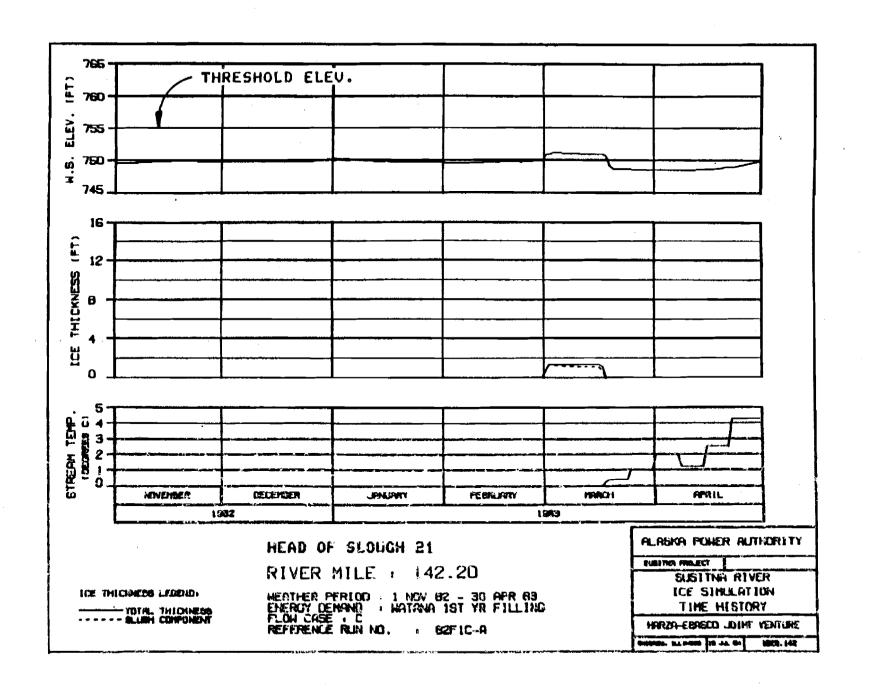




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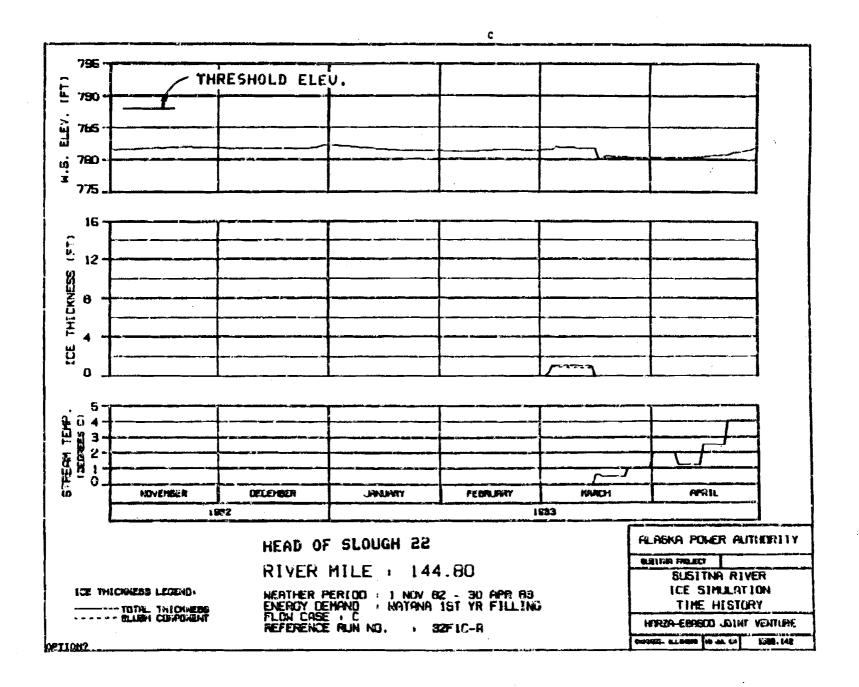
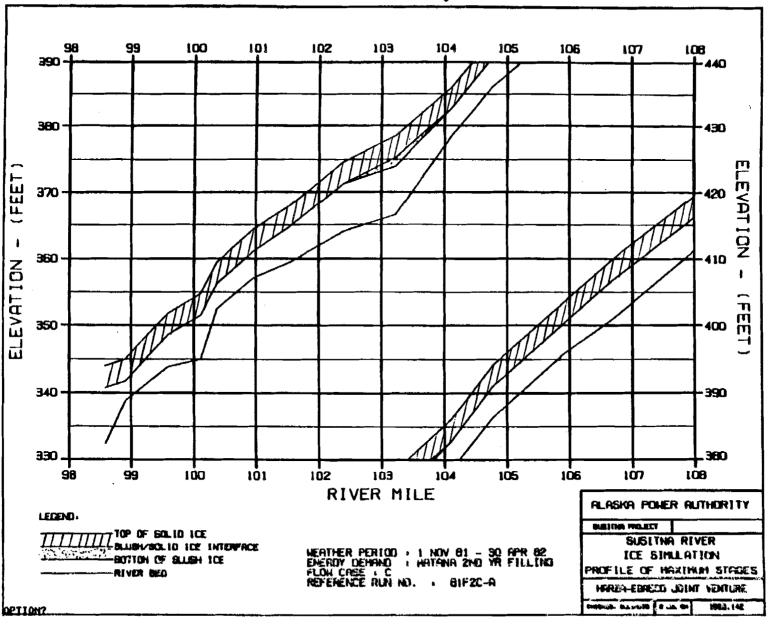


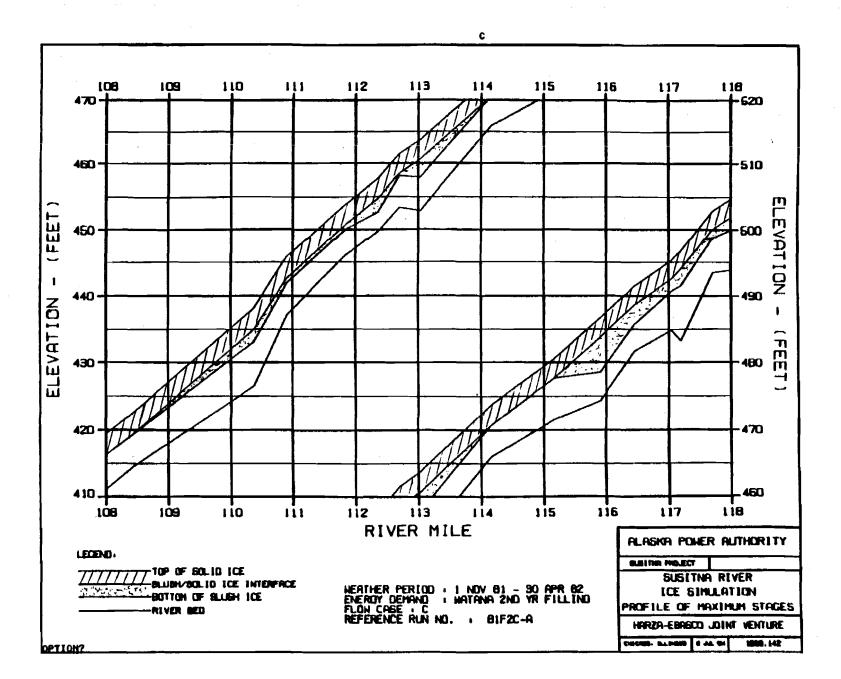
EXHIBIT T

The following study, entitled "Watana-Second Year Filling" corresponds to the winter of 1992-93, as depicted in Exhibit E.2.138 of the License Application. The weather used corresponds to the winter of 1981-82, which is a cold winter. Releases from Watana under these conditions would be made thru the mid-level outlet.

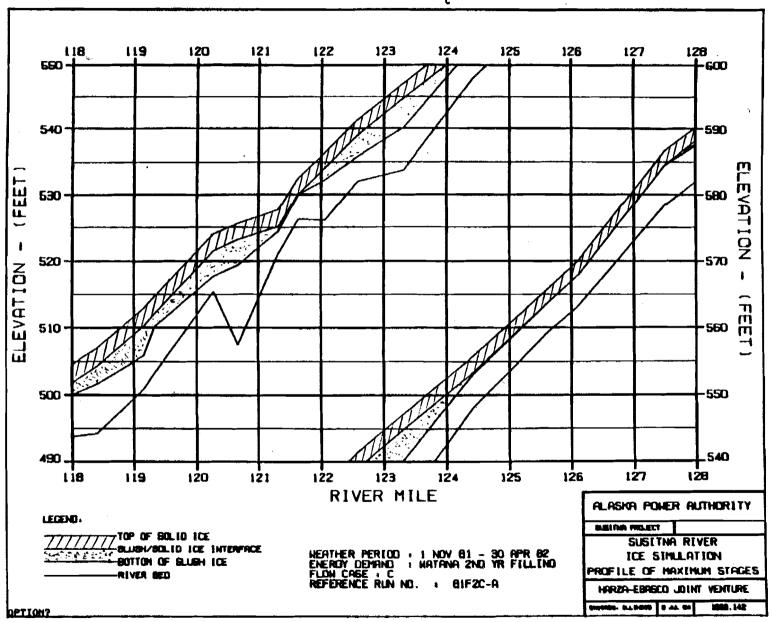




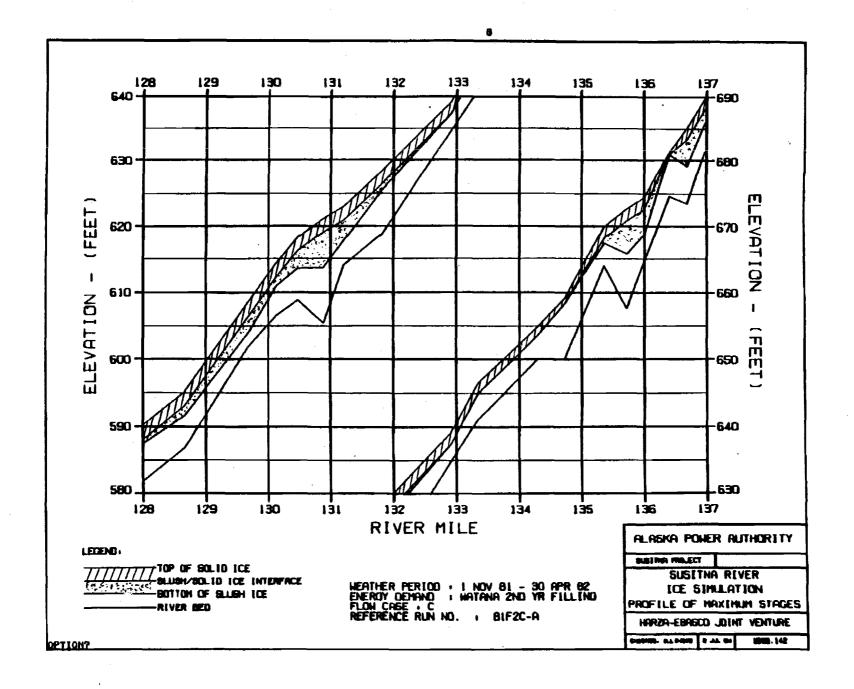
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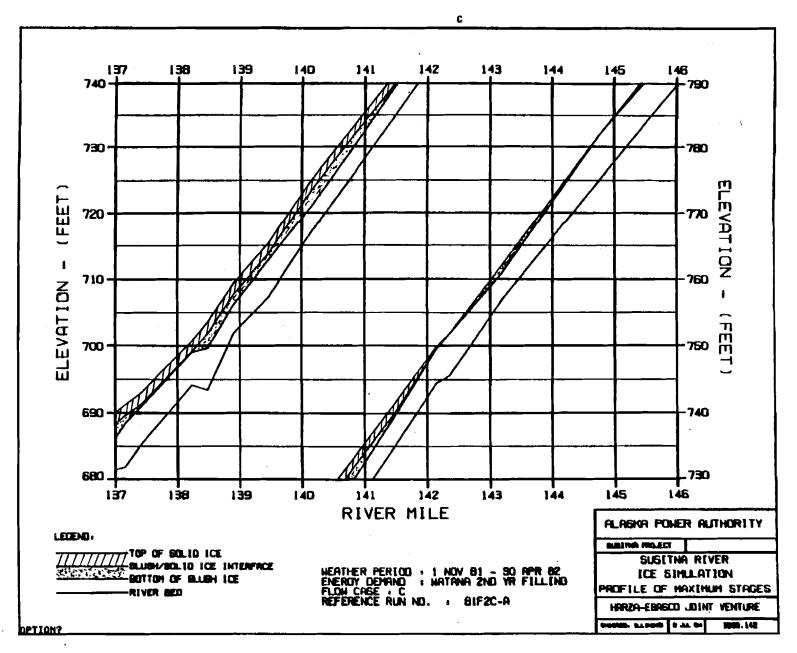


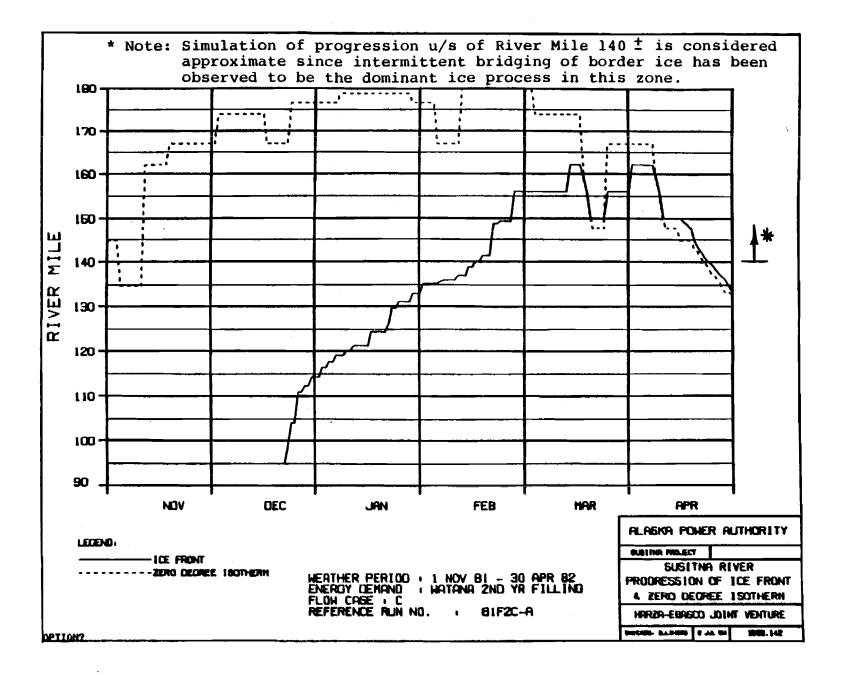


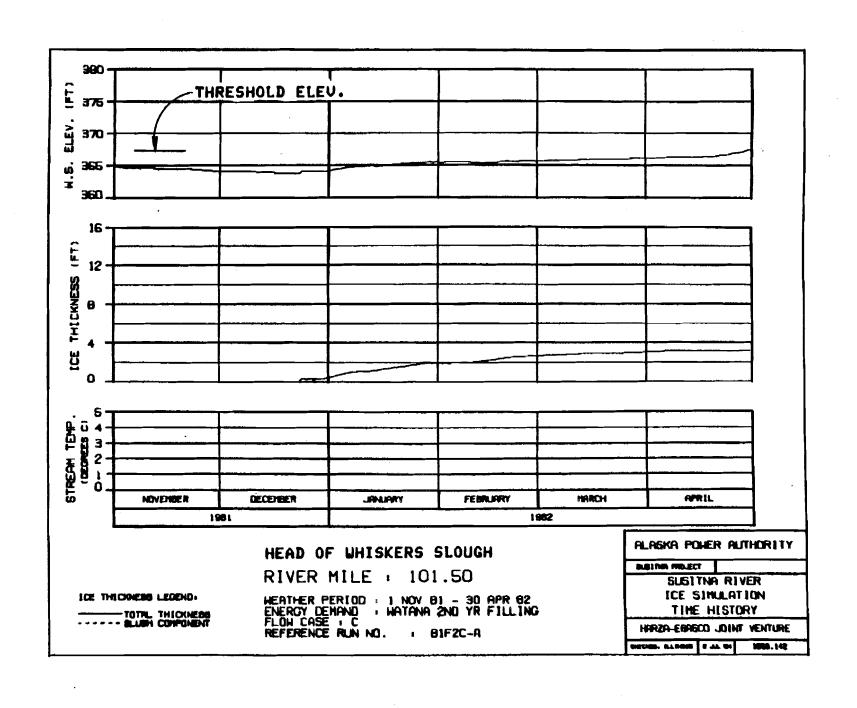


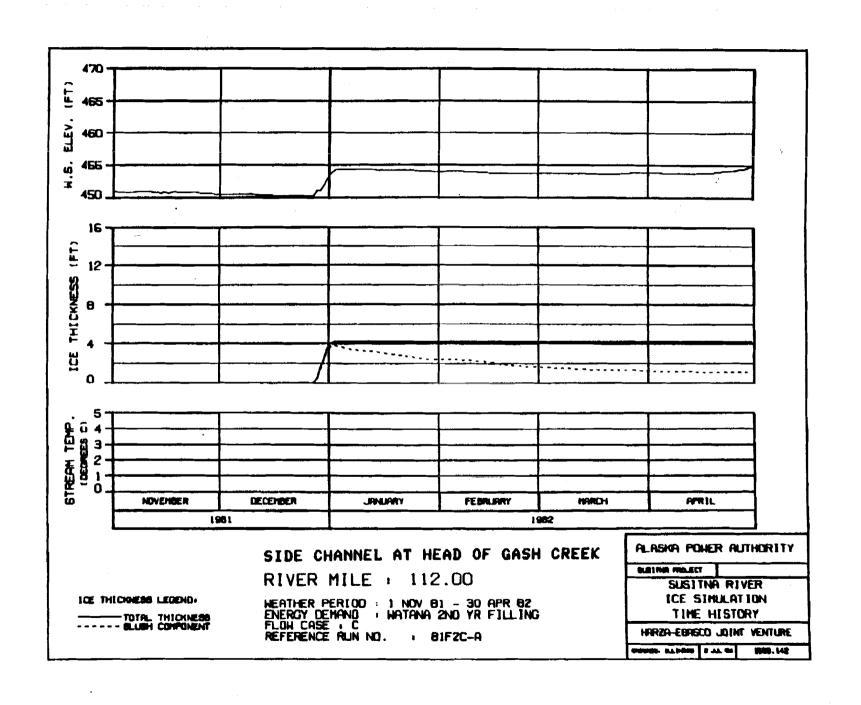
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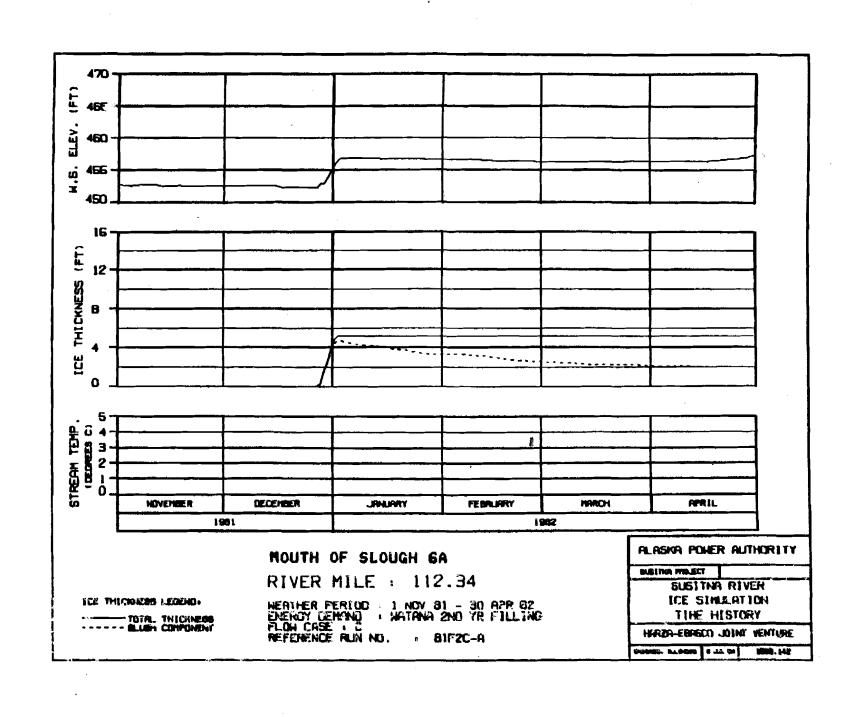


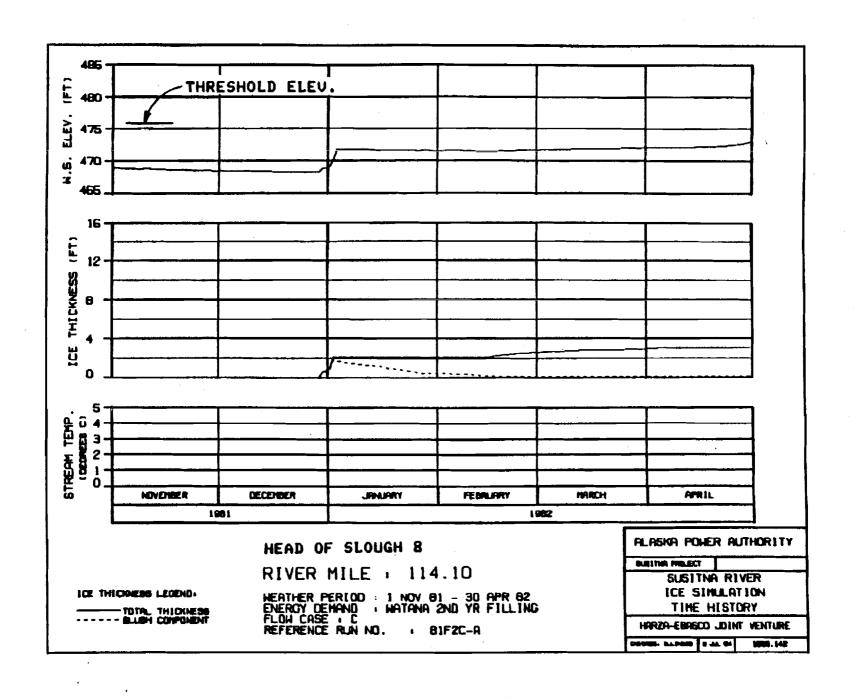


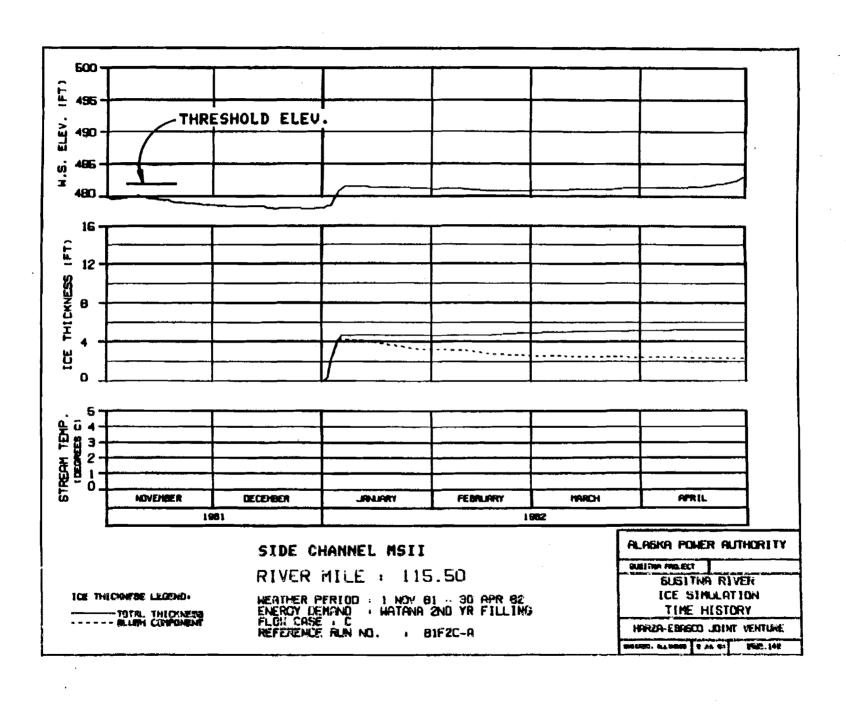


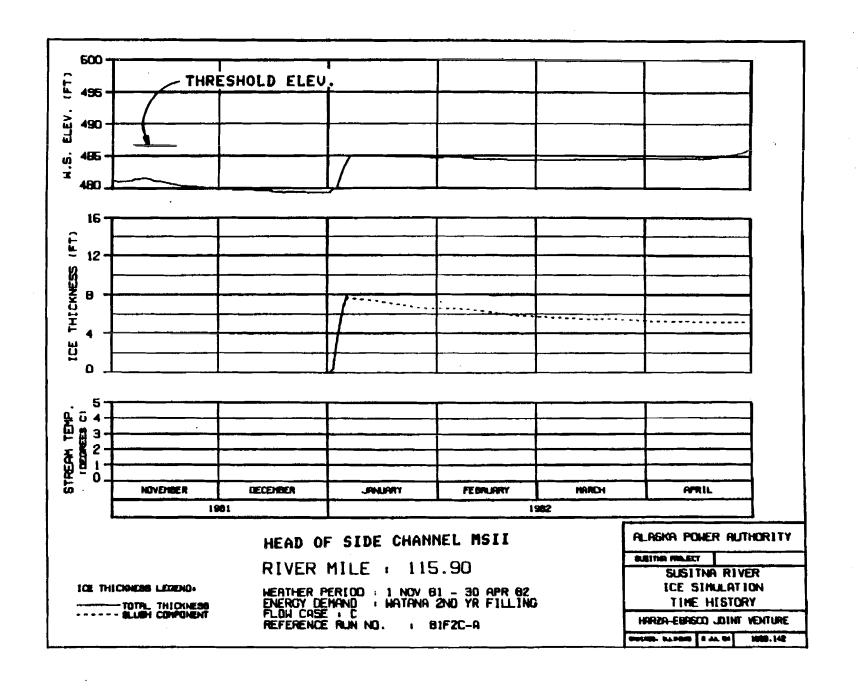


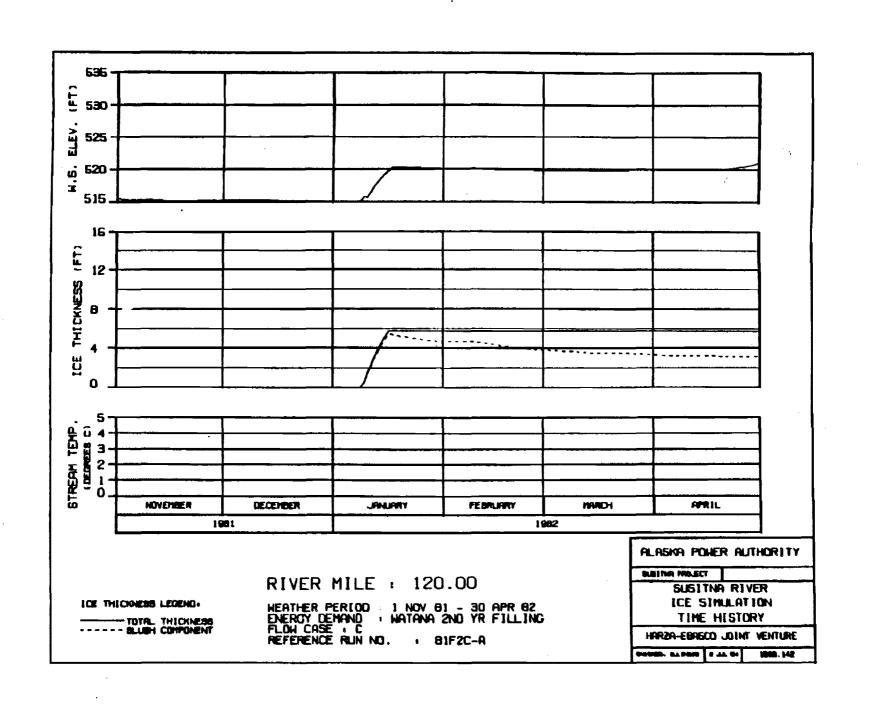


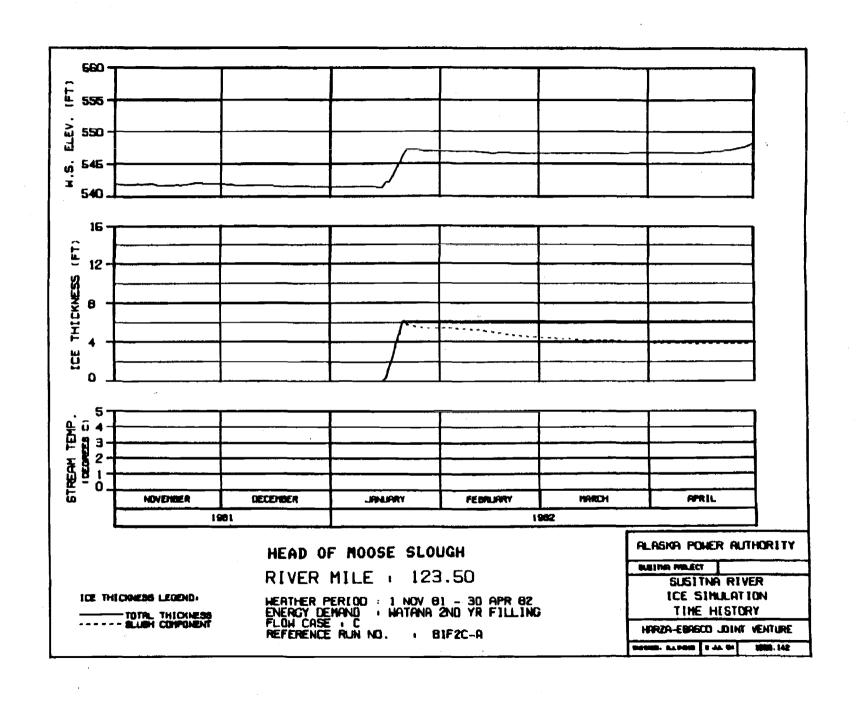


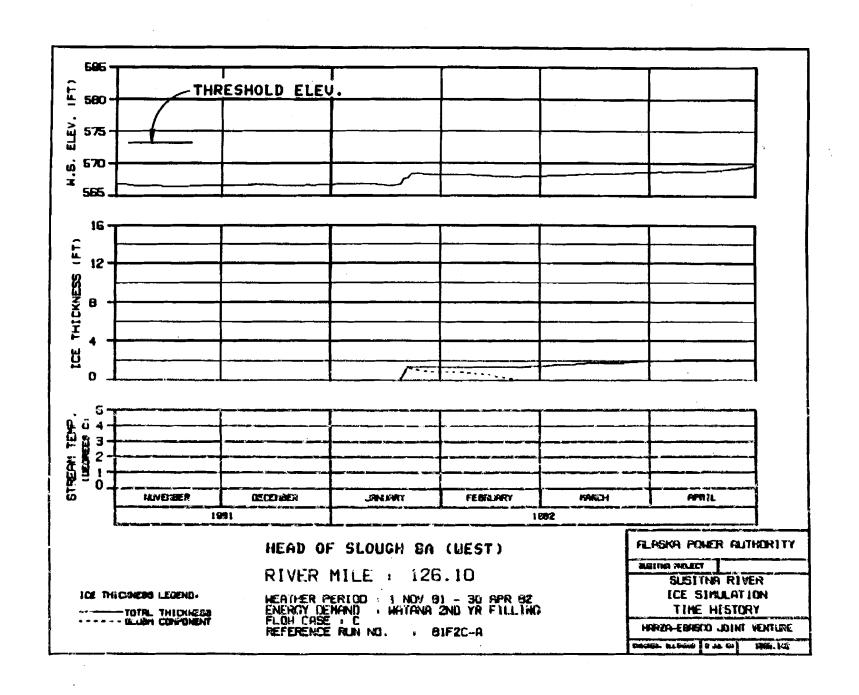




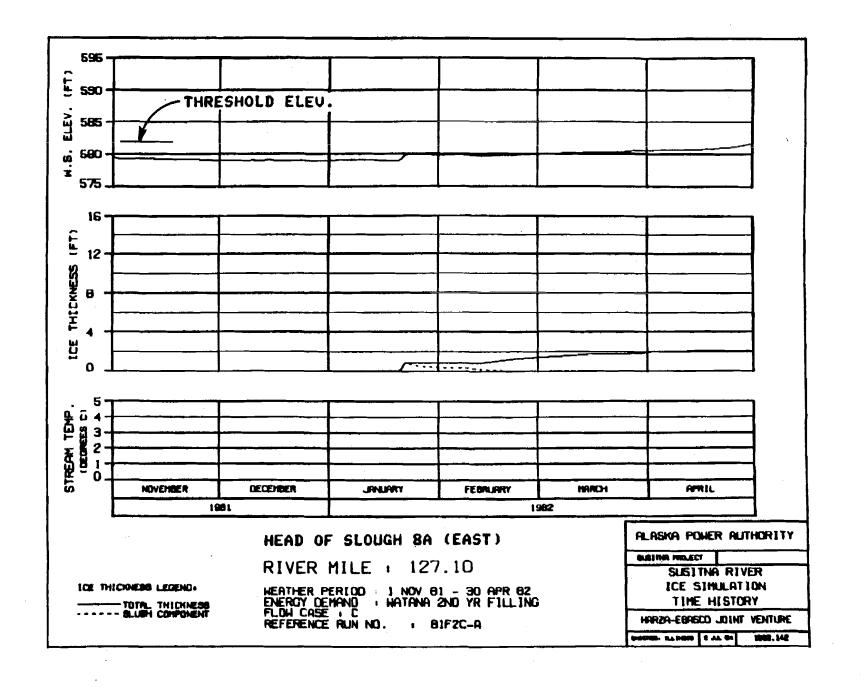


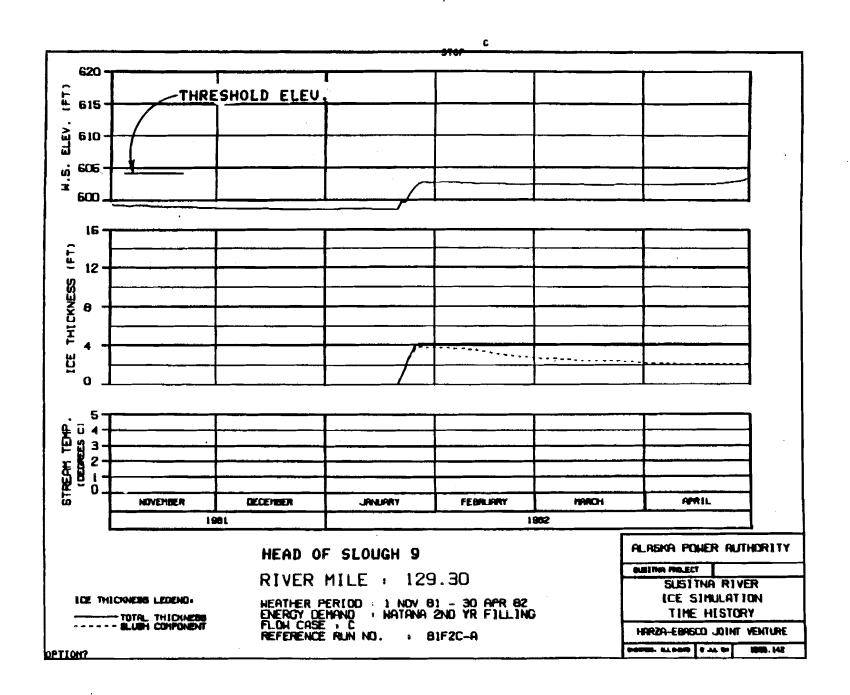




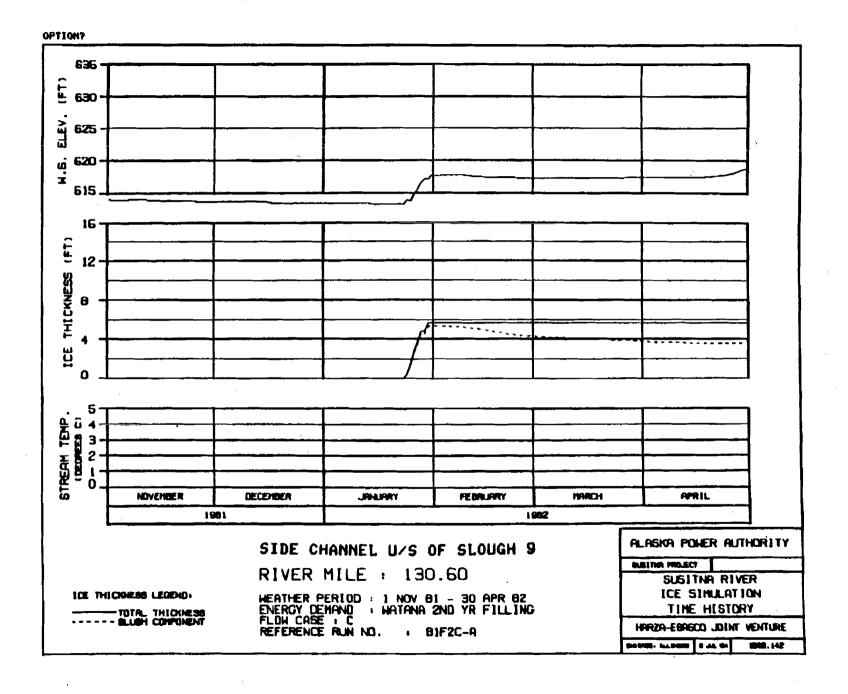


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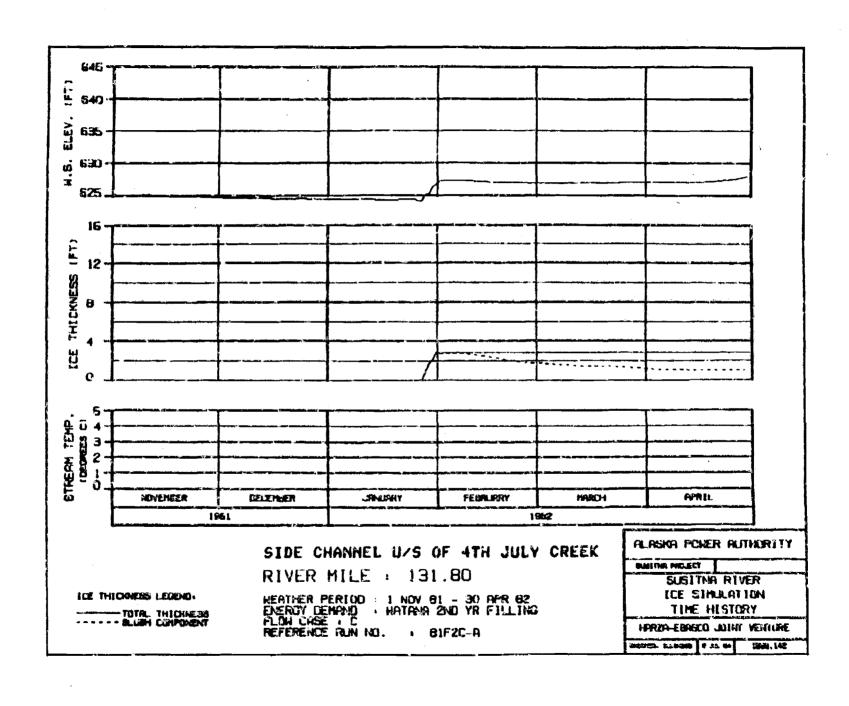




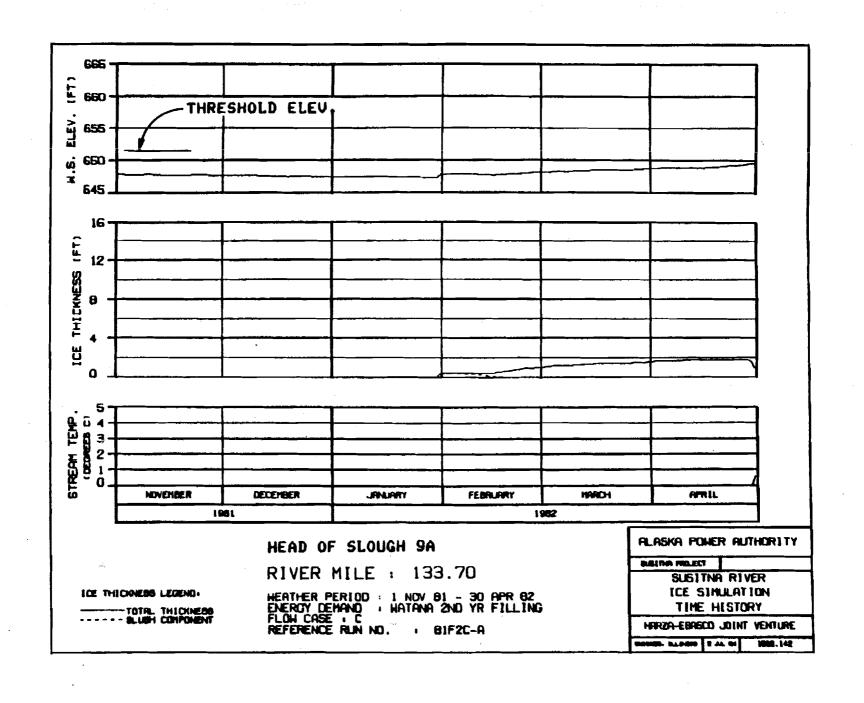
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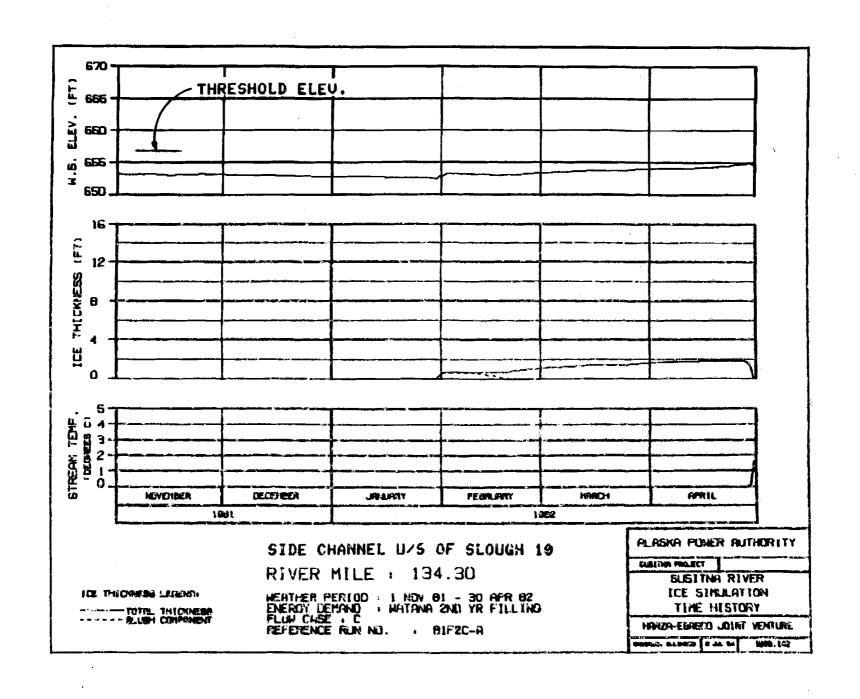
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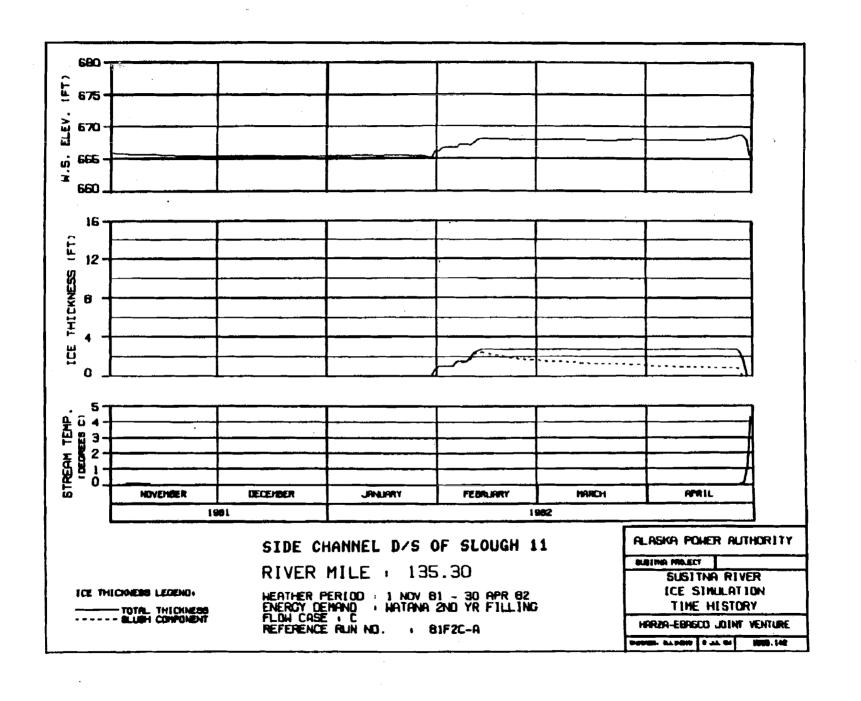
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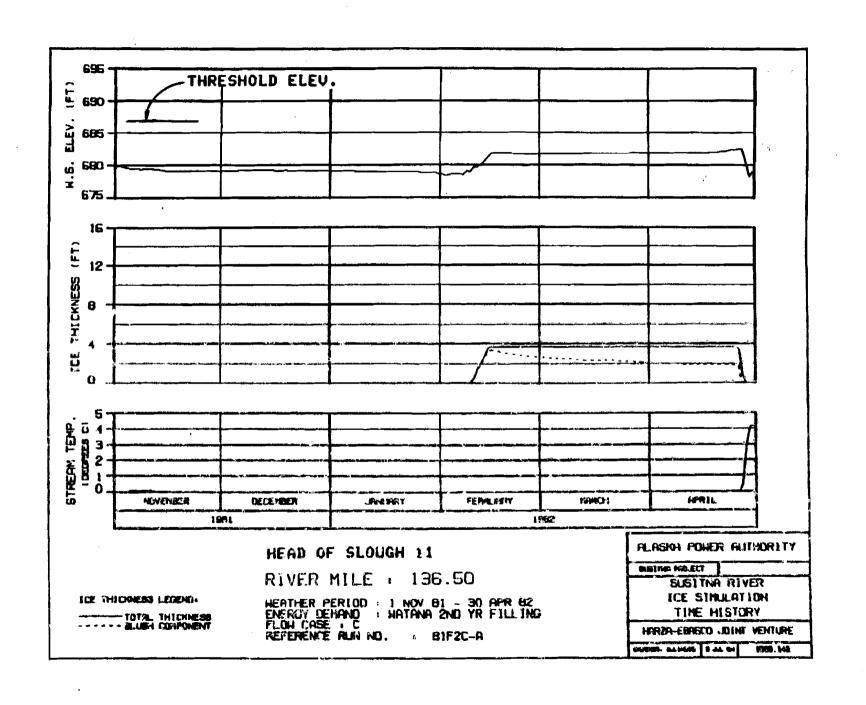


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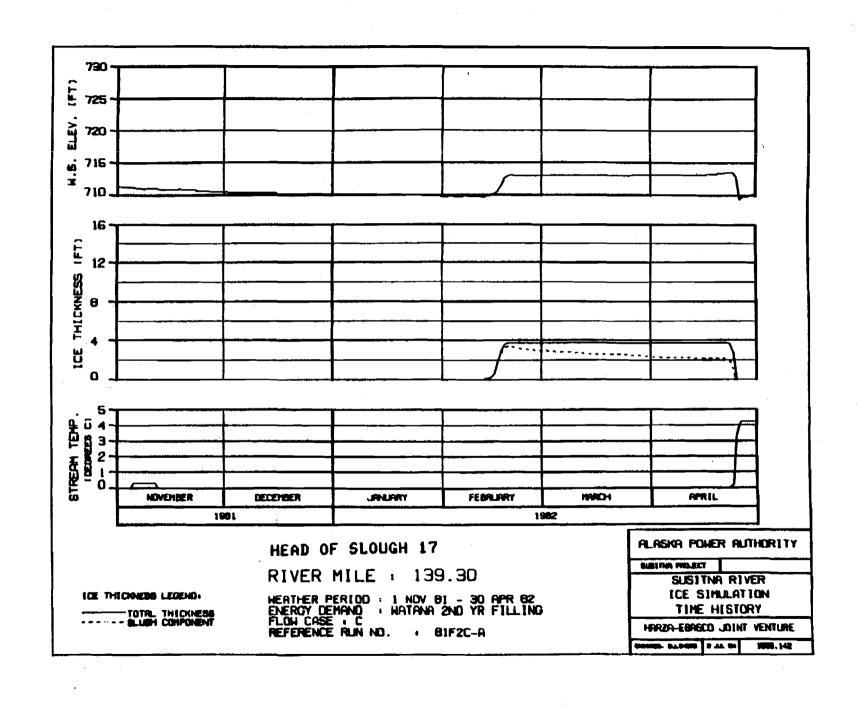


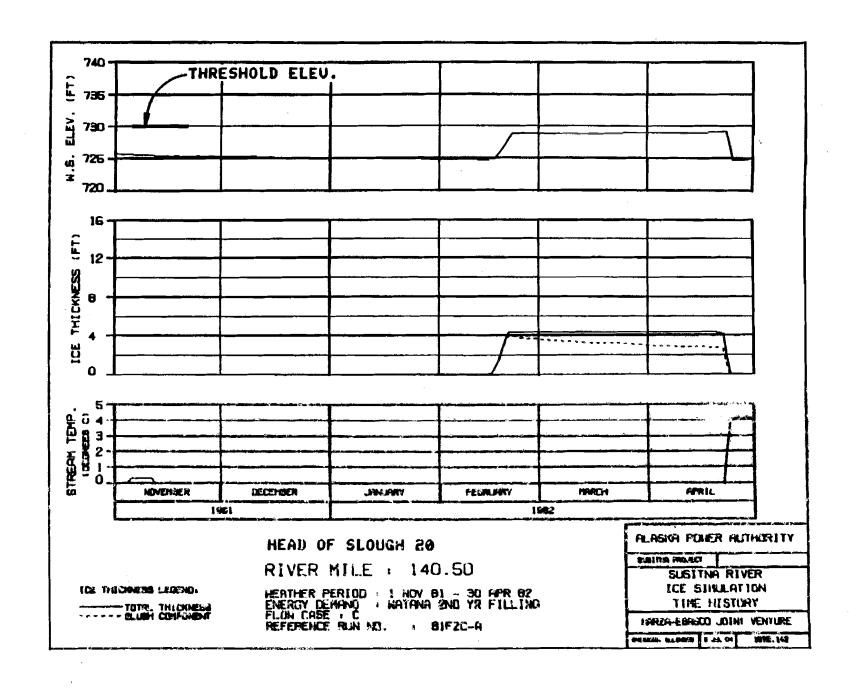
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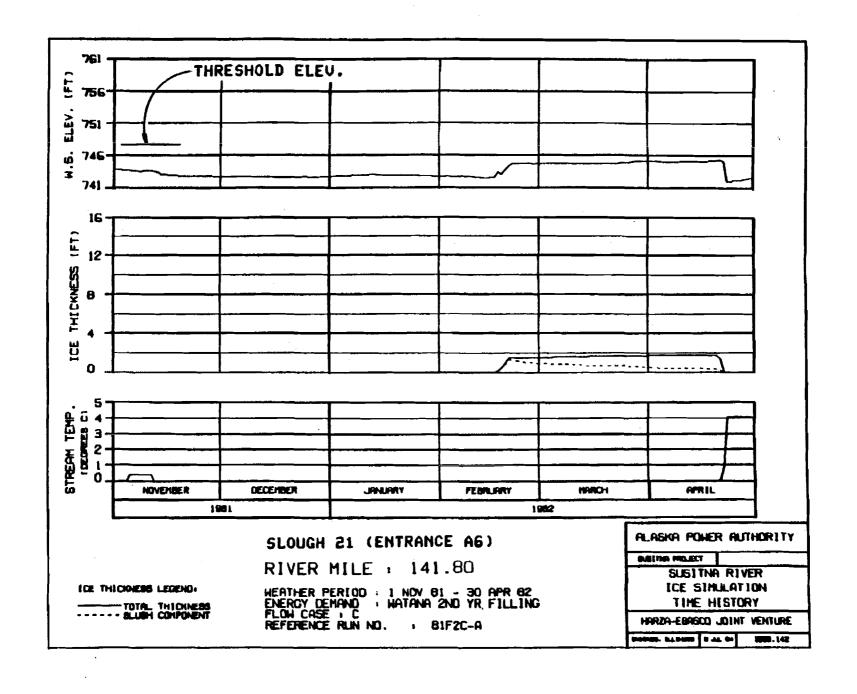
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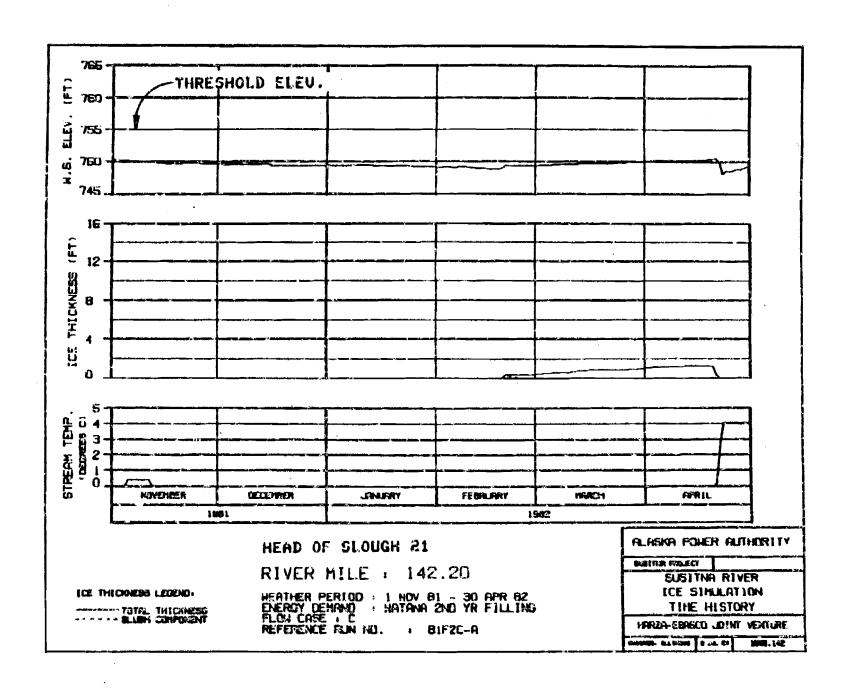




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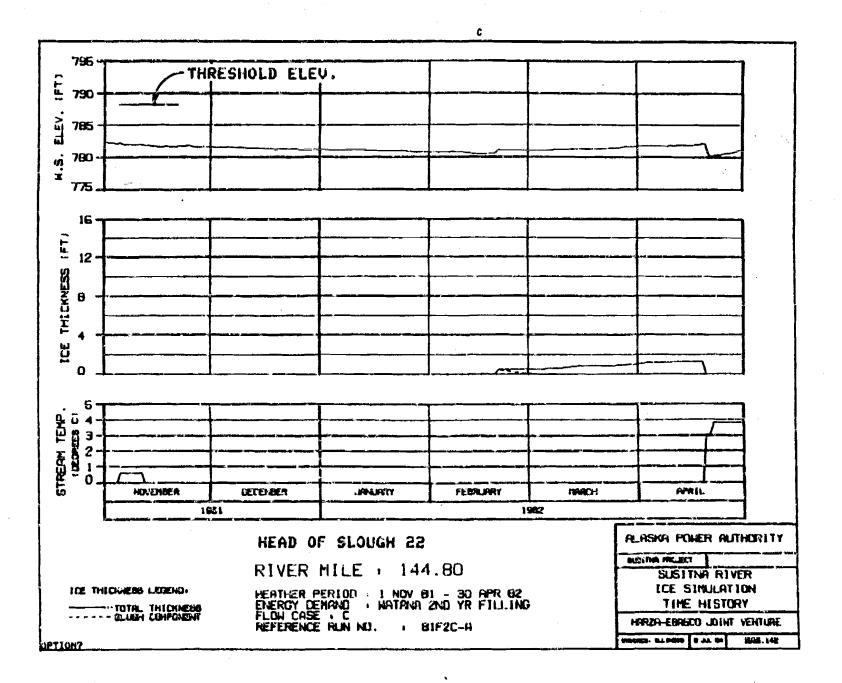
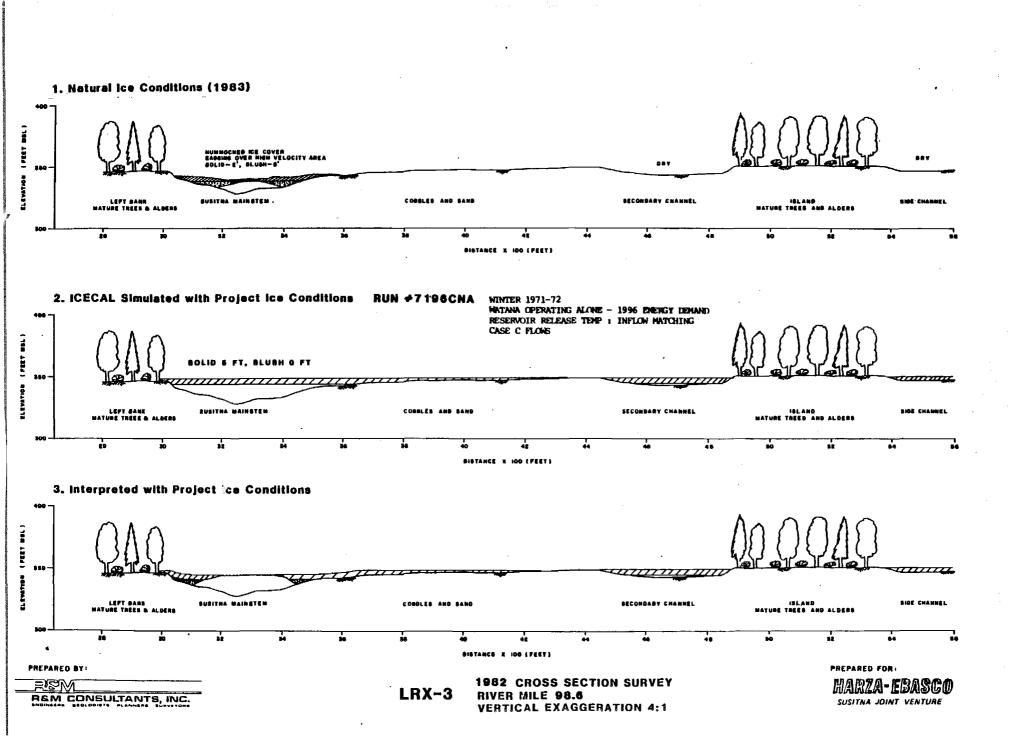
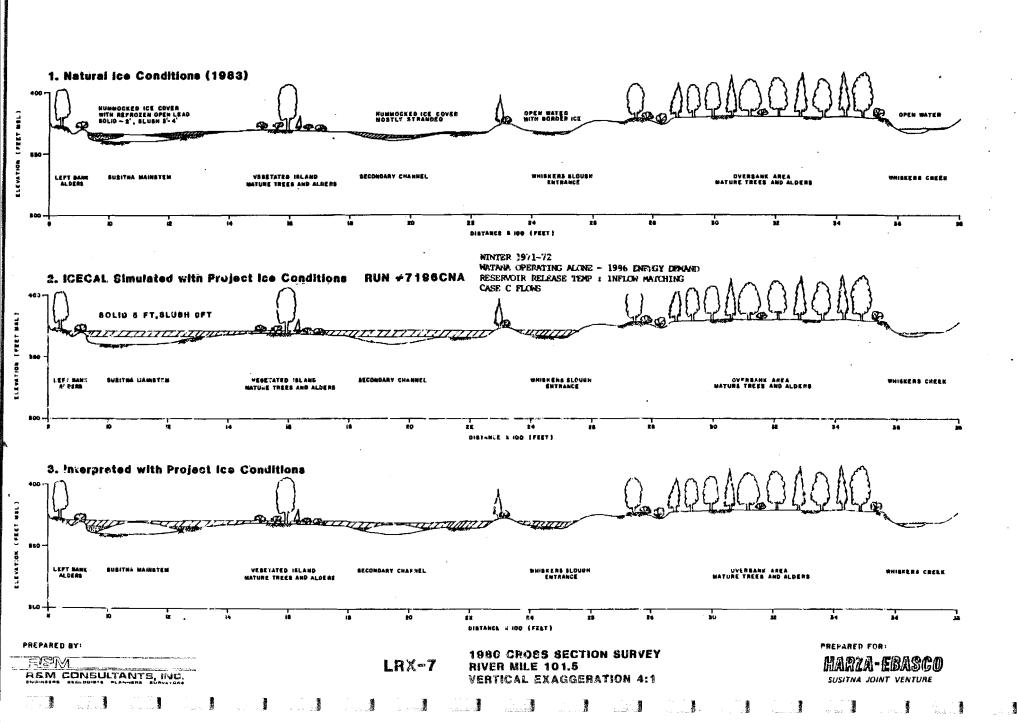
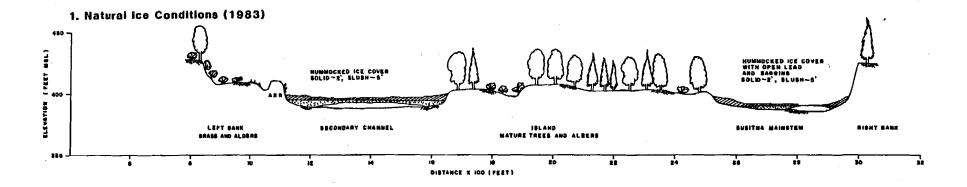
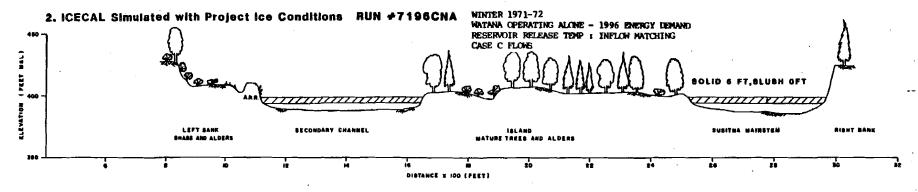


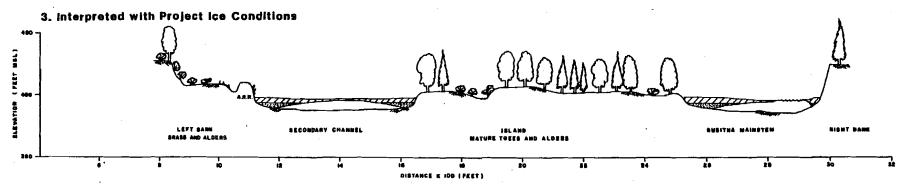
EXHIBIT U











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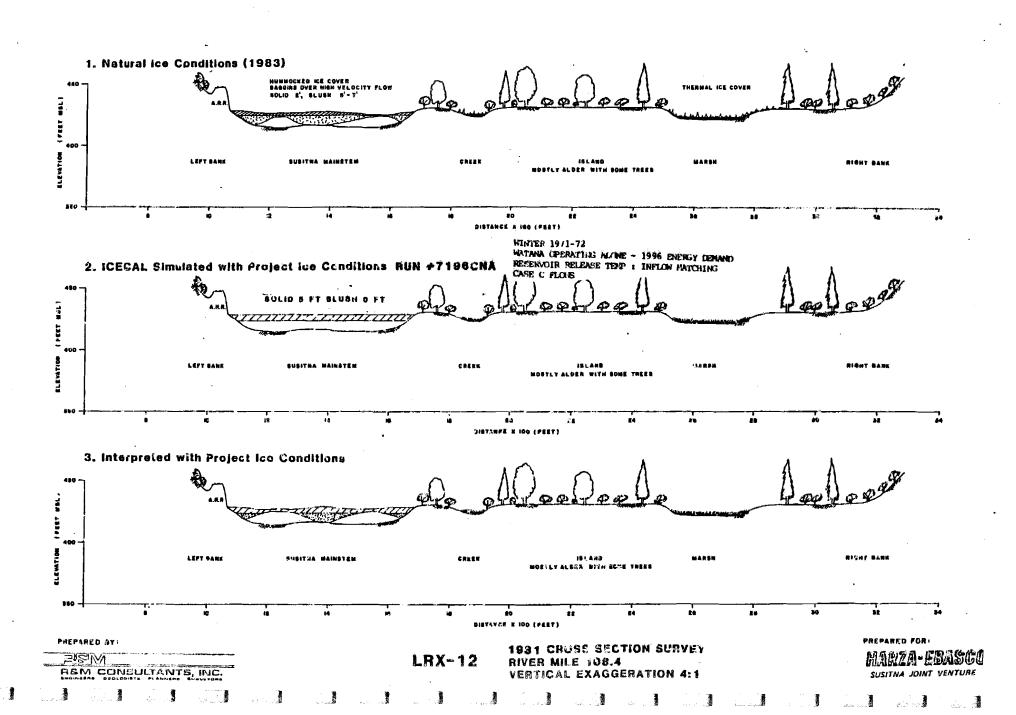
REM CONSULTANTS, INC.

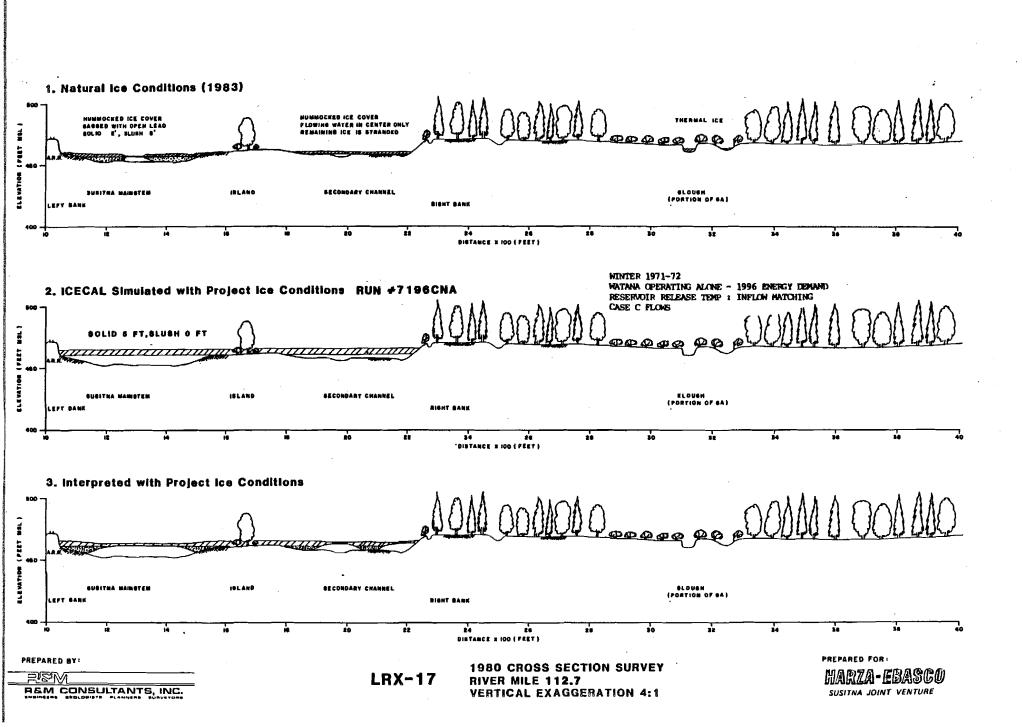
LRX-10 1980 CROSS SECTION SURVEY RIVER MILE 104.8 VERTICAL EXAGGERATION 4:1

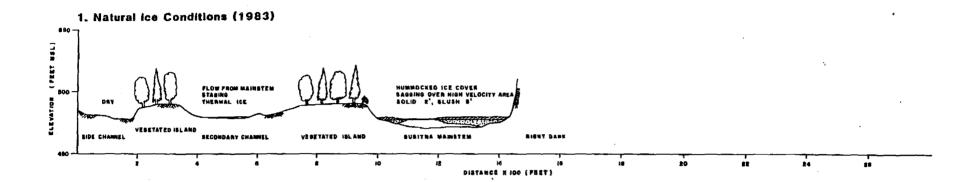
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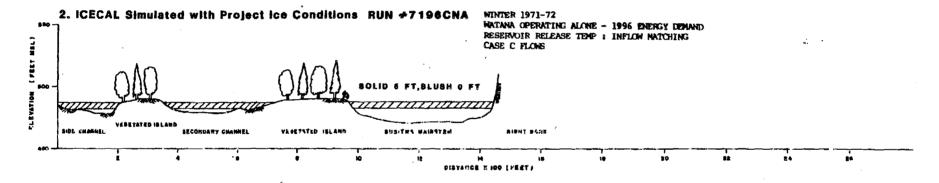
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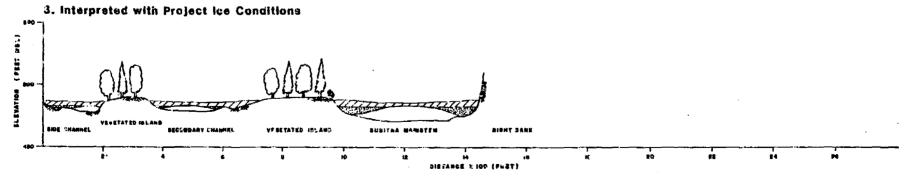
SUSITNA JOINT VENTURE











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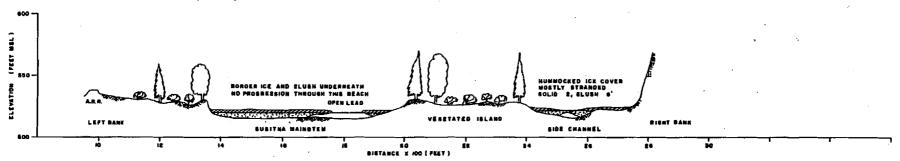
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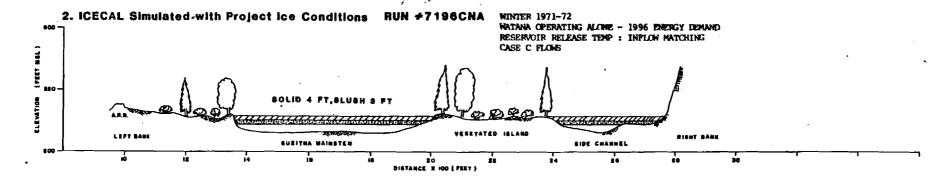
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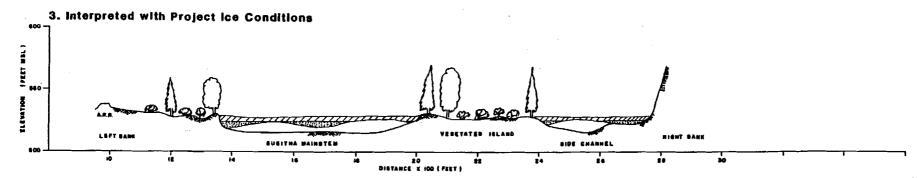
LRX-18.2 1982 CROSS SECTION SURVEY RIVER MILE 113.1 VERTICAL EXAGGERATION 4:1

PREPARED FOR PARZA BASCO SUSITNA JOINT VENTURE

1. Natural Ice Conditions (1983)







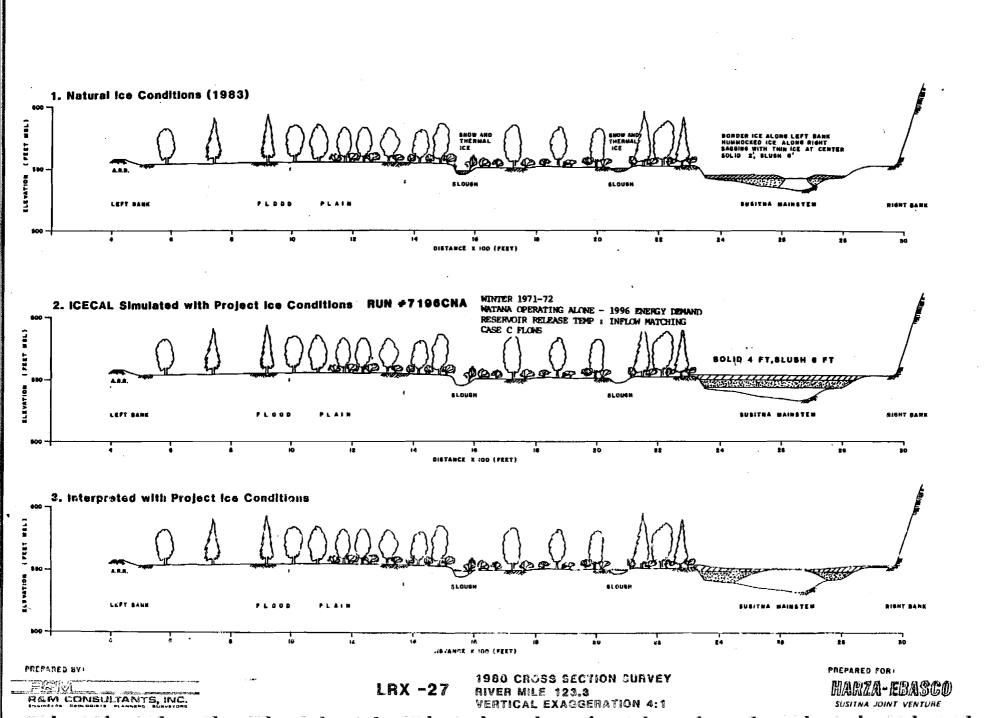
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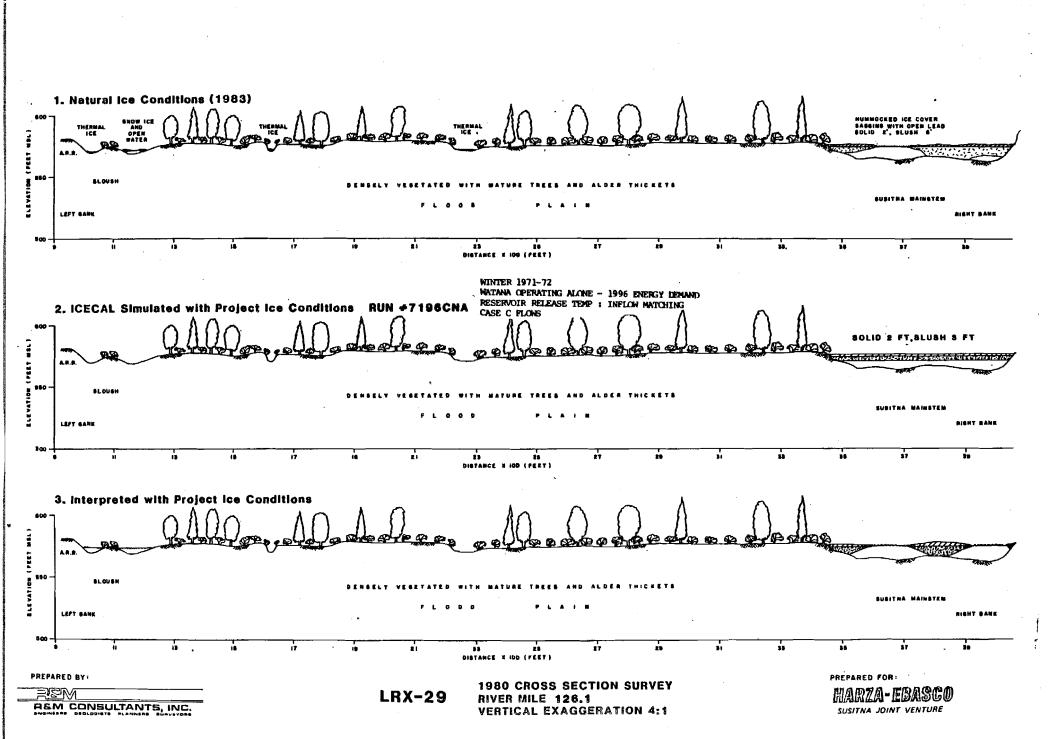
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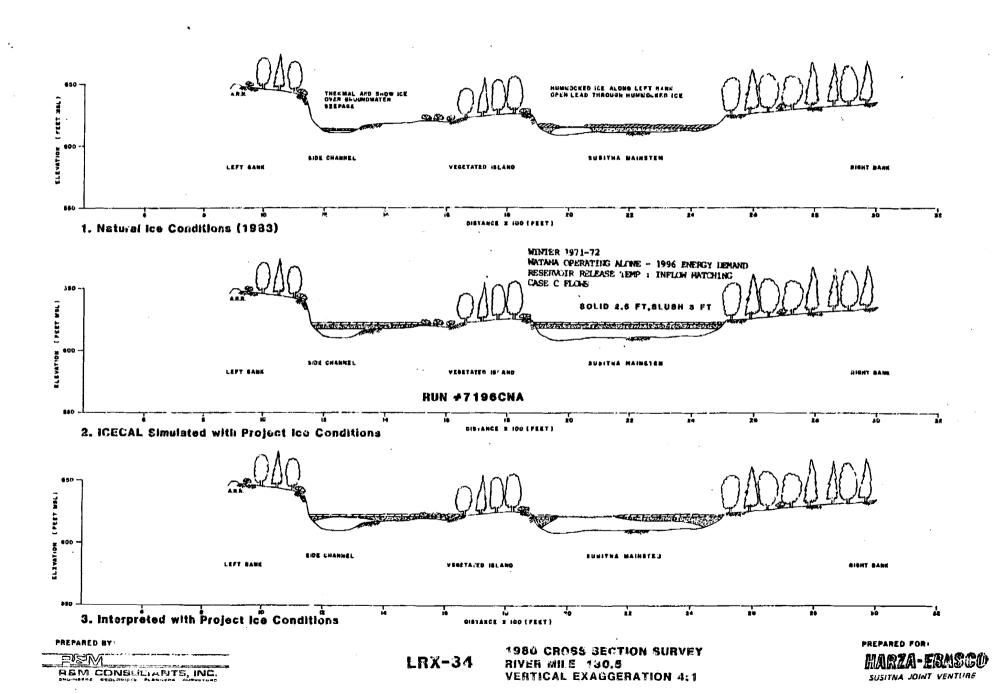
LRX-23

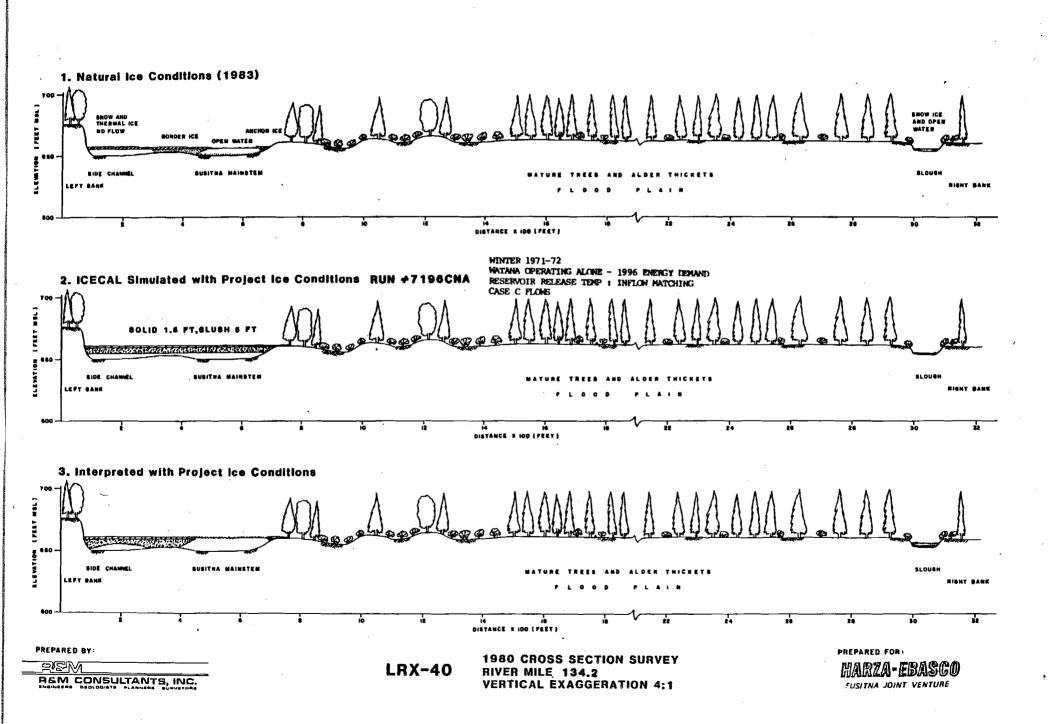
1980 CROSS SECTION SURVEY RIVER MILE 120.2 VERTICAL EXAGGERATION 4:1 PREPARED FOR:

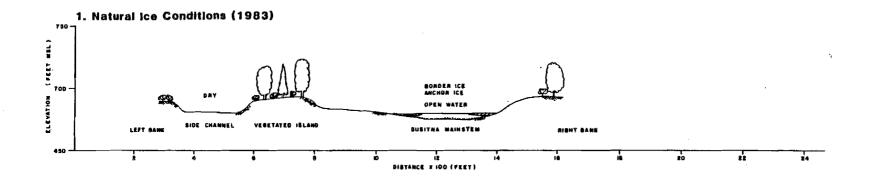
WARZA-EBASCO
SUSITNA JOINT VENTURE

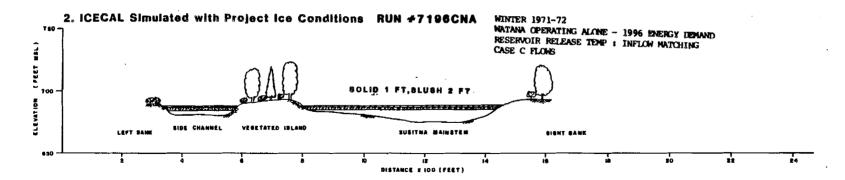


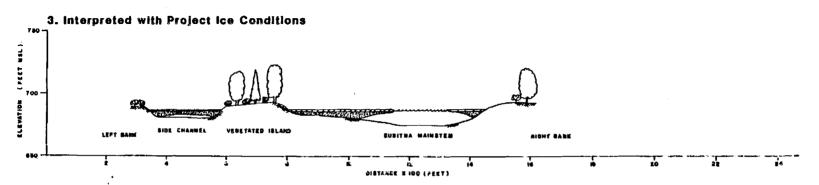












PREPARED BY:

REM CONSULTANTS, INC.

LRX-44

1980 CROSS SECTION SURVEY RIVER MILE 136.4 VERTICAL EXAGGERATION 4:1 HARZA-EBASO

SUSITNA JOINT VENTURE

EXHIBIT V

1. Natural Ice Conditions (1983) NUMMOCKED ICE COVER SAGEING OVER MIBN VELOCITY AREA SOLID-2', BLUSH-5' ISLAMP MATURE TREES AND ALDERS LEFT SANK MATURE TREES & ALDENS SUSITNA MAINSTER COBBLES AND SAND SECONDARY CHANNEL BIDE CHANNEL DISTANCE E 100 (PEET) 2. ICECAL Simulated with Project Ice Conditions RUN≠7696CNA WINTER 1976-77 WATANA OPERATING ALONE - 1996 ENERGY DEMAND RESERVOIR RELEASE TEMP : INFLOW MATCHING CASE C FLOWS SOLID O FT, SLUSH 0.5 FT LEFT-BANK MATURE TREES & ALDERS BUSITRA MAINSTEN COBBLES AND SAND SECONDARY CHANNEL HATURE TREES AND ALDERS SIDE CHANNEL BISTANCE X 100 (FEET) 3. Interpreted with Project ice Conditions LEFT BANK MATURE TREES & ALDERS BUSITHA MAINSTEM ISLAND MATURE TREES AND ALDERS SIDE CHANNEL SECONDARY CHARNEL COSSLES AND BAND DISTANCE R 100 (FEET) PREPARED BY PREPARED FOR

LRX-3

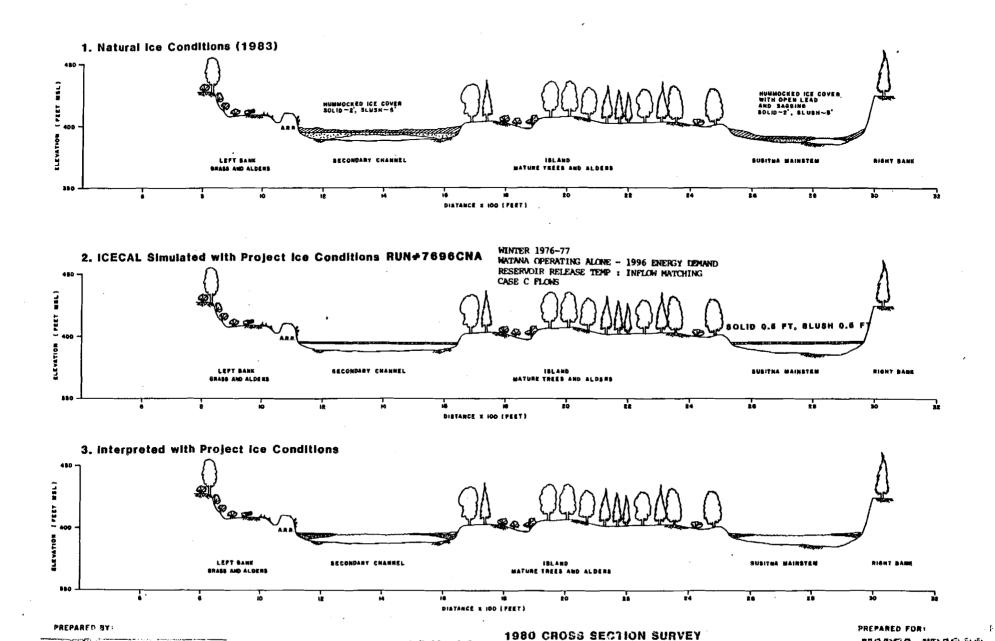
ASM CONSULTANTS, INC.

1982 CROSS SECTION SURVEY

VERTICAL EXAGGERATION 4:1

SUSITNA JOINT VENTURE

RIVER MILE 98.6



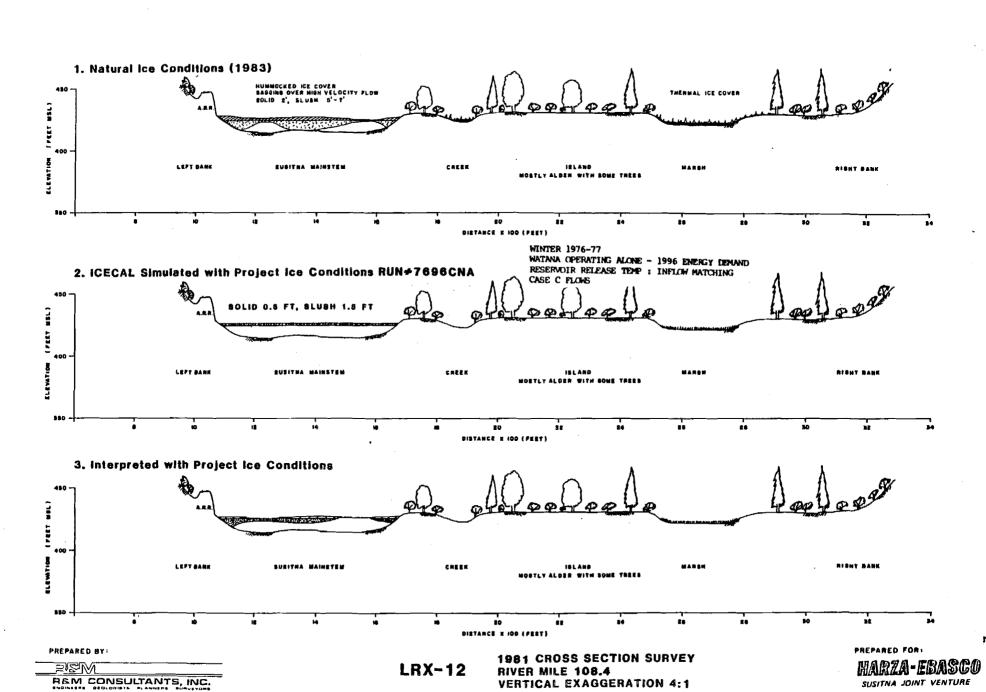
LRX-10

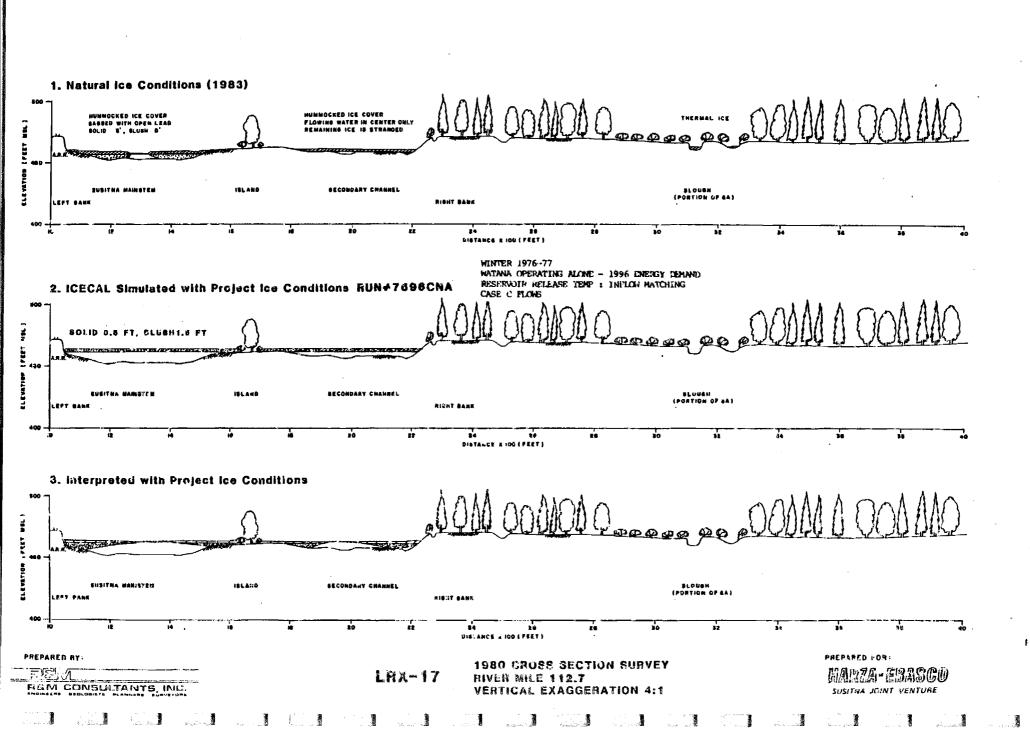
RAM CONSULTANTS, INC.

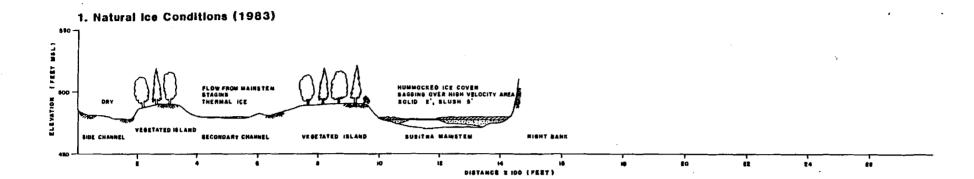
RIVER MILE 104.8

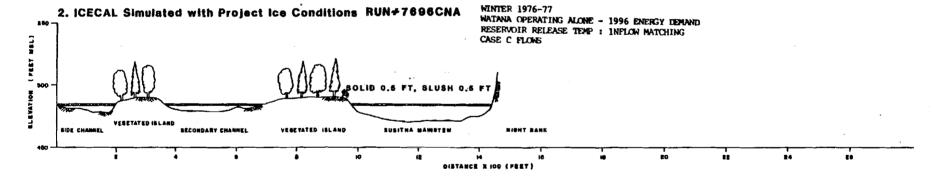
VERTICAL EXAGGERATION 4:1

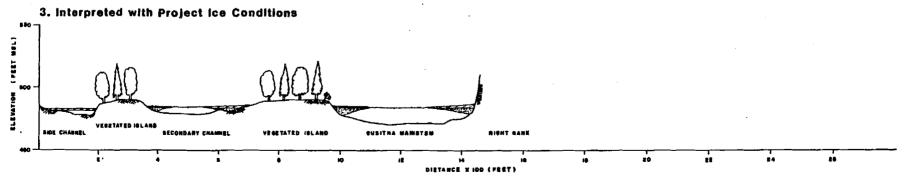
SUSITNA JOINT VENTURE











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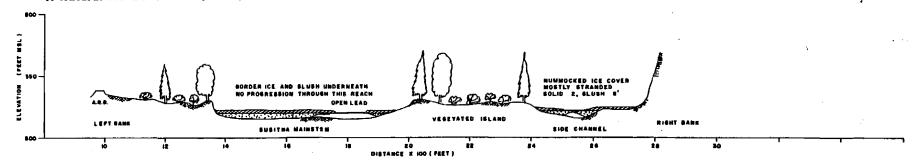
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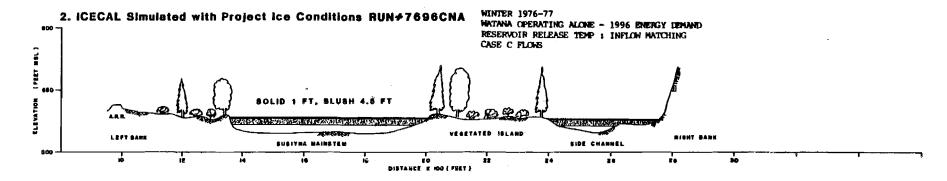
REM CONSULTANTS, INC.

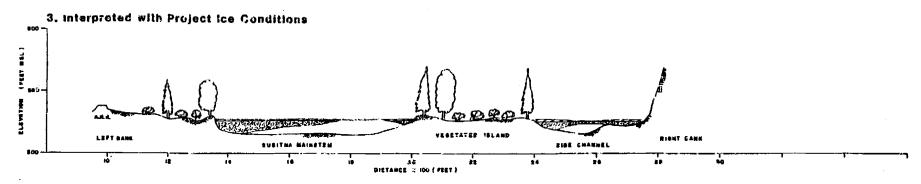
LRX-18.2 1982 CROSS SECTION SURVEY RIVER MILE 115.1 VERTICAL EXAGGERATION 4:1

PREPARED FOR:
HARZA-EBASCO
SUSITNA JOINT VENTURE

1. Natural Ice Conditions (1983)



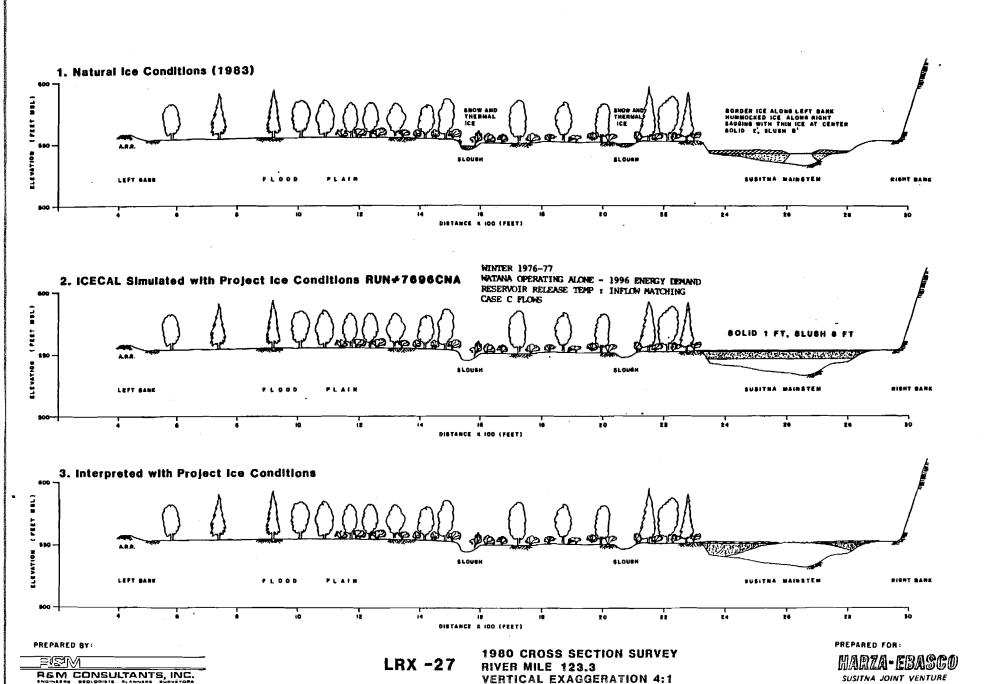


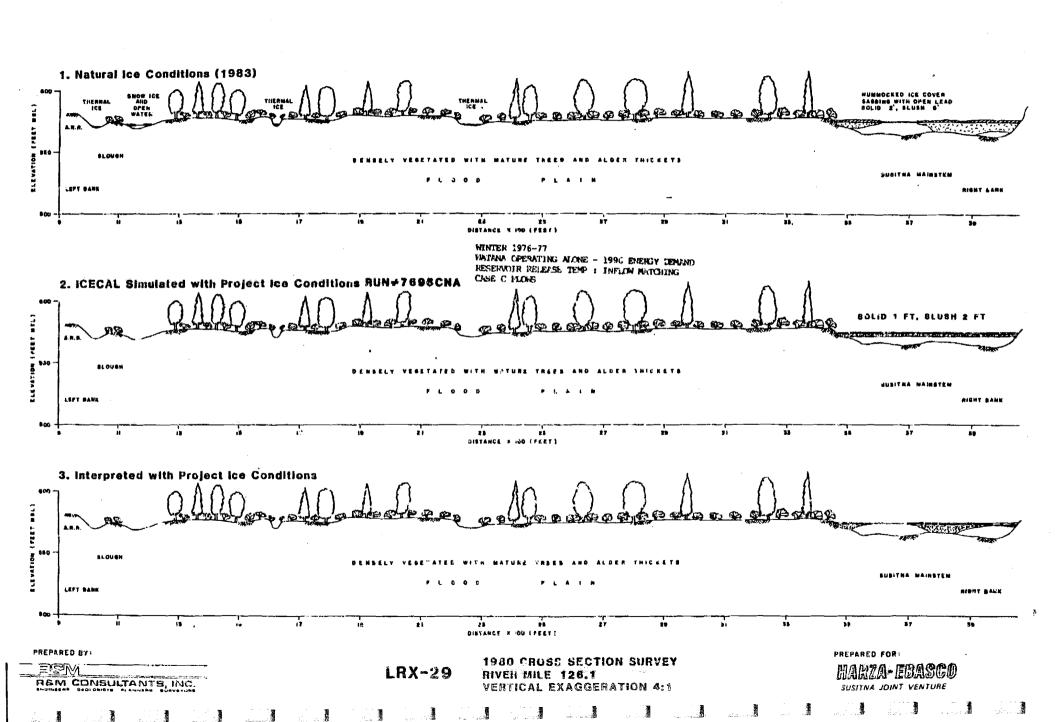


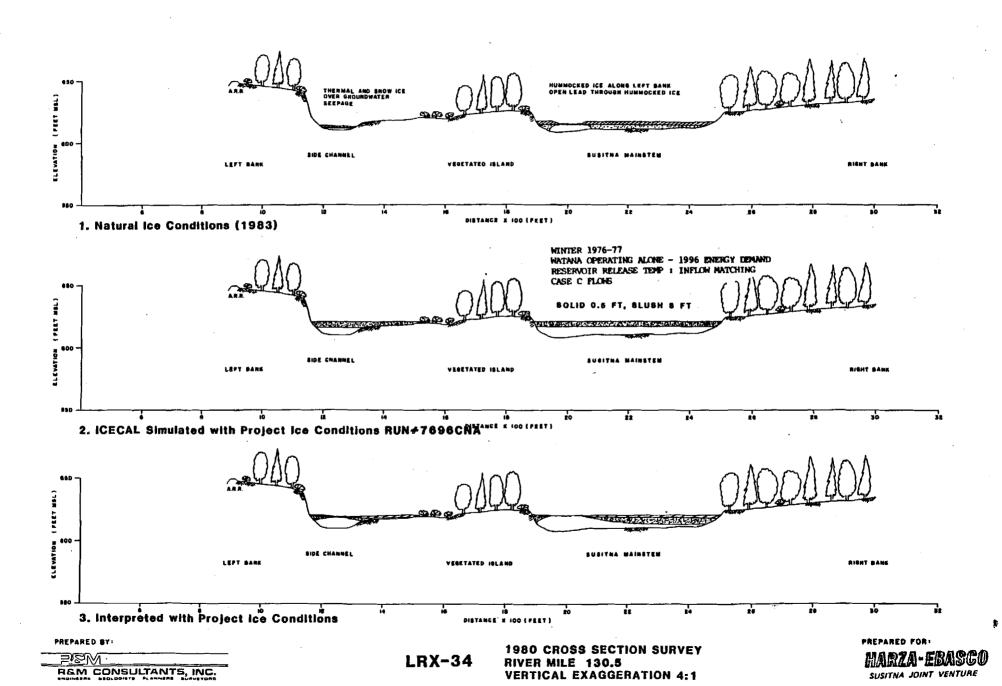
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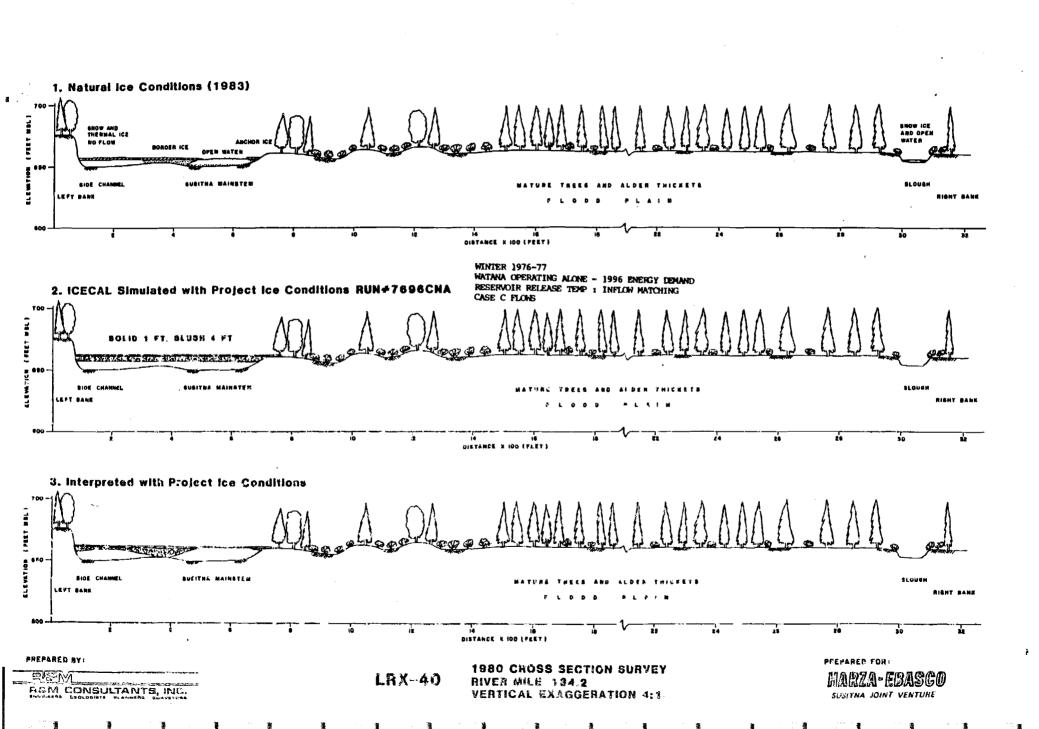
LRX-23

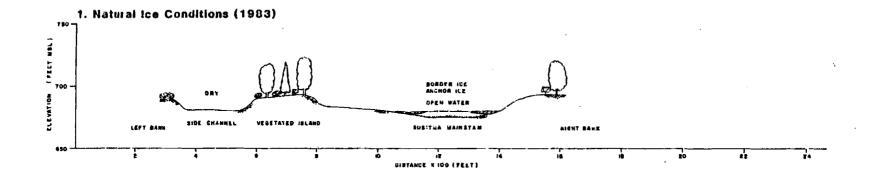
1980 CROSS SECTION SURVEY RIVER MILE 120.2 VERTICAL EXAGGERATION 4:1 HARZA-EKASCO Susitna Joint Venture

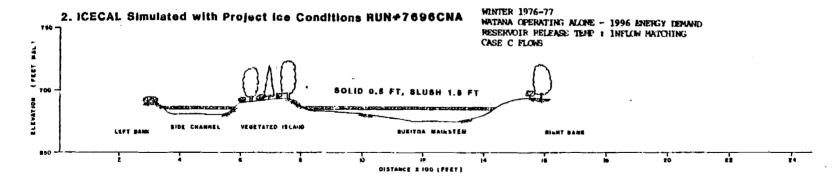


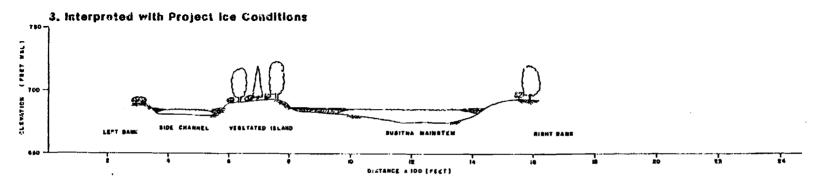












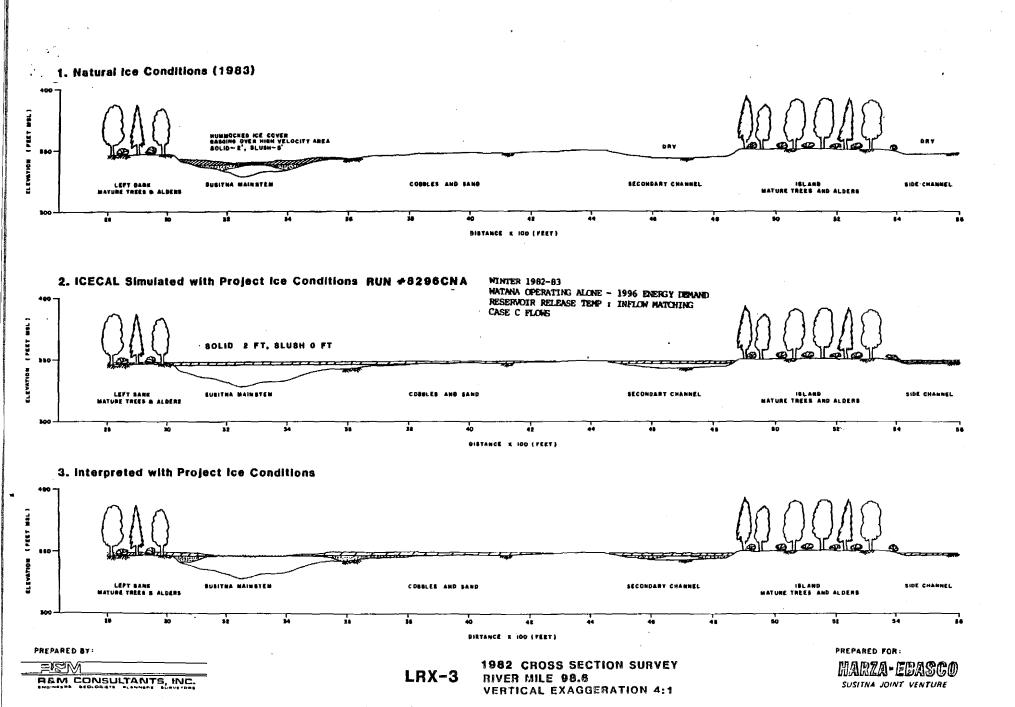
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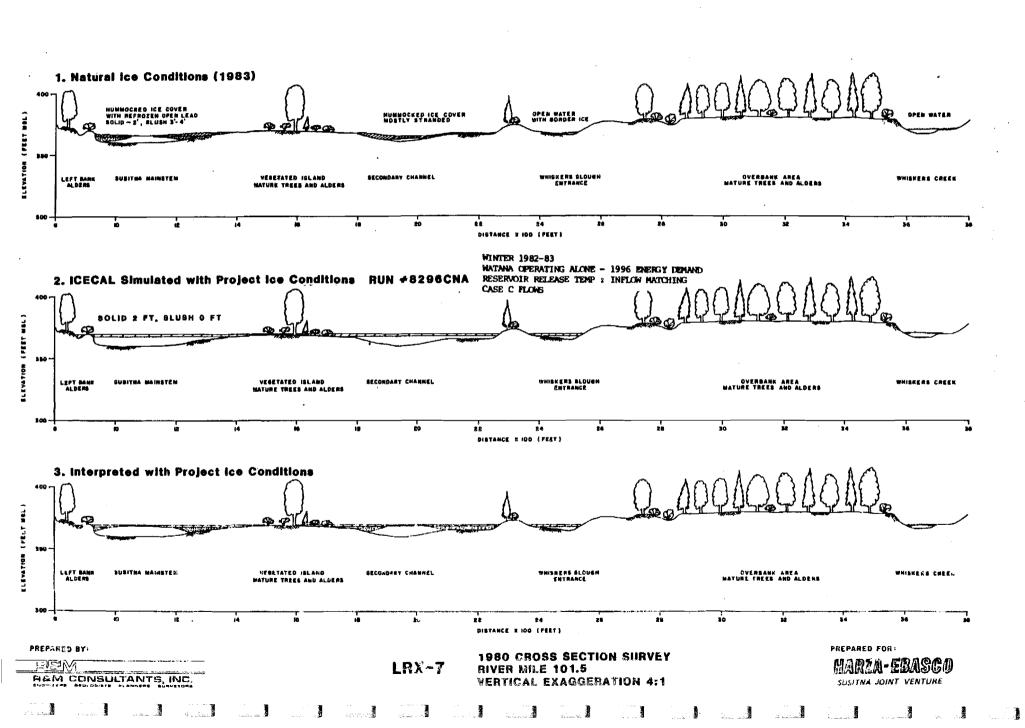
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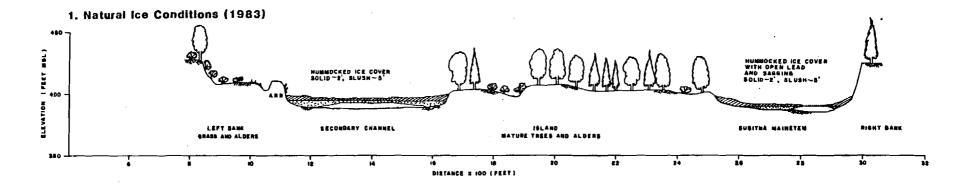
1980 CROSS SECTION SURVEY BIVER MILE 130.4 VERTICAL EXAGGERATION 4:1 PREPARED FOR .

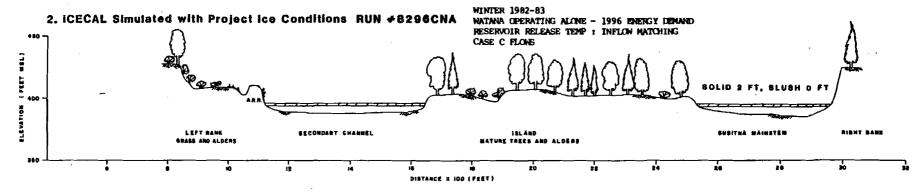
MARZA-EBASCO
SUSITHA JOINT VENTURE

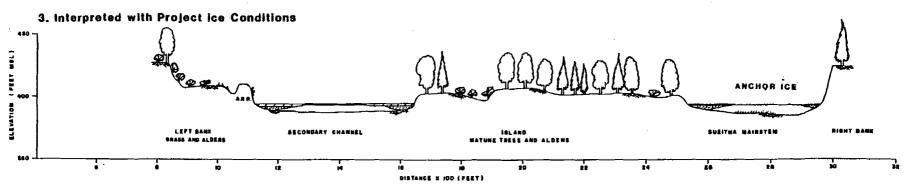
EXHIBIT W











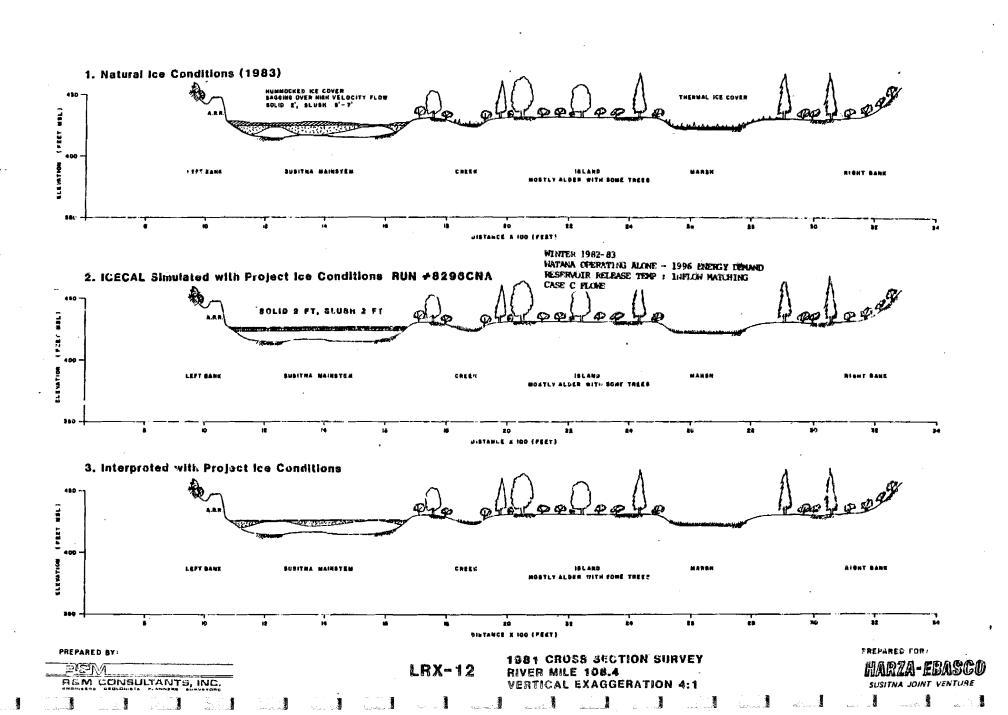
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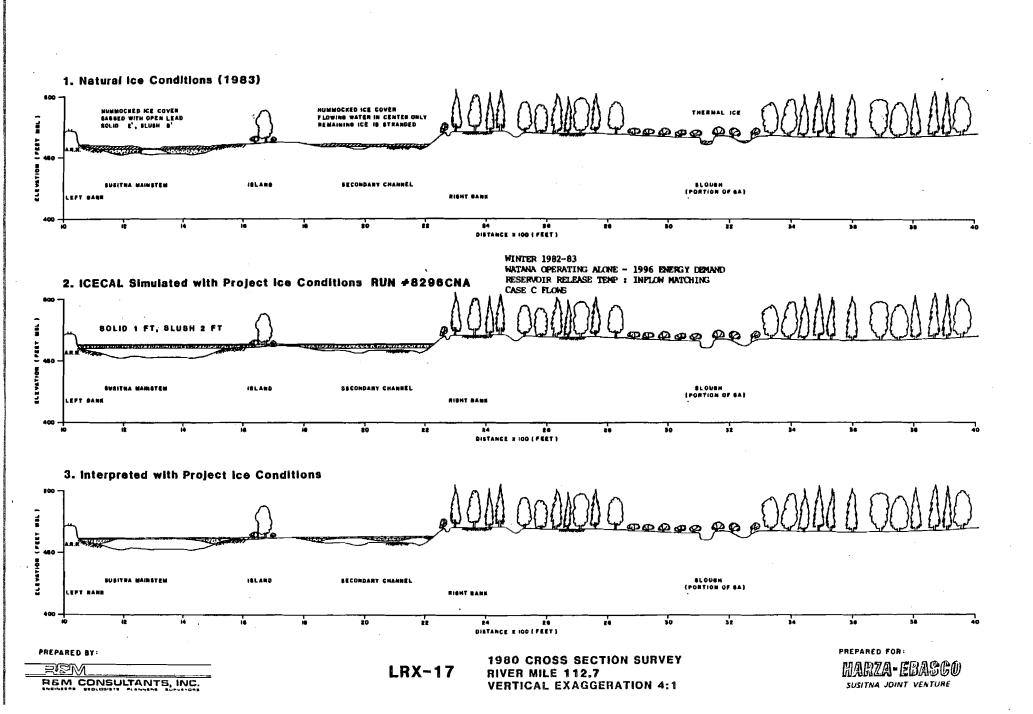
REM CONSULTANTS, INC.

LRX-10

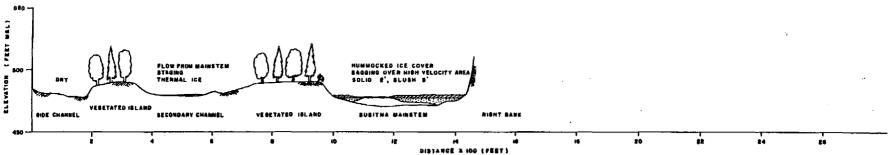
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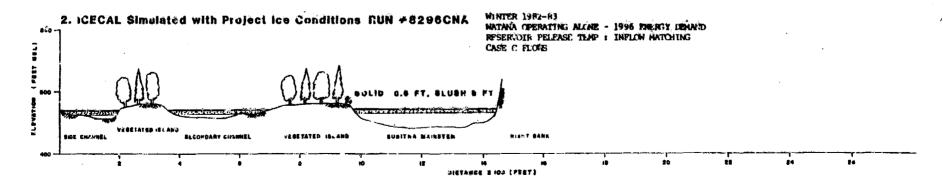
HARZA-EBASCU SUSITNA JOINT VENTURE



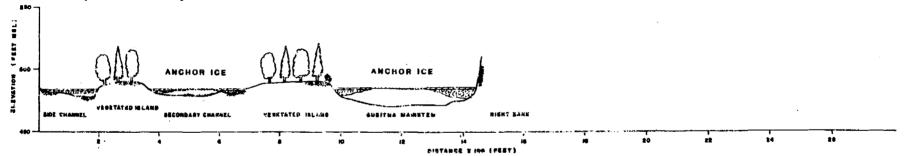












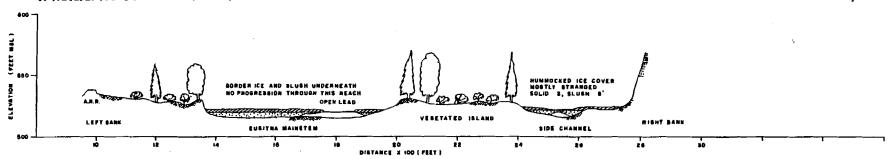
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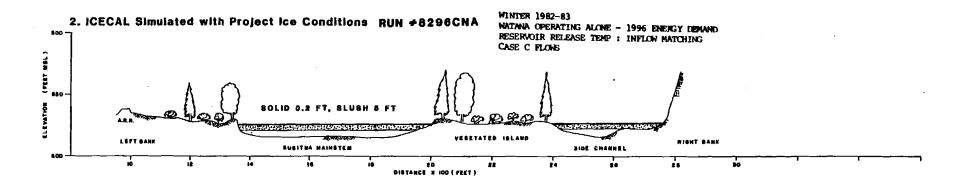
REM CONSLITANTS, INC.

LRX-18.2 1982 CROSS SECTION BURVEY RIVER MILE 113.1 VERTICAL EXAGGERATION 4:1

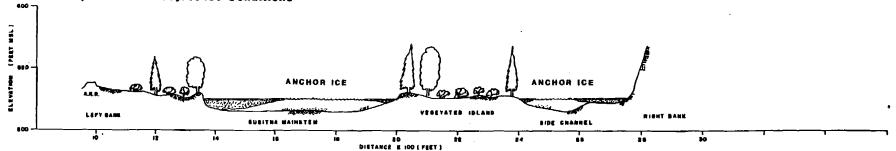
PREPARED FOR BARRAS EBASCU SUSTINA JOINT VENTURE

1. Natural Ice Conditions (1983)









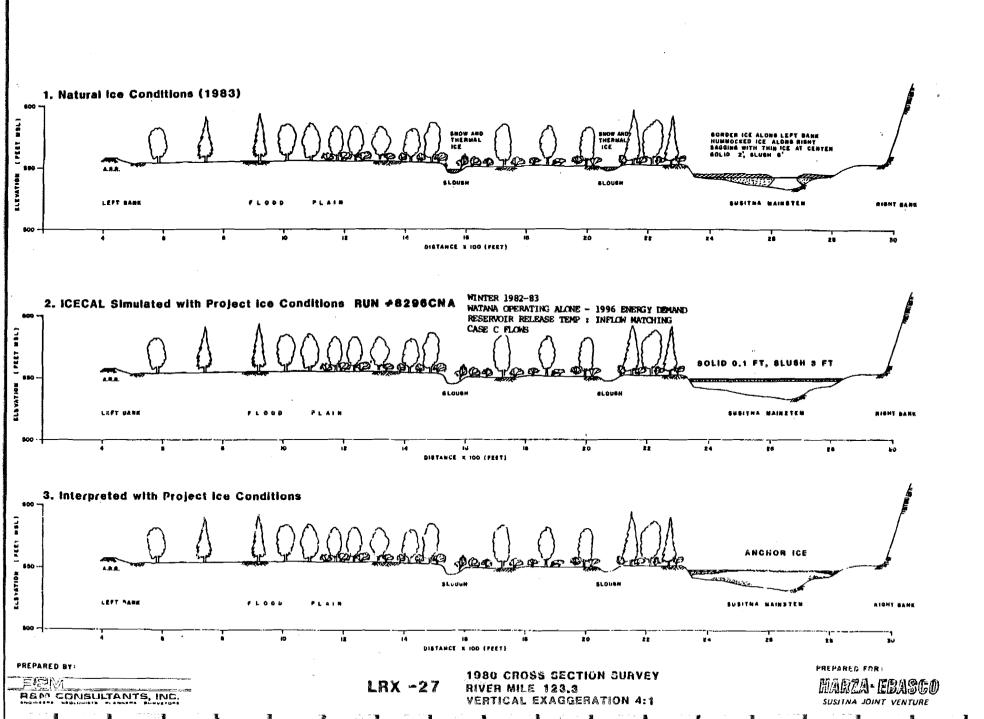
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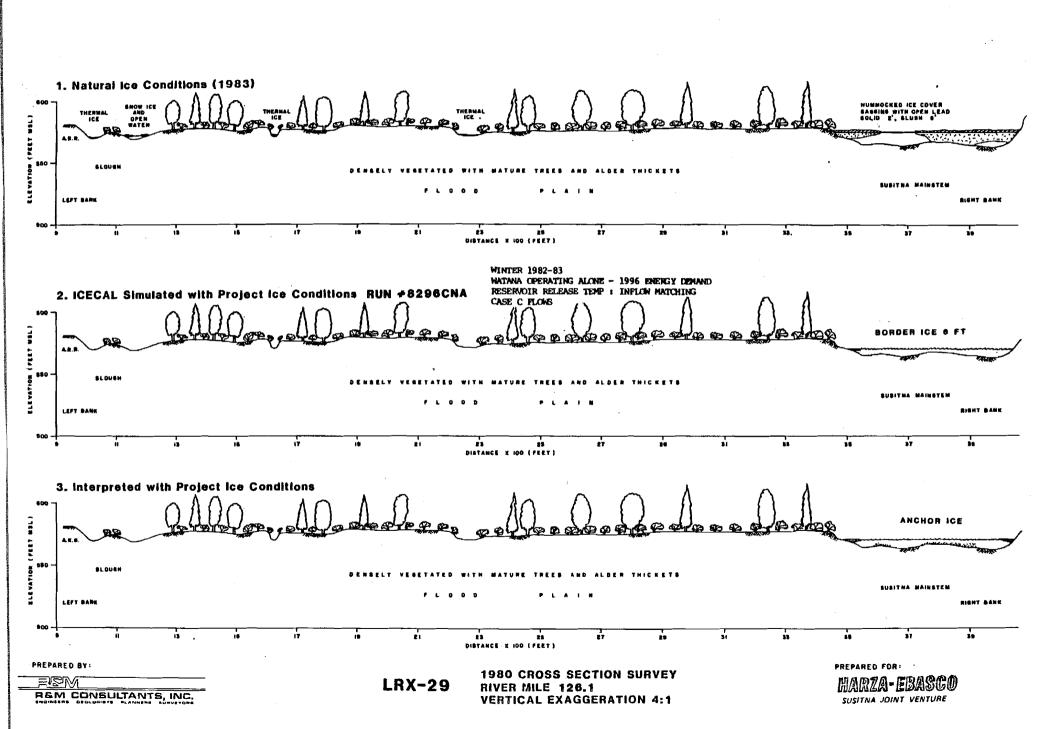
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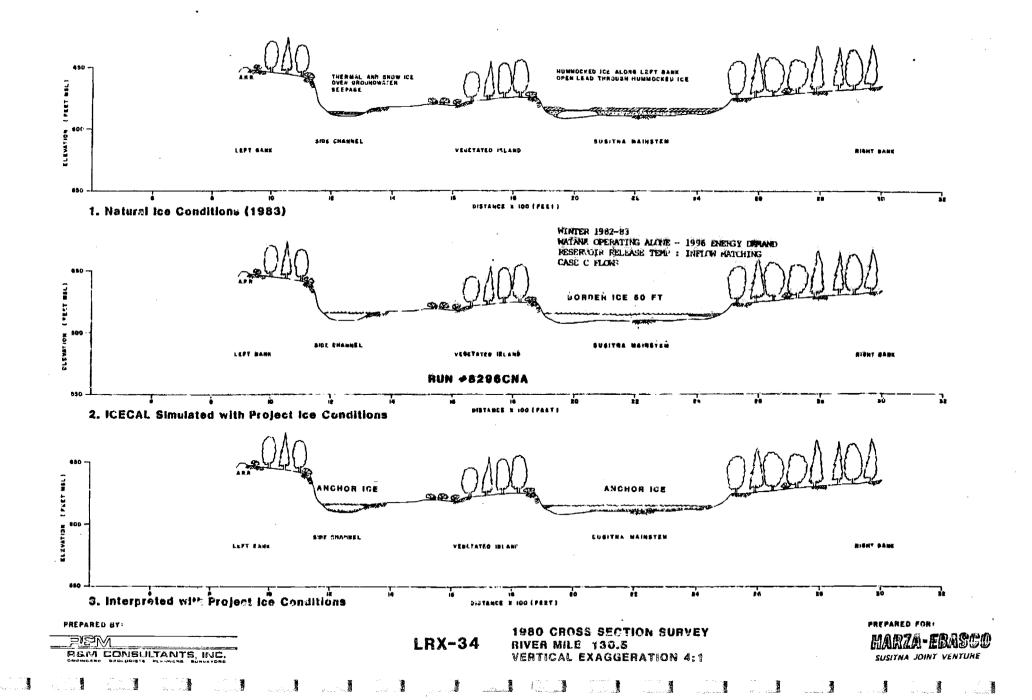
LRX-23

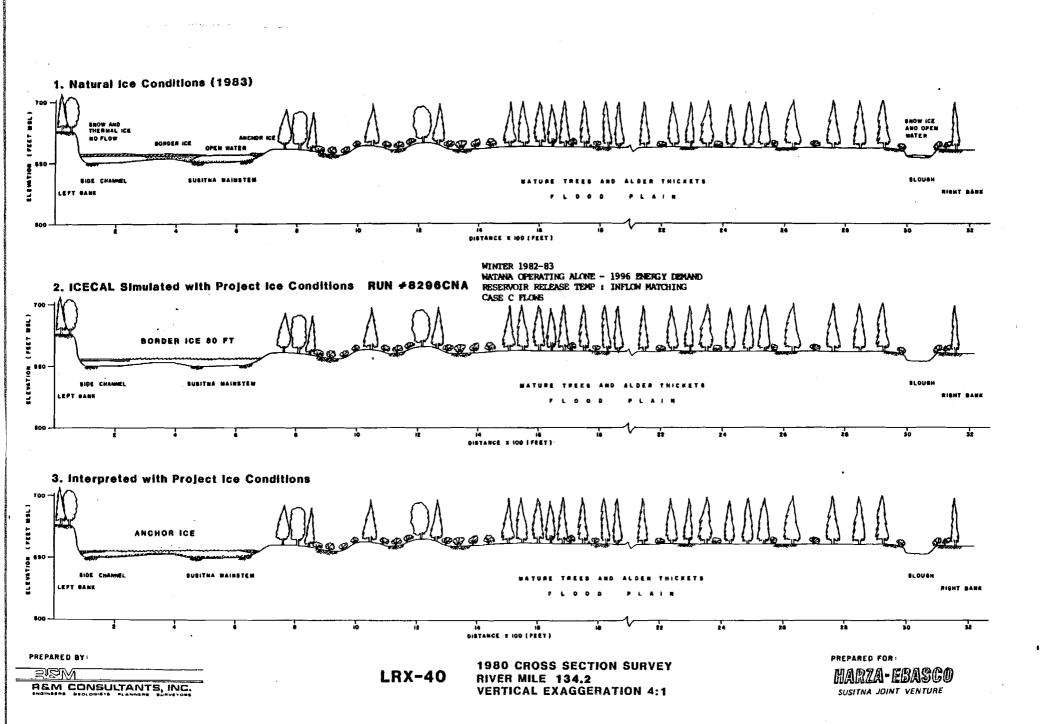
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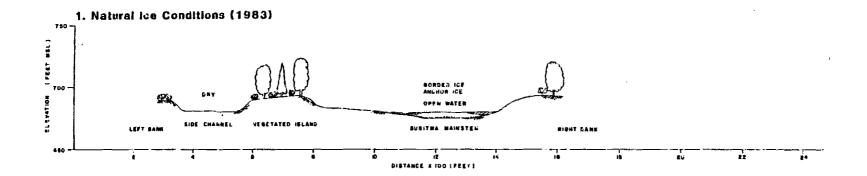
HARZA-EBASGO SUSITNA JOINT VENTURE

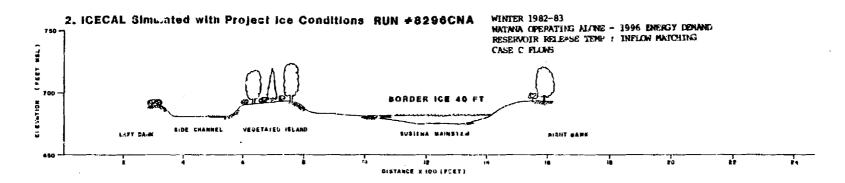


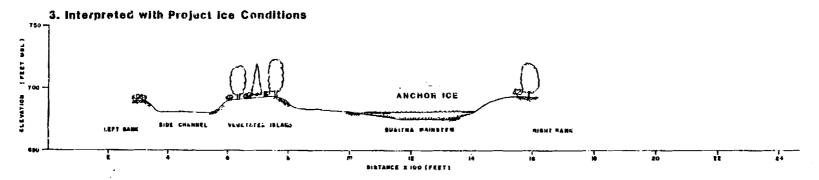












PREPARED BY:

PSM

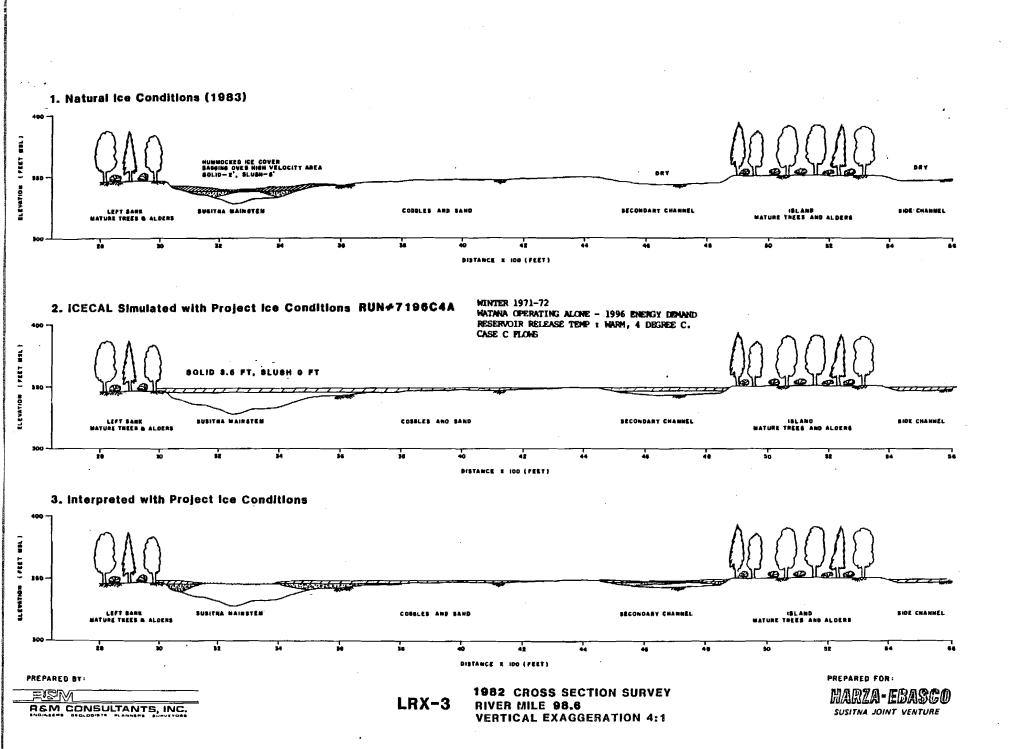
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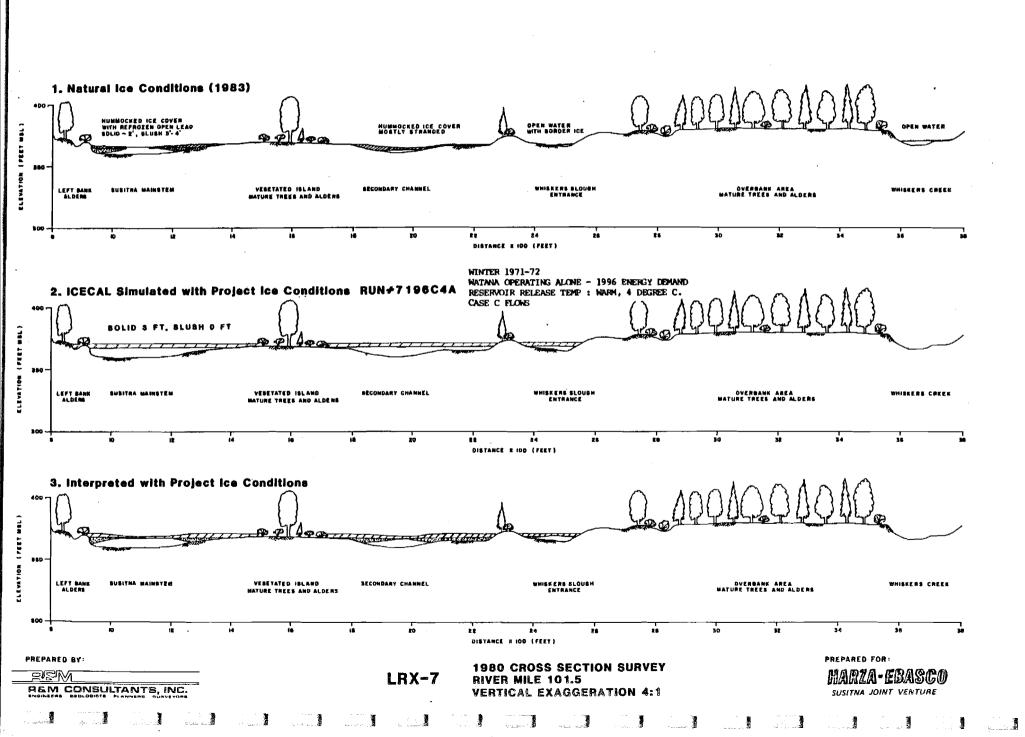
LRX-44

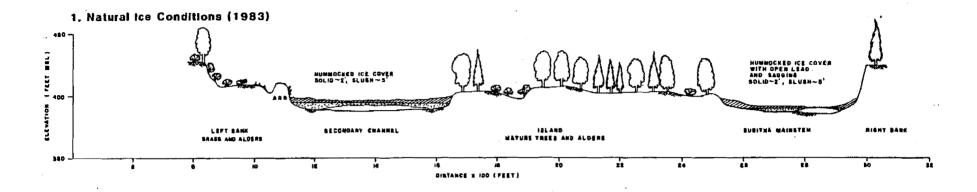
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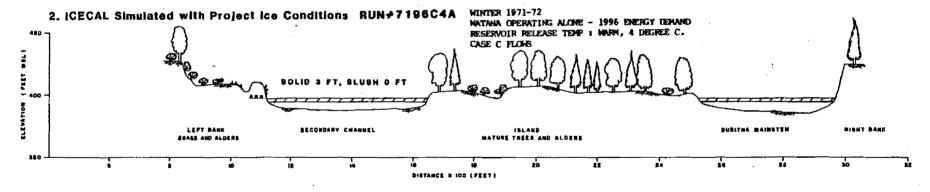
MARZA-EBASCI
SUSITNA JOINT VENTURE

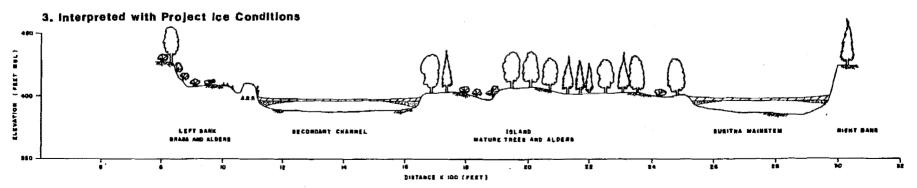
EXHIBIT X









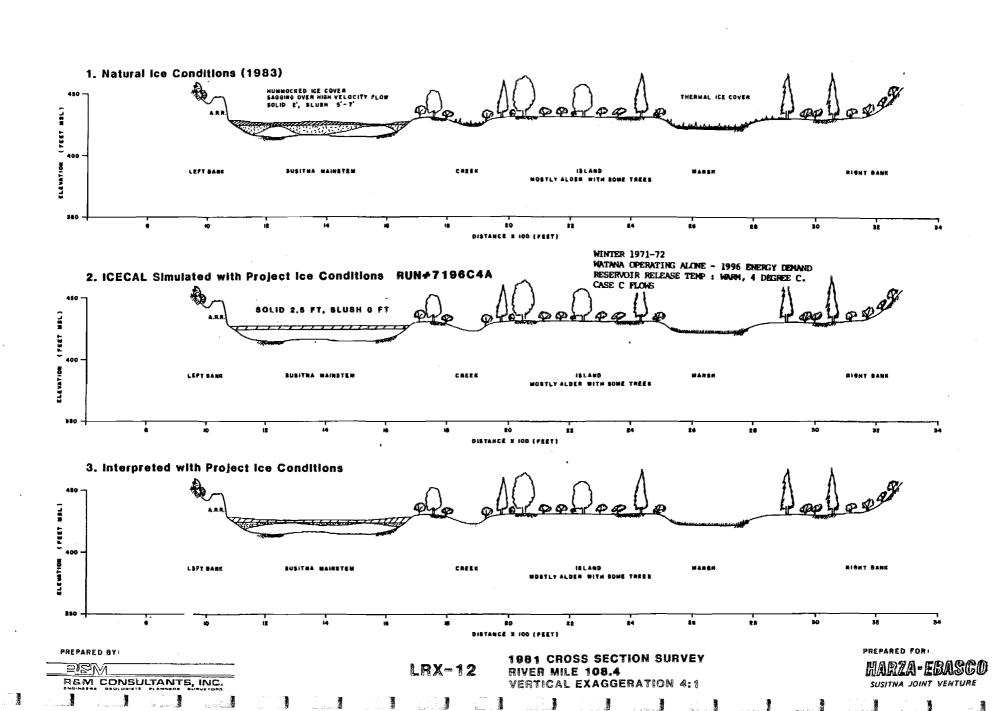


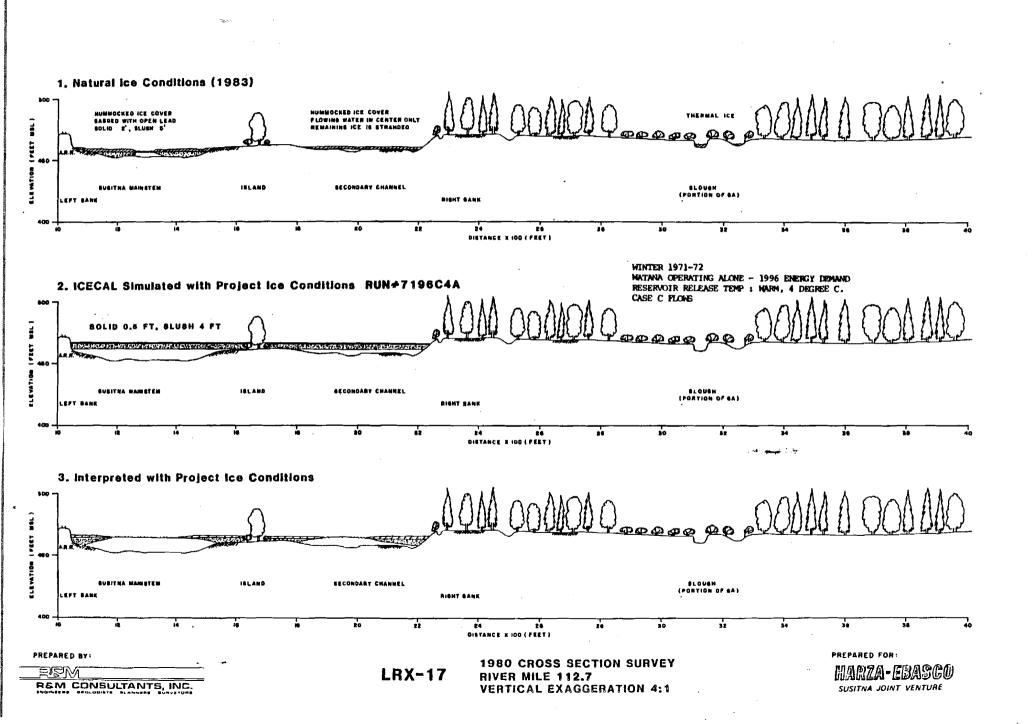
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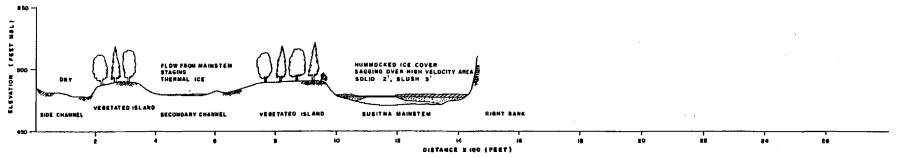
LRX-10 1980 CROSS SECTION SURVEY RIVER MILE 104.8 VERTICAL EXAGGERATION 4:1

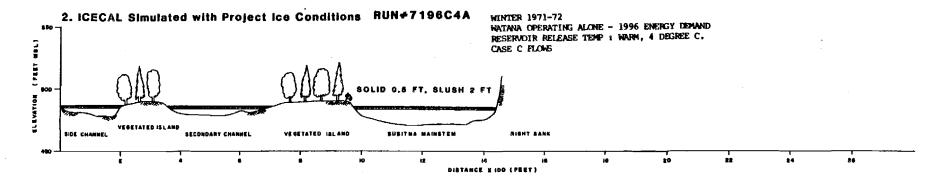
PREPARED FOR:
HARZA-EBASCO
SUSITNA JOINT VENTURE



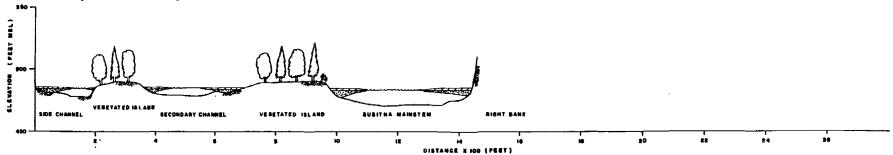












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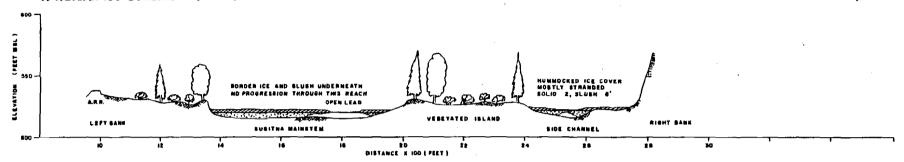
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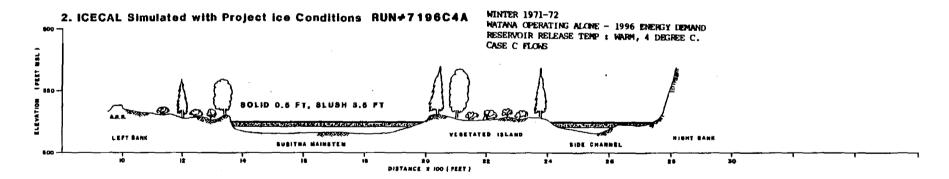
LRX-18.2 1982 CROSS SECTION SURVEY RIVER MILE 115.1

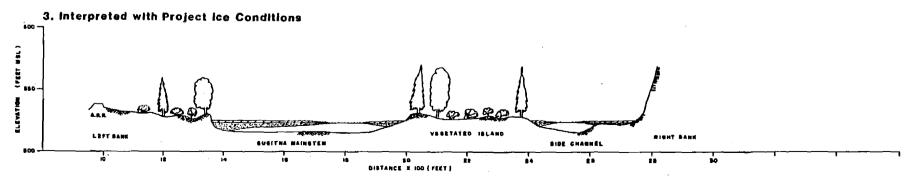
PREPARED FOR

MARKER TRIBER

1. Natural Ice Conditions (1983)





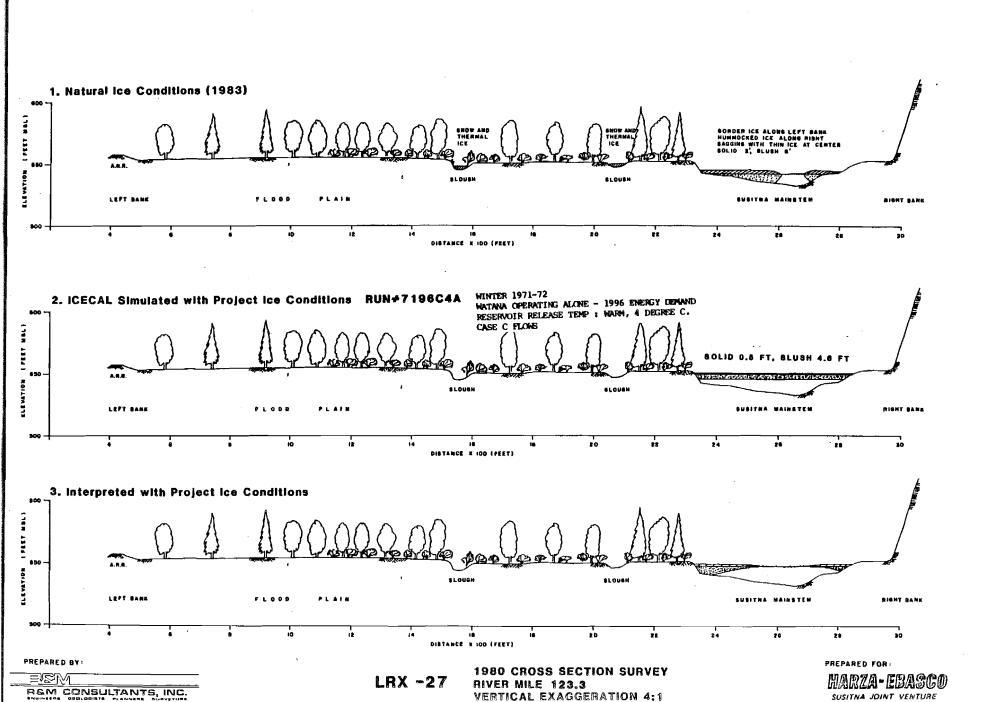


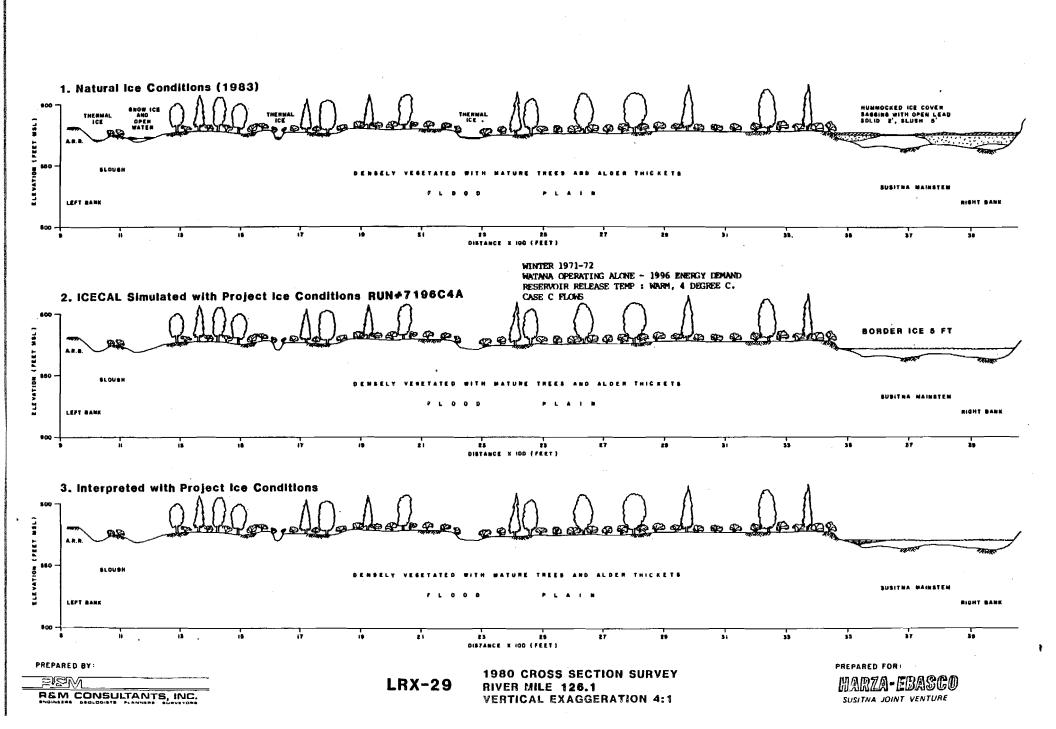
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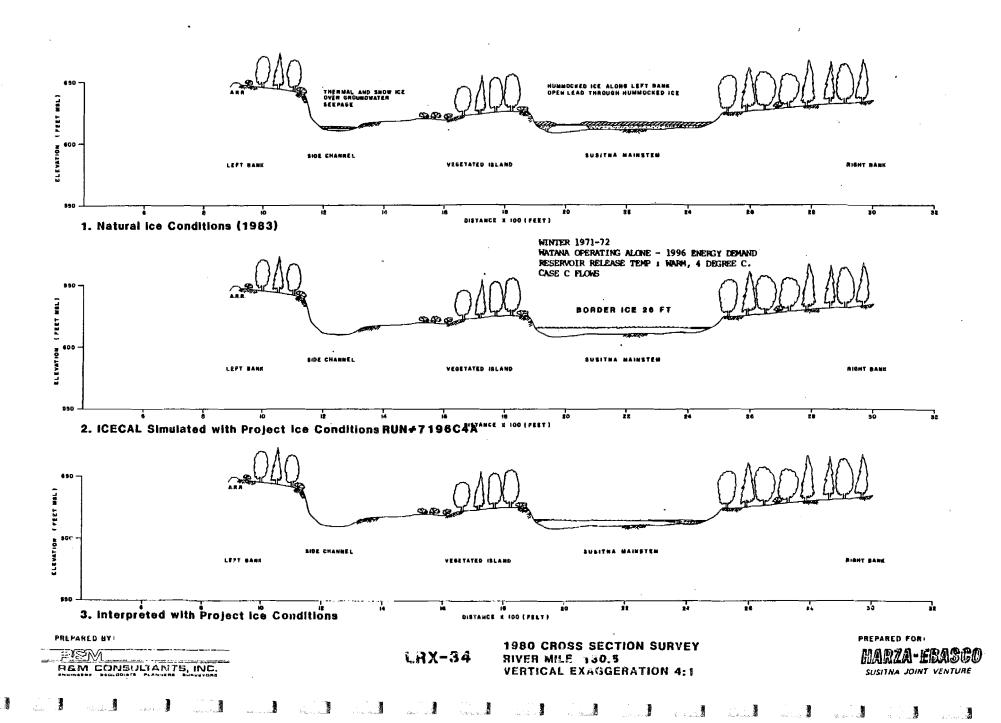
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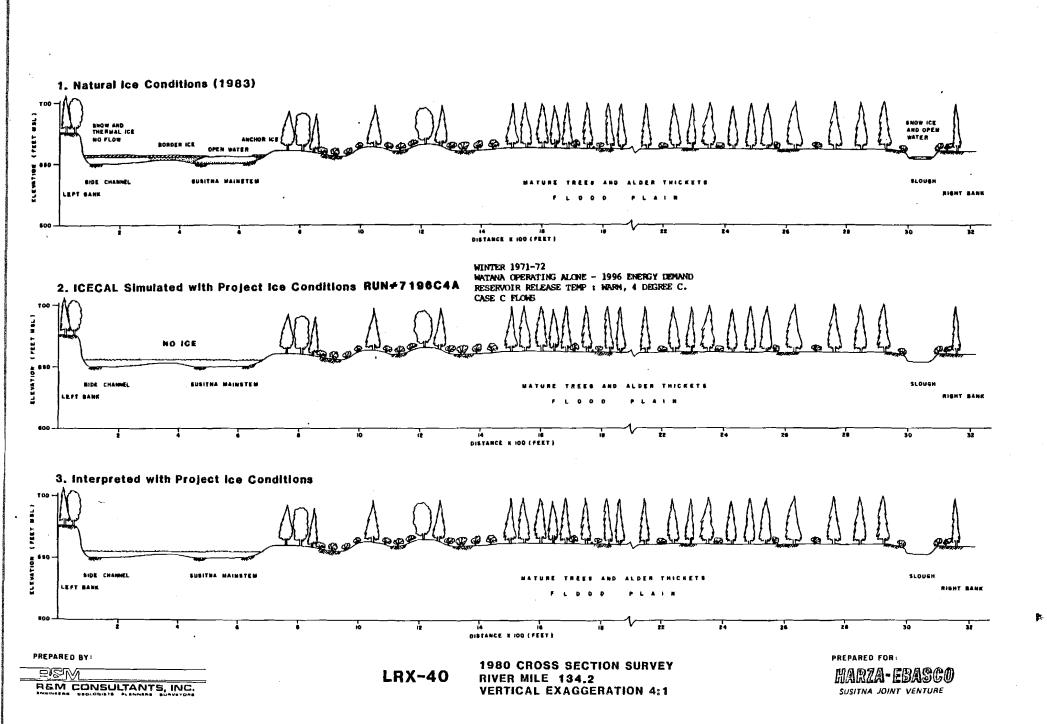
LRX-23

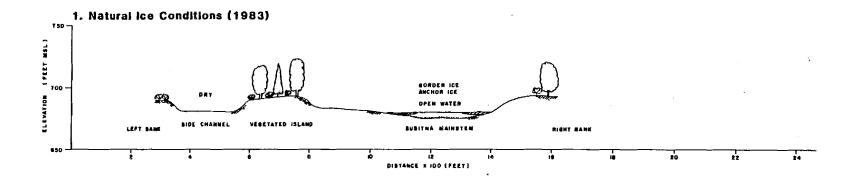
1980 CROSS SECTION SURVEY RIVER MILE 120.2 VERTICAL EXAGGERATION 4:1 PREPARED FOR SUSITIVE SUSITIVE POINT VENTURE

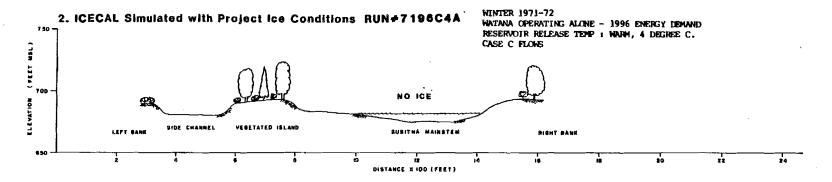


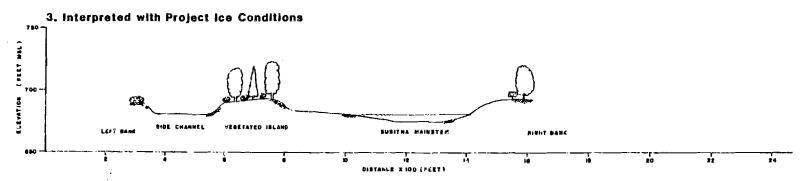












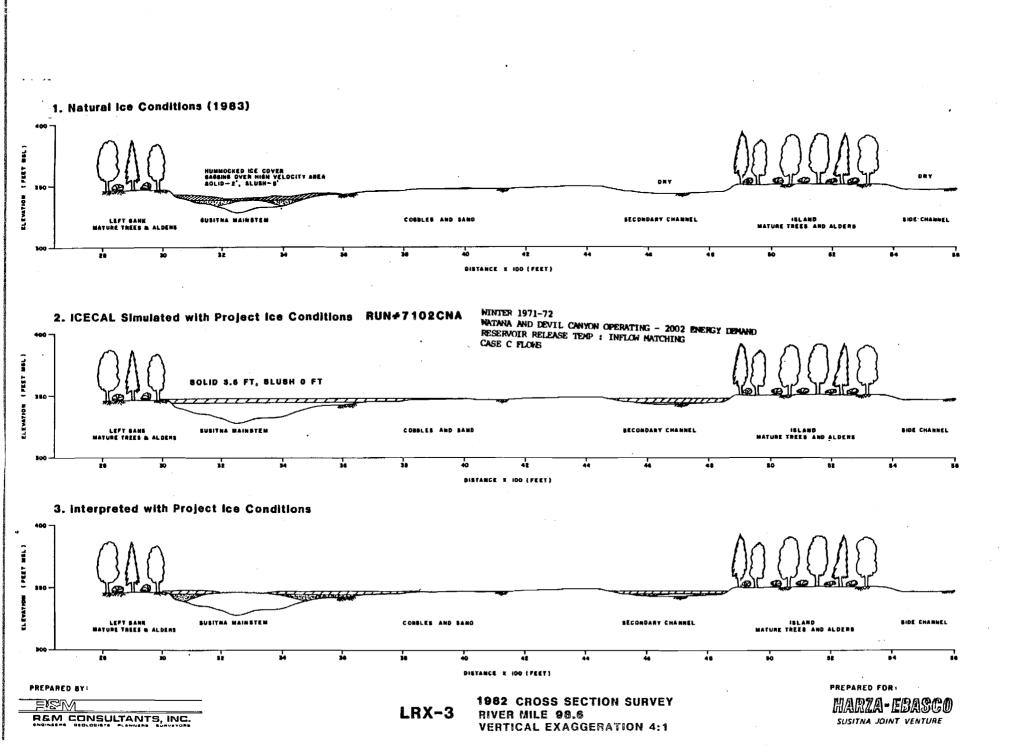
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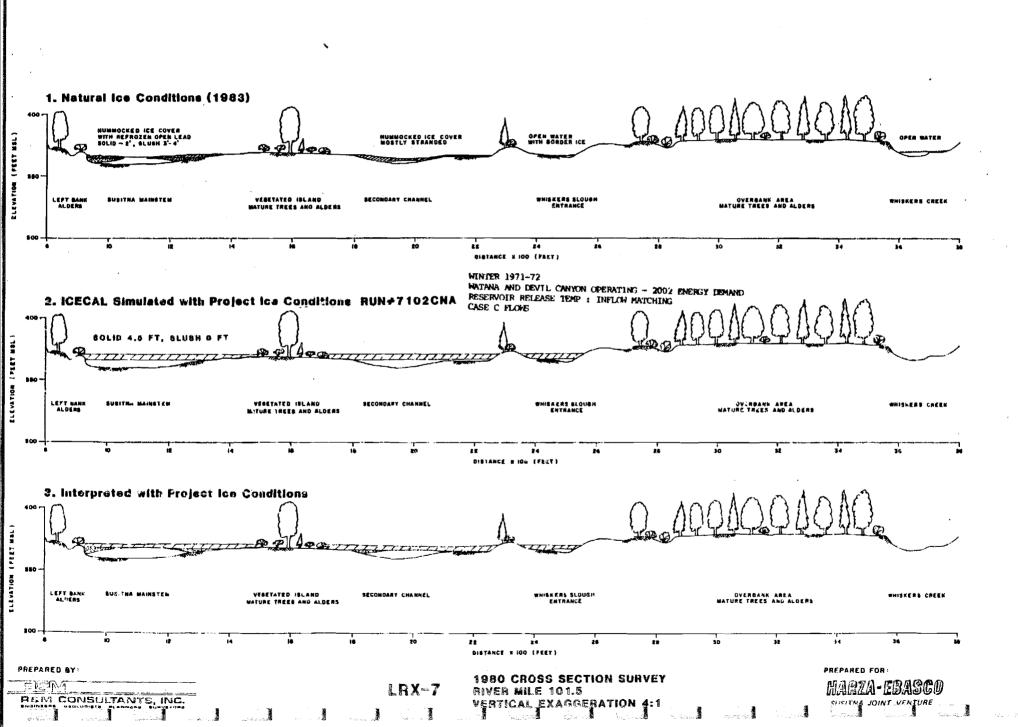
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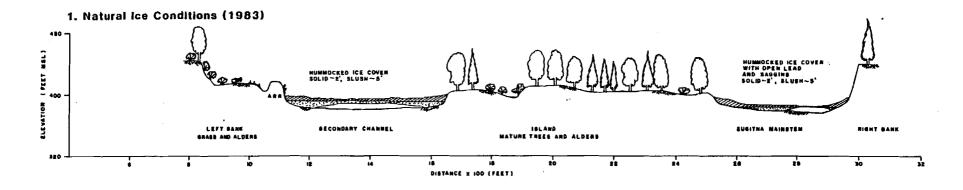
LRX-44

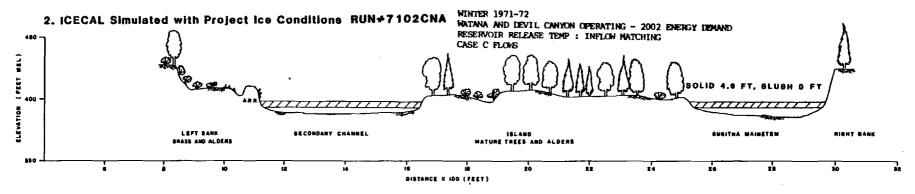
1960 CROSS SECTION SURVEY RIVER MILE 126.4 VERTICAL EXAGGERATION 4:1 HARZA EBASC

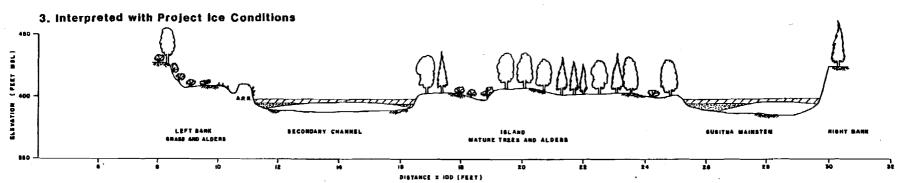
EXHIBIT Y











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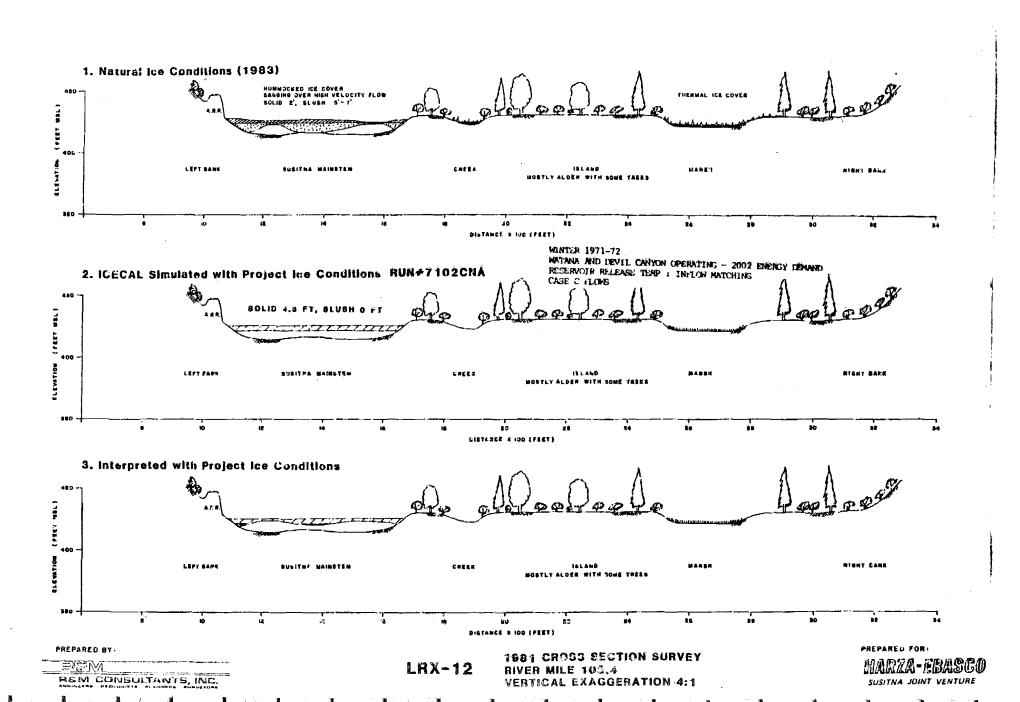
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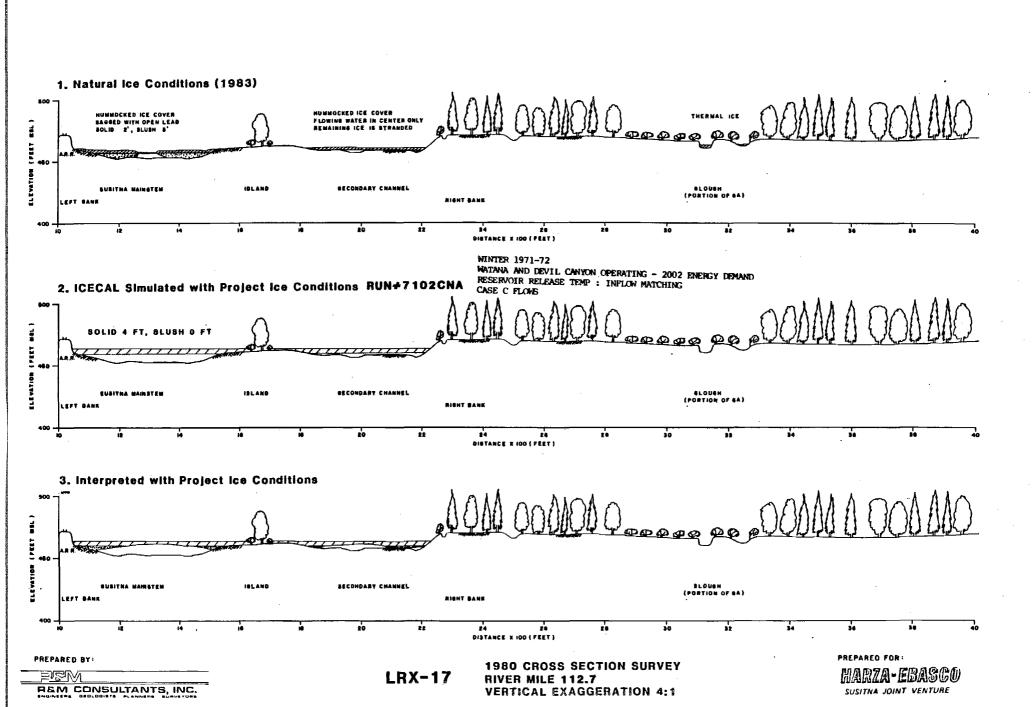
LRX-10

1980 CROSS SECTION SURVEY RIVER MILE 104.8 VERTICAL EXAGGERATION 4:1 PREPARED FOR:

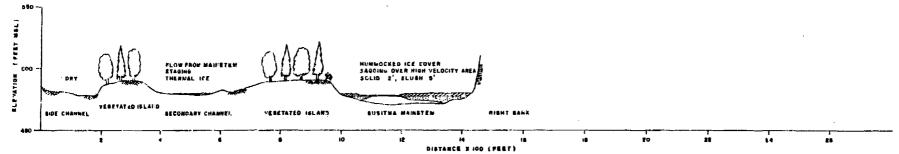
WARZA-EBASGO

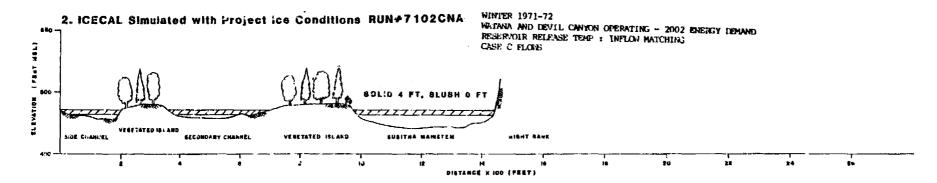
SUSITNA JOINT VENTURE



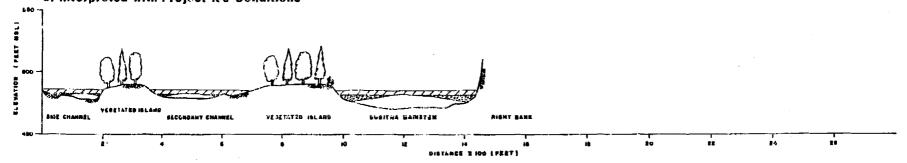








3. Interpreted with Project Ice Conditions



PREPARED BY:

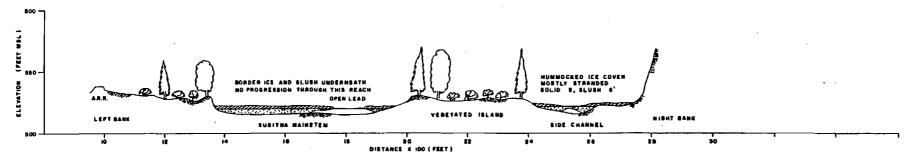
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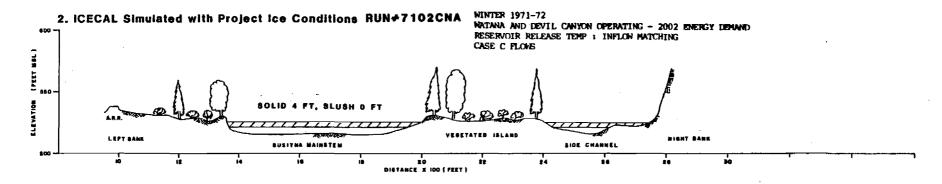
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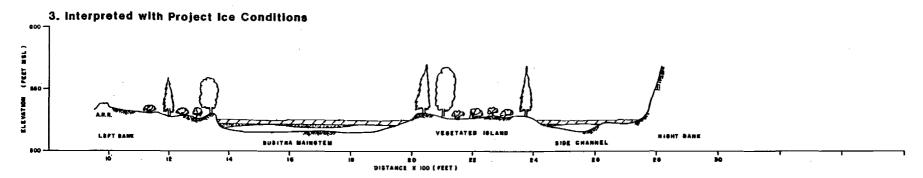
1932 CROSS SECTION SURVEY RIVER MILE 115.1 VERTICAL EXAGGERATION 4:1 PREPARED FOR:

MARZA-EBASCO

1. Natural Ice Conditions (1983)







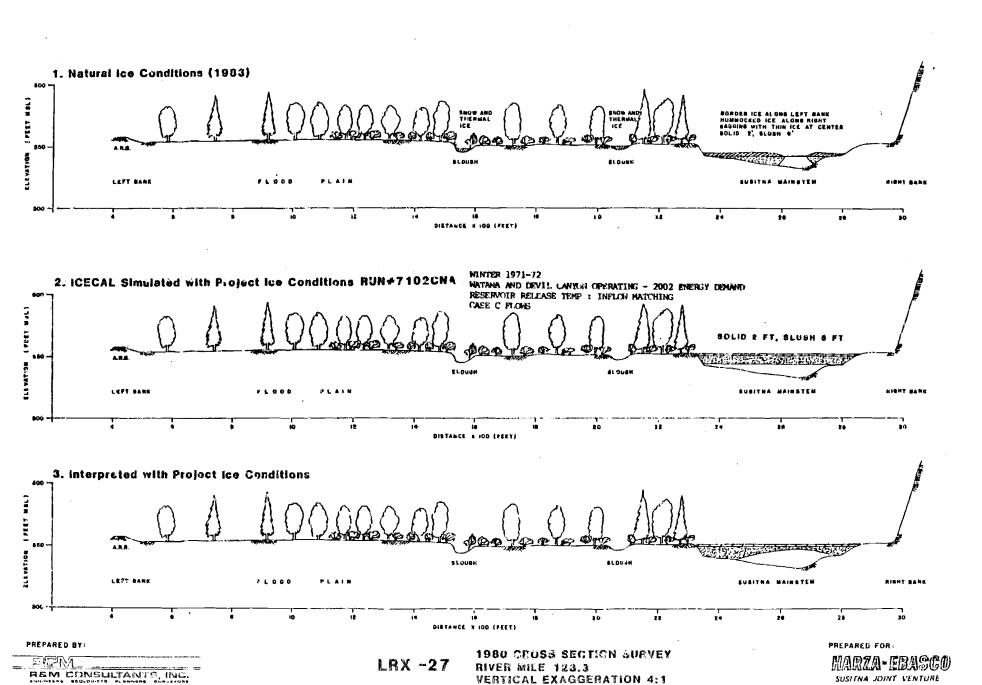
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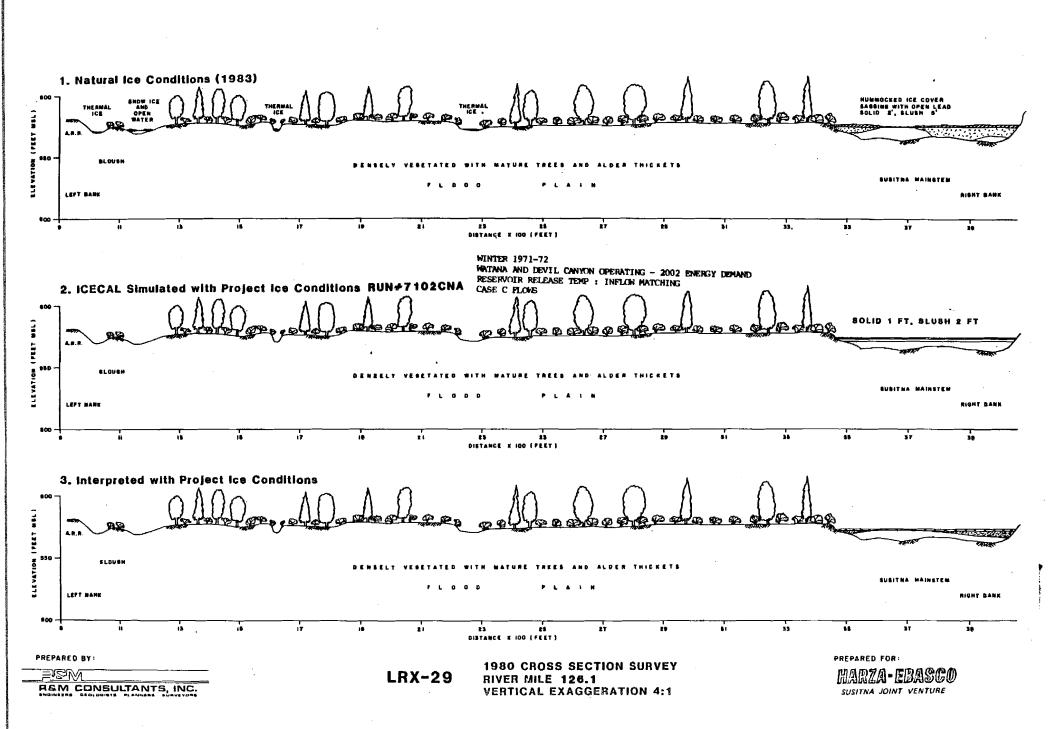
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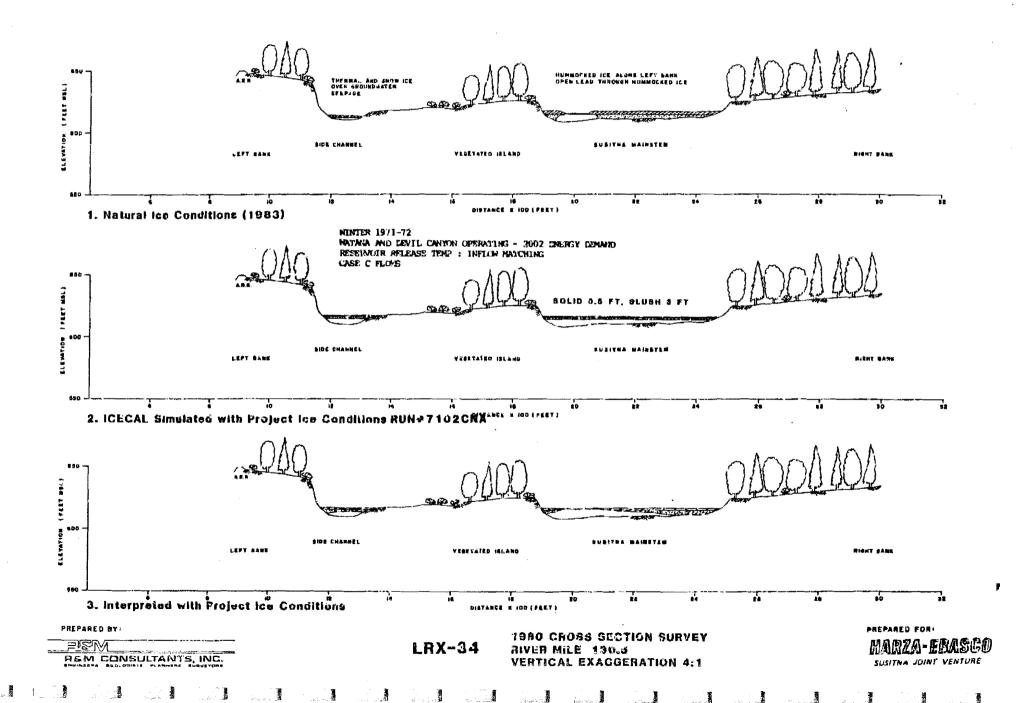
LRX-23

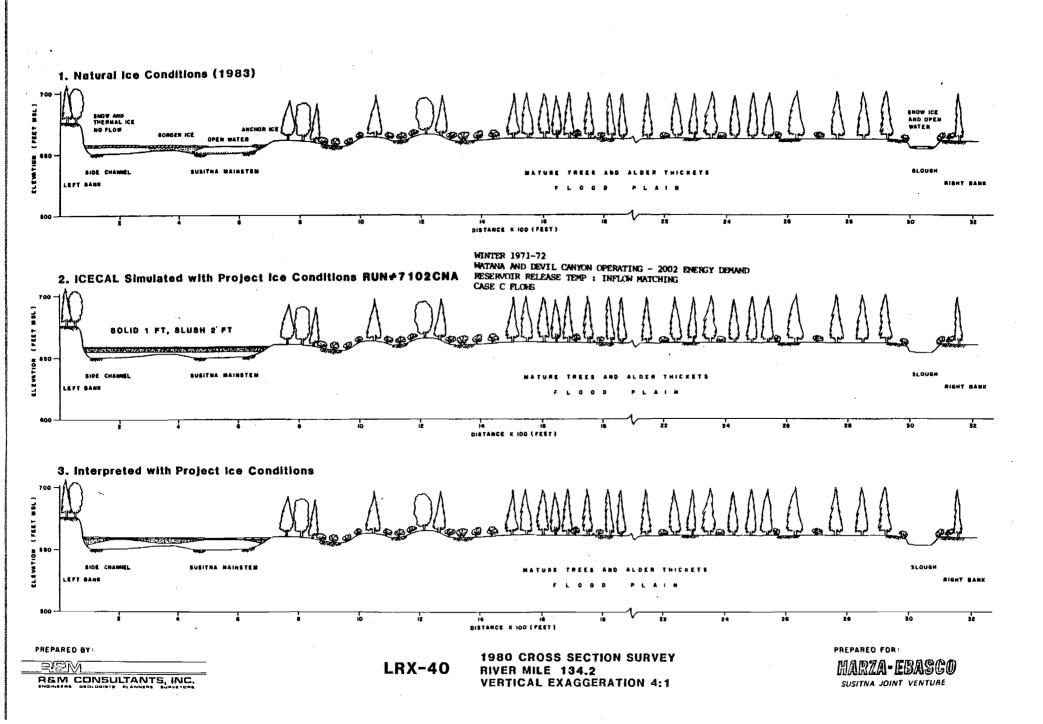
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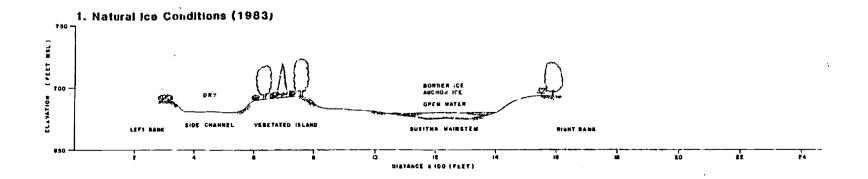
HARZA-EBASCO

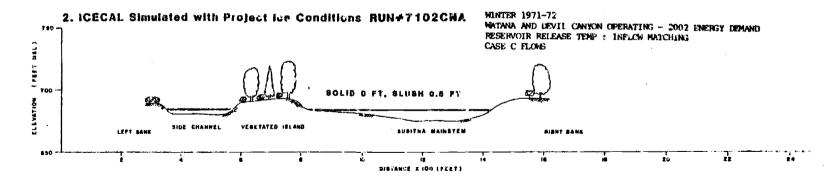


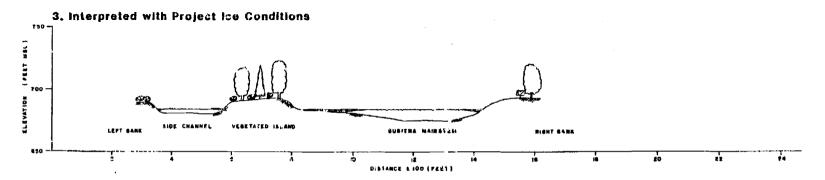












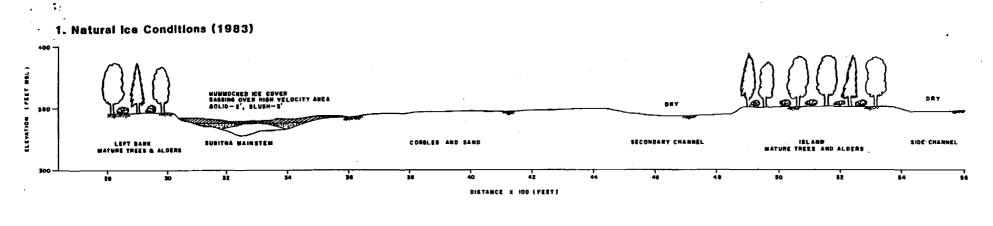
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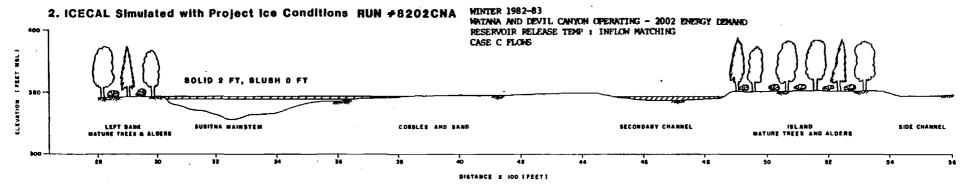
LRX-44

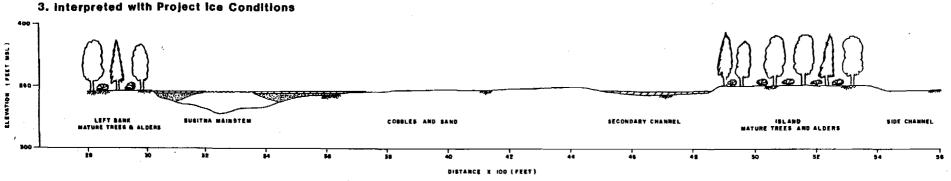
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MARZA-EBASCO
SUSITNA JOINT VENTURE

EXHIBIT Z





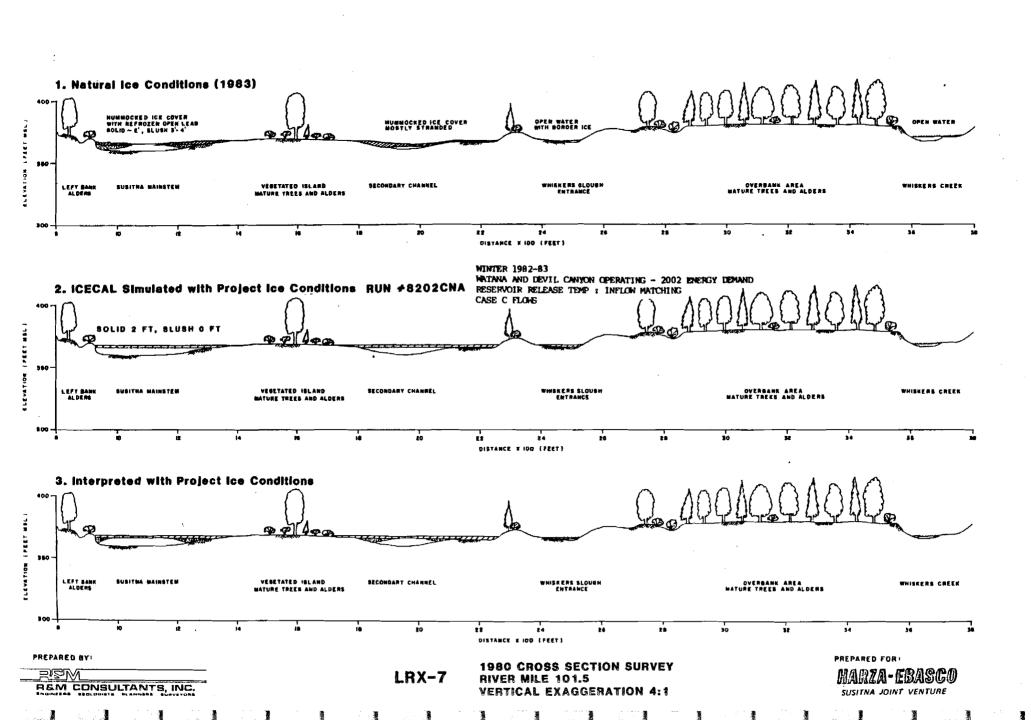


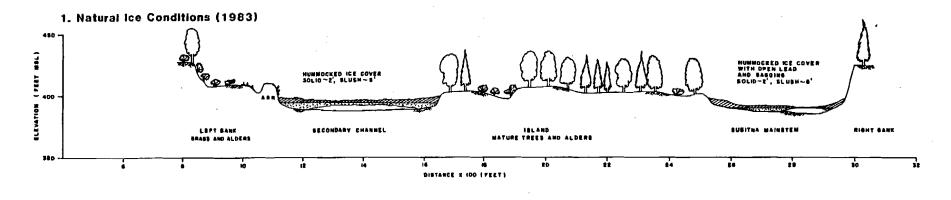
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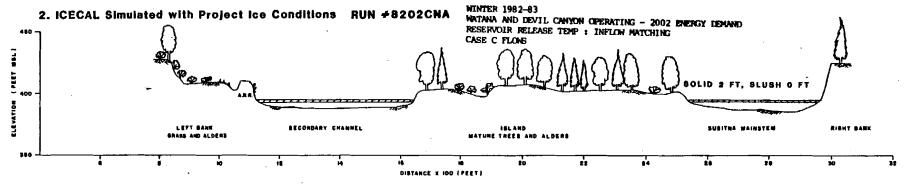
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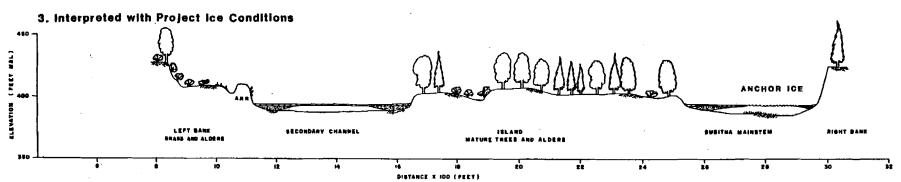
1982 CROSS SECTION SURVEY RIVER MILE 98.6 VERTICAL EXAGGERATION 4:1 PREPARED FOR:

MARZA-EBASCO
SUSITNA JOINT VENTURE









PREPARED BY:

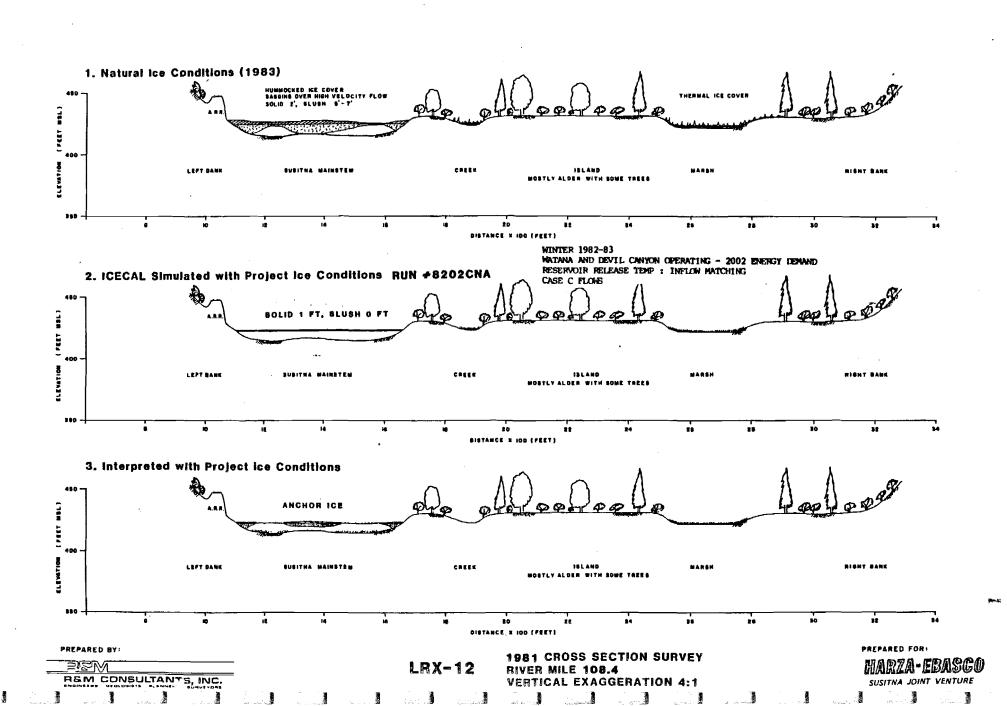
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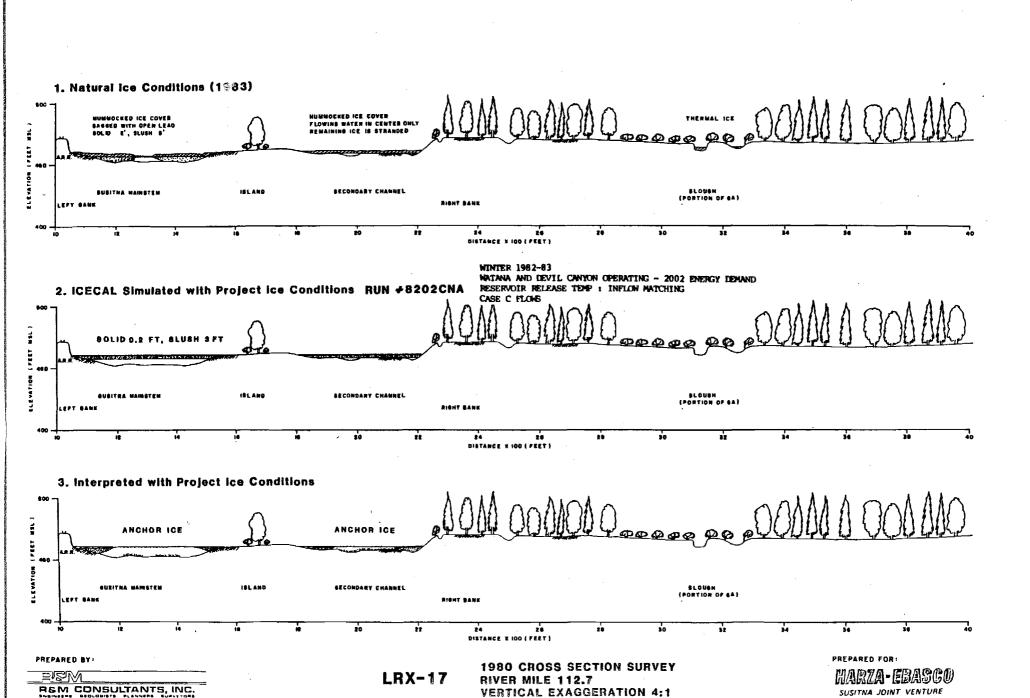
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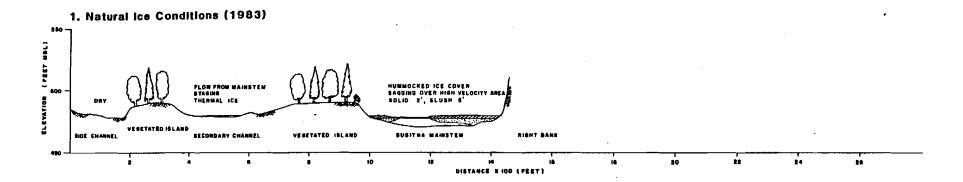
LRX-10

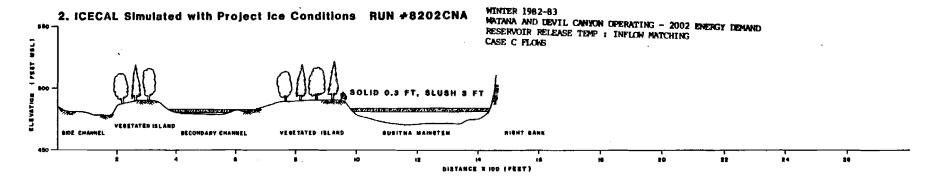
1980 CROSS SECTION SURVEY
RIVER MILE 104.8
VERTICAL EXAGGERATION 4:1

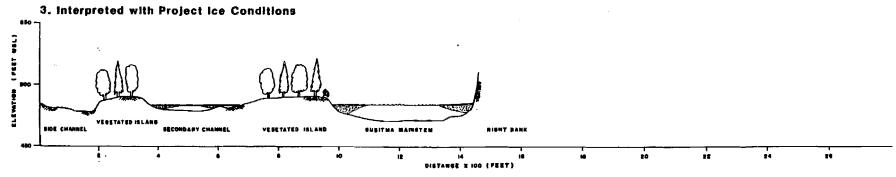
PREPARED FOR:
HARZA-EBASCU
SUSITNA JOINT VENTURE











PREPARED BY:

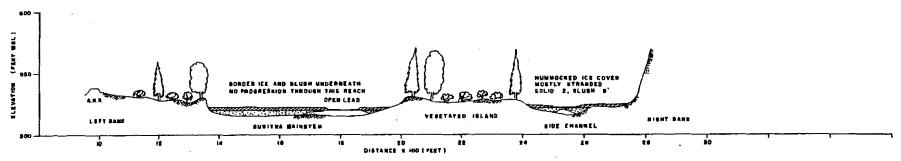
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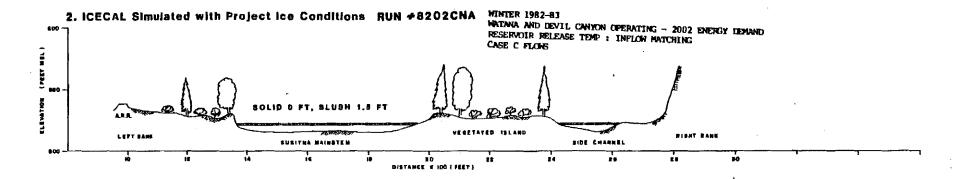
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LRX-18.2 1982 CROSS SECTION SURVEY RIVER MILE 115.1 VERTICAL EXAGGERATION 4:1

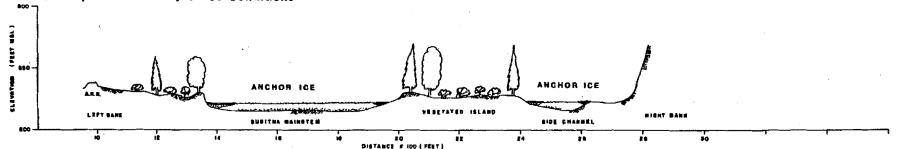
PREPARED FOR:
HARZA-EBASCO
SUSITNA JOINT VENTURE

1. Natural Ice Conditions (1983)









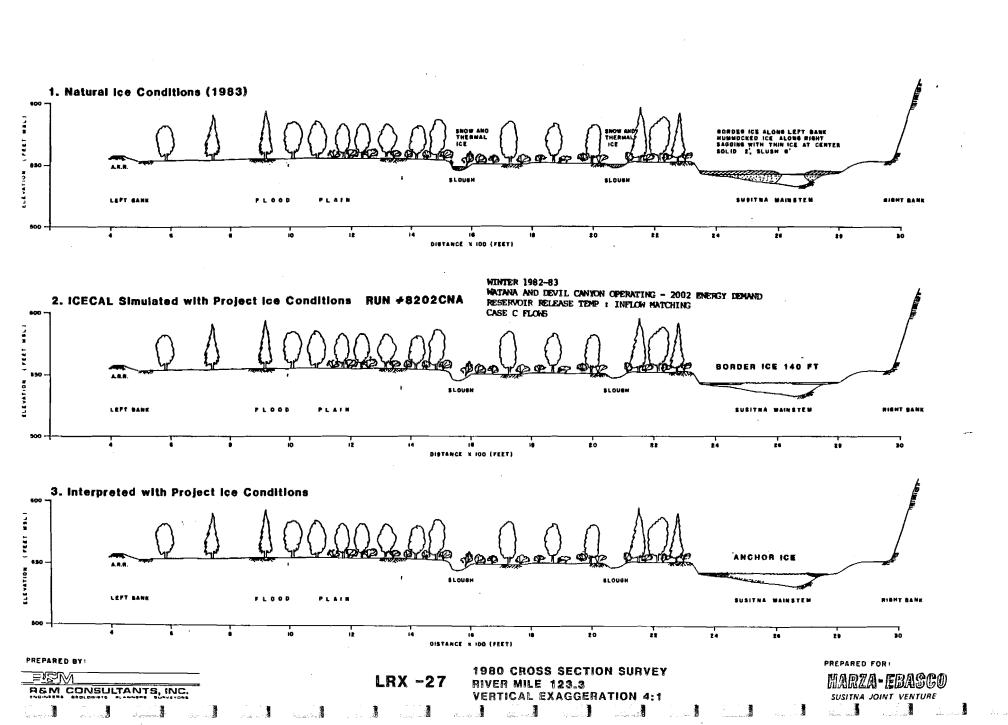
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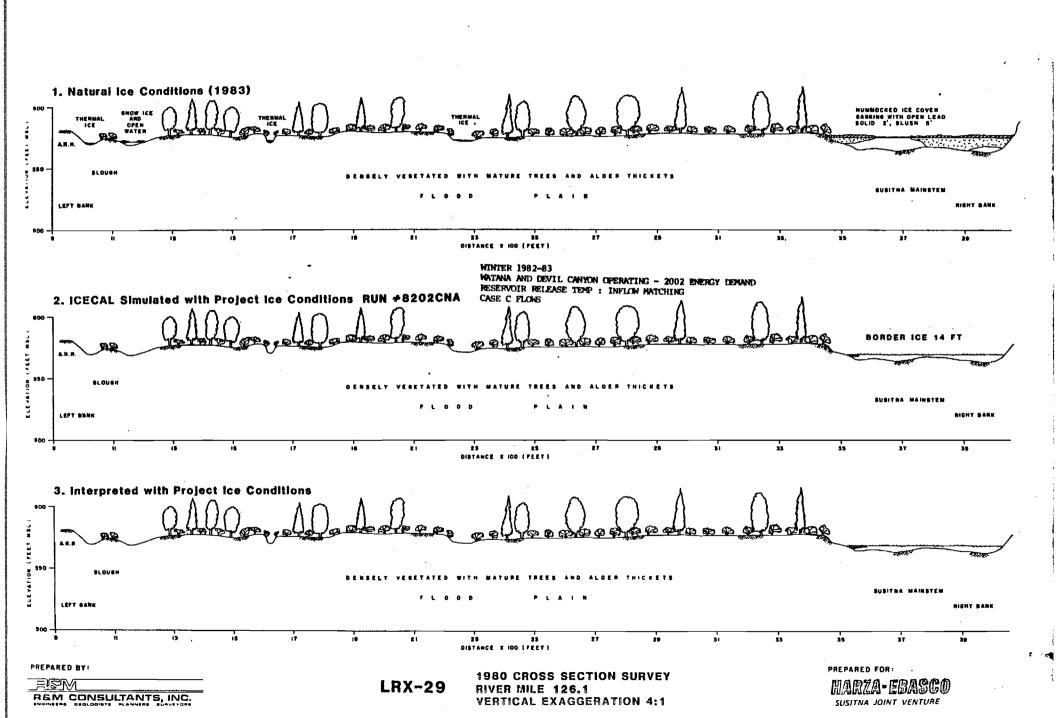
RSM CONSULTANTS, INC.

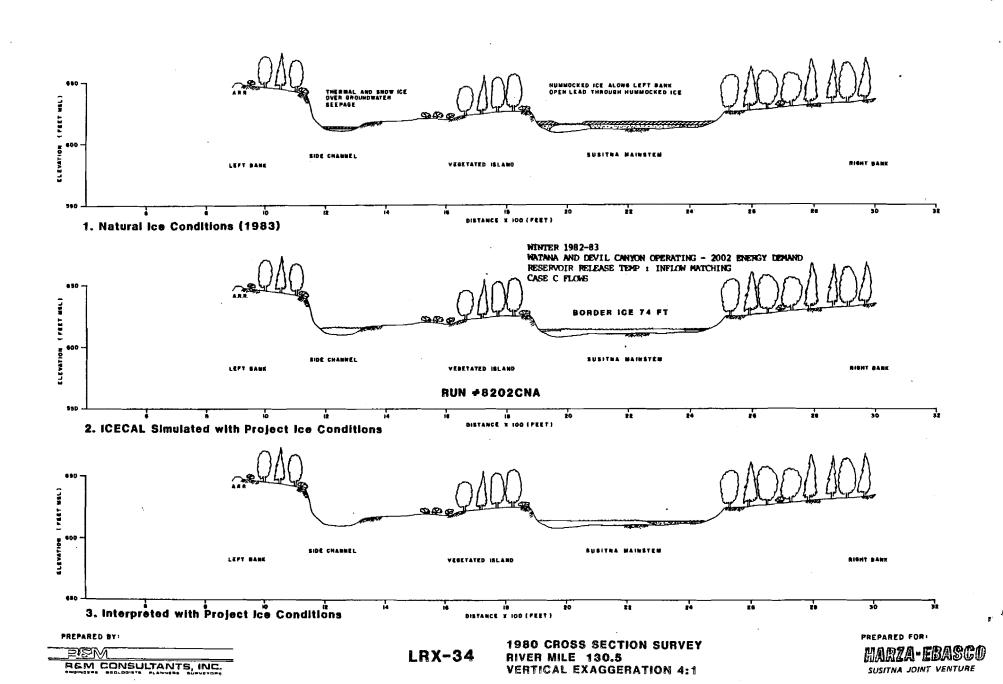
LRX-23

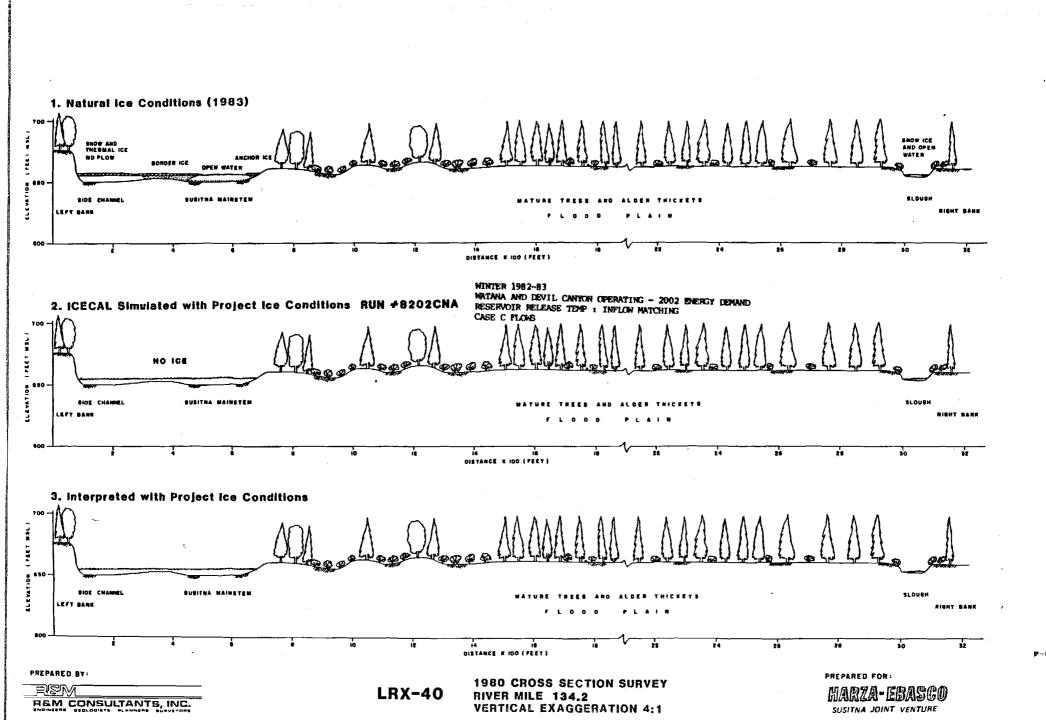
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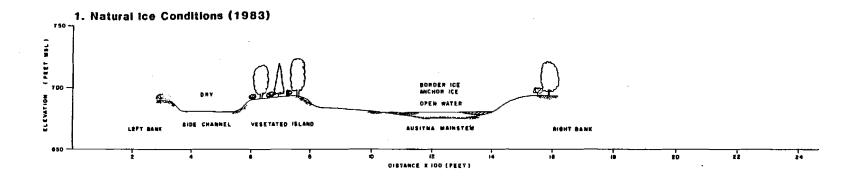
WARZA-EBASGO
SUSITNA JOINT VENTURE

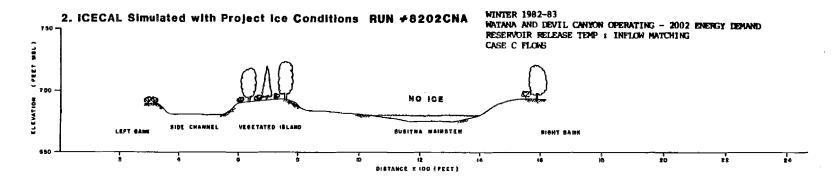


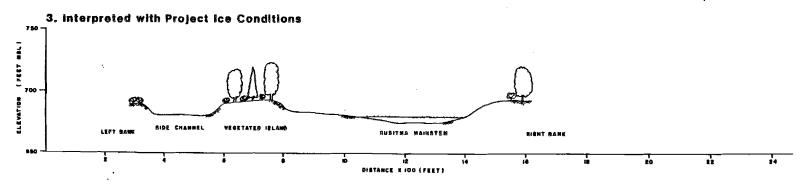












PREPARED BY:

PIEM

PROM CONSULTANTS, INC.

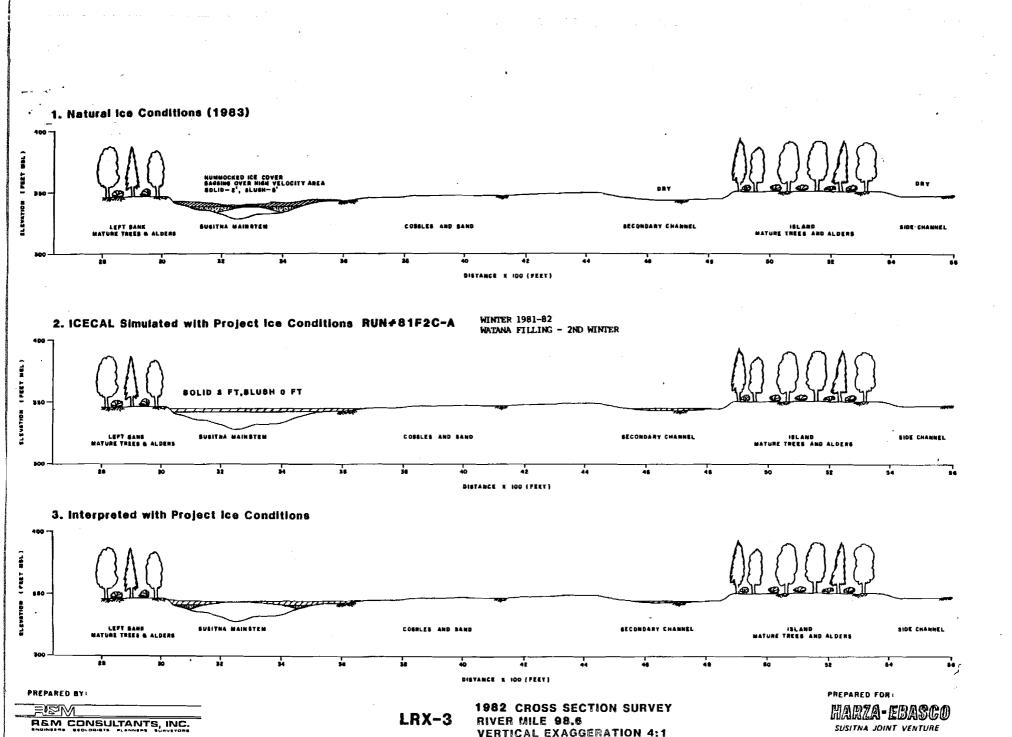
LRX-44 RIV

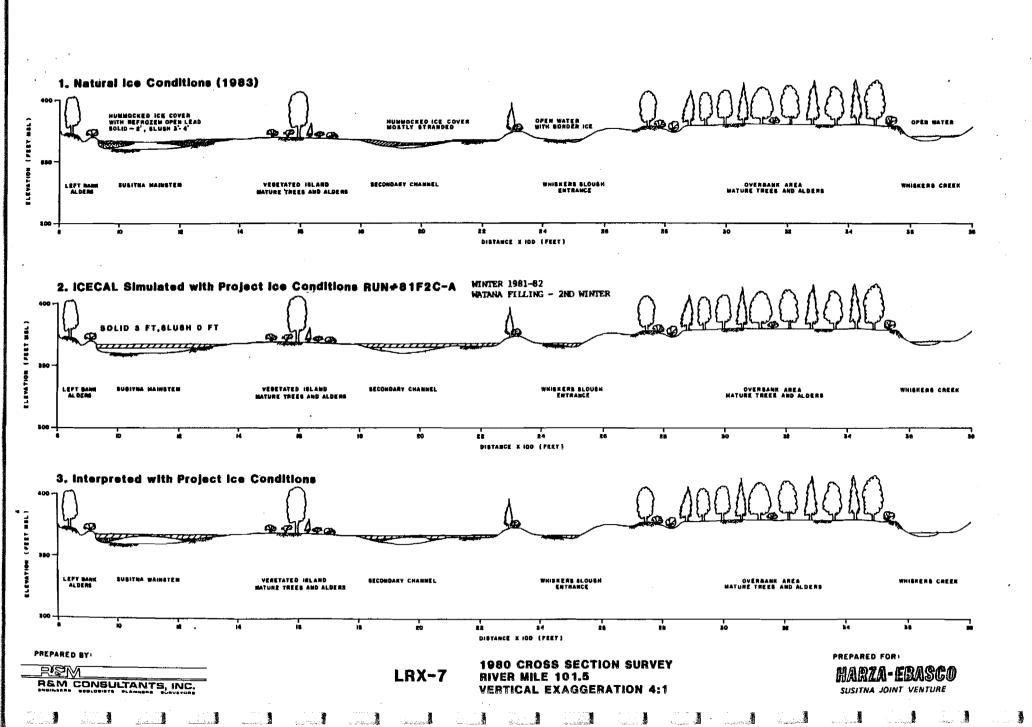
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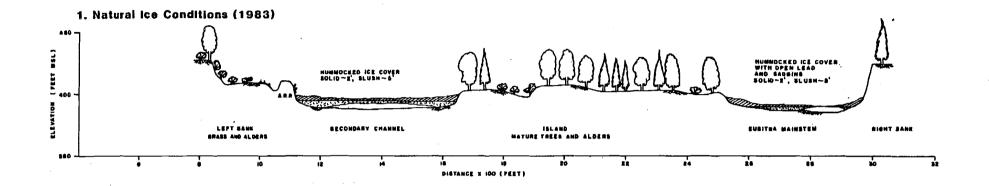
MARZA-EBASCO

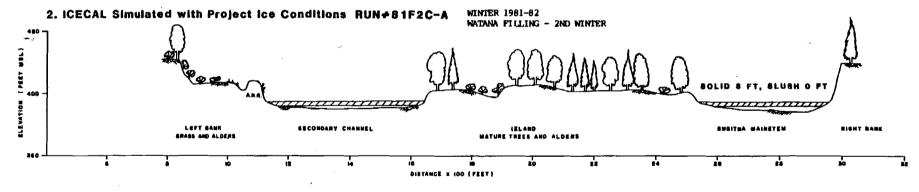
SUSITNA JOINT VENTURE

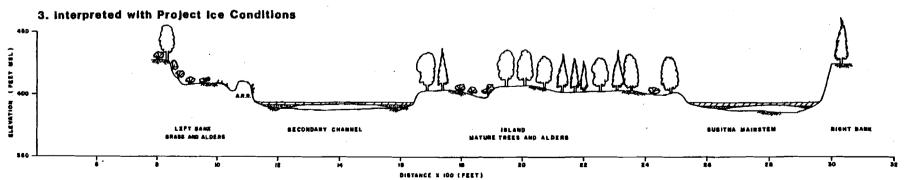
EXHIBIT A1









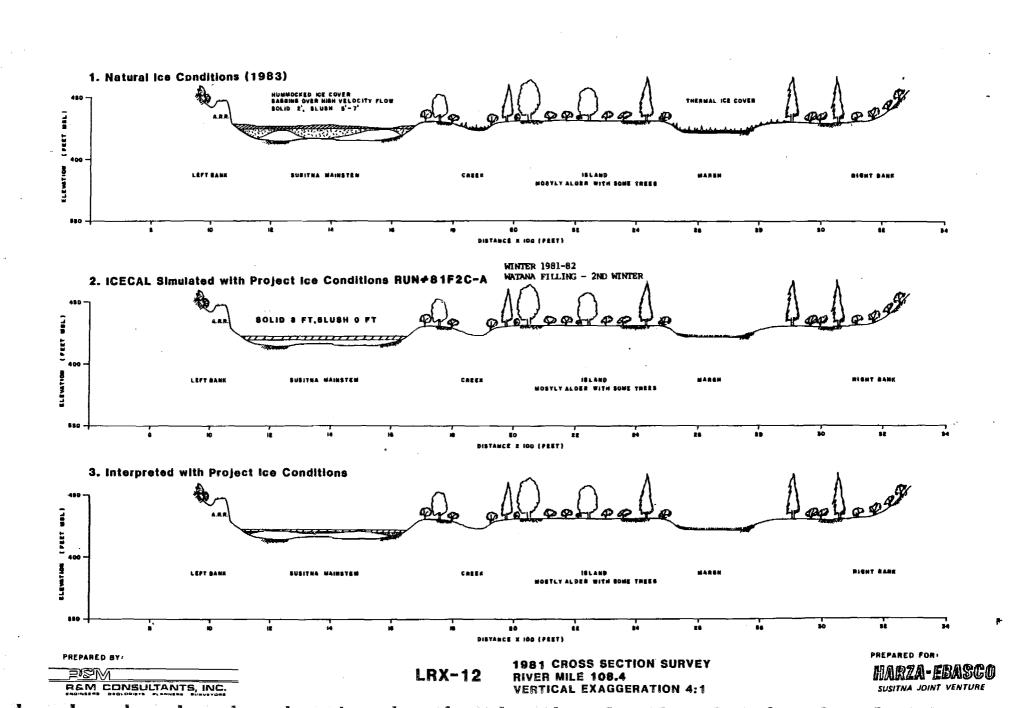


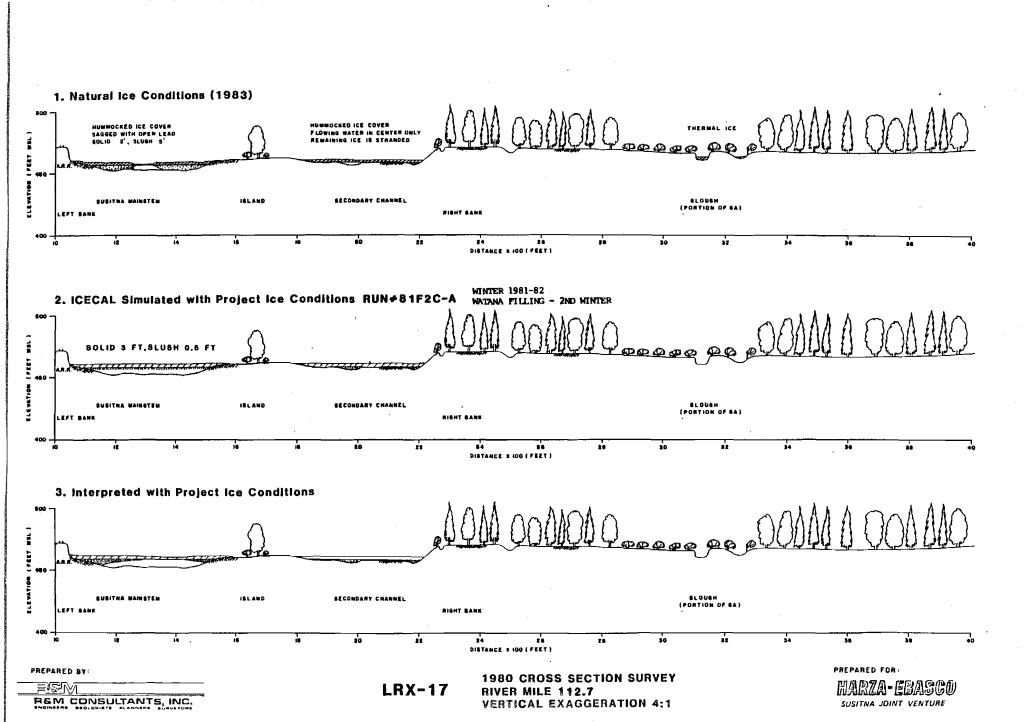
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REM CONSULTANTS, INC.

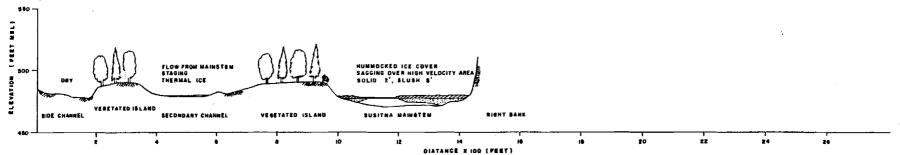
LRX-10

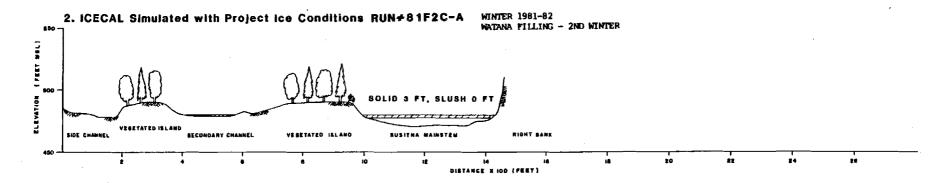
1980 CROSS SECTION SURVEY RIVER MILE 104.8 VERTICAL EXAGGERATION 4:1 PREPARED FOR:
HARZA-EBASCO
SUSITNA JOINT VENTURE



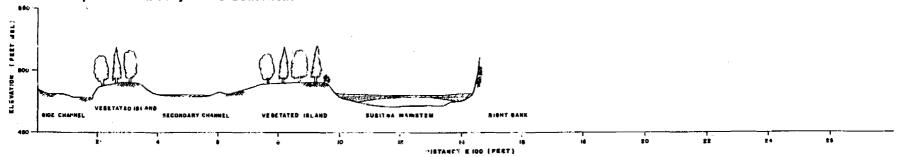








3. Interpreted with Project Ice Conditions



PREPARED BY:

REM CONSULTANTS, INC.

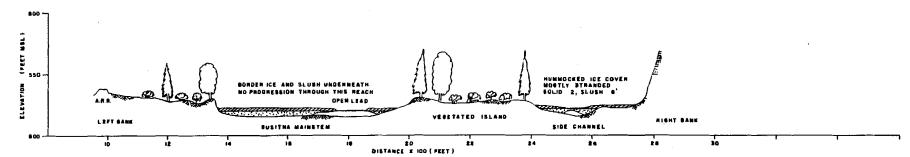
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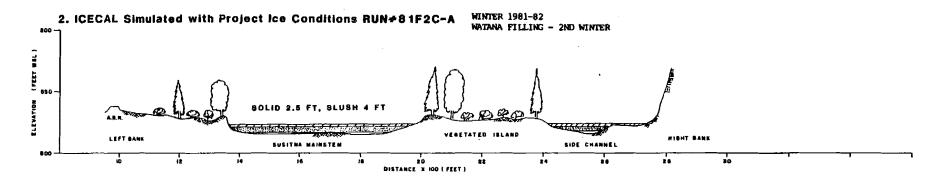
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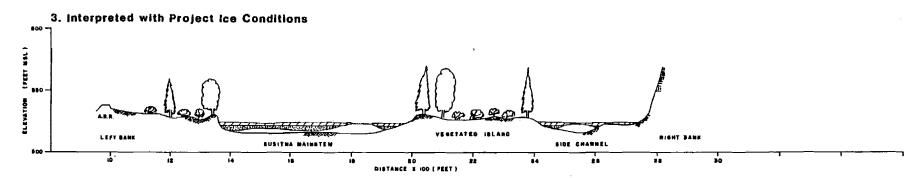
MANZA SHASO

SUSTINA JOINT VENTURE

1. Natural ice Conditions (1983)







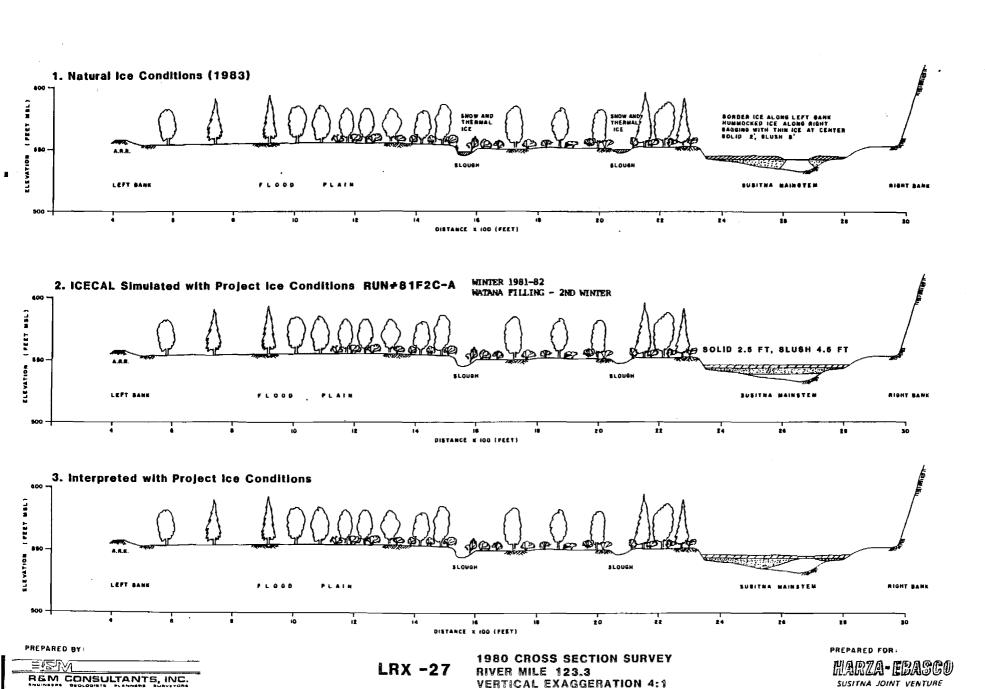
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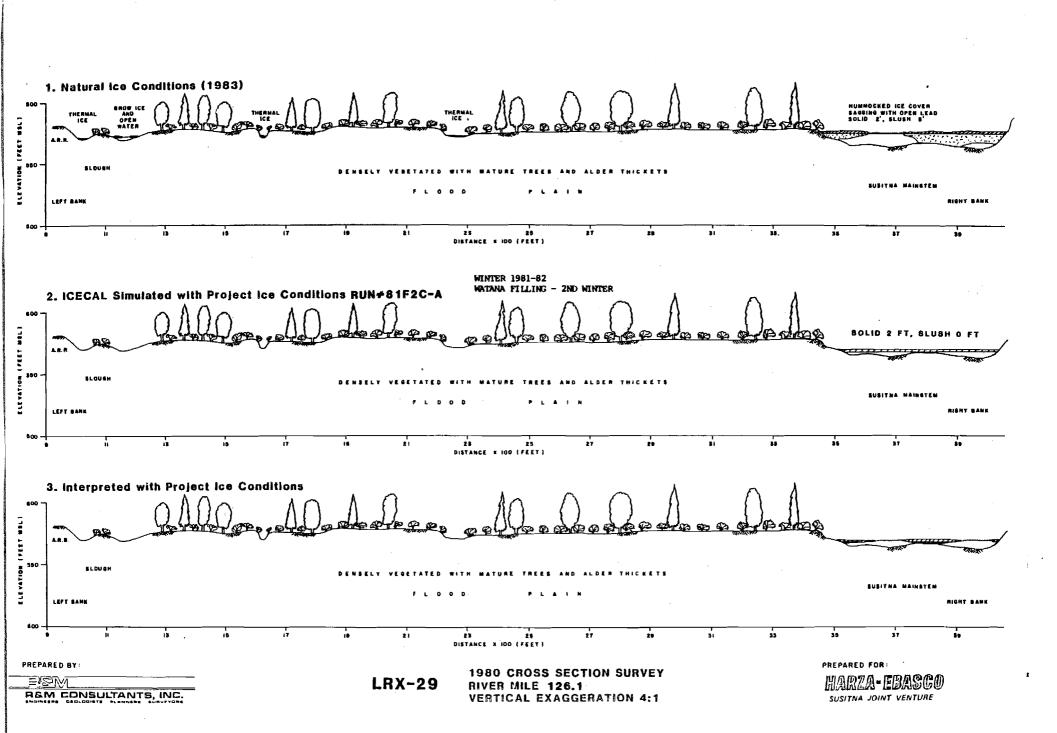
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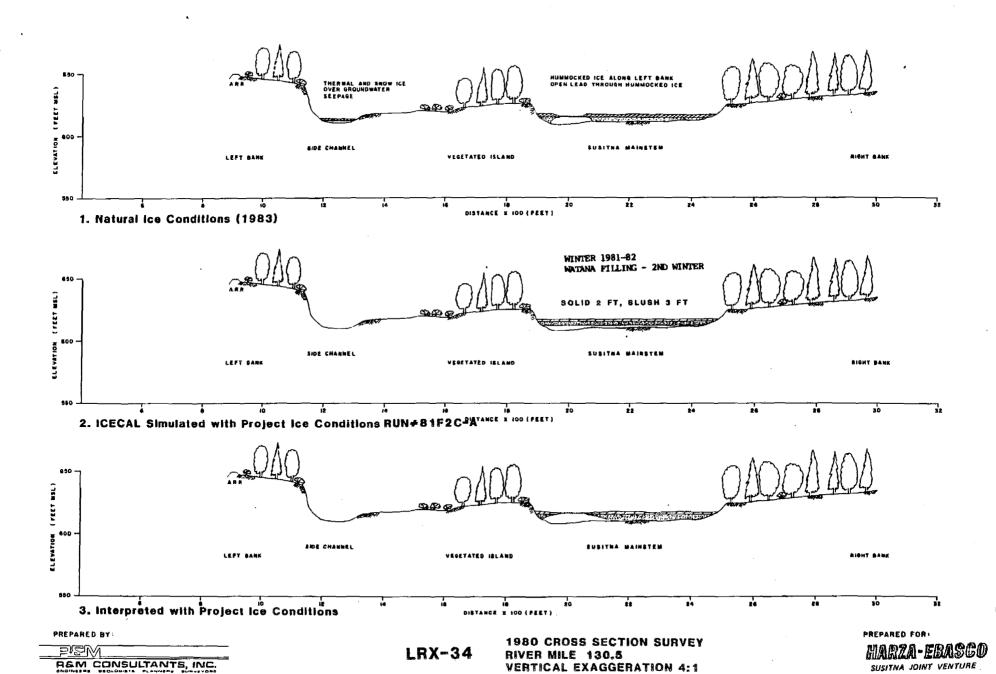
LRX-23

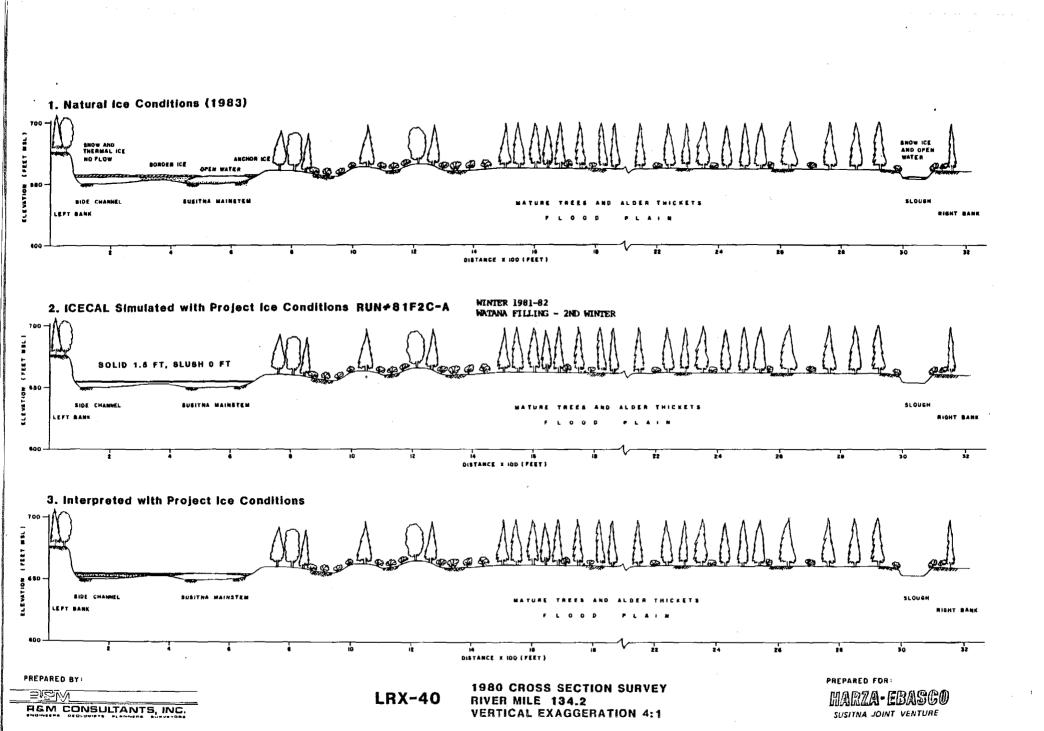
1980 CROSS SECTION SURVEY RIVER MILE 120.2 VERTICAL EXAGGERATION 4:1 PREPARED FOR .

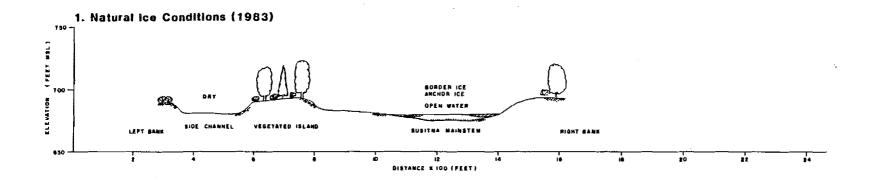
MANZA-EBASCU
SUSITNA JOINT VENTURE

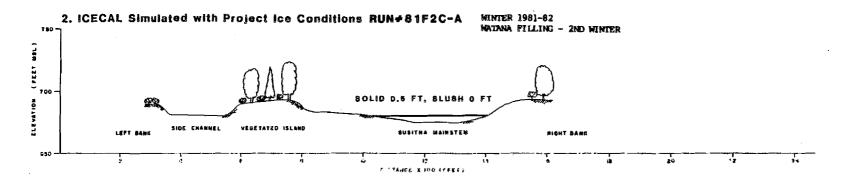


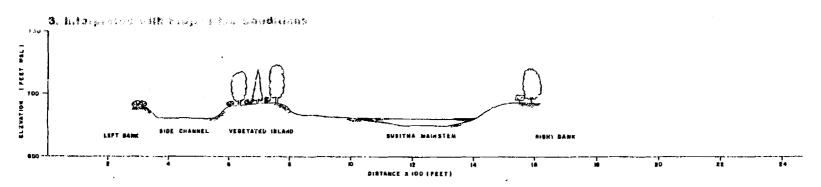












PREPARED BY:

ASM CONSULTANTS, INC.

LRX-44

1980 CROSS SECTION SURVEY RIVER MILE 136.4 VERTICAL EXAGGERATION 4:1 PREPARED FOR SUSITIVA JOINT VENTURE