ALASKA POWER AUTHORITY

SUSITNA HYDROELECTRIC PROJECT

ALC: NO.

NOTES ON STUDY STATUS FOR SUBMISSION TO FERC

APRIL 1981

ACRES AMERICAN INCORPORATED 1000 Liberty Bank Building Main at Court Buffalo, New York 14202 Telephone: (716) 853-7525

TABLE OF CONTENTS

- 1 EXTRACTS FROM PROJECT OVERVIEW REPORT
- 2 PROJECT SCHEDULES

3 - NOTES ON SUSITNA BASIN DEVELOPMENT SELECTION

3.1 - Introduction

3.2 - Evaluation of Susitna Basin Development Plans

3.3 - Comparison of Generation Scenarios

APPENDIX

System Generation Plans - Backup Information and Summary Tables



1. EXTRACTS FROM PROJECT OVERVIEW REPORT

4

1

The Project Overview Report is intended to be a summary of the status of feasibility studies undertaken during 1980. This report is reproduced on the following pages.

ALASKA POWER AUTHORITY

SUSITNA HYDROELECTRIC PROJECT

PROJECT OVERVIEW

0

TABLE OF CONTENTS

				Page
	1	-	INTRODUCTION	• 1
	2	-	THE DECISION PROCESS	. 3
	3	-	ALASKA POWER AUTHORITY	. 3
	4	-	HISTORY OF THE SUSITNA PROJECT	. 4
	5	-	ECONOMIC SCENARIOS AND PARAMETERS	. 6
	6	-	MARKET AREA AND POWER DEMAND FORECASTS	. 7
	7		SUSITNA BASIN STUDIES	. 9
			 7.1 - Hydrology. 7.2 - Site Exploration and Geology. 7.3 - Seismic Considerations. 7.4 - Dam Site Selection. 	9 9 12 12
	8	-	GENERATION EXPANSION PLAN	. 14
	9	-	SUSITNA HYDROELECTRIC DEVELOPMENT	. 16
1	.0		ENVIRONMENTAL PROGRAM	. 23
1	.1	•	ANALYSIS OF SOCIOECONOMIC IMPACTS	. 24
1	.2	-	ECONOMIC FEASIBILITY AND NET ECONOMIC BENEFITS	. 24
1	.3		POWER AND ENERGY MARKETING	25
1	4	**	PUBLIC PARTICIPATION PROGRAM	25
1	.5	-	LICENSING AND PERMITTING PROCEDURES	25
1	.6	-	FINANCIAL FEASIBILITY ANALYSIS.	26
1	.7		SECURITY OF PROJECT COST AND REVENUE STRUCTURES	27
1	.8	- - -	ORGANIZATION AND MANAGEMENT	28
1	Q	-	TMPI TCATTONS OF PROCEENTNO	2.0
			ATH STORETOND OF LUNGEDING	20

PROJECT OVERVIEW

SUSITNA HYDROELECTRIC PROJECT

1 - INTRODUCTION

Acres American Incorporated (Acres) was commissioned by the Alaska Power Authority (Power Authority) on December 19, 1979, to conduct a detailed feasibility study of the Susitna Hydroelectric Project, evaluate the environmental consequences of any proposed development, and prepare a license application to be filed with the Federal Energy Regulatory Commission (FERC) in the event that the State of Alaska regards filing such an application as being in its best interests.

If development ever takes place in the Susitna River Basin (see Figure 1 for a basin map annotated to show potential dam sites), it is likely that extensive, costly and lengthy construction activity will occur there. Benefits of long-term and relatively low-cost electrical energy may be possible. Yet, permanent alteration of the environmental setting in the Basin will be inevitable.

The basis for a decision to proceed with the Susitna Hydroelectric Project requires that a variety of scientific, engineering, financial and economic disciplines be brought together. Investigations and analysis in each of these areas must necessarily be thorough and, further, should be consistent with state-of-the-art techniques. Documentation of these activities tends to be voluminous as well as highly technical in nature. The purpose of this Project Overview is to provide a review of all major aspects of the project and its objectives, determining in principle whether these can be met. In effect, it brings together complex issues and detailed technical results so that decision makers within the State of Alaska and interested members of the public can assess results achieved to date and determine what the future course of action should be with respect to the Susitna Hydroelectric Project.

Succeeding sections are arranged to present the framework within which the Susitna Study is conducted and the preliminary results achieved after the first full year of effort. Section 2 describes the decision process which requires two reports which the Power Authority must make to the Legislature. The nature and the role of the Power Authority are addressed in Section 3. After a brief history of the Susitna Project is presented at Section 4, Sections 5 through 13 consider technical, economic, environmental and marketing aspects. An introduction to the important public participation program follows at Section 14. Licensing and permitting is described in Sections 15. Financial matters, including financial risks, are discussed in Sections 16 and 17. Section 18 describes the organizational arrangements necessary for effective project implementation. A final section (19) reviews the implications of proceeding with the work after the first decision point on March 31, 1981.

A detailed appendix to this overview has been prepared. It contains a complete chapter to correspond to each of the sections appearing herein. Copies of the detailed appendix have been furnished to the Power Authority and to its external review panel.



In addition to this project overview, a second major document bears upon the March 31, 1981, decision process. The Development Selection Report (some of which is encapsulated in Sections 7, 8 and 9 below) provides the detailed basis upon which a recommendation has been made by Acres to APA regarding the proposed site on which the 1981 program will focus.

2 - THE DECISION PROCESS

Two important decision points have been designated by HCSSB 294. This legislation requires that the Power Authority, by March 30, 1981, submit a preliminary report to the Governor and to the State Legislature "recommending whether work should continue on the project." A second decision point, also explicitly legislated, occurs in April 1982, when the Power Authority must submit a second report recommending whether work should continue on the Susitna Hydroelectric Project and other viable alternatives. It is important to note that neither of these decision points is intended to produce a commitment to construct a project. Indeed, construction of dams and other facilities in the river channel is not possible until or unless an FERC license is awarded.

In addition to work being accomplished by the Acres team, several other ongoing activities bear upon the decision making process. A separate comprehensive study of alternative means of satisfying future Railbelt energy and load projections will be accomplished by an independent consulting firm under contract to the State of Alaska. The Susitna project will represent one of many possible alternatives considered in that effort. Other alternatives include, but are not necessarily limited to, thermal energy (particularly coal fired, since Alaska is richly endowed with significant undeveloped coal resources), wind, solar, non-Susitna hydropower, and tidal power (for which a preliminary assessment of potentials and constraints is now underway). In addition, the Power Authority has contracted with a major consulting firm specializing in electrical transmission to consider an intertie between Anchorage and Fairbanks. This latter project may be beneficial irrespective of whether the Susitna River Basin is ever developed, but the results of the study will necessarily be important to the analysis of transmission facilities required for a Susitna Project.

3 - ALASKA POWER AUTHORITY

The Power Authority was created in 1976, by action of the State Legislature, as an autonomous branch of the Alaska Department of Commerce and Economic Development. The basic mission of this agency is to develop energy generation projects (excluding nuclear) in an economical manner. Governed by a Board of Directors, the Power Authority employs an Executive Director and a staff which carry out day-to-day activities. Directors of Engineering, Finance, and Public Participation assist the Executive Director in performing his functions. The staff also includes a full-time Native Inspector, an Administrative Assistant, and Project Engineers and other supporting personnel. An organization chart is provided as Figure 2.

As of the end of 1980, the Power Authority was engaged in six reconnaissance studies, four design projects, two license application submittals, five construction projects, and eleven feasibility studies (Susitna being the largest).

Procedures adopted by the Power Authority for the Susitna study include the formation of a Steering Committee to ensure that interested State and Federal Agencies are kept informed throughout the course of the work and to provide a vehicle whereby their concerns and recommendations can be taken into account as the study progresses. Heavy emphasis is also placed on the opinions and concerns of the public, and an aggressive Public Participation Program is conducted.

4 - HISTORY OF THE SUSITNA PROJECT

Because of its strategic location between Anchorage and Fairbanks, the Susitna River has long been regarded as worthy of consideration for development of its hydroelectric potential. Shortly after World War II, the U.S. Bureau of Reclamation (USBR) did an initial Territory-wide reconnaissance, noting the vast hydroelectric potential in Alaska, and placing particular emphasis upon the perceived advantages of a Susitna Hydroelectric Project.

The U.S. Department of Interior (of which USBR was a part) undertook geotechnical and other field investigations and, in 1961, proposed authorization of a two-dam system on the Susitna River. This report was later updated in 1974 by the Alaska Power Administration (also then a part of DOI) and the desirability of proceeding with the project was reaffirmed.

The U.S. Army Corps of Engineers (COE) was also active in hydropower investigations in Alaska in the 1950's and 1960's. Focusing its initial attention on the Rampart Project on the Yukon River, the COE found by the early 1970's that the environmental consequences and limited market for Rampart power militated against its development. The 1973 energy crisis rekindled interest in hydropower development and the COE was commissioned by the U.S. Congress in 1974 to conduct a pre-feasibility study of the Susitna Project. The results of this effort were first referred to the Office of Management and Budget in 1976. Further geotechnical work followed and a new COE report was issued in 1979.

The State of Alaska itself commissioned an assessment of the Susitna Project by the Henry J. Kaiser Company in 1974.

Although differences appeared in the various proposed development schemes, all of the foregoing organizations were unanimous in recommending that Susitna hydroelectric potential be developed.

After the Power Authority was formed, the State of Alaska elected to proceed independently with a major feasibility study. A detailed Plan of Study was distributed widely in February 1980. Subsequent modifications, some of which



ALASKA POWER AUTHORITY ORGANIZATION

and the state of the state

FIGURE 2

were occasioned by statements of public concerns, were directed by the Power Authority itself as well as by the State Legislature. Salient features of the Plan as it now stands are these:

- The development of electrical energy demand forecasts has been accomplished independently by the Institute for Social and Economic Research (ISER), University of Alaska.
- The study of alternatives, as noted earlier, is being accomplished separately from the Susitna Study.
- The Public Participation Program is handled by the Power Authority itself rather than by Acres as originally proposed.
- Major tasks have been designated to handle each facet of the work. These tasks include such activities as load forecasting, surveys and field support activities, hydrology, seismic studies, geotechnical investigations, design studies, environmental studies, transmission studies, development of cost estimates and schedules, licensing activities, finance and marketing studies, public participation and administration. Each task is further subdivided into subtasks so that more than 150 separately defined study activities will be completed prior to submitting a license application to FERC in June 1982--if affirmative decisions are made at the March 1981 and April 1982 milestones.

5 - ECONOMIC SCENARIOS AND PARAMETERS

The viability of a Susitna Hydroelectric Project depends to a great extent on the costs of generating electrical energy by alternative means. Thus, for example, if the cost of natural gas from the Cook Inlet area rises more rapidly in future years than the general inflation rate, it is likely that utilities will turn to sources other than gas for future expansion of generating systems. Hydropower might then enjoy a more favorable position. Conversely, if certain fuel prices rise less rapidly than the general inflation rate, hydropower may not necessarily represent an economical choice for future system expansion.

Other factors will also affect Susitna viability. For example, demographic variables, energy demand, unit labor costs, other commodity prices, overall price inflation, and interest and discount rates must be projected. An economic analysis was conducted so that, to the extent possible, logical and non-contradictory views of the world would emerge. No matter how carefully such an analysis is conducted, however, it is necessarily imprecise simply because it depends upon the prediction of an uncertain future. Thus a range of values bounding each selected parameter was selected as the basis for testing the sensitivity of a Susitna Project to possible deviations from most likely values.

Forecasts of world energy balances indicate a worldwide shortfall in oil supplies within ten years. By 1990, the United States is expected to be importing 16 percent of its energy needs (an improvement over the 22 percent level of 1978). It is likely that fossil fuel prices in the U.S. will continue

to escalate at rates on the order of two to four percent above the overall inflation rate. Gas and oil price escalation will be at the upper end of this range, with coal escalation somewhat less. Fuel prices in Alaska will generally reflect market prices in the United States and abroad, less the cost of getting Alaskan fuels to the market.

Insofar as prospects for economic growth in Alaska are concerned, three different economic scenarios were developed by ISER. The lowest assumes only modest population and employment growths at just over two percent. The highest forecasts these values at closer to four percent. If the volume of State government expenditures varies significantly from current levels, these ranges will be broadened.

Opportunity values and escalation rates in Alaska in dollars per million Btu (where a Btu is a unit of energy) were selected as follows:

	<pre>\$/Million Btu Opportunity Value (1980 Dollars)</pre>	1980 - 2005 Escalation in Excess of Normal Inflation	
Natural Gas	\$2.00	3.98%	
Coal	\$1.15	2.93%	
Oil	\$4.00	3.58%	

Exclusive of inflation, a real interest and discount rate of three percent was adopted as most likely.

6 - MARKET AREA AND POWER DEMAND FORECASTS

ā

The forecasting methodology employed by ISER relied upon an end-use model rather than on the extrapolation of past trends as the basis for projecting future demand. As its name implies, an end-use model considers electricity consumption in terms of end use in various sectors of the economy. In the residential sector, for example, electricity consumption is largely attributed to space heating, refrigerators, water heaters, lights, cooking ranges, and certain other major appliances. Knowledge of the number, type, and expected changes in households can lead to assessment of future residential demand for electricity.

The annual growth in total Railbelt Utility Sales ranged from 2.8 percent to 6.1 percent in the lowest and highest economic growth scenarios respectively. These values may be compared to an actual average annual rate of 15.2 percent for the period 1940 to 1978 and to 11.7 percent for the 1970's. Figure 3 illustrates alternate demand forecasts.

Peak load forecasts were derived by applying historical load patterns by sector to the ISER demand forecasts. Peak loads are expected to increase at approximately the same percentage as total electrical energy demand for each of the selected ranges.



ALTERNATIVE UTILITY SALES FORECASTS

FIGURE 3

If more extreme measures are taken (probably through legislative action rather than voluntary efforts), some potential for further energy conservation and for load management could lead to a lower forecast than the lowest noted above. An extreme low forecast was selected for sensitivity tests in later analysis.

7 - SUSITNA BASIN STUDIES

During the past year, a massive field data collection effort got underway. Operating primarily out of a base camp constructed at the Watana site, investigative teams were engaged in environmental data collection, survey activities, geotechnical exploration, geological mapping, seismological investigations and hydrological and climatological data collection.

7.1 - Hydrology

Gaging stations and weather monitoring stations were added to the network which had been installed and operated by State and Federal agencies in prior years. Information collected at new stations has been useful in correlating data obtained there with longer term records at older stations.

The Susitna River exhibits two distinct seasons of flow. High spring and summer flows (produced by snow and glacial melt and heavy rainfall) contribute about 90 percent of the annual total between May and October. The winter flow is relatively low and most of the smaller tributaries do not sustain flow during the coldest months. Figure 4 illustrates flow data at Gold Creek. Based on data collected to date, initial determinations have been made of probable maximum floods (the theoretical maximum which could be produced given the physical nature of the Susitna Basin) and design floods (1 in 10,000 year events) which must be safely passed by dams that might be constructed on the Susitna. In addition, of course, hydrological data was used to estimate probable average and firm energy outputs from potential developments. It is worth noting that less than 20 percent of the total Susitna River flow into Cook Inlet is contributed by the Susitna and its tributaries above Gold Creek. Significant contributions downstream occur from the Chulitna, Talkeetna, and Yentna Rivers. Figure 5 displays percentage composition of total flow by major tributary.

Ice formation, both in potential reservoirs and downstream of possible dams, continues to be studied, for it must be dealt with during construction and its impacts during operation must be determined.

7.2 - Site Exploration and Geology

The Susitna Basin has a complex geology. Studies have been made of the region in general and detailed information was collected at particular dam sites and potential sites (borrow areas) for materials with which to construct the project. Three core holes per site were drilled at Watana and Devil Canyon during 1980; 15 auger holes were placed to explore borrow



FIGURE 4

FIGURE 5

AVERAGE ANNUAL FLOW DISTRIBUTION WITHIN THE SUSITNA RIVER BASIN



a and the second

areas; and approximately 28,000 feet of seismic lines were run. While geotechnical data gathered to date has generally confirmed the suitability of Watana and Devil Canyon sites for dam construction, a geotechnical program has been designed for 1981 further to define the nature of the sites and to answer questions about certain subsurface features which could influence the type and precise location of dams and other project features.

7.3 - Seismic Considerations

The Upper Susitna River Basin is a seismically active area. Thus, a major seismic program was started in 1980. A microseismic network of 10 stations was installed and operated to collect microearthquake data for the region. Potential faults and lineaments were identified by air and ground reconnaissance, satellite imagery, airborne remote sensing and aerial photography. A detailed screening of all identified features resulted in the selection of 13 for further study in 1981.

On the basis of the current state of knowledge, the Denali Fault (65 km north of the sites) and the Benioff Zone (60 km underground below the sites) are regarded as the most likely severe seismic hazards. Figure 6 illustrates the seismic setting. Initial estimates of maximum credible earthquakes from these features suggest a magnitude of 8.5 on the Richter Scale. Dam design to safely withstand ground accelerations associated with such an event is within the state of the art.

A study of Reservoir Induced Seismicity (RIS) was also initiated in 1980. RIS may be caused by the increased weight of water in a new reservoir or by lubrication and hydraulic action upon highly stressed rock. Based on evidence gathered to date, an RIS event will not exceed the maximum credible earthquake that could be associated with a fault. Thus, RIS is not likely to affect the determination of design earthquakes.

7.4 - Dam Site Selection

A total of 12 dam sites was considered in the site selection process (See Figure 1). By combination of two or more sites as a system, the total basin potential can be developed in a variety of ways. A detailed screening of individual sites and logical combinations of sites permitted elimination of those whose relative costs were high or whose obvious environmental disadvantages were large. Preliminary layouts were developed for each of the most promising sites.

Candidates selected for further analysis in generation planning and for more thorough environmental consideration included (1) the Watana and Devil Canyon dam sites (the combination found most suitable by the COE in the 1976 and 1979 studies); (2) High Devil Canyon (favored by Kaiser in 1974) and Vee; and (3) a combination of a Watana dam, a relatively low re-regulation dam midway between Watana and Devil Canyon and a tunnel from the low dam with a downstream portal near Devil Canyon. Within these groups, further



SUSITNA PROJECT SEISMIC SETTING

. *

FIGURE 6

variations were studied in terms of alternative dam types and heights and possible schedule variations.

8 - GENERATION EXPANSION PLAN

The current generation system in the Railbelt is primarily based upon thermal power. Natural gas is used heavily in the Anchorage area, oil fired units predominate in Fairbanks, and several small coal-fired plants operate at Healy and in the Fairbanks area. Hydroelectric energy, primarily from the Eklutna project, also contributes a small portion of the current Railbelt electric generation.

The present system will evolve in future years as demand increases and as old units reach the end of their useful lives. Regardless of whether or not a Susitna Project is ever developed, new system additions will be needed. For planning purposes, it was assumed that the Bradley Lake Project (now being pursued by the COE) and certain thermal units now under construction will be on line by the early 1990's. New capacity is necessary after 1992, but the amount and type to be added in any particular year will vary as a function of the demand and peak load forecasts.

A generation planning exercise was conducted to determine how each of the potential Susitna developments might fit into future Railbelt generation systems. The General Electric Optimized Generation Program (OGP) was the primary tool used for this purpose. In addition to Susitna and present and planned capacity, major alternatives including coal-fired plants, gas turbines, gas-fired combined-cycle plants, and the ten best non-Susitna hydroelectric sites were considered as candidates for future expansion. On an economic basis, it was determined that Watana/Devil Canyon, High Devil Canyon/Vee, and Watana/Tunnel all produced total generation system present worth costs which were less than the least cost system without Susitna. Of the total sets considered, the Watana-Devil Canyon combination was favored economically. In the case of the most likely ISER forecast, the most appropriate time to bring an initial 400 MW Watana project on line was found to be 1993. Figure 7 provides a system energy comparison for the mid-load forecast for a base case thermal system and for a Watana/Devil Canyon development (Susitna 3AE).

Detailed generation planning analysis of the most promising development plans indicates that the Watana-Devil Canyon development plan is the preferred option. The studies to date clearly show that the tunnel option is higher in cost and provides less energy, but it may offer certain environmental advantages, in that approximately 15 miles of the Susitna River, including a part of Devil Canyon itself, would not be inundated. However, the environmental benefit would not at this time appear to be justified by the substantial additional cost and energy loss of this alternative.

Preliminary studies of tidal power potential have commenced. Tidal power development, if found feasible, would necessarily lag the earliest possible Susitna development simply because time-consuming detailed environmental and engineering investigations would have to be undertaken before a license application could be submitted to the FERC. Tidal power characteristics and



A

Ĩ

•

SUSITNA 3AE

SYSTEM ENERGY COMPARISON MID LOAD FORECAST

costs will be available by mid-1981 as an input to the independently conducted Railbelt Alternatives Study. For generation planning purposes in the Susitna study, it has been assumed that tidal power generation is not available in 1993 when Watana could be brought on line economically.

A series of sensitivity tests was run to determine how variations in key parameters would affect the choice of favored plans. These tests generally demonstrated that the Watana-Devil Canyon development is the most cost effective alternative among Susitna Basin plans through a reasonable range of fuel costs, fuel escalation rates, real interest rates, and the like.

9 - SUSITNA HYDROELECTRIC DEVELOPMENT

The development selection activities are not yet complete, but the extensive study of the alternative dam and tunnel schemes for developing the power potential of the Susitna Basin indicate that High Devil Canyon and Watana are the two largest and most economic energy producers in the basin.' Other sites such as Devil Canyon, Olson and Gold Creek are competitive provided they have additional upstream streamflow regulation. Sites such as Vee and Susitna III are medium energy producers although somewhat more costly than the larger dam sites. Sites such as Denali, Maclaren and Tyone are expensive compared to other sites. A comparison of the Devil Canyon site to the best tunnel alternative shows that the tunnel scheme is more

The environmental impacts of the various sites are a function of their

Under existing conditions, salmon migrate as far as Devil Canyon, utilizing Portage Creek and Indian River for spawning. The development of any dam downstream of Portage Creek would result in a loss of salmon habitat. The necessary FERC license and permits for such development would probably be difficult to acquire. Between Devil Canyon and Watana, the concerns associated with development relate mainly to the inundation of Devil Canyon, which is considered a unique scenic and white water reach of the river, and has dam safety aspects associated with the occurrence of major geological faults. In addition, the Nelchina caribou herd has a general migration crossing in the area of Fog Creek. In the next upstream reach, between Watana and Vee, there are concerns which relate to the loss of some moose habitat in the Watana Creek area and the inundation of sections of Deadman and Lokina Creeks. Other aspects include the effect on caribou crossing in the Jay Creek area, and the potential for extensive reservoir shoreline erosion and dam safety because of the possibility of geological faults. Between Vee and Maclaren, inundation of moose winter range, waterfowl breeding areas, the scenic Vee Canyon and the downstream portions of the Oshetna and Tyone Rivers are all potential environmental impacts. In addition, caribou crossing occurs in the area of the Oshetna River. area surrounding this section of the river is relatively inaccessible and

Revised April 16, 1981

development would open large areas to hunters. The segment between Maclaren and Denali, appears to be more sensitive than the area downstream of Vee. Inundation could affect grizzly bear denning areas, moose habitat, waterfowl breeding areas and moist alpine tundra vegetation. Improved access would open wilderness areas to hunters. The area upstream of Denali is similar to the reach immediately downstream with the exception of grizzly bear denning areas. Human access to this area would not impact to the same extent that it would downstream. However, due to the proximity to the Denali highway, the inflow of people could be greater.

Detailed generation planning analysis of the most promising development plans indicates that the Watana-Devil Canyon development plan is the preferred option. The studies to date clearly show that the tunnel option is higher in cost and provides less energy, but it may offer certain environmental advantages, in that approximately 15 miles of the Susitna River, including a part of Devil Canyon itself, would not be inundated. However, the environmental benefit would not at this time appear to be justified by the substantial additional cost and energy loss of this alternative.

It is considered essential that the continuation of studies in the Susitna Basin and, if appropriate, submission of a license application should be based on a preferred total Basin development concept. Thus, for the purposes of this report, it will be assumed that the Watana-Devil Canyon plan is the selected development.

The most appropriate plan of Watana-Devil Canyon development involves constructing the full height dam at Watana with a minimum installed capacity of 400 MW initially. The second stage involves adding an additional 400 MW capacity at the Watana site. The third major stage involves constructing the Devil Canyon dam and installing a minimum of 400 MW at that site. It should be stressed that these installed capacities are still approximate and subject to refinement during the 1981 studies.

Conceptual Design

The engineering layouts described are also preliminary and a considerable amount of additional study is currently underway to complete many of the details associated with these developments. In particular, further studies are being undertaken to firm up the general arrangement of the two dam projects; i.e., to determine the exact location of the dams, the dam types, the number and location of spillways, diversion and power tunnels and powerhouses. Also, the exact dam heights will be determined from more detailed economic studies and additional studies of reservoir operation will be undertaken to determine optimum operating policies. Throughout 1981 the environmental studies will be continued and the required reservoir operational constraints and necessary mitigation measures will be determined in more detail and incorporated in the design of the project. The river and ice field surveys and computer model studies also will continue with the results incorporated into the engineering studies.

<u>Watana</u> - The conceptual design involves a fill type dam incorporating a central core of impervious material. Properly graded filters are located both upstream and downstream of the core, supported by shells comprised of compacted, quarried rockfill and/or gravels and cobbles.

At this stage it is assumed that foundations will be excavated to bedrock beneath the entire dam and to sound rock beneath the core and filters. The bulk of the rockfill material will be taken from quarry areas located on the left abutment although some will be recovered from excavations for the various structures.

Gravels and cobbles and filter materials will be recovered from the excavated riverbed borrow areas and processed as necessary. Core material will be taken from borrow. The extent to which river gravels and cobbles can be utilized in the dam shells will be investigated from both technical and economic considerations in 1981.

The overall maximum height of the dam is approximately 840 feet above existing rock level. Allowance has been made for static and dynamic settlement, wave runup and freeboard, and potential deformation under seismic shaking. Upstream and downstream slopes average 1:2.75 and 1:2, respectively, and crest width is 80 feet. Shafts and galleries will be provided within the rock foundations and abutments for grouting and pressure relief drains.

18

Revised April 16, 1981

Construction of an alternative concrete arch dam at Watana appears to be technically feasible but greater in cost. This option will be investigated further in 1981, but at this time, a fill dam appears to be the most suitable at this site.

Devil Canyon - A thin concrete arch dam, similar to that proposed by the U. S. Bureau of Reclamation (USBR), with a central integral spillway, is currently being analyzed for gravity, hydrostatic, temperature and seismic loadings.

The preliminary geometry for a two-center arch dam designed around the asymetric shape of the valley has been laid out, and stress analysis under gravity, hydrostatic and temperature loadings is proceeding. Vertical sections through the center of the dam take the form of a cupola with upstream and downstream faces formed by simple vertical curves. The foundation at the center is somewhat thicker than proposed by the USBR with a general increase in area occuring at the more highly stressed sections.

The overall maximum height of the dam is approximately 625 feet above existing rock level, with a crest width of 20 feet. As currently conceived, the power facilities including the power intake structure, will be kept separate from the dam. Shafts and galleries will be provided outside the dam to facilitate grouting and drainage.

Studies are currently underway to confirm the technical feasibility of constructing the thin arch dam and to evaluate in more detail the costs associated with this type of concrete dam. Evaluation of alternative rockfill and concrete dams at this site is also being undertaken.

Spillways

9.

The reservoirs at Devil Canyon and Watana will be operated in accordance with "rule curves" defining normal operating water surface levels over a given period. These levels are contained by an envelope of extreme upper and lower surface elevations for normal operating conditions. If the reservoir level rises above the maximum normal operating level and the excess reservoir inflows cannot be absorbed by the power facilities, this excess flow must be released from the reservoir and discharged downstream. Spillways are provided at both sites to accommodate these releases.

The spillways may consist of one or more facilities each combining a gated control or a simple overflow structure, a discharge chute and some means of dissipating the energy of the released water downstream of the dam. The combined facilities at each site are designed to contain reservoir levels below an allowable surcharge level for floods corresponding to a frequency of occurrence of 1 in 10,000 years. These flows will be discharged with no significant damage at the site. The discharge capacity of the structures also will be checked to ensure their ability to pass flows corresponding to the probable maximum flood (the maximum flood that may occur from a coincidence of extremes of all influencing factors such as precipitation, temperature and snowpack) without overtopping the dam crest. At present, spillways have been examined as part of the concept of comparing various sites from an economic and energy standpoint and selecting certain sites for further study. To simplify this comparison, a common form of spillway has been utilized which will be viable at all sites, but may not represent the most economic arrangement at any one particular site. During 1981, comparisons of various types of spillways at the selected sites will be made before a particular type is decided upon. Consideration is also being given to separate emergency spillways to handle extreme floods in excess of the 1 in 10,000 year or other selected design floods.

<u>Watana</u> - At its upstream end, the spillway consists of a concrete gravity control structure with five water passages, incorporating ogee-crested weirs and vertical lift gates. Downstream of the control structure is an inclined open chute excavated in rock. The chute is lined with concrete and runs to an intermediate stilling basin where the energy at that point is dissipated in the form of a hydraulic jump. An additional lined chute continues to a downstream stilling basin situated close to river level.

Possibly more economical spillway systems such as one or more single-chute flip-bucket and plunge-pool arrangements, or a combination of single-chute flip-bucket and stilling basins are currently being studied together with a separate emergency spillway with a breachable fuse plug.

Devil Canyon - At Devil Canyon a similar system to Watana has been located on the right abutment. It is envisaged that future studies will consider a spillway of restricted capacity discharging through openings below the dam crest with near vertical discharge into a plunge pool, in combination with one or more chutes and flip-buckets discharging into a separate downstream plunge pool. Alternatively, concrete lined tunnels and flips also discharging into a plunge pool, will be evaluated as well as a separate emergency spillway with a breachable fuse plug. Spillways may be situated on either or both of the abutments.

An alternative dam design in which it will be possible to discharge over the dam crest via a chute located on the downstream face into a lined stilling basin, is also being evaluated.

Power Generating Facilities and Equipment

For the preliminary planning purposes, a similar arrangement of the power facilities has been utilized at all sites, including Watana and Devil Canyon. The system consists of an upstream approach channel and intake structure discharging into concrete-lined penstocks dropping to an underground powerhouse complex. Concrete-lined tailrace tunnels lead from the powerhouse to the river located downstream of the toe of the dam.

The intake is a concrete structure founded in a rock cut and situated at the end of the approach channel. Provision is made for drawing off water at different levels within the reservoir in order to control the temperature of water released downstream. The present scheme allows for separate water intakes at three levels. Separate penstocks are provided for each turbine/ generator unit. These are inclined at 55 degrees with steel-lined sections

·20 Revised

immediately upstream of individual turbines which are located in an underground powerhouse. The turbine/generator units, service bay, workshop, switchgear room and some offices are located within the main powerhouse cavern. The turbines and generators are serviced by overhead cranes running the length of the powerhouse cavern including the service bay area.

A separate transformer gallery is located upstream of the powerhouse cavern and a draft tube gate gallery just downstream of the powerhouse cavern with gates operating in vertical shafts descending to the four draft-tube tunnels. Isolated phase bus ducts located in separate inclined galleries connect each generator to a separate transformer. Power cables exit via vertical shafts to the switchyard at the surface. Vehicle access to the caverns is via unlined tunnels with additional personnel access provided by an elevator shaft to the surface.

The control room and administration offices are housed in a separate building at the surface adjacent to the switchyard.

The draft tube tunnels terminate in a common manifold. Two tailrace tunnels exit from the manifold and terminate in outlet structures located at the river downstream of the dam. These downstream tunnels are concrete-lined, and provision is made to seal off the tunnels for maintenance by inserting stop logs at their outlets.

<u>Watana</u> - The power facilities described are presently assumed to be within the left abutment and are based upon 4 - 200 MW turbine/generator units. However, it is possible that the rock quality and orientation of the jointing in this abutment will prevent the economical excavation of the long power caverns. Alternatively, relocation to the right abutment or a surface powerhouse on either abutment could be utilized. These alternatives will be examined and the most suitable system selected.

<u>Devil Canyon</u> - A similar layout to that at Watana is presently assumed at Devil Canyon based upon 2 X 200 MW turbine/generator units and located within the right abutment, with the intake located upstream of the dam.

Access Roads

Ì

A study is currently underway to determine the most desirable location for an access route and the most economical transportation modes. R&M Consultants are conducting this work as a subcontractor to Acres.

Three general corridors have been selected to provide access to potential dam sites. These include a corridor located to the North and another to the south of the Susitna River linking each site either to Highway 3 near Hurricane, or the railroad near Gold Creek (alternatives 1 and 2) or road access from the Denali Highway to the east of the project sites (alternative 3).

Using design criteria generally conforming to primary highway design several feasible alignments within the selected corridors were sketched on contour maps. From these the route within each corridor showing the most advantageous grade, alignment and length characteristics were selected. These routes allow consideration of a number of transportation alternative plans including allowance for staged upgrading of the road and utilizing rail transporation segments.

The environmental considerations of each route as well as land ownership constraints are currently being addressed, in addition to transportation economics. In March, 1981, a series of public workshops will be held to gain public input to the route selection process. It is anticipated that a final decision on the selected route will take place during 1981, following which further engineering and field studies will be undertaken for the selected route.

Mitigating Measures

In developing the detailed project designs a range of mitigating measures required to minimize the impact on the environment will be incorporated. This is achieved by involving the environmental studies coordinator as a member of the engineering design team. This procedure ensures constant interaction between the engineers and environmentalists and facilitates the identification and design of all necessary mitigation measures.

There are two basic types of mitigation measures that are being developed: Those which are incorporated in the project design and those which are included in the reservoir operating rules. These are briefly discussed below.

<u>Design Features</u> - The two major design features currently incorporated include multi-level power intake structures to allow some temperature control of released water and provision of a downstream re-regulation dam to assist in damping the downstream discharge and water level fluctuations induced by power peaking operations at the dam. During the 1981 studies these two features will be designed in more detail and other features incorporated as necessary. Of particular importance will be the design of the spillways to eliminate or minimize the impact of increased nitrogen in the downstream river reaches.

Consideration will also be given to developing mitigation meaures to limit the impact on the environment during the project construction period. The access roads, transmission lines and construction and permanent camp facilities will also be designed to incorporate mitigation measures as required.

<u>Operating Rules</u> - Limitations on seasonal and daily reservoir level drawdown, as well as on downstream minimum flow conditions have been imposed in plan formulation studies. During 1981, more detailed studies will be undertaken to refine these current constraints and to look at detailed operational requirements to adequately control downstream water level fluctuations, water temperature and sediment concentration.

10 - ENVIRONMENTAL PROGRAM

A major environmental investigation program got underway in 1980. In addition to necessary exhaustive field data collection, effort was devoted in particular to two other major components: (1) addressing major environmental concerns including those expressed by government agencies (at Federal, State, and local level) and the general public, and (2) environmental participation in the design process with a view toward avoiding or minimizing impacts by making design decisions which account for environmental concerns from the start.

The environmental studies are divided into nine specific study components:

- Fisheries

1

2

- Wildlife
- Land Use
- Archaeological (Cultural Resources)
- Recreation
- Plant Ecology
- Corridor Selection
- Socioeconomic (See paragraph 11 below)
- Management and Coordination

At least one more year of data must be collected in each area before detailed impact statements can be prepared and proposals developed as appropriate for mitigative measures. Even so, no evidence has been discovered to date to indicate environmental impacts which are so severe as to conclusively rule out the possibility of developing the Susitna River for hydroelectric power production. Certain environmental impacts on fisheries experienced at other major hydroelectric projects will be absent from or less severe at the Susitna Project if it is ever constructed. These include:

- (a) No direct blockage of fish migration or escape will result from the dam itself.
- (b) No significant river diversions resulting in low flows in the diverted river will occur for the Watana-Devil Canyon combination.
- (c) Regulation is being factored into design to eliminate significant daily fluctuations in flow.
- (d) Nitrogen entrainment will not be increased by numerous sequential reservoirs such as are found on the Columbia River. In addition, design studies will incorporate the latest available technology to reduce the occurrence of such phenomena.

11 - ANALYSIS OF SOCIOECONOMIC IMPACTS

A major socioeconomic study program was launched in 1980 with the objectives of describing existing socioeconomic conditions, forecasting future conditions if no Susitna Project is built, and determining which conditions are most likely to be impacted by a Susitna development.

Major efforts have been devoted to development of socioeconomic profiles during 1980. The 1981 work will focus upon preliminary assessments of impacts which implementation of the recommended development plan could cause.

12 - ECONOMIC FEASIBILITY AND NET ECONOMIC BENEFITS

The analysis of the net economic benefits of the recommended development plan is being developed within the framework of traditional methodology. The general procedure considers the total costs associated with the project (construction, operation, maintenance, transmission, etc.). Benefits are the avoided costs of providing the equivalent power and energy from the next best alternative generating source.

A preliminary life-cycle cost analysis has been conducted for the recommended development plan as well as for other alternatives surviving the initial site screening process. This economic analysis assumed a three percent discount rate in real terms (i.e., the cost of money is assumed to be three percent higher than actual inflation rates during the planning period). In 1980 dollars, the present value costs of the recommended hydroelectric development (operated in the Railbelt System during a 60 year period for economic analysis) were less than the costs of the best thermal generation alternative. More precise values for life-cycle net benefits will be determined as cost estimates are developed in detail for the optimized development plan in 1981.

13 - POWER AND ENERGY MARKETING

Į

Whereas it can be shown that the Susitna Hydroelectric Project would be economical in the long term, it is nonetheless true that the relatively high capital cost of a major hydroelectric power development can lead to difficulties in financing the project or in marketing power and energy during the first few years of operation.

Preliminary financial studies have been conducted to determine the probable nature and extent of the problem of high front-end loading as well as to identify potential strategies for alleviating this. These studies will continue in $19\mathcal{E}_{-}$. Insofar as marketing is concerned, it must be assumed that the maximum price which Railbelt Utilites would pay at any given time for Susitna power and energy is equal to or less than the avoided cost of producing power and energy by the best available alternate means.

In the initial year of operation deliveries from Susitna will replace power and energy generated by existing thermal power plant and the avoided cost will be related to fuel, operating and maintenance expense. Only when the existing capacity reaches the point of needing replacement or new demand emerges, with which this existing capacity cannot cope, will it be possible to edge the Susitna price of energy up to the full cost.

The ongoing studies will deal with practical arrangements which can be made with the Railbelt Utilities to achieve equitable marketing terms under which Susitna energy can be introduced to meet a substantial portion of future system needs.

14 - PUBLIC PARTICIPATION PROGRAM

An aggressive public participation program was initiated for the Susitna Hydroelectric Project. Conducted directly by the Power Authority, major objectives are:

- To distribute information to the public,
- To solicit information from the public, and
- To ensure that public input is fully considered in the decision-making process.

Community meetings, workshops, an action system to ensure that response is provided to every comment or question written by the public, newsletters and mailing lists are vehicles by which these objectives are satisfied.

Of particular note is the fact that public comment and concern has directly influenced the course of the Susitna study. Such major changes from original study plans as the commissioning of a separate and independent alternatives study, the addition of a sociocultural study and an increased level of study for alternative developments in the Susitna Basin were largely prompted by public concerns.

The high level of activity in the Public Participation Program is expected to continue throughout the course of the study.

15 - LICENSING AND PERMITTING PROCEDURES

Regulatory requirements at Federal, State and local levels tend to be voluminous, complex, and time-consuming for any major power development. For the first several years, satisfaction of regulatory requirements will be the controlling factor on the schedule for final completion of a Susitna project.

The most significant initial regulatory requirement is the necessity to obtain a license from the Federal Energy Regulatory Commission (FERC). Should project feasibility be established and a decision made to proceed with the work, current plans call for submittal of an application in mid-1982 and for receipt of a license by 1985.

A detailed analysis of licensing and permitting requirements was conducted early in the course of the work in 1980 and a blueprint was drawn up to ensure that critical regulatory schedules can be met.

16 - FINANCIAL FEASIBILITY ANALYSIS

Financial analysis and risk assessment has been initiated but only carried forward to a limited extent pending the selection of the preferred development plan and the availability of appropriate capital costs of construction. One purpose of the preliminary financial feasibility analysis has been to establish the "envelope" within which the staging, design and operating configurations of Susitna are amenable to market financing based upon reasonable assumptions concerning financial markets and the inclinations of investors over the next 20 to 30 years. A computer model, developed earlier for financial analysis of major capital intensive projects, has been tailored specifically to meet the unique requirements of Susitna. Using this model, it is possible to analyze the effect on financial feasibility resulting from variations in input assumptions. These inputs include phasing of major project stages, scheduling of construction outlays, energy and power production during initial years, pricing and revenues, returns on investment, contingency provisions, debt requirements, taxes, and financial market conditions. There has been close correlation with work carried out on generation planning, employing the OGP-5 modeling capability (as described in Paragraph 8).

Preliminary financial analysis indicates that viable options do exist for funding the project with various levels of involvement of the State of Alaska. Work during 1981/82 will focus on financial feasibility of the optimized development selection and will proceed in close collaboration with the financial consultants selected by the Power Authority at the end of 1980.

17 - SECURITY OF PROJECT COST AND REVENUE STRUCTURE

Decision makers responsible for public policy and for action within the financial and credit markets, as well as those at regulatory agencies, must be confident that the probability of unforeseen events seriously distorting the objectives of the Power Authority and its planners is sufficiently remote that government and private investors should commit substantial financial resources to the Susitna Project. A detailed risk analysis will be made of the various influences and possibilities, no matter how remote, that might impact the security of the project cost structure and its revenue flow. In particular, consideration will be given to risks, and to the formulation of contingency plans, applicable to:

- Potential variations in capital costs
- Cost escalation
- Cost overruns
- Delays

- Events leading to noncompletion
- Serious outages during operation
- Failure of revenue from power resources
- Regulatory issues

Arising from the study of project cost and revenue structure will be consideration of the need for completion and/or other guarantees and revenue assurance requirements. The aim will be to develop strategies and procedures which will minimize risk in each category and provide for an acceptable balance of residual exposure and benefit for the financing entities which might be involved in the Project.

18 - ORGANIZATION AND MANAGEMENT

Project control structures, policies and procedures have been developed and put in place to ensure that continuing project activities are in the best interests of the State of Alaska and its populace. The Executive Director of the Power Authority serves as Project Manager for the State of Alaska. He is assisted in turn by a project staff which includes Assistant Project Managers for Technical Output and Schedule and for Budget and Finance. A Project Engineer within the Power Authority devotes his full-time attention to monitoring and coordinating project work.

Within the Acres organization, a Project Manager is responsible for direction of the activities of a large group of technical personnel. He is assisted by a Deputy Project Manager, a Technical Study Director, and a Resident Manager (in Anchorage).

External Review Panels have been established both at the Power Authority's level and at Acres' level to provide an independent check on the adequacy and accuracy of completed and proposed study activities.

Major subcontractors assisting Acres in the performance of its work include:

- R&M Consultants, Incorporated
- Cook Inlet Region Incorporated in association with Holmes and Narver
- Terrestrial Environmental Specialists
- Woodward Clyde Consultants

- Frank Moolin and Associates
- Robert W. Retherford Associates
- Other Alaskan firms providing transportation, supplies, and logistical support

19 - IMPLICATIONS OF PROCEEDING

The Governor of Alaska and the State Legislature will receive a report on or before March 30, 1981, wherein the Power Authority must recommend whether work should continue on the Susitna Hydroelectric Project. The Power Authority has selected four particular issues for detailed consideration. Conclusive proof that any one of these issues presents an insurmountable barrier would lead to a recommendation by the Power Authority to terminate the study. Briefly summarized, the issues are as follows:

- Are the forecasts too low to require any major generation additions over the next 30 years?
- Are seismic risks so great that safe development cannot occur?

- Are anticipated environmental losses unacceptable?

Į

Ĵ

9

- Is there a significantly lower-cost set of alternatives which will satisfy demand forecasts through the year 2010?

No barriers have been discovered during the initial year of study which would lead to an affirmative answer to any of the listed questions. Even so, definitive answers have not yet been developed for all of the issues. Continuing the study would provide the State with an opportunity to make sound decisions in the future as to whether Susitna hydroelectric potential should ultimately be developed. Terminating study efforts at this time would result in avoiding the significant costs of further investigation and analysis on Susitna.

2 - PROJECT SCHEDULES

 $_{2}$

: : شجارت

J

0

0

2. PROJECT SCHEDULES

ł

V

\$. ₹ The Plan of Study Master Schedule is shown on the 3 attached Figures.

Real Provide State
Г								1					-	وعنتمجت																								
	ASK NO	DESCRIPTION		نيونيو _ا يو		1360		ACIA	VIIES	1	10	LICEN	ISE A	PLICA		سخبيت						982	من ور م			J	R.5. P.	184	10 11	ORAN 1	07 .00	INSTRU	ETEDH	LICENS	1HG			يسعبنا
1			3 8	MA	N J	111	4 8	0 1	0	II	F M	A	R 1	ĪJ	AS	0	ND	1	FW		1 1	Ţ.	A	5 0	N			1000	-	6/2/0	ATTAL	A NULL	ann	-	57.75	1.1944	Man I	
٩	100	POWER STITLES										H		H		H		$\left - \right $		\mathbf{H}				-	\square		_	-	_		\neg							
	102	FORCAST MEAN LOND DEMAND TRANS					-			100		\square		\square		H				H					\square				-						-	=		ا حسبت ا مسبقه
[196	ILANALION ALPORT			- 6				22.00			H		\square		F		FŦ	—	H	-	1-			H				=		=	_	_		\square			يجنبون خفت بنه
·[200	SURVEYS AND SHE FACLITES					-				_									1.0				10 8.1	612	18 31		D19 81	-	1818			31418			-) 8 18
ļ	203	RESIPTUT AND ENERGENCY SERVICE															-		1					亡				_	_									محمد کند محمد کند
Ē	205	LAND ACOUSITON ANALYSS												\pm	1-				1-					1						=								
1	201	SITE SPECIFE SURVEY																\vdash										-	-									- 11 -
- F	208	AN PHOTOS AND HAPPING CONTROL NETWORK SLAVEYS									=	T		$\left\{ -\right\}$				\square		-+				+	-			-	-								~~~.	
F	210	ACCESS ROAD		-							=	1				H		I T		H			T-	7	F	7-		<u> </u>	-							=		معينيند. إمصابيت
[212	FIELD RECON FOR RESERVOR CLEAR.							-					1-1	1		-	\square	=	1	1	1		1-	11						=]		
ļ	214	COST EST. FOR RESERVON CLEARING				1-1-			1				1	1-1	=	口	=		1-	1-1	1	1		1	11				_									بنينمب
	216	HYDROGRAPHIC SLITVEYS						-				E								\Box				1										Concession .				
	300	HTDHOLOGY									1-				1-		1-		1-	H		-		13 41	ein			818 a		1013	41918	510(8			ini		-	
	301	FIELD DATA NOER OPERATION	1== + = = h									<u></u>	-1-							H		1-	EF		+	-		f						7.00		-		
	303	FELD DATA COLLECTION 80 - 82 WATER RESOURCES - STUDIES																		H				-	+					-			{				-	
•[305	FLOCO STUDIES HYDRALLIC AND KE STUDIES	+							(a = =			-							\square				+	H				\neg						-1			
	307	SEDIMENT YELD AND RIVER MORPHOLDER									_ _=	-	-	1		F		F		F		1-	F	1	1-1	1	-	_	_							_		
	303	ACLESS ROAD HIDSOLDGT		-1-1		1-1-		1-1-	1-											11	1	1-	口	1		=			_						=	[مىلىتىنە ئىجىمىدە
0						11	1		1-	ĒĒ	1								1																		- [-
ł	400	NEVEW AVALANCE DATA	130				1-		-																											11868.0		
ł	402	SHORT TERM MONSTORING PROGRAM	┨━┼━╎╹			Reads			Cas	1		+		$\left - \right $		\vdash			- -			-															- [
	404	REMOTE SENSING MARE ANALYSIS								1		H				H				F					$\left \cdot \right $												-	
ļ	406	PRELM EVALUATION AND REPORT									-	H		1-1		H	1	17		H	-	1-	17	1			-1-					_			F	=		
	108	DAN STABLITY					1					÷						1	1	11	1			1	口			=										,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,
6	4 10	RESERVOR NEWCED SEISMOTY						<u>+-</u>	+				1-							\square		1																
	411	SEISHIC GEOLOGY FIELD STUDY EVALUATION AND REPORT	╂╾┠╾╂			++	+-							÷															_								1.7. Milena	
	4 (3	GROUND MOTION STUDES			FF	-		\square	+	-										-					$\left\{ \cdot \right\}$			-+		-							5 G. 90 G	
	412	SOL SUSCEPTOLITY TO STENC FALLER				1-1-	= =	++	7	F	=	-			7	F-F		H					FI.		\square			-	_						=		1	ينجيون - جسمي
	500	CLOTECH EXPLORATION							1		= =	\square		1-1		口		1	=		41 815			181811	-						81018+							
	302	AR PHOTO INTERITIE TATION						10 E 10 E	-					11					=		1	1=	Lt.	+		=		=									المعجدة. المعجدة	مشمود مریدیک
	503	1980 PROGRAM DESKA 1980 EXPLORATION PHOGRAM							1					$\pm \pm$								1-		士		1					LEGEN	0	I	لمسيما	line l			
	505	1981 EXPLORATION PROGRAM				\pm			Bea			<u></u>		_		H	1			H		1-	H	1				-				ia WQA	к сони	R.ETED		-	1, 1901	
	507	DATA COMPLATION			F-F		F			H			- 1		-			+	Ŧ	H		F	F		\square				[K PEW	Lines .	FROM T	ERAM	NY 1. 104	
						11		1-1-	7-	1-1		T				$\frac{1}{1}$		F			7	- -	F		\square							UN CON	Incico	WCRM	failor		TNOT	1.1
	مرحد ني جيُوب تستعيد مع		1-1-1			11	1	十十	1	17		11				11		1-1	-1-	1	=	1-		4				_							APPLIC	ALCH.		
		-				1+		1-1-	1														\square	1						<u> </u>								
4A		1			L		بوليو	11	1			1		لببك	in the second	1_1	-	1-1		<u>L_</u>			<u>11</u>		4-4		 L		Ļ							بر جبر متندر	41,81 4444 ain	أحجج
										•	SL	ISIT	NA	HY	DRO	ELE	CTF	SIC	PR	JE	СТ														••••			
										PI	AN	0	FS	STI	IDY	M	AST	FER	8 S	СН	ED	UL	E															
											9 99 39 					3944																						
										Q																											IN	91
							خانیم رو						: 			معيني		- 11 									مىرىمى			· .				FIGL	JRE I	OF 3	INUI	111
		* 30 *		t		•		1		7		1	:	1			1		5		1		4			1		سيسر		1			2 		1) ~)	
																									t i	l		l		1	I				I F	1		
	1. j																																					
																													1									

*• * * s



3 - NOTES ON SUSITNA BASIN DEVELOPMENT SELECTION

3.1 - Introduction

Section 3.2 of these notes briefly outlines the results of the development selection process undertaken to arrive at the proposed Susitna Basin plan, i.e. the Watana/Devil Canyon dam development. A brief description of the results of the comparison of railbelt generating scenarios, both with and without the Susitna Basin development, is also presented in Section 3.3.

The Appendix contains tables summarizing the parameters used for the systemwide economic evaluation of the various Susitna Basin development plans and the all thermal generating scenario. It also contains results from the generation planning model used for economic evaluation.

3.2 - Evaluation of Susitna Basin Development Plans

(a) Introduction

The Susitna Basin development studies commenced with the selection of 12 potential dam sites within the basin (see Table 1 and Figures 1 and 2). As shown in Figure 3, these sites were then subjected to a screening process incorporating economic, environmental, and total energy contribution criteria. In cases where two sites were located sufficiently close to each other and could be regarded as alternative sites one of them was also screened out. This screening exercise resulted in the most upstream sites such as Tyone and Butte Creek being screened out by the environmental, economic, and total energy contribution criteria. The energy potential at these sites is of a smaller order of magnitude that the major basin development options. Although also of low energy potential, the Maclaren and Denali sites were retained as they have potential for upstream regulation of flow for the larger power developments downstream. The two downstream sites, Gold Creek and Olson, were screened mainly because dams at these sites would impact upstream anadromous fish spawning areas in Portage Creek. All other dam sites are located upstream of Portage Creek which is known to represent the upstream limit of fish migration on the Susitna. The Devil Creek site was screened as it represents an alternative to the High Devil Canyon site.

Following the screening exercise and utilizing the assistance of operations research techniques and engineering layout and cost studies, the most economic basin development plans were selected. These plans were based on developing combinations of dams at the sites remaining after the screening exercise. This process revealed that the development plans incorporating dam combinations at Watana/Devil Canyon, High Devil Canyon/Vee, and High Devil Canyon/Watana are the most economic. Table 2 lists all the development plans selected and the associated costs and energy yields. Preliminary economic analyses indicated that it is not appropriate to stage actual dam construction but that the powerhouse construction at the larger dams such as Watana and High Devil Canyon is warranted.

Environmental assessment of the plans indicated that river flows resulting from daily peaking operations from the downstream dams could not be accepted. This required the introduction of reregulation facilities in certain cases and reductions in installed capacities at downstream dams in others. Table 3 lists the modified plans.

Based on the above information, it was decided to conduct a more thorough evaluation of the following two basic plans.

- <u>Plan E1.5</u>: Watana dam with two 400 MW powerhouse stages followed by Devil Canyon dam with a 400 MW powerhouse.
- <u>Plan E2.3</u>: High Devil Canyon dam with two 400 MW powerhouse stages followed by Vee dam with a 400 MW powerhouse.

It was also decided to investigate a long power tunnel alternative to developing the head at the Devil Canyon site as an alternative to the dam. This plan is referred to as 1.5 in Table 2.

The following subsection outlines the plan evaluation process and describes the selected development plan.

(b) Evaluation of Basin Development Plans

The evaluation process used involved consideration of the attributes of the various plans and a ranking of these plans based on comparisons of these attributes.

(i) <u>Attributes</u>

The following attributes are used to evaluate the short listed basin development plans:

- Economic

The parameter used is the total present worth cost of the total railbelt generating system for the period 1980 to 2040. This parameter is evaluated using an "economic" discount rate of 3%, 0% general escalation and specified rates of fuel cost escalation (see Appendix). The generation planning model OGP5 was used to plan the generation sequences for the 1980-2010 period. The 2010 generating system configuration was assumed to remain constant for the 2010 to 2040 period for purposes of evaluating the total system present worth cost.

- Environmental

A qualitative assessment of the environmental impact on the ecologic, cultural, and aesthetic resources is undertaken for each plan. Emphasis is placed on identifying major concerns so that these could be combined with the other evaluation attributes in an overall assessment of the plan.

- <u>Social</u>

This attribute includes determination of the potential nonrenewable resource displacement, the impact on the state and local economy and the risks and consequences of major structural failures due to seismic events.

- Energy Contribution

The parameter used is the total amount of energy produced from the specific development plan. An assessment of the energy development foregone is also undertaken. This energy loss is inherent to the plan and cannot easily be recovered by subsequent staged developments.

(ii) Evaluation Process

The various attributes outlined above have been determined for each plan and are summarized in table form. Some of the attributes are quantative while others are qualitative. Overall evaluation is based on a comparison of similar types of attributes for each plan. In cases where the attributes associated with one plan all indicate equality or superiority with respect to another plan, the decision as to the best plan is clear cut. In other cases where some attributes indicate superiority and other inferiority, these differences are highlighted and trade-off decisions are made to determine the preferred development plan. In cases where these trade-offs have had to be made, they are relatively convincing and the decision making process can, therefore, be regarded as fairly robust.

In order to simplify the overall evaluation process, it is conducted in a series of steps. At each step, only a pair of plans is evaluated. The superior plan is then passed on to the next step for evaluation against an alternative plan. The results of this exercise are discussed in the following subsection.

(iii) <u>Results of the Evaluation Process</u>

The <u>first step</u> in the process involves the evaluation of the Watana/Devil Canyon dam plan and the Watana/Devil Canyon tunnel plan. As Watana dam is common to both plans, the evaluation is based on a comparison of the Devil Canyon dam and tunnel schemes.

- Devil Canyon Dam Versus Devil Canyon Tunnel

Table 4 lists the total present worth costs and Table 5 summarizes the economic evaluation. The results clearly demonstrate the economic superiority of the Devil Canyon dam scheme. The difference in present worth system costs amounts to \$680 million. A general description of the environmental impacts associated with developing the Devil Canyon/Watana plan is given in Table 6. This information has been used to set up the environmental evaluation in Table 7 which indicates that the tunnel scheme has less environmental impact than the dam scheme. Table 8 lists the social attributes and indicates that the dam scheme has a higher potential for displacing nonrenewable resources than the tunnel scheme, and is therefore, superior. The impacts on the state and local economy and risks due to seismic exposure are judged to be similar for both schemes. Table 9 deals with the energy contribution attributes and illustrates that the dam scheme develops more of the basin potential than the tunnel scheme. The overall evaluation of the two schemes is summarized in Table 10. The dam scheme is judged to be superior since the cost savings associated with the dam are

considered to outweigh the relatively modest reduction in the overall environmental impact.

The second step of the development selection process involves a comparison of the Watana/Devil Canyon and the High Devil Canyon/Vee development plans.

- Watana/Devil Canyon Versus High Devil Canyon/Vee

Table 4 summarizes the economic parameters while Table 5 outlines the economic evaluation of the plans. The Watana/ Devil Canyon plan is economically superior by \$520 million. Table 6 outlines the environmental impacts associated with the two plans while Table 11 summarizes the environmental evaluation. The Watana/Devil Canyon plan is judged to be environmentally superior. Table 8 summarizes the social evaluation and Table 12 the energy contribution evaluation. The Watana/Devil Canyon plan is superior in terms of both these attributes. Table 13 summarizes the overall evaluation and demonstrates the overall superiority of the Watana/Devil Canyon plan.

(c) <u>Selected Development Plan</u>

Based on the above discussion, the Watana/Devil Canyon development plan is regarded as the optimum Susitna Basin plan. Currently, engineering studies are in progress to further refine the size of the development (dam heights, installed capacities, etc.) and the design concepts. Figures 4 to 6 illustrate the operational characteristics of this development plan for a typical 30 year period.

3.3 - Comparison of Generation Scenarios Plan

The selected Susitna Basin development plan has been compared with a limited number of alternatives by comparing generation scenarios for the Railbelt Region with and without the Susitna Basin development.

The two basic Railbelt generation scenarios compared are the all thermal scenario which relies on coal and gas fired generation and the with Susitna scenario incorporating the Watana/Devil Canyon dam plan as well as supplementary coal and gas fired generating facilities. Comparison of these two scenarios is based on the same attributes used for the Susitna Basin development selection. Table 14 summarizes the economic attributes and clearly indicates the superiority of the generation scenario incorporating the Watana/Devil Canyon plan. The superiority is maintained over wide ranges of anticipated future load projections and of the economic variables such as capital cost estimates, discount rate, fuel costs, fuel cost escalation, and economic plant life. The social comparison is summarized in Table 15. The scenario incorporating the Watana/Devil Canyon plan offers greater potential nonrenewable resource conservation. However, there is insufficient information currently avai. Sle to undertake quantitative comparisons of impacts on state and local economies or of relative seismic exposures. Comparisons at this stage are, therefore, somewhat subjective. Table 16 broadly summarizes the environmental impacts associated with the two scenarios. However, specific information on potential future coal-fired generating sources is not available at this time and overall comparison is consequently uncertain. An attempted comparison is summarized in Table 17 from which it is tentatively concluded that the scenario with the Watana/ Devil Canyon plan appears to be superior.





SUSITNA BASIN PROFILE AND POTENTIAL DAM SITES





OPERATION OF THE WATANA / DEVIL CANYON DEVELOPMENT PLAN E 1.3

STAGE I-WATANA RESERVOIR (400 MW)





	7								•					
المر			Λ,	ľ,		ſĹ	R I	المر ا		Λ,			ſL I	M.
Y	r	P		۲	r	L.F.I	RM	ſ	P	ſ	P		r	r
u									•					
1965	1966	1967	1968	1969	1970	1971	1972	1973	1974	1975	1975	1977	1978	1979

FIGURE 4





i Calenta

.

53 28



E)am			Capital	Installed	Average Apoual	Economic*	Sauree
۳۰ <u>۵۰۰ ۲۵۱</u> ۰ ۲۰۰ - ۲۰۰ ۲۰۰ ۲۰۰ - ۲۰۰ - ۲۰۰ - ۲۰۰ - ۲۰۰ - ۲۰۰ - ۲۰۰ - ۲۰۰ - ۲۰۰ - ۲۰۰ - ۲۰۰ - ۲۰۰ - ۲۰۰ - ۲۰۰ - ۲۰	Proposed	Height	Upstream	Cost	Capacity	Energy	Energy	of
Site	Туре	Ft.	Regulation	$$ \times 10^{6}$	(MW)	Gwh	\$/1000 kWh	Data
Gold Creek**	Fill	190	Yes	900	260	1,140	37	USBR 1953
Olson		•						
(Susitna II)	Concrete	160	Yes	600	200	915	31	USBR 1953
								KAISER 1974 COE 1975
Devil Canyon	Concrete	675	No	830	250	1,420	27	This Study
			Yes	1,000	600	2,980	17	H
High Devil Canyon								13
(Susitna I)	Fill	855	No	1,500	800	3,540	21	33
Devil Creek**	Fill	Approx 850	No	-			-	-
Watana	Fill	880	No	1,860	800	3,250	28	n
Susitna III	Fill	670	No	1,390	350	1,580	41	11
Vee	Fill	610	No	1,060	400	1,370	37	11
Maclaren**	Fill	185	No	500	55	180	124	13
Denali	Fill	230	No	440	60	245	81	1
Butte Creek**	Fi11	Approx 150	No		40	▲ 130***		USBR 1953
Tyone**	Fill	Арргох 60	No		6	22***		USBR 1953
and the second		Constant and the						Lin estrations (

TABLE 1 - POTENTIAL HYDROELECTRIC DEVELOPMENT

*Includes AFOC, Insurance, Amortization, and Operation & Maintenance Costs.

3

**No detailed engineering or energy studies undertaken as part of this study.

***These are approximate estimates and serve only to represent the potential of these two dam sites in perspective.

TABLE 2 - Susitna Development Plans

				Stage/Inc	remental	Data		Cu Sy	mulati stem D	ve lata
			Capital Cost \$ Millions	Construction	Earliest On-lina	Reservoir Full Supply	Maximum Seasonal Draw-	Annua Energ Produ Firm	l y ction Avg.	Plant Factor
Plan	Stage	Construction	(1980 values)	Period yrs.	Date ¹	Level - ft.	down-ft	GWH	GWH.	*
1.1	.1	Watana 2225 ft 800MW Devil Canvon 1470 ft	1860	9	1993	2200	150	2670	3250	4,65
		600MW TOTAL SYSTEM 1400MW	<u>1000</u> 2860	6-1/2	1996	1450	150	5310	6230	51
1.2	.1 .2	Watana 2060 ft 400MW Watana raise to	1570	8	1992	2000	100	1710	2110	6印
	.3	2225 ft Watana add 400MW	360	3	1995	2200	150	2670	2990	8.5
	.4	capacity Devil Canyon 1470 ft	130	2	1995	2200	150	2670	3250	4.55
		TOTAL SYSTEM 1400MW	3060	6-1/2	1996	1450	100	5510	6230]. ≥0
1.3	.1	Watana 2225 ft 4COMW Watana add 400MW	1740	9	1993	2200	150	2670	2990	85
		capacity Devil Conver 1470 ft	150	3	1994	2200	150	2670	3250	46
	• 2	600 MW- Total System 1400MW	<u>1000</u> 2890	6-1/2	1996	1450	100	5310	6230	51
1.4	1	Devil Canyon 1470 ft 250MW	830	6	1990	1450	100	1258	1420	65
	2	Watana 2225 ft 400MW Watana	1740	9	1996	2200	150	3920	4410	73
	4	add 400MW Devil Canvon	150	• 3	1997	2200	150	3920	4670	51
		add 350MW TOTAL SYSTEM 1400MW	<u>200</u> 2920	3	1997	1450	100	5310	6230	51

. . . .

. **h**.

				Stage/Inc	remental	Data		Cu Sy	mulati stem D	ve ata
			Captial Cost \$ Millions	Construction	Earliest On-line	Reservoir Full Supply	Maximum Seasonal Draw-	Annua Energ Produ Firm	l y ction Avg.	Plant Factor
Plan	Stage	Construction	(1980 values)	Period yrs.	Date	Level - ft.	down-ft.	GWH	GWH	84 - 73 - 1
1.5	1	Watana 2225 ft 800MW Watana add 50MW	1860	9	1993	2200	150	2670	3250	465
		TOTAL SYSTEM 1180MW	3380	2	1775	1472	4	4070	5490	
2.1	1	High Devil Canyon								
	2	1775 ft 800MW Vee 2350ft 400MW Total system 1200MW	1500 <u>1060</u> 2560	8 7	1994 ² 1997	1750 2330	150 150	2860 3870	3540 4910	5-1) 4.77
2.2	1	High Devil Canyon								
	2	1630 ft 400MW High Devil Canyon	1140	7	1993 ²	1610	100	1850	2110	60)
	3	add 400MW Capacity raise dam to 1775 ft Vee 2350 ft 400 MW TOTAL SYSTEM 1200MW	500 <u>1060</u> 2700	3 7	1996 1997	1750 2330	150 150	2860 3870	3540 4910	51 47
2.3	1 1	High Devil Canyon			9					
	2	1775 ft 400MW High Devil Canvon	1390	8	1994	1750	150	2400	2730	78
	3	add 400MW capacity Vee 2350 ft 400MW TOTAL SYSTEM 1200	140 <u>1060</u> 2590	3 7	1995 1997	1750 2330	150 150	2860 3870	3540 4910	51 47
3.1	1	Watana				• • •				
	2	2225 ft 800MW High Devil Canvon	1860	9	1995 ²	2200	150	2670	3250	46
	3	1470 ft 400MW Portage Creek	860	6	1998	1450	100	4550	5280	50
		1030 ft 150MW TOTAL SYSTEM 1350MW	$\frac{650}{3370}$	5	2000	1020	50	5110	5960	50

NOTES: 1. Allowing for a 3 year overlap construction period between major dams.

2. Assumes FERC license can be filed by June 1984, ie. 2 years later than for the Watana/Devil Canyon Plan 1.

TABLE 3 - Selected Susitna Development Plans (Environmental)

	<u> </u>						Cumula	tive
·	· ·		Stage/J	ncremental Det	a		System	Data
						Annua	1	•
Į					Maximum	Energy	¥ .	
			Capital Cost	Reservoir	Seasonal	Produ	ction	Plant
1			\$ Millions	Full Supply	Draw-	Firm	Avg.	Factor
Plan	Stage	Construction	(1980 values)	Level - ft.	down-ft.	GWH	GWH	ž
F1 3	1	Weters 2225 ft 400MW	1740	2200	150	2670	2900	83
	2	Watana add åANAW canacity				2070		
	•	and Re-regulation dam	250	2200	150	2670	3250	46
	3	Devil Cervon 1470 ft 400MW	900	1450	150	5520	6070	58
		TOTAL SYSTEM 1200MW	2890	1420				~~
E2.3	1	High Devil Canyon 1775 ft 400MW	1390	1750	150	2400	2730	78
	2	High Devil Canyon						
		add 400MW capacity and						
		re-regulation dam	280	1750	150	2860	3540	51
	3	Vee 2350 ft 400MW	1060	2330	100	3870	4910	47
		TOTAL SYSTEM 1200MW	2730					
E2.4	1	High Devil Canvon 1775 ft 400MW	1390	1750	150	2400	2730	78
	2	Hinh Devil Canvon						
		add 400MW capacity	140	1750	150	2860	3540	51
		Portage Creek 1030 ft 150MW	650	1020	50	3410	4190	50
	3	Vee 2350 ft 400MW	1060	2330	100	4430	5540	47
		TOTAL SYSTEM 1350MW	3240		•		en e	

TABLE 4 - Economic Backup Data for Evaluation of Plans

.

0

3

Total Present Worth Cost for 1981-2040 Period \$ Million (% Total)

Parameter	Generation Plan with High Devil Canyon/Vee	Generation Plan with Watana/ Devil Canyon	All Thermal Generation Plans
Capital Investment	2840 (44)	2750 (47)	2520 (31)
Fuel	3230 (50)	2750 (47)	5200 (64)
Operation and Maintenance	390 (6)	350 (6)	410 (5)
Total:	6460 (100)	5850 (100)	8130 (100)

TABLE 5

ECONOMIC EVALUATION OF DEVIL CANYON DAH AND TURNEL SCHEMES AND WATANA/DEVIL CANYON AND HIGH DEVIL CANYON/VEE PLANS

		Prevent worth of Net Ben sys	efit (\$ million) of total generation tem costs for their	
	• • • • • • • • • • • • • • • • • • •	Devil (anyon Dam over the lunne) Scheme	Watana/DovII Canyon Dam over the High DovII Canyon/Vee Dama	Remarks
ECONOMIC EVALUATION: Base Case		680	520	Economic ranking: Devil Canyon dam scheme is superior to Tunnel echeme. Watana/Devil Canyon dam plan is superior to the High Devil Canyon dam plan.
SENSITIVITY ANALYSES: Parameter	Sensitivity Analyses			
LGAD GROWTH	Low High	650 N.A.	210 H.A.	The net benefit of the Watens/Devil Canyon Plan re- mains positive for the range of load forecasts con- sidered. No change in ranking.
CAPITAL CUST ESTIMATE		Higher uncertainty assoc- isted with tunnel scheme.	Higher uncertainty associated with H.D.C./Vee plan.	Higher cost uncertainties associated with higher cost schemes/plans. Cost uncertainty therefore does not affect acomomic ranking.
PERIOD OF ECONOMIC ANALYSIS	Period shortened to (1980 - 2010)	230	160	Shorter period of evaluation decreases economic dif- ferences. Ranking remains unchanged.
DISCOUNT RATE	5% 8% (interpolated) 9%			
FUEL COST	80% basic fuel cost	As both the capital and fu scheme and H.D.C./Vee Plan	el costs associated with the tunnel a are higher than for Watana/Devil	Ranking remains unchanged.
FUEL CUST ESCALATION	OX fuel escalation OX coal escalation	Lanyon pian any changes to Davil Canyon or Watana/Dav	incee parameters cannot reduce the il Canyon net benefit to below zerc.	
ECONDMIC THERMAL PLANT LIFE	50% extension 0% extension			

River Reach	Environmental Attributes	Concerns	Difference in impact of two piens	Identification of difference	Appraisal Judgement
Dawnstream of Devil Canyon	Ecological	Change in water quality and quantity as it affects fish and wildlife.	NO Significant difference between plans.		Not a factor in plan comparison.
	Cultural	No downstream archeological concern.			Not a factor in plan comparison.
		Possible socio-cultural effects on downstream com- munities.	NO Significant difference betwaen plans.		
	Acsthetic/ Land Use	Change in flow as it affects utilization of the lower river.	NA Significant difference between plans.		Not a factor in plan comparison.
Devil Canyon	Ecological	Minimal ecological concern in the canyon.	Minimal difference in potential impact.		Not a factor in plan comparison.
	Cultural	Potential inundation of archeological sites.	Probable minimal difference due to rugged nature of the canyon,		Not a factor in plan comparison.
	Assthatic/ Land Use	Inundation of unique Davil Canyon.	Hinimal difference in impacts scauning a re-regulation dam is built downstream of HDC.		Not a factor in plan comparison.
Devil Canyon to Watana Dam Site	Ecological	Utilization of the river valley by moose and bear. Caribou crossing in Fog creek area.	Difference between plans.	In the upper portions of this reach wore of the river valley would be inundated with the HDC/V plan (HDC pool elevation is 1750 - M/DC pool elevation is 1450') with a potential greater impact on wildlife re- sources.	The wildlife impacts in this section would be less with the W/DC plan however due to the relatively small area involved this difference is not a major factor in plan evaluation.
		Resident Fisheries	Minimal difference between plans.	Both plans inundate approxi- mately the same reach of the Susitna River however the HDC/V plan would extand ap- proximately 1 more mile up Devil Creek and 3 more miles up the Tsusena Creek.	The HDC/V plan would create a greater im- pact on resident fisheries although the relative difference in this section of the river is minimal. This difference is con- sidered a minor factor in plan evaluation.
	Cultural	Inundation of Archeological sites.	Hinimal difference between plans.	Known and suspected archeolog- ical sites exist in this sec- tion of the river. HDC/V with its higher pool elevation has a greater possibility of inun- dated more archeological sites	Since none of those archeological sites have been designated as having a major significance and miliyation measures are available, this minimal difference is considered a minor factor in plan evaluation.
	Aesthetic/ Land Use	Loss of land use potential. Loss of sesthet:	Minimal disterence between plans.	HDC reservoir would inundate the scenic Tsusena Falls loss of land use potential similar for both plans.	HDC/V plan results in a slightly great- er loss of sesthetic and land use re- sources. The difference has a minor influence in the overall comparison of the plans.

0

TABLE 6

ENVIRONMENTAL IMPACTS ASSOCIATED WITH WATANA/DEVIL CANYON AND HIGH DEVIL CANYON/VEE DEVELOPMENT PLANS

River Reach	Environmental Attributes	Egncerns	Difference in impact of two plans	Ident if icat ion of difference	Appraisal Judgement
Watana to Vee Dam Site	Ecological	Loss of moose habitat.	Difference between plans.	Watana reservoir floods to el- evation 2200' HDC reservoir floods to elevation 1750'. The lower reach of the Watana Creek ingin, identified as an important moose area, would be inundated by the Watana resor- voir. The quality of the hab- itat and condition of the sub- population of moose in this area appears to be decreasing.	The Watama plan would create a greater impact on moose in this reach of the river however considering the declining nature of this moose habitat the signi- cance of this impact is considered less than impacts that could occur upstream in the Vee reservoir.
		Impacta on Caribou migra- tion.	Potential difference between plana.	Carlbou crossing has been doc- umented in Kosina/Jay Crosk area. Due to the large winten drawdown and potential for ice shelving the Watana reservois could inhibit carlbou crossing in the spring. Although the HDC reservoir could have a similar effect the probability of impact is greater for the Watana reservoir.	The Watana plan could create a greater restriction on caribou crossing in this aaction of the river. The potential impact on caribou is compared with po- tential impacts upstream and considered to be less significant.
		Loss of river bollow and valley habitat.	Difference in river valley habitat lost.	The loss of river bottom hab- itat is similar for both achemes. Loss of forest slong the valley slopes would be greater with the Watans scheme. This habitst has been identified as being important for birds and bears.	The Watana acheme would create a greater loss of important habitat along the valley slopes in this section of the river. This factor is considered of accarate importance in plan evaluation.
	Culturel	Loss of archeological sites.	No significent difference iden- tified to date.	Due to the larger area of the Matana reservoir in this sec- tion, the probability of inun- dating archeological eltes is increased.	Not a mojor factor in plan evaluation.
	Assthetics/ Land Use	Resource agencies are con- cerned about creating access to extensive wilder- ness areas. On the other hand certain segments of the public desire improved access.	Location and extent of access could vary between plans.	Hore extensive road access would probably result from the HDC/V plan due to the con- struction requirements at Yee site. Access created directly by the reservoirs is similar for both schemes in this reach of the river.	Any Susitna development will increase access to this relatively wilderness area. As it is easier to extend access than to limit it, achemes with the least inforent access are considered superior. This is considered a moderate factor favoring the Watana acheme.
Vee dam aite and upstream	Ecological	Inundation of reaident ficheries.	Difference between plans.	The Vec reservoir maximum pool elevation is 2330'. The Matana reservoir maximum pool elevation is 2200'. The addi- tional 130' elevation associ- ated with the Vec dam would result in the inudation of epproximately 12 additional miles of the Susitna River in this reach, 1-1/2 additional miles of the Oshetna River and 12 miles of the Tyone River.	The HDC/V plan results in a significant increase in the loss of resident fisheries habitst in this reach of the river.

TABLE 6 (Cont'd)

ENVIRONMENTAL IMPACTS ASSOCIATED WITH WATANA/DEVIL CANYON AND HIGH DEVIL CANYON/VEE DEVELOPMENT PLANS

River Reach	Environmental Attributes	Concerns	Difference in impact of two plans	Identification of difference	Appraies1 Judgezent
		Loss of moose hebitat.	Significant difference between plans.	In addition to areas inundated by the Matana reservoir, the Vee impoundment would flood 20 additional miles or criti- cal winter river bottom habi- tat in this reach utilized by st lesst three subpopulations of moose that range over large areas east of the Susitia and north of the MacLaren River reach.	The HDC/V plan would create a greater impact on moose in this section of the river. This impact on moose is judged to be of greater significance than the loss of moose hebitat in the Watana Creek area resulting from the Watana reservoir.
		Impact on caribou migra- tion.	Significant difference between plans.	Area flooded by HDC/V plan is historically used by Nelchins caribou hord. Due to increas- ed length of river flooded the HDC/V plan would create a greater division of the Nelchina herd's range.	This potential negative effect on caribou is considered a major factor in the evaluation of the HDC/V plan.
		Impact of furbearers.	Difference between plana.	hims flooded by HDC/V plan considered important to some key furbairers, particularly red fox.	This furbearer loss is judged to be greater than furbearer losses associ- atod with the inundation of the Matana Creek area.
	Cultural	Impact on archeological sites.	Potential difference between plans.	Preliminary studies indicate a high potential for discovery of archeological sites along lakes, streams and rivers in the easterly region of the Upper Susitna Basin. Addi- tional sites are expected to be located near caribou cros- sing areas. The HDC/V plan has a greater probability of inundating potential sites.	The HDC/V plan is judged to have a greater potential for creating cultural impacts in this section of the river. This is considered a moderate factor in the evaluation of plans.
	Aesthetic/ Land Use	Loss of Vee Canyon.	No significant difference ba- tween plans.	With the HDC/V plan a dam would be situated in the lower reaches of the Vee canyon thus eliminating the existing assthetic value of the canyon With the W/DC plan the Vee canyon would be inundated to depth of approximately 175'.	Not a factor in evaluation of plans.
		Access to wilderness areas.	Significant difference between plans.	In addition to the divference created by road access the formation of the Vee reservai would open a large amount of the northeast section of the basin, an isolated area pre- sently used extensively by caribou and moose.	Due to the possible impacts on caribou the access into this region created by the HDC/V plan considered a major nega- tive factor associated with this plan.

TABLE 6 (Cont'd)

ENVIRONMENTAL INPACTS ASSOCIATED WITH WATANA/DEVIL CANYON AND HIGH DEVIL CANYON/VEE DEVELOPMENT PLANS

NOTE

4

W = Watana dam DC = Devil Canyon dam HDC = High Devil Canyon dam V = Vee dam

TABLE 7

ENVIRONIZENTAL EVALUATION OF DEVIL CANYON DAH AND TUNNEL SCHEME

	, 	Appraisal			Schese Jud	jed to have
Environmental	6	(Differences in impact	Identification		the least pot	tential impact
ALEFIDUEB	LONCELUS	JE CWO SCHERES/	er difference	Appraisal Judgement	lunnel	<u>DE</u>
Ecological						
Downstream Fisheries and Wildlife	Effects resulting from changes in water quantity and quality.	No significant difference between schemes regarding effects downstream;of Devil Canyon.		Not a factor in evaluation of scheme.		
		Difference in reach be- tween Devil Canyon dam and tunnel re-regulation dam.	With the tunnel scheme con- trolled flows between regula- tion daw and downstream power- house offers potential for anadromous fisheries enhance- ment in this 11 mile reach of the river.	If fisheries enhancement oppor- tunity can be realized the tun- nel scheme offers a positive mitigation measure not available with the Devil Canyon dam scheme. This opportunity is considered moderate and favors the tunnel scheme.	X	
Resident Fisheries	Loss of resident fisheries habitat.	Hinimal differences between schemes.	Devil Canyon dam would inundate 27 miles of the Susitna River and approximately 2 miles of Devil Creek. The tunnel scheme would inundate 16 miles of the Susitna River.	This reach of river is not con- aidered to be highly significent for resident fisheries and thus the difference between the schemes is minor and favora the turnel scheme.	X	
Wildlife	Loss of wildlife habitat.	Hinimal differences between schemes.	The most sensitive wildlife has bitat in this reach is upstreas of the tunnel re-regulation das where there is no significant difference between the schemes in oddation insholates the true valley between the two das sites resulting in a moderate increase in impacts to wildlife.	The difference in loss of wild- life habitat is considered mod- erate and favors the tunnel acheme.	X	
Cultural	Inundation of archeological sites	Potential differences between schames.	Due to the larger area inun- dated the probability of inun- dating archeological sites is increased.	No significant sites have been Identified. If discovered miti- gation measures are easily im- plemented. Therefore this con- cern is not considered a factor in acheme evaluation.		
Aesthetic/ Land Use	Inundation of Devil Canyon.	Significent difference between schemes.	The Devil Canyon is considered a unique resource, 80 percent of which would be inundated by the Dévil Canyon daw scheme. Hhis would result in a loss of both an easthetic value plus the potential for white water recreation.	The sesthetic and to some extend the recreational losses associ- ated with the development of the High Devil Canyon dam is the main aspect favoring the tunnel scheme.		

OVERALL EVALUATION: The funnel scheme has overall a lower impact on the environment.

• X

Social Aspect	Parameter	TunnelDevil CanyonHigh Devil Canyon/WatanaSchemeDam SchemeVee PlanCanyon	/Devil Plan <u>Remarks</u>
Potential non-renewable resource displacement	Million tons Beluga coal, over 50 years	80 110 170 21	Devil Canyon dam scheme opotential higher than tunnel scheme. Watana/ Devil Canyon plan higher than High Devil Canyon/ Vee plan.
Impact on State economy, Impact on local economy		All projects would have similar impacts on the stat and local economy.	te Essentially no differen
Seismic exposure	Risk of major structural failure	All projects designed to similar levels of safety.	between plans/schemes.
	Potential impact of failure on human life	Any dam failures would effect the same downstream population.	

TABLE 8 - Social Evaluation of Susitna BasinDevelopment Schemes/Plans

3

2. Watana/Devil Canyon superior to High Devil Canyon/Vee plan.

TABLE 9

1

Ĵ

Î

9

1

l

4

ENERGY CONTRIBUTION EVALUATION OF THE DEVIL CANYON DAM AND TUNNEL SCHEMES

Perameter	Devil		
	Lanyon	lunnel	Remarks
Total Energy Production	an a		a an
Capability			
Annual Average Energy GWH	2850	2240	Devil Canyon dam annu-
	n an sin an		ally developes 610 GWH
Firm Annual Energy GWH	2590	2050	and 540 GWH more average
			and firm energy re-
			spectively than the
			the Tunnel scheme.
% Basin Potential			Devil Conver schemes
Developed (1)	43	37	develops more of the
			hasin notential
			odorn hoccurrat
Energy Potential Not			
Developed GWH	60	380	As currently envisaged,
			the Devil Canyon dam
			does not develop 15 ft
			gross head between the
		•	Watana site and the
			Devil Canyon reservoir.
			the tunnel scheme in-
			corporates additional
			tuppels Also the set
			nensation flow released
			from re-regulation dam
			is not used in conjunc-
		•	tion with head between
			re-regulation dam and
			Devil Canyon.
			stef.

Votes:	(1)	Based on a	innual average	e energy.	Full	potential	based	on USBR	four
		dam scheme	(Reference).					di sa di

TABLE 10 - OVERALL EVALUATION OF TUNNEL SCHEME AND DEVIL CANYON DAM SCHEME

is

.

Î

-11

ATTRIBUTE	SUPERIOR SCHEME			
ECONOMIC	DEVIL CANYON DAM			
ENERGY CONTRIBUTION	DEVIL CANYON DAM			
ENVIRONMENTAL	TUNNEL			
SOCIAL	DEVIL CANYON DAM (MARGINAL)			
OVERALL EVALUATION	DEVIL CANYON DAM SCHEME IS SUPERIOR			

DEVIL CANYON DAM SCHEME IS SUPERIOR

TRADE OFFS MADE:

ECONOMIC ADVANTAGE OF DAM SCHEME IS JUDGED TO OUTWEIGH THE REDUCED ENVIRONMENTAL IMPACT ASSOCIATED WITH THE TUNNEL SCHEME.

TABLE 11 ENVIRONMENTAL EVALUATION OF WATANA/DEVIL CANYON AND HIGH DEVIL CANYON/VEE DEVELOPMENT PLANS

. .

.

			Plan judged to have the		
Environmental Attribute	Plan Comparison	Appraisal Judgement	HDC/V	W/DC	
Ecological 1) Flateries	No significant difference in effects on downstream anadromous fisheries. HDC/V would inundate approximately 95 miles of the Susitha River and 28 miles of tributary streams, in- cluding the Tyone River. W/DC would inundate approximately 84 miles of the Susitha River and 24 miles of tributary streams, including Watena Creek.	Due to the avoidance of the Tyone Rivar, lesser inundation of reaident fisherles habitat and no significant difference in the effects on anadromous fisherles, the N/DC play is judged to have less impact.			
2) Wildlife a) Hoose	HDC/V would inundate 123 miles of critical winter river bottom habitat.	Due to the lower potential for direct impact on moose populations within the Suaitna, the M/DC plan is judged superior.			
	W/DC would inundate 100 miles of this river bottom habitat.				
	HDC/V would inundate a large area upstress of Vee utilized by three sub-populations of mess that range of large areas of the northeast section of the basin.				
	W/DC would inundate the Matana Creek area utilized by moose. The condition of this sub-population of moose and the quality of the habitat they are using appears to be decreasing.				
b) Caribou	The increased length of river flooded, especially up- etrees from the Vee dam site, would result in the HDC/V plan creating a greater potential division of the Neichina herd's range. In addition, an increase in range would be directly inundated by the Vee rea- ervoir.	Due to the potential for a greater impact on the Melchina caribou hard, the HDC/V acheme is considered inferior.			
c) Furbearers	The area flooded by the Vee reservoir is considered important to some key furbearers, particularly red fox. This area is judged to be more important than the Watana Creck area that would be inundated by the W/DC plan.	Due to the lesser potential for impact on fur- bearers the W/DC is judged to be superior.			
d) Birds and Bears	Foreat habitat, important for birds and bears, exists along the valley slopes. The loss of this habitat would be greater with the W/DC plan.	The HDC/V plan is judged superior.			
<u>Eultural</u>	There is a high potential for discovery of archeologi- cel sites in the easterly region of the Upper Susitna Basin. The HDC/V plan has a greater potential of affecting these sites. For other reaches of the river the difference between plans is considered minimal.	The W/DC plan is judged to have a lower po- tential effect on archeological sites.		X	

TABLE 11 ENVIRONMENTAL EVALUATION OF NATANA/DEVIL CANYON AND HIGH DEVIL CANYON/VEE DEVELOPMENT PLANS

			Plan judged least poten	to have the
Environments1 Attribute	Plan Comparison	Appraisal Judgement	HDC/V	W/DC
Aesthatic/ Land Use	With either scheme, the mesthetic quality of both Davil Canyon and Vee Cenyon would be impaired. The HDC/V plan would also inundate Tausena Falls. Due to construction at Vee Dam site and the size of	Both plans impact the valley seathetics. The difference is considered minimals As it is easier to extend access then to	-	• • • • • • • • • • • • • • • • • • •
	the Vee Reservoic, the PDC/V pion would inherencify create access to more wilderness area then would the W/DC plan.	considered detrimental and the W/DC plan is judged superior. The ecological sensitivity of the area opened by the HDC/V plan rein- forces this judgement. Due to the lower potential for direct impact on moose populations within the Susitna, the W/DC plan is judged superior.		

DVERALL EVALUATION: The W/DC plan is judged to be superior to the HDC/V plan. (The lower impact on birds and bears associated with HDC/V plan is considered to be outweighed by all the other impacts which favour the W/DC plan.)

NOTE:

- W = Watone Dam DC = Devil Canyon Dam HDC = High Devil Canyon Dam V = Veo Dam

TABLE 12

.

Í

Parameter	Watana/ Devil Canyon	High Devil Canyon/Vee	Remarks
Total Energy Production Capability			
Annual Average Energy GWH	6070	4910	Watana/Devil Canyon plan annually devel-
Firm Annual Energy GWH	5520	3870	opes 1160 GWH and 1650 GWH more average
			and firm energy re- pectively than the High Devil Canyon/Vee Plan.
<u>% Basin Potential</u> <u>Developed</u> (1)	91	81	Watana/Devil Canyon plan develops more of the basin potential
Fnergy Potential Not			
<u>Developed</u> GWH (2)	60	650	As currently con- ceived, the Watana/- Devil Canyon Plan does not develop 15
			ft of gross head between the Watana
			site and the Devil Canyon reservoir.
			ine High Devil Canyon/Vee Plan does not develop 175 ft

ENERGY CONTRIBUTION EVALUATION OF THE WATANA/DEVIL CANYON AND HIGH DEVIL CANYON/VEE PLANS

<u>Notes</u>: (1) Based on annual average energy. Full potential based on USBR four dam scheme (Reference). (2) Includes losses due to unutilized head.

.

gross head between Vee site and High

Devil reservoir.

TABLE 13 - OVERALL EVALUATION OF THE HIGH DEVIL CANYON/VEE AND WATANA/DEVIL CANYON DAM PLANS

ATTRIBUTE	SUPERIOR PLAN			
ECONOMIC	WATANA/DEVIL CANYON			
ENERGY CONTRIBUTION	WATANA/DEVIL CANYON			
ENVIRONMENTAL	WATANA/DEVIL CANYON			
SOCIAL	WATANA/DEVIL CANYON (MARGINAL)			

OVERALL EVALUATION

16

Í

Í

Ì

Ĩ

PLAN WITH WATANA/DEVIL CANYON IS SUPERIOR TRADEOFFS MADE: NONE

TABLE 14

ECONOMIC SENSITIVITY OF COMPARISON OF GENERATION PLAN WITH WATANA/DEVIL CANYON AND THE ALL THERMAL PLAN

Present worth of Net Benefit (\$ willion) of total generation system costs for the Watana/Devil Canyon plan over the all thermal plan.

Parameters		Present worth (\$ million)	Remarka
ECONOMIC EVALUATION: Base Case		2280	Watana/Devil Canyon plan more economical than the all thermal plan.
SENSITIVITY ANALYSES: Parameter	Sensitivity Analyses		
LOAD GROWTH	Low LHC Low High	1280 1570 2840	The net benefit of the Watana/Davil Canyon Plan re- mains positive for the range of load forecasts con- sidered.
CAPITAL COST ESTIMATE	Low Thermal Cost" High Hydroelectric Cost"	1850 1320	System costs relatively insensitive. Capital cost estimating uncertainty does not effect economic ranking.
PERIOD OF ECONOMIC ANALYSIS	Period shortened to (1980 - 2010)	2260 960	Shorter period of evaluation decreases aconomic dif- ferences. Ranking remains unchanged.
DISCOURT RATE	5% 8% (interpolated) 9%	940 0 -80	Below discount rate of 8% the Watene/Devil Canyon plan is economically superior. o
FUEL COST	Low***	1810	
FUEL COST ESCALATION	0% escalation for all fuels 0% escalation for coal only	200 ×	Watana/Davil Canyon plan remains economically super- ior for wide range of fuel prices and escalation rates.
ECONOMIC THERMAL PLANT LIFE	50% extension to all thermal plant life	1800	Economic benefit for Watana/Devil Eanyon plan rela- tively insensitive to extended thermal plan economic life.

*Thermal capital cost decreased by 22% **Based on estimated Susitna cost plus 50% **Fuel Costs reduced by 20%

TABLE 15 - Social Comparison of System Generation Plan with Watana/Devil Canyon and the All Thermal Plan

Social Aspect	Parameter	All Thermal Generation Plan	Generation Plan with Watana/Devil Canyon	Remarks
Potential non-renewable resource dis- placement	Million tons of Beluga coal, over 50 years		210	With Watana/Devil Canyon plan is superior.
Impact on state economy Impact on local economy	Direct & indirect employment and income. Business invest- ment.	Gradually, continuously growing impact.	Potentially more disruptive impact on economics.	
Seismic exposure	Risk of major structural failure	All projects designed safety	to similar levels of	
	Potential impact of failure on human life	Failure would effect only operating personnel. Forecast of failure would be impossible	Failure would effect larger number of people located downstream, however, some degree of forecasting dam failure would be impossible	

1. 8. 1

Overall Comparison

• • •

• द्वा द्व

> с. .

> > Inconclusive

TABLE 16

GENERIC COMPARISON OF ENVIRONMENTAL IMPACTS OF A SUSITNA BASIN HYDRO DEVELOPMENT VERSUS COAL FIRED THERMAL GENERATION IN THE BELUGA COALFIELDS

Ĵ

3

Environmental	Concerns	
Attributes	Susitna Basin Development	Thermal Generation
Ecological:	Potential impact on fisheries due to alteration of downstream flow distribution and water quality. Inundation of Moose and	Potential for impact on fisheries resulting from water quality impairment of local streams and local habitat destruction due to
	furbear habitat and potential impact on Caribou migration. No major air quality problems, only minor microclimatic changes would occur.	surface disturbances both at mine and generating facilities. Impact on air quality due to emission of particulates SO ₂ , NO _X , trace metals and water vapours from generating facilities.
Cultural:	Inundation of archeological sites.	Potential destruction of archeological sites.
Aethetic/ Land Use:	Inundation of large area and surface disturbance in construction area. Creates additional access to wilderness areas, reduces river recreation but increases lake recreational activities.	Surface disturbance of large areas associated with coal mining and thermal generation facilities. Creates additional access and may restrict land use activities.

5
TABLE 17 - OVERALL EVALUATION OF ALL THERMAL GENERATION PLANS WITH THE GENERATION PLAN INCORPORATING WATANA/DEVIL CANYON DAMS

3

5

ATTRIBUTE	SUPERIOR PLAN					
ECONOMIC	WITH WATANA/DEVIL CANYON					
ENERGY CONTRIBUTION	NO DIFFERENCE					
ENVIRONMENTAL	UNABLE TO DISTINGUISH DIFFERENCE IN					
	THIS STUDY					
SOCIAL	NO DIFFERENCE					
•						
OVERALL	PLAN WITH WATANA/DEVIL CANYON IS SUPERIOR					
EVALUATION	TRADEOFFS MADE: NOT FULLY EXPLORED					



TABLE 1

SALIENT FEATURES OF GENERATION PLANNING PROGRAMS

Program/ Developer	Load Modeling	Generation Modeling	Optimization Available	Reliability Criterion	Production Simulation	Availability and Cost/Run
GENOP/ Westinghouse	Done by two external programs	Done by one external program	yes	LOLP or % reserve	Deterministic or Modified Booth - Baleriaux	\$500 to validate Learning Curve Costs \$300 - \$800//vun
PROMOD/EMA	Done by one external program	Done by one external program	no	LOLP or % reserve	Modified Booth - Baleriaux	\$2,500 to validate on TYMSHARE Learning Curve Costs \$300 - \$500/run
OGP/GE	Done by one external program	Done by one external program	yes	LOLP or % reserve	Deterministic or Stochastic	AAI validated Columbia & Buffalo Experienced Personnel \$50 - \$800/run

Ŷ

TABLE Z

2

Low Fo	recast	Mid Fo	recast	High F	orecast
MW	GWn	MW	GWh	MW	GWh
514	2,789	514	2,789	514	2,789
578	3,158	650	3,565	695	3.859
641	3,503	735	4,032	920	5,085
797	4,351	944	5,171	1,294	7,119
952	5,198	1,173	6,413	1,669	9,153
1,047	5,707	1,379	7,526	2,287	12,543
1,141	6,215	1,635	8,938	2,209	15,933
	Low Fo MW 514 578 641 797 952 1,047 1,141	Low Forecast MW GWh 514 2,789 578 3,158 641 3,503 797 4,351 952 5,198 1,047 5,707 1,141 6,215	Low Forecast Mid Fo MW GWh MW 514 2,789 514 578 3,158 650 641 3,503 735 797 4,351 944 952 5,198 1,173 1,047 5,707 1,379 1,141 6,215 1,635	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c c c c c c c c c c c c c c c c c c c $

~1

LOAD AND ENERGY FORECASTS* ALASKA RAILBELT AREA

* Derived from the Woodward-Clyde Consultants submittal of September 23, 1980, adjusted to eliminate industrial self-supplied and two-thirds of the military sector.

TABLE . 3

· .

ŝ

ANNUAL FIXED CARRYING CHARGES USED IN GENERATION PLANNING MODEL

	Project Life/Type					
	30-Year	35-Year	50-Year	20-Year		
	Thermal	Thermal	Hydro	Thermal		
	(%)	(%)	(%)	(%)		
ECONOMIC PARAMETERS (0%-3%)					
Cost of Money	3.00	3.00	3.00	3.00		
Amortization	2.10	1.65	0.89	3.72		
Insurance	<u>0.25</u>	0.25	<u>0.10</u>	0.25		
TOTALS	5.35	4.90	3.99	6.97		

TABLE 4

4

FUEL PRICES AND ESCALATION RATES

	Natural Gas	Coal	Distillate
Base Period (January 1980) Prices (\$/million Btu)			******
Market Prices Shadow (Opportunity) Values	\$1.05 2.00	\$1.15 1.15	\$4.00 4.00
Real Escalation Rates (Percentage Change Compounded Annually)	je		
1980 - 1985 1986 - 1990 1991 - 1995 Composite (average) 1980 - 1995 1996 - 2005 2005 - 2010	1.79% 6.20 3.99 3.98 3.98	9.56% 2.39 -2.87 2.93 2.93	3.38% 3.09 4.27 3.58 3.58
	ΰ	0	0 · · · ·

2.4

えご

TABLE 5.

41

•

SUMMARY OF ECONOMIC PARAMETERS FOR GENERATION PLANNING 1 - Base Period (January 1980) Energy Prices (\$/million Btu) 1.1 - Natural Gas 1.2 - Coal 2.00 1.3 - Distillate 1.15 4.00 2 - General Price Inflation Per Year (%) not applicable 3 - Discount & Interest Rates Per Year (%) 3.1 - Real Discount Rate 3.2 - Nominal Interest Rate 3 (Non-exempt Case) not applicable 3.3 - Nominal Interest Rate not applicable (Tax-exempt Case) 4 - Non-energy Cost Escalation Per Year (%) 0 5 - Energy Price Escalation Per Year (%) 5.1 - Natural Gas 1980 - 2005 2006 - 2010 3.98 5.2 - Coal 0 1980 - 2005 2006 - 2010 2.93 5.3 - Distillate 0 1980 - 2005 2006 - 2010 3.58 0 6 - Economic Life (Years) 6.1 - Large Steam Turbine 6.2 - Small Steam Turbine 6.3 - Hydro 30 35 6.4 - Diesel and Gas Turbine 50 (Gas-fired) 30 6.5 - Gas Turbine (Oil-fired) 20

TABLE	6 TEN	YEAR	BASE	GENERATION	PLAN	MTD	INAD	FORECAS	T

VEAD	and a second		SYSTEM (MW)					TOTAL	
TEAK	Committed	MW Retired	COAL	NG GT	OIL GT	OIL DIESEL	CC	HY	CAPABILITY (MW)
1980			54	470	168	65	141	49	947*
1981	an an ann an Anna an Anna. Ann an Anna Anna Anna Anna Anna Anna An	andar († 1969), andar 1979 - H ard State 1979 - Antonio State	54	470	168	65	141	49	947
1982	60 CC		54	470	168	65	201	49	1007
1983			54	470	168	65	201	49	1007
1984			54	470	168	65	201	49	1007
1985		14 (NGGT)	54	456	168	65	201	49	993
1986			50	456	168	65	201	49	993
1987		4 (Coal)	50	456	168	65	201	49	989
1988	95 HY	-	50	456	168	65	201	144	1084
1989		5 (Coal)	45	456	168	65	201	144	1079
1990		•	45	456	168	65	201	144	1079
								•	

*This figures varies slightly from the 943.6 MW reported due to internal computer rounding.

<u>Plan</u>	Stage	Description	On-line Month/Year	Construction Period (Yrs)	Total Cost* Million 1980\$	Installed Capacity	Peak Month Firm Capacity
ELO	1	Watana Low Dam	1/92	8	1774	400 ML	000 374
EnZ	2	Kaise Watana Dam	1/95	3 s ta 25	376	ALL DOL	206 MW
	3	Add Capacity	1/97	3	136	400 MU	194 MW
	4	Devil Canyon Dam	1/02	7	000	400 MH	400 MW
					JJJ	TAL 1200 MU	352 MW
	1	High Watana Dam					1152 MW
	2	Add november of the	6/93	9	1984	400 MU	AOO MEL
E1.3	2	Add powernouse capacity	1/96	3	157	400 MW	400 FIN
	3	Devil Lanyon Dam	1/00	7	999	400 MW	400 FIN 252 Mil
					TC	TAL 1200 MW	1152 MW
	1	Watana High Dam	6/93	0	1001		
ter 📥 🖓 🖓	2	Devil Canyon Dam	1/00	 	1984	400 MW	400 MM
			1) 00		· · · · · · · · · · · · · · · · · · ·	400 MW	337 MW
					10	IAL 800 MW	737 MW
	1	High Devil Canyon Dam	1/94	R	1670		
1	2	Vee Dam	1/00	7	1370	400 MW	351 MW
			~, 00		11//	400 MW	315 MW
	• . * •				10	TAL 800 MW	666 MW
	. 1	Watana High Dam	6/93	Q	1004		
1.5	2	Add powerhouse capacity	1/96	3	1984	400 MW	400 MW
	3	Add tunnel capacity	1/00	5	10/	400 MW	400 MW
			1700	J	1015	<u>380 MW</u>	194 MW
					10	IAL 1180 MW	994 MW
Comp.	1	Chakachamna	1/93	10	1201	500 MU	·
Hydro	2	Keetna	1/97	0	1201	500 MW	500 MW
	3	Snow	1/02	C C	403	120 MW	77 MW
			↓ 1 ∨f ω		223 ·	50 MW	22 MW
					nden en de la 10. En entre	IAL 670 MW	599 MW
				an an taon ann an taonach an taon an ta			

TABLE ? SUSITNA BASIN HYDROELECTRIC ALTERNATIVES

*Includes Interest During Construction (IDC) But excludes cost of levergulation dams *+ Two tunnel scheme

TABLE 8 SUMMARY OF BASE GENERATION PLANS - MID LOAD FORECAST - 1200MW SUSITNA ALTERNATIVES

		SUSITNA ALTERNATIVES							
	W/DC 1.2	W/DC E1.3	HDC/VEE E 2.3	HDC/CC	W/ 1 ** 1.5				
PARAMETER / JOB I.D.#	L5Y9	L8J9	L601	LEB3	1.607				
1990 MW	1079 MW	1079 MW	1079 MW	1079 MW	1079 MW				
1990-2010 THERMAL ADDS:									
Coal (MW)	200	300	300	300	200				
NGGT (MW)	300	225	450	525	450				
Diesels (MW)		_0	20	_220	30				
TOTAL	500 MW	525 MW	770 MW	1045 MW	680 MW				
RETIREMENTS (MW)	(734)	(734)	(734)	(734)	(734)				
HYDRO ADDS:	1/92 W400								
MONTH/YEAR NAME MW	1/95 + Dam	6/93 W400	6/93 HDC400	6/93 HDC400	6/93 W400				
	1/97 W400	1/96 W400	1/96 HDC400	1/96 HDC400	1/96 W400				
	1/02 DC400	1/00 DC400	1/00 VEE400	1/00 CC500	1/00 T380				
TOTAL FIRM* (2010)	1997 MW	2023 MW	2230 MW	2690 MW	2034 MW				
$$ \times 10^6$ (80\$)									
10 Year PW	\$ 873.7	\$ 873.7	\$ 873.7	\$ 873.7	\$ 873.7				
20 Year PW	2509.4	2360.6	2487.8	2624.5	2591.0				
TOTAL	\$3383.1	\$3234.3	\$3361.5	\$3273.2	\$3464.7				
LONG TERM (2040) PW	\$6028	\$5851	\$6372	\$6209	\$6528				

*In Peak Month (December)

** Two funnel schene

.

	SUSITNA ALTERNATIVES							
	W800	HDC800	W400/DC400	HDC/Vee				
PARAMETERS / JOB I.D.#	L7W7	LE07	LCK5	LB25				
1990 MW	1079 MW	1079 MW	1079 MW	1079 附以				
1990-2010 THERMAL ADDS: Coal (MW) NGGT (MW) Diesels (MW)	500 450 -	500 450 <u>30</u>	200 525 <u>50</u>	400 450 <u>60</u>				
TOTAL	950 MW	980 MW	775 MW	910 NW				
RETIREMENTS (MW)	(734)	(734)	(734)	(734)				
HYDRO ADDS: MONTH/YEAR NAME MW	6/93 W400 1/96 W400	6/93 HDC400 1/96 HDC400	6/93 W400 1/00 DC400	1/94 HDC 400 1/00 VEE 400				
TOTAL FIRM* MN (2010)	2095 MW	2125 MW	1858 MW	1921 NW				
$\frac{$ \times 10^{6} (80$)}{10 \text{ year PW}}$ 20 year PW	\$ 873.7 <u>2765.1</u>	\$ 873.7 <u>2628.0</u>	\$ 873.7 	\$ 873.7 <u>2624.5</u>				
TOTAL	\$ 3638.8	\$ 3501.7	\$ 3223.3	\$ 3498.2				
LONG TERM (2040) PW	\$ 6955	\$ 6715	\$ 5891	\$ 6620				

TABLE 9 SUMMARY OF GENERATION PLANS - MID LOAD FORECAST - 800 MWALTERNATIVES

* In peak month - December

U

		ALTER	NATIVE			
TABLE IO	SUMMARY	OF BASE	GENERATION	PLANS -	MID	LOAD FORECAST

10

	THERMAL			
PARAMETER / JOB I.D.#	RENEWS LME3	NO RENEWS LME1	AND OTHER HYDRO LFL7	actided 19200
1990 MW	1079 MW	1079 MW	1079 MW	•
1990-2010 THERMAL ADDS: Coal (MW) NGGT (MW) Diesels (MW)	456 RN** 900 150 <u>40</u>	900 600 50	700 300 10	
TOTAL	1546 MW	1550 MW	1010 MW	
RETIREMENTS (MW)	(734)	(734)	(734)	
HYDRO ADDS: MONTH/YEAR NAME MW			1/93 Chaka 500 1/97 Keetna 120 1/02 Snow 50	
TOTAL FIRM* MW(2010)	1891 MW	1895 MW	1954 MW	
$\frac{$ \times 10^{6} (80$)}{10 \text{ Year PW}}$ 20 Year PW	\$ 873.7 <u>3308.3</u>	\$ 873.7 <u>3319.4</u>	\$ 873.7 2802.2	
TOTAL	\$4182.0	\$4193.1	\$3675.9	
LONG TERM (2040) PW	\$8109	\$8133	\$7038	

*In Peak Month (December) **RN - renews

J

TABLE 11 SUMMARY OF SUSITNA GENERATION PLANS - HIGH LOAD FORECAST

	SUSITNA ALTERNATIVES						
PARAMETER / JOB I.D.#	3AE LA73	HDC/VEE LBV3	HDC/VEE/CC LBY1	W/W/DC/CIC LBV7			
1990 MW (+100 MW COAL)	1179 MW	1179 MW	1179 MW	1179 MW			
1990-2010 THERMAL ADDS: Coal (MW) NGGT (MW) Diesels (MW)	900 750 –	1200 750 90	900 675 <u>10</u>	700 450 <u>60</u>			
TOTAL	1650 MW	2040 MW	1585 MW	1210 MW			
RETIREMENTS (MW)	(734)	(734)	(734)	(734)			
HYDRO ADDS: MONTH/YEAR NAME MW	6/93 W400 1/96 W400 1/00 DC400	6/93 HDC400 1/96 HDC400 1/00 VEE400	6/93 HDC400 1/96 HDC400 1/00 VEE400 1/03 CC500	6/93 W400 1/96 W400 1/00 DC400 1/05 CC500			
TOTAL FIRM* MU (2010)	3248 MW	3600 MW	3645 MW	3308 MW			
<u>\$ x 10⁶ (80\$)</u> 10 year PW 20 year PW TOTAL	\$ 1060.5 <u>4094.6</u> \$ 5155.1	\$ 1060.5 <u>4462.4</u> \$ 5522.9	\$ 1060.5 <u>4252.9</u> \$ 5313.4	\$ 1060.5 <u>3946.3</u> \$ 5006.8			
LONG TERM (2040) PW	\$10,678	\$11,719	\$11,037	\$10,048			

*In peak month - December **RMArenews

.

TABLE 12 SUMMARY OF SUSITNA GENERATION PLANS - LOW LOAD FORECAST

PARAMETER / JOB I.D. #	W400/DC400 LC07	HDC/VEE LGO ?	HDC400 LBU1	W400 LBK7	W400//T** L609
1990 MW	1079MW	1079MW	1079MW	1079MW	10790W
1990-2010 THERMAL ADDS: Coal (MW) NGGT (MW) Diesels (MW)	150 40	100 225 <u>30</u>	400 300	200 300 <u>80</u>	375 20
TOTAL	190MW	355MW	700MW	580MW	395MW
RETIREMENTS (MW)	(734)	(734)	(734)	(734)	(734)
HYDRO ADDS: MONTH/YEAR NAME MW	6/93 W400 1/02 DC400	6/93 HDC400 1/02 VEE400	6/93 HDC400	6/93 W400	6/93 W400 1/02 T380
TOTAL FIRM* (2010)	1272MW	1367MW	1396MW	1325MW	1319MW
$\frac{$ \times 10^{6} (80$)}{10 \text{ year PW}}$ 20 year PW	\$ 744.1 <u>1835.8</u>	\$ 744.1 <u>1894.9</u>	\$ 744.1 1961.6	\$ 744.1 2029.7	\$ 744.1 2048.5
TOTAL	\$ 2579.9	\$ 2639.0	\$2705.7	\$2773.8	\$2792.6
LONG TERM (2040) PW	\$ 4350	\$ 4557	\$4852	\$4940	\$4997
					the second s

*In peak month - December

Two tunnel scheme

• :

TABLE 13

.

Í

Ì

SUMMARY OF GENERATION PLANS - LOAD MANAGEMENT AND CONSERVATION

PARAMETER / JOB I.D.#	THERMAL NO RENEWS LBT7	SUSITNA #400/D400
1990-2010 THERMAL ADDS: Coal (MW)	1079 MW	1079 MW
NGGT (MW) Diesels (MW)	500 225 90	450
TOTAL RETIREMENTS (MW)	815 MW	500 MW
HYDRO ADDS: MONTH/YEAR NAME MW	(734)	(734)
TOTAL FIRM* MW 2010	1160 MW	1/97 W400 1/05 DC400
$\frac{5 \times 10^{\circ} (80\$)}{10 \text{ year PW}}$ 20 year PW	\$ 721.9	1582 MW \$ 721 a
TOTAL	\$ 2756.2	1556.0
	\$ 4931	\$ 3648

*In peak month - December

TABLE 14. SUMMARY OF GENERATION PLANS - PROBABILISTIC LOAD FORECAST

PARAMETER / JOB I.D.#	THERMAL NO RENEWS LOF3	SUSITNA 3AE 1875
1990 MW	1079 MW	1070 MU
1990-2010 THERMAL ADDS: Coal (MW)		1079 MW
NGGT (MW) Diesels (MW)	1100 1575 100	200 1275 140
TOTAL	2775 MW	1615 MW
RETIREMENTS (MW)	(734)	(734)
HYDRO ADDS: MONTH/YEAR NAME MW		6/93 W400 1/96 W400 1/02 DC400
TOTAL FIRM* MW 2010	3120 MW	3112 MW
$\frac{5 \times 10^6 (805)}{10 \text{ year PW}}$ 20 year PW	\$ 873.7 3353.6	\$ 873.7 2546.5
TOTAL	\$4227.3	\$3420.2
ONG TERM (2040) PW	۶ 8324 ه	\$6292

*In peak month - December

-

.

.

TABLE 15 INPUT PARAMETERS - INTEREST RATE SENSITIVITY

×.,

1

Input Variable	3 Percent	Interest Rates 5 Percent	9 Percent
Annual Fixed Carrying Charges (%)			
30 Year Thermal	5.35%	6.75%	9.98%
20 Year Thermal	6.97	8.27	11.20
50 Year Hydro	3.99	5.58	9.37
Total Capital Costs (\$ x 10 ⁶)			
250 MW Coal	\$ 686	\$ 727	\$ 815
75 MW NGGT	26	26.3	27
10 MW Diesel	10	10.3	10.4
1 - Watana 400	\$ 1984	\$ 2175	\$ 2589
2 - Watana 400	157	161	168
3 - Devil Canyon 400	999	1069	1224

TABLE16SENSITIVITY ANALYSIS - INTEREST RATES

16

THERMAL			SUSITNA - 3AE			
BASECASE LME1	SENSI LEA9	TIVITY LEB1	BASECASE L8J9	SENSIT LF85	IVITY LF87	
0% - 3%	0% - 5%	0% - 9%	0% - 3%	0% - 5%	0% - 9%	
900 600 50	900 600 50	900 600 50	300 225	300 225 -	300 225	
1550 MW	1550 MW	1550 MW	525 MW	525 MW	525 MW	
(734)	(734)	(734)	(734)	(734)	(734)	
-			6/93 W400 1/96 W400 1/00 DC400	6/93 W400 1/96 W400 1/00 DC400	6/93 W400 1/96 W400 1/00 DC400	
1895 MW	1895MW	1895 MW	2023 MW	2023 MW	2023 MW	
\$ 873.7 3319.4 \$4193.1	\$ 791.1 2441.7 \$3232.8	\$ 714.8 1367.2 \$2082.0	\$ 873.7 2360.6 \$3234.3	\$ 791.1 1977.3 \$2768.4	\$ 714.8 1469.2 \$2184.0	
\$8133	\$5172	\$2609	\$5851	\$4226	\$2691	
	BASECASE LME1 0% - 3% 900 600 50 1550 MW (734) (734) - 1895 MW \$873.7 3319.4 \$4193.1 \$8133	THERMALBASECASE LME1SENSI LEA9 $0\% - 3\%$ $0\% - 5\%$ 900 600 50 900 600 50 1550 MW 900 600 50 1550 MW 1550 MW (734) (734) (734) (734) 1895 MN 1895 MW $$873.7$ 3319.4 $$791.1$ 2441.7 $$4193.1$ $$3232.8$ $$3232.8$ $$8133$ $$5172$	THERMALBASECASE LME1SENSITIVITY LEA9 $0\% - 3\%$ $0\% - 5\%$ $0\% - 9\%$ 900 600 50 900 600 50 900 600 50 1550 MW 1550 MW 1550 MW (734) (734) (734) (734) (734) (734) 1895 MW 1895 MW $\$ 873.7$ 3319.4 $\$ 791.1$ 2441.7 $\$ 714.8$ 1367.2 $\$4193.1$ $\$ 3232.8$ $\$ 2082.0$ $\$8133$ $\$5172$ $\$ 2609$	THERMALBASECASE LME1SENSITIVITY LEA9BASECASE LBJ9 $0\% - 3\%$ $0\% - 5\%$ $0\% - 9\%$ $0\% - 3\%$ 900 900 900 300 600 300 225 50 50 50 $ 1550$ MW 1550 MW 1550 MW 525 MW (734) (734) (734) (734) $ 6/93$ M400 $1/96$ W400 $1/00$ DC400 1895 MN 1895 MW 1895 MW 2023 MW\$ 873.7 3319.4 $$791.1$ $$ 3232.8$ $$714.8$ $$2082.0$ $$873.7$ $$3234.3$ \$8133\$5172\$2609\$5851	THERMALSUSITNA - 3AEBASECASE LME1SENSITIVITY LEA9BASECASE LEB1SENSIT LB39SENSIT LF85 $0\% - 3\%$ $0\% - 5\%$ $0\% - 9\%$ $0\% - 3\%$ $0\% - 5\%$ 900 600 600 600 600 50 900 50 300 225 $-$ $ 300$ $-$ $ 1550$ MW 1550 MW 1550 MW 525 MW 525 MW (734) (734) (734) (734) (734) $ 6/93$ W400 $1/96$ W400 $1/00$ DC400 $1/96$ W400 $1/00$ DC400 1895 MW 1895 MW 2023 MW 2023 MW $\$ 873.7$ $$319.4$ $\$791.1$ $$3232.8$ $\$2082.0$ $\$3234.3$ $\$2768.4$ $\$8133$ $\$5172$ $\$2609$ $\$5851$ $\$4226$	

*In Peak Month (December)

TABLE 17. SENSITIVITY ANALYSIS - FUEL COSTS

THE	RMAL	SUSITNA - 3AE		
BASECASE, LME1	SENSITIVITY L1K7	BASECASE L8J9	SENSITIVITY L533	
\$1.15 \$2.00 \$4.00	\$0.92 \$1.60 \$3.20	\$1.15 \$2.00 \$4.00	\$0.92 \$1.60 \$3.20	
900 600 50	800 675 70	300 225	100 375 20	
1550 MW	1545 MW	525 MW	495 MW	
(734)	(734)	(734)	(734)	
		6/93 W400 1/96 W400 1/00 DC400	6/93 W400 1/96 W400 1/00 DC400	
1895 MW	1890 MW	2023 MW	1993 MW	
\$ 873.7 3319.4	\$ 716.5 2880.0	\$ 873.7 2360.6	\$ 716.5 2145.2	
\$4193.1	\$3596.5	\$3234.3	\$2861.7	
\$8133	\$7072	\$5851	\$5260	
	THE BASECASE, LME1 \$1.15 \$2.00 \$4.00 900 600 50 1550 MW (734) (734) 1895 MW \$873.7 3319.4 \$4193.1 \$8133	THERMAL BASECASE, SENSITIVITY LME1 L1K7 \$1.15 \$0.92 \$2.00 \$1.60 \$4.00 \$3.20 900 800 600 675 50 70 1550 MW 1550 MW (734) (734) 1895 MW \$ 873.7 \$ 716.5 3319.4 2880.0 \$ 4193.1 \$ 3596.5 \$8133 \$ 7072	THERMAL SUSITY BASECASE, LME1 SENSITIVITY BASECASE L8J9 \$1.15 \$0.92 \$1.15 \$2.00 \$1.60 \$2.00 \$4.00 \$3.20 \$4.00 900 800 300 600 675 225 50 70 - 1550 MW 1545 MW (734) (734) (734) - - 6/93 W400 1/96 W400 1/00 DC400 1895 MW 1890 MW 2023 \$ 873.7 \$ 716.5 \$ 873.7 \$ 3319.4 2880.0 \$ 84193.1 \$ 33596.5 \$ 33234.3 \$ \$8133 \$ 8133 \$ 7072 \$ 5851	

* In Peak Month (December)

1

2

NOTE: Sensitivity analysis performed using 0% escalation, 3% interest rate and the midload forecast.

TABLE :	18	SENSITIVITY	ANALYSIS -	FUEL	COST I	ESCALATION	
		the second s	والمتحافظ والمحافظ فالمتك مستحين فتنتج ومستحين فيشته والمستجرين	the state of the s			

		THERMAL			SUSITNA - JAE			
PARAMETER / JOB I.D.#	BASECASE LME1	SENSITI L547	VITY L561	BASECASE L8J9	SENSITI L557	L563		
ENEL COST ESCALATION DATES	(4)							
Natural Gas Coal Oil	3.98% 2.93% 3.58%	0% 0% 0%	3.98% 0% 3.58%	3.98% 2.93% 3.58%	0% 0% 0%	3.98% 0% 3.58%		
1990-2010 THERMAL ADDS: Coal (MW) NGGT (MW) Diesels (MW)	°900 600 50	1500 10	1100 525 10	300 225 -	450 30	300 225		
TOTAL	1550 MW	1510 MW	1635 MW	525 MW	480 MW	\$25 MW		
RETIREMENTS (MW)	(734)	(734)	(734)	(734)	(734)	(734)		
HYDRO ADDS: MONTH/YEAR NAME MW				6/93 W400 1/96 W400 1/00 DC400	6/93 W400 1/96 W400 1/00 DC400	6/93 W400 1/96 W400 1/00 DC400		
TOTAL FIRM* MW 2010	1895 MW	1855 MW	1980 MW	2023 MW	1978 MW	2023 MW		
<u>\$ x 10⁶ (80\$)</u> 10 year PW 20 year PW	\$ 873.7 3319.4	\$ 721.8 1835.0	\$ 865.4 2854.6	\$ 873.7 2360.6	\$ 721.8 1806.4	\$ 865.4 2307.1		
TOTAL	\$4193.1	\$2556.8	\$3720.0	\$3234.3	\$2528.2	\$3172.5		
LONG TERM (2040) PW	\$8133	\$4558	\$6916	\$5851	\$4357	\$5586		

* In Peak Month (December)

ju:

NOTE: Sensitivity analysis performed using 0% escalation, 3% interest rate and the mid load forecast.

TABLE ______ SENSITIVITY ANALYSIS - THERMAL PLANT RETIREMENT POLICY

	THE	RMAL	SUSITN	SUSITNA - 3AE		
PARAMETER / JOB I.D.#	BASECASE LME1	SENSITIVITY L583	BASECASE L8J9	SENSITIVITY L585		
RETIREMENT POLICY (YRS.) Coal-fired Steam Natural Gas GT Oil GT	30 Yrs 30 Yrs 20 Yrs	45 Yrs 45 Yrs 30 Yrs	30 Yrs 30 Yrs 20 Yrs	45 Yrs 45 Yrs 30 Yrs		
1990-2010 THERMAL ADDS: Coal (MW) NGGT (MW) Diesels (MW)	900 600 50	1100 75	300 225			
TOTAL	1550 MW	1175 MW	525 MW	O MW		
RETIREMENTS (MW)	(734)	(290)	(734)	(290)		
HYDRO ADDS: MONTH/YEAR NAME MW			6/93 W400 1/96 W400 1/00 DC400	6/93 W400 1/96 W400 1/00 DC400		
TOTAL FIRM* MW 2010	1895 MW	1973 MW	2023 MW	1951 MW		
$\frac{$ \times 10^6 (80$)}{10 \text{ year PW}}$ 20 year PW	\$ 873.7 3319.4	\$ 873.7 3318.3	\$ 873.7 2360.6	\$ 873.7 2382.7		
TOTAL	\$4193.1	\$4192.0	\$3234.3	\$3256.4		
LONG TERM (2040) PW	\$8133	\$7850	\$5851	\$6100		

* In Peak Month (December)

C

1

ć --

.

NOTE: Sensitivity analysis performed using 0% escalation, 3% interest rate and the midload forecast.

TABLE . 20

SENSITIVITY ANALYSIS - THERMAL PLANT CAPITAL COSTS (1980\$)

PARAMETER / JOB I D #	BASECASE	HERMAL	SUSITNA - BAF	
THERMAL PLANT CAPITAL COSTA	LME1	LAL9	BASECASE L8J9	SENSITIVITY
Coal-fired Steam (250 MW) Natural Gas GT (75 MW) Diesels (10 MW) 1990-2010 THERMAL ADDS:	\$2744/kW ¹ 350/kW 778/kW	\$2135/kW ² 350/kW 778/kW	\$2744/kw ¹ 350/kw 778/kw	\$2135/kW ² 350/kW 778/kW
NGGT (MW) Diesels (MW)	900 600 50	1100 525 10	300 225	300 225
RETIREMENTS (MW) HYDRO ADDS:	1550 MW (734)	1635 MW (734)	525 MW (734)	525 MW
MONTH/YEAR NAME MW			6/93 W400	6/93 W400
TOTAL FIRM* MW 2010 <u>\$ x 10⁶ (80\$)</u>	1895 MW	1980 MW	1/00 DC400 2023 MW	1/96 W400 1/00 DC400 2023 MW
20 year PW TOTAL	\$ 873.7 3319.4	\$ 873.7 3095.3	\$ 873.7 2360.6	\$ 873.7 2344.6
LONG TERM (2040) PW	\$4193.1 \$8133	\$3969.0 \$7585	\$3234.3 \$5851	\$3218.3 \$5744

*In Peak Month (December)

-

NOTE: Sensitivity analysis performed using 0% excalation, 3% interest rate and the mid load forecast.

11.8 Alaskan Adjustment Factor 21.4 Alaskan Adjustment Factor

WATANA/ DEVIL CANYON

21

TABLE 21 SENSITIVITY ANALYSIS - CAPITAL COSTS (1980\$)

PARAMETER / JOB I.D.#	SUSITNA -		
	L8J9	SENSIT L5G1	IVITY LD75
SUSITNA COST (\$x10 ⁶) (80\$) Watana Dam Devil Canyon Dam Tunnel	\$1984 999	\$1984 1110	\$2976 1498
1990-2010 THERMAL ADDS: Coal (MW) NGGT (MW) Diesels (MW)	300 225	300 225	- 300 225
TOTAL RETIREMENTS (MW)	525 MW	525 MW	525 MW
HYDRO ADDS: MONTH/YEAR NAME MW	6/93 W400 1/96 W400 1/00 DC400	6/93 W400 1/96 W400 1/00 DC400	(734) 6/93 W400 1/96 W400
TOTAL FIRM* MW 2010 $$ \times 10^6 (80$)$	2023 MW	2023 MW	2023 MW
10 year PW 20 year PW	\$ 873.7 2360.6	\$ 873.7 2546.2	\$ 873.7 2836.3
TOTAL LONG TERM (2040) PW	\$3234.3	\$3419.9	\$3710.0

*In Peak Month (December)

8

1.

NOTE: Sensitivity analysis performed using 0% escalation, 3% interest rate and the midload forecast.

WATANA/ TABLE 22 SENSITIVITY ANALYSIS - TUNNEL CAPITAL COSTS

Ś

	TUNNEL COST HALVED - MEDIUM LOAD	TUNNEL COST HALVED - LOW LOMAD W/T I.5 L613	
PARAMETER / JOB I.D.#	W/T にち L615		
1990 MW	1079 MW	1079 MW	
1990-2010 THERMAL ADDS: Coal (MW) NGGT (MW) Diesels (MW)	200 450 <u>30</u>	375 20	
TOTAL	680 MW	395 MW	
RETIREMENTS (MW)	(734)	(734)	
HYDRO ADDS: MONTH/YEAR NAME MW TOTAL FIRM* (2010)	6/93 W400 1/96 W400 1/00 T	6/93 W400 1/02 T	
(100)			
10 Year PW 20 Year PW	\$ 873.7 <u>2474.2</u>	\$ 744.1 <u>1955.8</u>	
TOTAL	\$3347.9	\$2699.9	
LONG TERM (2040) PW	\$6232	\$4726	

*In Peak Month (December)

4

•