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FLOOD CHARACTERISTICS OF ALASKAN STREAMS

25133

$$Q_T = \frac{Q_{50}}{Q_5} \times P_5$$

$$Q_{50} = 0.65 M^{1.024} D^{2.325}$$

Q₅

$$Q_2 = 1.16 \frac{M^{0.988}}{D^{0.05}} = 1.16 \frac{(2,450)^{0.988}}{(1.38)^{0.05}} = 2,550 \text{ ft}^3/\text{s}$$

Prepared by the United States
Department of the Interior
Geological Survey
in cooperation with
State of Alaska
Department of Transportation
and
U.S. Department of Transportation
Federal Highway Administration

$$Q_T = C M^a D^k$$

Q₂

WATER RESOURCES INVESTIGATIONS 78-129



UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

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no. 78-129

FLOOD CHARACTERISTICS OF ALASKAN STREAMS

by

R. D. Lamke

Techniques for calculating magnitude and frequency
of floods in Alaska, with compilations of flood
data through October 1, 1975.

Prepared in cooperation with
STATE OF ALASKA
DEPARTMENT OF TRANSPORTATION
and
U.S. DEPARTMENT OF TRANSPORTATION
FEDERAL HIGHWAY ADMINISTRATION

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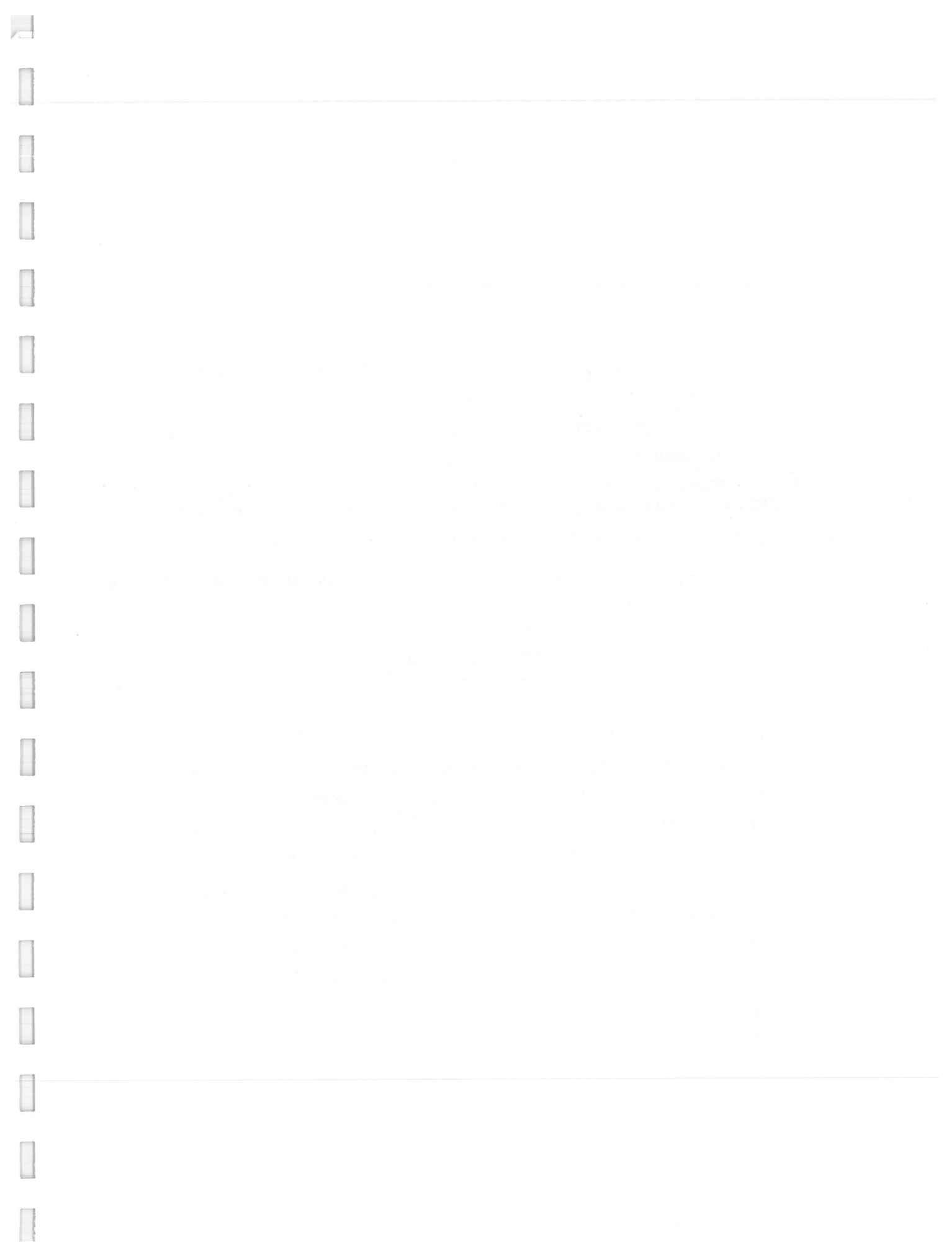
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CONVERSION TABLE

<u>Multiply inch-pound units</u>	<u>by</u>	<u>to obtain SI units</u>
cubic feet per second (ft ³ /s)	0.0283	cubic meters per second (m ³ /s)
cubic feet per second per square mile [(ft ³ /s)/mi ²]	0.0109	cubic meters per second per square kilometer [(m ³ /s)/km ²]
square miles (mi ²)	2.589	square kilometers (km ²)
feet (ft)	0.3048	meters (m)
inches (in.)	2.540	centimeters (cm)
degrees Fahrenheit (°F)	5/9 (°F-32)	degrees Celsius (°C)



FLOOD CHARACTERISTICS OF ALASKAN STREAMS

R. D. Lamke

ABSTRACT

Peak discharge data for Alaskan streams are summarized and analyzed. Alaska is divided into two regions, one having a maritime climate with fall and winter rains and floods (Area I), the other having spring and summer floods of a variety or combinations of causes (Area II).

Multiple-regression equations relate the magnitude of a discharge that has a given frequency to the climatic and physical characteristics of a stream's drainage basin. The physical characteristics include drainage area, amount of storage in the lakes and ponds, and the amount of forested land (significant only in Area II). The climatic characteristics found to be significant are annual precipitation and mean minimum January temperature. Maps show the lines of equal intensity of these climatic variables and locations of the 260 sites used in the multiple-regression analyses.

The equations resulting from the analyses for 260 gaged basins can be used to estimate floods of specified exceedance probability (or average recurrence interval) at ungaged sites. These equations are for the 1.25-, 2-, 5-, 10-, 25-, and 50-year average recurrence intervals (80 to 2 percent exceedance probability). Average standard errors of the multiple-regression equations for Areas I and II are 48 and 74 percent, respectively. Statistical methods are also presented to estimate flood discharges with low exceedance probability at sites with only a short record of flood discharges or at ungaged sites whose basin characteristics are similar to those at a nearby gaged site where there is a long record of yearly flood peaks.

Little information on floods in western and arctic Alaska has been collected, and the predictive equations for those areas are therefore less reliable than for areas for which there are more data.

Maximum recorded floods at more than 400 sites throughout Alaska are tabulated.

INTRODUCTION

Knowledge of flood characteristics is necessary to evaluate flood hazards and to design economical structures along streams. One way of evaluating flood characteristics at a gaging station or a crest-stage gage is to relate the magnitudes of instantaneous peak discharges to their frequencies of occurrence. However, flood records have been collected in Alaska at few such gaged sites.

This report presents methods for calculating the magnitude and frequency of flood discharges at ungaged sites. The methods described utilize flood magnitude and frequency data collected at gaged sites and relate the data to physical and climatic characteristics of these gaged basins. (See tables 1 and 2 at the back of this report for the basin characteristics of sites used in developing equations, the bottom of table 2 for definitions of basin characteristics, and tables 3 and 4 for the flood data used.)

No attempt is made in this study to predict peak discharges from glacier-dammed lakes. A report entitled "Glacier Dammed Lakes and Outburst Floods in Alaska" by Post and Mayo (1971) shows the location of those lakes and describes their recent history, as well as delineating areas where outburst flooding may be expected.

Maximum known peak discharges for all Alaskan gaging stations and numerous miscellaneous measurement sites are listed in table 5. The maximum discharge in cubic feet per second per square mile provides an estimate of the largest floods that might be expected at ungaged sites in a region.

Floods can result from causes other than high rates of runoff from rain or snowmelt. Floods may occur when the water surface along a stream rises above some predetermined level because of backwater from a downstream obstruction such as an ice jam. Peak discharges can occur from the sudden release of water impounded by temporary dams of earth or snow slides. Another common type of flood that occurs in Alaska results from the formation of excessive ice in the channel. This ice formation (aufeis or icing) frequently spreads beyond the channel banks; any runoff from snowmelt or rain then travels over the ice surface or beside the ice formation. The probability of these flood events, their importance in designing a structure, or the possibility of a developed area being inundated are not susceptible to a regional analysis but must be estimated for each site by field investigations or from a history of past occurrences.

This report is based on flood data collected by the Geological Survey in cooperation with several federal, state, and local agencies. Of special importance is a continuing program of flood data collection on small streams throughout Alaska under a cooperative agreement with the State of Alaska Department of Transportation (formerly Department of Highways).

BASIN CHARACTERISTICS

The characteristics of gaged basins comprise selected physical and topographic parameters, as well as climatic variables of the drainages of the individual gaged sites. The basin characteristics of the stations used in this analysis are listed in tables 1 and 2. Descriptions and definitions of the characteristics are shown at the bottom of table 2.

FLOOD DATA

The annual maximum instantaneous peak discharge records collected at 260 gaging stations in Alaska were analyzed to determine their flood magnitude and frequency relations. The method used in the analysis was

the log-Pearson Type III distribution as recommended by the U.S. Water Resources Council (WRC) in Bulletin 17A (1977). The criteria in Bulletin 17A, that 10 or more years of flood record be used in the analysis, were relaxed because a number of records with less than 10 years were available for otherwise ungaged areas of the state. The results are presented in tables 3 and 4.

The following criteria were used to select flood-frequency data for use in the analysis:

(1) All stations with 5 or more years of flood record prior to October 1, 1975, were used if peak discharges were not significantly affected by outburst floods from glacier-dammed lakes.

(a) The flood records were not used for the following stations:

15008000 Salmon River near Hyder

15202000 Tazlina River near Glenallen

15243500 Snow River near Divide

(b) Only the parts of the flood record that were not outburst floods from Lake George were used for 15281000, Knik River near Palmer.

(2) Only the 1.25-, 2-, and 5-year peaks were used for stations having less than 8 years of record.

(3) Only the 1.25- through the 10-year peaks were used for stations having 8 to 12 years of record.

(4) Only the 1.25- through the 25-year peaks were used for stations having 13 to 17 years of record.

(5) Only the 1.25- through the 50-year peaks were used for stations having 18 to 22 years of record.

(6) The 1.25- through the 100-year peaks were used for stations having more than 22 years of record.

(7) The means and standard deviations of log-Pearson Type III analyses are shown in tables 3 and 4 for all stations with more than 10 years of record.

(8) The station skew coefficient is also shown for all stations with more than 20 years of record.

Some of the flood records were adjusted as outlined below:

(1) Some peak discharges were augmented by the failure of natural dams or diversion from an adjacent stream during the floods of August 1971.

Appropriate adjustments were made for the following stations:

- 15284000 Matanuska River at Palmer
- 15292900 Goose Creek near Montana
- 15294500 Chakachatna River near Tyonek

(2) Some records were adjusted for historical peaks according to the methods recommended in WRC Bulletin 17A (1977). These records were:

- 15283500 Eska Creek near Sutton
- 15484000 Salcha River near Salchaket
- 15493000 Chena River near Two Rivers
- 15511000 Little Chena River near Fairbanks
- 15514000 Chena River at Fairbanks
- 15515500 Tanana River at Nenana

(3) All records were analyzed by log-Pearson Type III analysis using WRC guidelines for low outliers and zero flow years.

(4) A few of the streamgaging stations have one or more years in which the instantaneous peak could not be determined. However, a maximum daily discharge was published. Figures for maximum daily discharge were not used in the log-Pearson Type III analysis except in a few selected instances.

In tables 3 and 4 the headings $P_{1.25}$ and P_{50} , for example, mean that the discharge values shown have recurrence intervals of 1.25 years and 50 years, respectively. The recurrence interval is the average interval in years within which the stated discharge will be exceeded once. The exceedance probability is the probability of the given discharge being exceeded in any given year and is the reciprocal of the recurrence

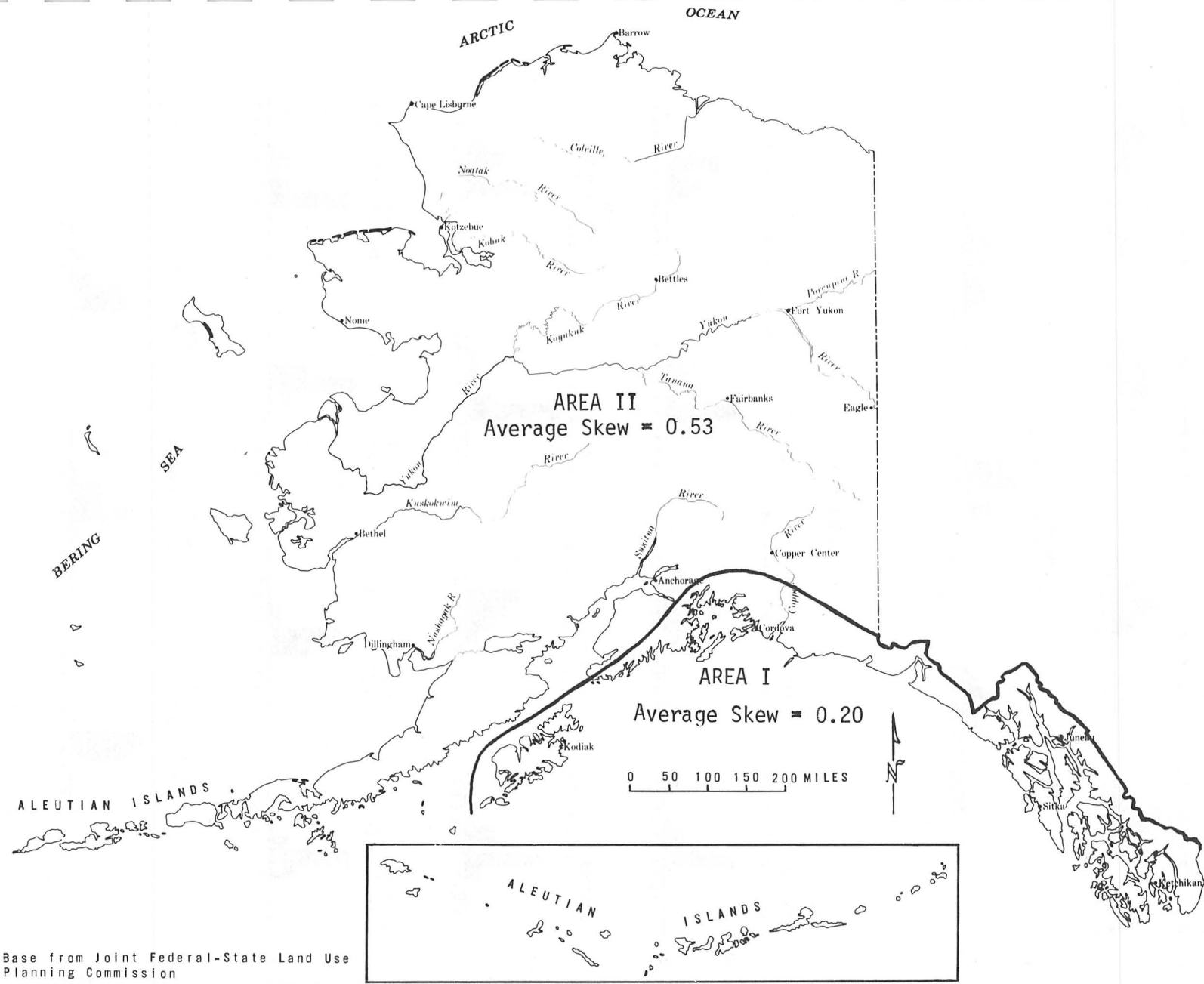
interval. A comparison of the recurrence interval and exceedance probability in percent is presented below:

<u>Recurrence interval, in years</u>	<u>Exceedance probability, in percent</u>
1.25	80
2	50
5	20
10	10
25	4
50	2
100	1

METHOD OF ANALYSIS

Statewide

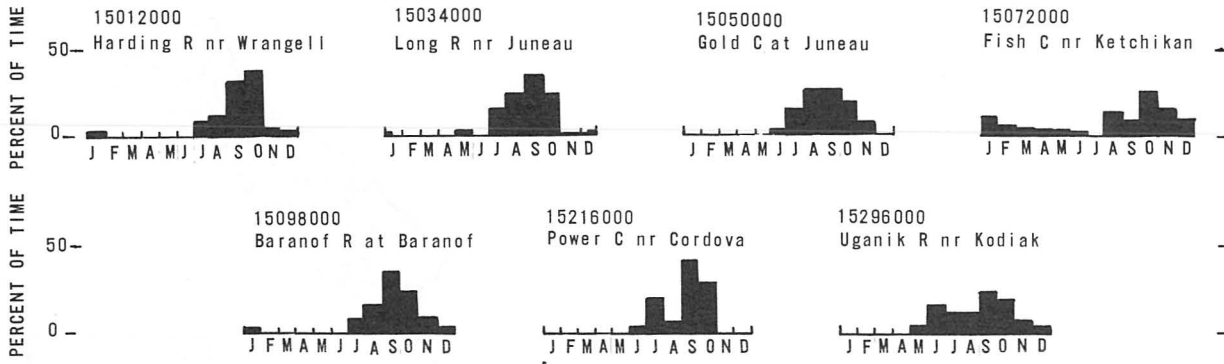
A preliminary multiple-regression analysis for all of Alaska was made of flood magnitude and frequency using basin characteristics of gaged sites (tables 1 and 2) and the seven flood-peak values, $P_{1.25}$ through P_{100} , at each site (tables 3 and 4). This computer analysis resulted in several versions of seven equations, $Q_{1.25}$ through Q_{100} , using various combinations of basin characteristics. Further analysis showed that drainage area (A), mean annual precipitation (p), and area of lake storage (St + 1) were the most significant variables. Another multiple-regression analysis was computed using only these three basin characteristics for each of the seven flood values. The ratios of calculated values to values based on actual flood peaks at the gaged sites were plotted on a map of Alaska. This plot showed that the results of the flood-frequency analysis for stations in a maritime climatic environment were different than those for the rest of Alaska. The state was therefore divided into two areas, Area I and Area II, for further analysis as shown in figure 1. Another difference between Areas I and II is that the annual maximum discharge occurs at a different time of the year (fig. 2).



Base from Joint Federal-State Land Use Planning Commission

Figure 1.--Areas of Alaska used in the flood-frequency analysis.

AREA I



AREA II

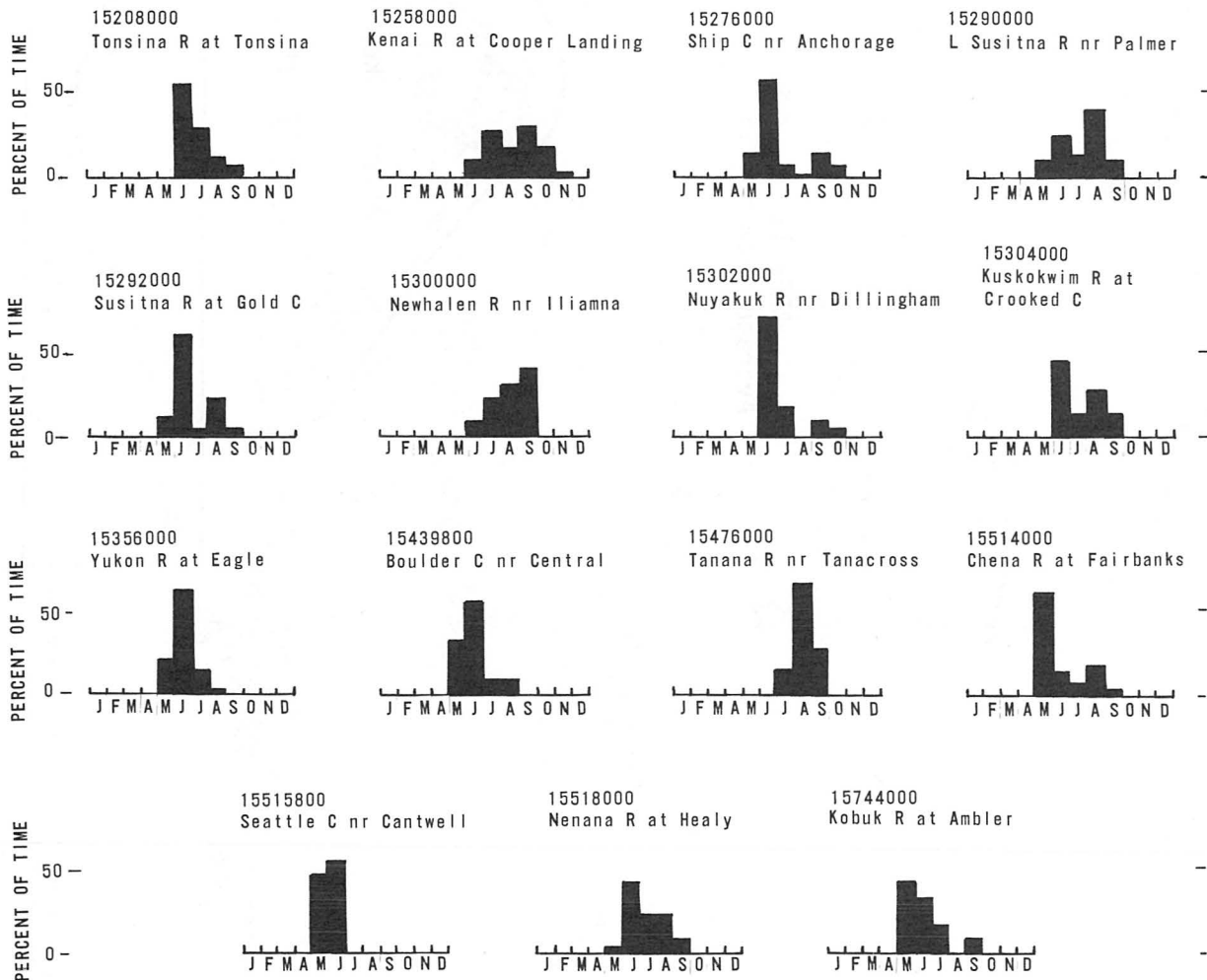


Figure 2.--Time of occurrence of highest peak of the year at selected long-term gaging stations throughout Alaska.

Area I

Area I consists of most areas in Alaska with a maritime climate, excluding the Aleutian Islands and the Pacific Ocean side of the Alaska Peninsula (Johnson and Hartman, 1969, plate 26). Area I includes those areas shown in figure 3 at the back of this report as the Kodiak-Shelikof area and southeast Alaska. It also includes that part of the Gulf of Alaska area south of the crest of the Chugach Mountains. The location of the stations used in the analysis is shown in figures 4-15 and 4-18 and in part of figure 4-17. Floods in maritime Alaska can occur any time during the year and generally are the result of rainstorms; most annual maximum peak discharges in Area I occur in August, September, and October (fig. 2).

Analysis

In addition to the variables mentioned previously, a fourth variable, mean minimum January temperature ($T + 1$), was found to be significant at the 5-percent level of significance. It is believed that ($T + 1$) is an indirect geographic indicator of the probability of winter floods. (A value of 1 is added to avoid zero or negative values.) Because these analyses involved a varying and decreasing number of values based on actual flood peaks at the stations, $P_{1.25}$ through P_{100} , the equations used to calculate $Q_{1.25}$ through Q_{100} sometimes resulted in irregular answers that did not increase as Q_T increased. Table 6 lists resultant equations, standard errors, and number of stations used in the analyses.

To overcome these drawbacks, a different method of analysis was chosen. The method used is based on the log-Pearson Type III distribution of the annual series of flood events at a station (WRC, 1977, p. 9). The general equation for floods of selected exceedance probabilities (Q_T) follows:

$$\text{Log } Q_T = \bar{X} + KS, \text{ where:}$$

\bar{X} is the mean logarithm of the annual series,

S is the standard deviation of the logarithms, and

K is a factor that is a function of the skew coefficient and selected exceedance probability.

A variant of this equation was used in the present analysis to determine prediction equations for ungaged sites:

$$Q_T = CM^a D^k, \text{ where:}$$

CM^a is the anti-log equivalent of \bar{X} for an ungaged site,
 D is the anti-log equivalent of S and
 k is an exponent that varies with the exceedance probability,
 C is a constant that varies with exceedance probability,
 M is an anti-log form of the mean (see below), and
 a is an exponent which is near a value of 1.00.

It was assumed that 10 years of flood record is sufficient to define the mean and standard deviations of the logarithms at each station. These logarithmic values are given in table 3 as "MEAN" and "SD". A multiple-regression analysis of \bar{X} and S at the 46 stations with 10 or more years of flood record was made using the basin characteristics. This resulted in two equations for a regional predictor of the mean value and the standard deviation:

$$M = 10.43 \frac{A^{0.812} p^{0.522} (T + 1)^{0.187}}{(St + 1)^{0.266}}$$

$$D = \frac{1.63}{(T + 1)^{0.049}}$$

The standard errors of the above equations were 38 and 9 percent, respectively, for the 46 values used.

The values of the constants (C) and the exponents (a) of each of the equations for $Q_{1.25}$ through Q_{100} were determined by a multiple-regression of $P_{1.25}$ through P_{100} in table 3 divided by D^k , calculated for each station listed in table 1, with the M values calculated for each station. The above equations were used to calculate M and D . The values of the exponent (k) were determined from the table of K values in Appendix 3 of WRC Bulletin 17A for an average regional skew coefficient of 0.20, and the values were modified slightly to reduce the standard error. See table 3 for station skew coefficients.

Equations

	<u>Standard error</u>
$Q_{1.25} = 1.02 \frac{M^{1.003}}{D^{0.85}}$	56 percent
$Q_2 = 1.16 \frac{M^{0.988}}{D^{0.05}}$	50 percent
$Q_5 = 1.24 M^{0.984} D^{0.70}$	48 percent
$Q_{10} = 0.97 M^{1.008} D^{1.30}$	45 percent
$Q_{25} = 0.66 M^{1.050} D^{1.85}$	48 percent
$Q_{50} = 0.70 M^{1.051} D^{2.20}$	42 percent

Discussion

The standard error of these equations cannot be calculated exactly. However, an approximation of the standard error was made. The standard errors of the equations presented above were slightly greater than for the equations in table 6. Most of the irregularities in the equations were removed (that is, there should be a gradual increase in the computed values from $Q_{1.25}$ through Q_{50}). However, no satisfactory equation could be determined for Q_{100} , partly because there are only 15 values of P_{100} to use in the regression. A reasonable estimate of Q_{100} can be made by using the exponent (k) equal to 2.5 instead of equal to 2.2 in the formula for Q_{50} . Also, the equations can be irregular for drainage areas of less than two square miles. (For some combinations of basin characteristics, Q_{25} is less than Q_{10} .) The only local area where the equations seriously underestimated peaks was a small area about 30 (east and west) by 20 (north and south) miles around Ketchikan and eastward (fig.4-18). For gaged streams with flood records, use the method shown on page 22 to determine the desired discharge at an ungaged site on the stream. Reasonable results can be obtained by multiplying the equation

results by 1.5 for ungaged streams in that area. This value of 1.5 is based on the average relation of the flood magnitudes computed by formulas, $Q_{1.25}$ to Q_{50} , to the actual magnitudes, $P_{1.25}$ to P_{50} , shown in table 3 for stations in the area.

Area II

Area II consists of those parts of Alaska with transitional, continental, and arctic climates; also included are the Aleutian Islands and Pacific Ocean side of the Alaskan Peninsula (Johnson and Hartman, 1969, plate 26) which have a maritime climate. The annual maximum peak discharges generally occur between May and October (fig. 2). The most common cause of the peak flows on the larger streams is snowmelt or a combination of snowmelt and rainstorms that cover a large general area. However, the larger annual maximum peak discharges at a station are the result of widespread general rains in August or later. Often these peak flows are augmented by sustained snowmelt from higher elevations and glaciers. Occasionally, these peak discharges are also augmented by high discharges caused by breakouts from glacier-dammed lakes. The likelihood of the peak discharge of the year being caused by rainstorms rather than by other causes is greater for those streams with smaller drainage areas, with little capacity for storage, and with drainage areas at lower elevations.

It was not feasible to further subdivide Area II into smaller areas for analysis primarily because there are not enough long-term flood records; only 26 stations in the area have 18 or more years of record.

Analysis

In addition to drainage area (A), mean annual precipitation (p), and area of lake storage (St + 1), the basin characteristics for forested area (F + 1) and mean minimum January temperatures (T + 30) were found to be significant at the 5-percent level. These characteristics, (T + 30) and (F + 1), are believed to be indirect geographic indicators of the absence or presence of permafrost. For a given frequency of flood occurrence and similar values of A, p, and (St + 1), the magnitude

of the flood is greater in a permafrost area than in a permafrost-free area because of the proximity to the surface of impermeable frozen soil. However, some permafrost areas have a deeper active layer of permafrost (the seasonally thawed layer of soil on top of the permafrost) than other areas. The presence of forested terrain in permafrost areas is a measure of the effect of the active layer.

The frequency curves using the equations derived from multiple-regression analysis were also irregular. (See table 6 for resultant equations and their standard errors.) The same method of suppressing the irregularities that was utilized to develop the equations for maritime Alaska was used here:

$$Q_T = C M^a D^k$$

The resultant solutions for M and D for the 100 sites with 10 or more years of flood records were:

	<u>Standard error</u>
$M = 1.94 \frac{A^{0.949} p^{0.762}}{(St + 1)^{0.192} (F + 1)^{0.148}}$	60 percent
$D = \frac{3.91}{A^{0.072} (T + 30)^{0.141}}$	30 percent

The values for the constants (C) and the exponents were determined in a manner similar to the method used for Area I. The values for the exponent (k) were taken from WRC Bulletin 17A for an average regional skew coefficient of 0.53.

Equations

	<u>Standard error</u>
$Q_{1.25} = 1.15 \frac{M^{0.984}}{D^{0.857}}$	83 percent
$Q_2 = 1.22 \frac{M^{0.977}}{D^{0.088}}$	77 percent
$Q_5 = 1.04 M^{0.988} D^{0.806}$	78 percent

$Q_{10} = 0.91 M^{0.999} D^{1.325}$	79 percent
$Q_{25} = 0.65 M^{1.025} D^{1.920}$	59 percent
$Q_{50} = 0.65 M^{1.024} D^{2.325}$	68 percent

Discussion

In general, the comments on the results of the regression analysis are the same as for Area I. No satisfactory equations could be determined for Q_{100} because there were only 19 values of P_{100} to use in the regression. However, a reasonable estimate of Q_{100} can be made by using the exponent (k) equal to 2.707 instead of equal to 2.325 in the formula for Q_{50} . The lower limit on drainage area for which these equations should be used to predict flood magnitudes and frequencies is one square mile.

The Aleutian Islands and the Pacific Ocean side of the Alaska Peninsula are included in Area II, even though the climate is maritime and flood peaks can occur in the wintertime. There are few flood records for the area. Only the three sites on Amchitka Island with 5 to 7 years of record were used in this analysis. The preliminary regression studies showed that the equations developed for Area II defined the flood magnitude and frequency relations for these three stations better than the equations for Area I.

The only area in which the equations for Area II appear to overestimate peaks is the Anchorage bowl area from Campbell Creek to Meadow Creek. It is difficult to determine the precipitation (p) for sites in the Anchorage bowl from figure 4-16. The flood peaks used in the analysis were for essentially nonurbanized conditions; urbanization will increase future peak flows. If these equations are used to estimate peaks in the Anchorage area, the results should be multiplied by a factor of about 0.5. (See page 12 for an example of the method used to determine this factor.) For greater accuracy, the most recent log-Pearson Type III analysis for gaging stations in the area may be used and the magnitude and frequency values can be transferred to the ungaged site. The magnitude

of the flood discharge for a given frequency at an ungaged site can be estimated by first computing Q_T for the ungaged site and also for a nearby gaged site with similar basin characteristics, and then multiplying the ratio of the above two Q_T values by the flood magnitude at the gaged site for the given frequency determined by log-Pearson Type III analysis.

Actual flood peaks on the small streams between Healy and Nenana, in the Livengood area, and near Chena Hot Springs were also higher than would be expected from the equations. Those streams are in an area affected by the 1967 flood (an extraordinary flood), and the 1967 flood values were used in the analysis. Applying a correction factor to the results probably is not warranted.

There is a probability that these equations underestimate the flood peak values for northwest Alaska and the Arctic Slope of Alaska (fig. 3). Only eleven sites in these regions were used in the regression equation, and the longest period of record is 11 years. The precipitation maps (figs. 4-1 through 4-5) may also underestimate the precipitation for these regions. The records of wintertime snow depths, expressed as inches of precipitation, are known to be too low. This problem has been recognized by several agencies, notably the Soil Conservation Service, National Weather Service, Cold Regions Research Engineering Laboratory, and the Geophysical Institute of the University of Alaska. During the summer there are only a few precipitation stations operating in these regions. The shortage of precipitation records is most evident for mountainous areas away from the Arctic Ocean. A multiplicative correction factor of 1.7 may be arbitrarily applied to the equation results. The factor is the average ratio of P_T to Q_T for stations in northwest Alaska and Arctic Slope of Alaska. A flood-magnitude and frequency study should be periodically updated; by the time the next study is made, a more accurate precipitation map may be available for these two regions. At that time, there will be more sites with peak records and a longer period of record for many of the stations shown in table 4.

REMARKS AND CAUTIONS

No attempt is made in the present study to predict the discharges of glacier-dammed lakes. Some flood values for streams affected by outbursts are presented in tables 3 and 4. General criteria used to determine which of the stations affected by outburst floods would be included in the analysis were: (1) an outburst flood peak that occurred within any given year might or might not be the highest peak of the year and (2) the magnitude of the outburst peaks was in the same general range as peak flows resulting from other causes.

Stream-gaging records long enough (5 years or more) to make a log-Pearson Type III analysis generally provide more reliable estimates of peak flow at the gages in Alaska than the equations do. (See Childers, 1970, p. 16, for an example.) Therefore, a logical extension of this statement would be that if the ungaged site is on the same stream as a gaged site and if there are no large differences between basin characteristics for the two sites, then the flood values obtained at the gaged site should be modified for the differences in basin characteristics and used for the ungaged site. No guidelines for establishing limits on adjusting a flood value determined at a gaged site to an ungaged site are presented. However, the user should be cautious in making such adjustments. See pages 14 and 15 for an explanation of the method to use; an example is shown on page 22.

Flood records of short length (5 to 9 years) can be used to determine a discharge for a low exceedance probability. For example, suppose the discharge for a flood with an exceedance probability of 2 percent (50-year recurrence interval) is needed at a station with 7 years of record. Q_{50} and Q_5 can be computed for the site, and P_5 can be determined by log-Pearson Type III analysis. The desired discharge can then be determined by multiplying the ratio of Q_{50} to Q_5 by P_5 ; see the example on page 20. The user might want to average the discharge computed by the above method and Q_{50} . For a more detailed discussion of the recommended guidelines for refinements of frequency curves with 10 or more years of

flood record at a gaging station consult pages 17 through 20 of WRC Bulletin 17A (1977).

There are large geographic areas of Alaska for which there are no flood records; figures 4-1 through 4-18 show the location of gaging stations that provide these records. The reliability of the flood prediction equations is less certain for those station-less areas than areas for which flood records have been obtained. Figures 4-1 through 4-18 also show lines of equal intensity for precipitation and mean minimum January temperatures.

Data that can be used to estimate the size of large floods that might be expected at ungaged sites are presented in table 5. The table lists maximum known discharges for all Alaskan gaging stations and miscellaneous sites. A plot comparing the maximum known floods in cubic feet per second per square mile $[(ft^3/s)/mi^2]$ and the drainage area for the sites in the area of concern can be prepared and an envelope curve drawn. The peak discharge at the ungaged site can be estimated by using the value in $(ft^3/s)/mi^2$ from the envelope curve and a measured drainage area. The peak magnitude thus determined would have an unknown frequency of occurrence or exceedance probability.

The standard error of estimate is a statistical measurement of the reliability of the equations and is expressed as a percentage of the average value of the characteristic being analyzed. The standard error is an estimated limit within which about two-thirds of the true long-term values of the predicted characteristic are expected to fall. Thus, for a standard error of 80 percent, two-thirds of the actual flood magnitudes at an ungaged site should lie between approximately 56 percent $(100/1.80)$ and 180 percent (100×1.80) of their predicted value.

As explained on pages 21 and 22 of WRC Bulletin 17A, these equations predict the flow exceedance probability, not the risk. There is a two-percent chance that Q_{50} (a discharge with an average recurrence interval of 50 years) will be exceeded in a given year. However, there is a 50-percent chance that the flood discharge with an annual exceedance probability of two percent (Q_{50}) will be exceeded one or more times in the

next 34 years (from fig. 10-1 of WRC Bulletin 17A).

Area I

The equations given in this report should not be used for the large rivers breaching the mountains along the United States-Canada border in southeast Alaska or the main stem of the Copper River. The equations for Area I can be used for the streams tributary to the Copper River south of the crest of the Chugach Mountains. A correction factor to the equations of 1.5 is suggested for a small area near Ketchikan for ungaged streams. (See p. 11 and fig. 4-18.) For sites on gaged streams, flood data from the gaged site can be transferred to the site in question.

Area II

Equations for Area II should be used for Copper River tributaries north of the crest of the Chugach Mountains. A correction factor of 1.7 is suggested if the equations are used for northwest and Arctic Slope Alaska. It is also suggested that the prediction equations for ungaged sites be used with caution for the Anchorage bowl area; to avoid unreliable results, either a correction factor of 0.5 may be applied or flood data from ungaged sites can be transferred to the site in question.

EXAMPLES OF CALCULATIONS

Area I

Problem: Compute Q_2 and Q_{50} for a stream with the following pertinent basin characteristics:

$$A = \text{drainage area} = 33.9 \text{ mi}^2$$

$$p = \text{annual precipitation} = 160 \text{ in.}$$

$$T = \text{mean minimum January temperature} = 28^\circ\text{F}$$

$$St = \text{area of lakes and ponds or "storage"} = 12 \text{ percent}$$

Solution:

First, determine M and D:

$$\begin{aligned} M &= 10.43 \frac{A^{0.812} p^{0.522} (T + 1)^{0.187}}{(St + 1)^{0.266}} \\ &= 10.43 \frac{(33.9)^{0.812} (160)^{0.522} (29)^{0.187}}{(13)^{0.266}} \\ &= 2,450 \text{ ft}^3/\text{s} \text{ (cubic feet per second).} \end{aligned}$$

$$D = \frac{1.63}{(T + 1)^{0.049}} = \frac{1.63}{(29)^{0.049}} = 1.38$$

Next, use the formula for Q_2 :

$$Q_2 = 1.16 \frac{M^{0.988}}{D^{0.05}} = 1.16 \frac{(2,450)^{0.988}}{(1.38)^{0.05}} = 2,550 \text{ ft}^3/\text{s}$$

Finally, use the formula for Q_{50} :

$$\begin{aligned} Q_{50} &= 0.70 M^{1.051} D^{2.20} \\ &= 0.70 (2,450)^{1.051} (1.38)^{2.20} = 5,190 \text{ ft}^3/\text{s} \end{aligned}$$

Problem: Assume that the site used in the computations on the preceding page has six years of flood record. The discharge with an exceedance probability of two percent is desired.

$$P_5 = 3,580 \text{ ft}^3/\text{s} \text{ from log-Pearson Type III analysis}$$

$$Q_{50} = 5,190 \text{ ft}^3/\text{s}$$

Solution:

First, determine Q_5 :

$$\begin{aligned} Q_5 &= 1.24 M^{0.984} D^{0.70} \\ &= 1.24 (2,450)^{0.984} (1.38)^{0.70} = 3,360 \text{ ft}^3/\text{s} \end{aligned}$$

Next, determine the desired discharge:

$$\begin{aligned} Q_T &= \frac{Q_{50}}{Q_5} \times P_5 \\ &= \frac{5,190}{3,360} \times 3,580 = 5,530 \text{ ft}^3/\text{s} \end{aligned}$$

Area II

Problem: Compute Q_{50} for a river with the following pertinent basin characteristics.

$$A = 1,910 \text{ mi}^2$$

$$p = 40 \text{ in.}$$

$$T = -8^\circ\text{F}$$

$$St = 1 \text{ percent}$$

$$F = \text{area of forests} = 8 \text{ percent}$$

Solution:

Use the formula for Q_{50} :

$$Q_{50} = 0.65 M^{1.024} D^{2.325}$$

or

$$Q_{50} = 0.65 \left[1.94 \frac{A^{0.949} p^{0.762}}{(St + 1)^{0.192} (F + 1)^{0.148}} \right]^{1.024}$$

$$\text{multiplied by} \left[\frac{3.91}{A^{0.072} (T + 30)^{0.141}} \right]^{2.325}$$

$$= 0.65 \left[1.94 \frac{(1,910)^{0.949} (40)^{0.762}}{(2)^{0.192} (9)^{0.148}} \right]^{1.024}$$

$$\text{multiplied by} \left[\frac{3.91}{(1,910)^{0.072} (22)^{0.141}} \right]^{2.325} = 54,500 \text{ ft}^3/\text{s.}$$

Problem: An alternate answer is desired for Q_{50} at the above ungaged site. There is a gage upstream with a long record. The pertinent basin and flow characteristics at the gage are:

$$A = 1,310 \text{ mi}^2$$

$$p = 38 \text{ in.}$$

$$T = -8^\circ\text{F}$$

$$St = 2 \text{ percent}$$

$$F = 7 \text{ percent}$$

$$P_{50} = 28,500 \text{ ft}^3/\text{s}$$

Solution:

First, determine Q_{50} for the gaged site:

M was determined as 16,800 ft^3/s and D as 1.508.

$$\begin{aligned} Q_{50} &= 0.65 M^{1.024} D^{2.325} \\ &= 0.65 (16,800)^{1.024} (1.508)^{2.325} = 36,200 \text{ ft}^3/\text{s}. \end{aligned}$$

Next, determine the desired discharge:

$$\begin{aligned} Q_T &= \frac{Q_{50} \text{ at site}}{Q_{50} \text{ at gage}} \times P_{50} \text{ at gage} \\ &= \frac{54,500}{36,200} \times 28,500 = 42,900 \text{ ft}^3/\text{s}. \end{aligned}$$

If the above value and the previously computed Q_{50} for the ungaged site are given equal weight, the design discharge would be 48,700 ft^3/s .

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- National Weather Service, 1972, Mean annual precipitation-- inches: National Weather Service [Alaska], map.
- Post, Austin, and Mayo, L. R., 1971, Glacier dammed lakes and outburst floods in Alaska: U.S. Geological Survey Hydrologic Investigation Atlas HA-455.
- U.S. Water Resources Council, 1977, Guidelines for determining flood flow frequencies: U.S. Water Resources Council Bulletin 17A, 106 p.

Table 1.--Basin characteristics* of Area I gages.

Station no.	Station name	Location		Drainage area (mi ²)
		Latitude (Degrees)	Longitude (Degrees)	
15010000	DAVIS R NR HYDER AK	55.7500	130.2000	80.0000
15010500	HALIBUT BAY TR NR HYDER AK	55.2500	130.1000	8.5800
15011500	RED R NR METLAKATLA AK	55.1400	130.5300	45.3000
15011900	CABIN C NR KETCHIKAN AK	55.3200	130.7800	8.8000
15012000	WINSTANLEY C NR KETCHIKAN AK	55.4200	130.8700	15.5000
15015600	KLAHINI R NR BELL ISLAND AK	56.0500	131.0500	58.0000
15018000	SHELOKAM LK OUTLET NR BELL ISLAND AK	55.9800	131.6500	18.0000
15019000	BLACK BEAR C NR MEYER CHUCK AK	55.7200	132.1600	16.5000
15020100	TYEE C AT MOUTH NR WRANGELL AK	56.2100	131.5100	16.1000
15022000	HARDING R NR WRANGELL AK	56.2100	131.6400	67.4000
15026000	CASCADE C NR PETERSBURG AK	57.0100	132.7800	23.0000
15030000	SWEETHEART FALLS C NR JUNEAU AK	57.9500	133.6800	27.0000
15031000	LONG R ABV LONG LK NR JUNEAU AK	58.1800	133.8800	8.2900
15034000	LONG R NR JUNEAU AK	58.1700	133.7000	32.5000
15036000	SPEEL R NR JUNEAU AK	58.2000	133.6100	226.0000
15038000	CRATER C NR JUNEAU AK	58.1400	133.7700	11.4000
15040000	DOROTHY C NR JUNEAU AK	58.2300	134.0400	15.2000
15042000	CARLSON C AT SUNNY COVE AK	58.3200	134.1800	22.3000
15044000	CARLSON C NR JUNEAU AK	58.3200	134.1700	24.3000
15048000	SHEEP C NR JUNEAU AK	58.2700	134.3100	4.5700
15050000	GOLD C AT JUNEAU AK	58.3100	134.4000	9.7600
15052000	LEMON C NR JUNEAU AK	58.3900	134.4200	12.1000
15052500	MENDENHALL R NR AUKE BAY AK	58.4200	134.5400	85.1000
15052800	MONTANA C NR AUKE BAY AK	58.4000	134.6100	15.5000
15053800	LAKE C AT AUKE BAY AK	58.3900	134.6300	2.5000
15054000	AUKE C NR AUKE BAY AK	58.3800	134.6400	3.9600
15054500	BESSIE C NR AUKE BAY AK	58.5900	134.9000	1.3500
15056100	SKAGWAY R AT SKAGWAY AK	59.4600	135.3200	145.0000
15056200	WEST C NR SKAGWAY AK	59.5300	135.3500	43.2000
15056210	TAIYA R NR SKAGWAY AK	59.5100	135.3400	179.0000
15056400	CHILKAT R AT GORGE NR KLUKWAN AK	59.6300	135.9300	190.0000
15057500	WILLIAM HENRY C NR AUKE BAY AK	58.7500	135.2400	1.5800
15058000	PURPLE LK OUTLET NR METLAKATLA AK	55.1000	131.4300	6.8000
15059500	WHIPPLE C NR WARD COVE AK	55.4400	131.7900	5.2900
15060000	PERSEVERANCE C NR WACKER AK	55.4100	131.6700	2.8100
15062000	WARD C NR WACKER AK	55.4300	131.6700	14.0000
15064000	KETCHIKAN C AT KETCHIKAN AK	55.3400	131.6300	13.5000
15066000	BEAVER FALLS C NR KETCHIKAN AK	55.3800	131.4700	5.8000
15068000	MAHONEY C NR KETCHIKAN AK	55.4200	131.5100	5.7000
15070000	FALLS C NR KETCHIKAN AK	55.6100	131.3500	36.5000
15072000	FISH C NR KETCHIKAN AK	55.3900	131.1900	32.1000
15072200	SEA LEVEL C NR KETCHIKAN AK	55.3700	131.1800	18.6000
15074000	ELLA C NR KETCHIKAN AK	55.5100	131.0200	19.7000
15076000	MANZANITA C NR KETCHIKAN AK	55.6000	130.9800	33.9000
15078000	GRACE C NR KETCHIKAN AK	55.6600	130.9700	30.2000
15079800	KLU C NR BELL ISLAND AK	55.8400	131.4200	5.9700
15080000	ORCHARD C NR BELL ISLAND AK	55.8300	131.4500	59.0000
15081490	YATUK C NR KLAWOCK AK	55.9000	133.1400	5.8000
15081501	STANEY C NR CRAIG AK	55.8200	133.1300	51.6000
15081800	NB TROCADERO C NR HYDABURG AK	55.3600	132.8700	17.4000
15082000	REYNOLDS C NR HYDABURG AK	55.2100	132.6000	5.7000
15084000	MYRTLE C AT NIBLACK AK	55.0700	132.1300	0.8400
15085100	OLD TOM C NR KASSAN AK	55.4000	132.4100	5.9000
15085200	DOG SALMON C NR HOLLIS AK	55.3400	132.5100	16.8000
15085600	INDIAN C NR HOLLIS AK	55.4500	132.6900	8.8200
15085700	HARRIS C NR HOLLIS AK	55.4600	132.7000	28.7000
15085800	MAYBESO C NR HOLLIS AK	55.4900	132.6800	15.1000
15086000	KARTA R NR KASAAN AK	55.5600	132.5800	49.5000
15086500	NECK C NR POINT BAKER AK	56.1000	133.1400	17.0000
15086600	BIG C NR POINT BAKER AK	56.1300	133.1400	11.2000
15086900	RED C NR POINT BAKER AK	56.2600	133.3300	11.2000
15087500	TWIN C NR PETERSBURG AK	56.7200	132.9300	3.8200
15088000	SAWMILL C NR SITKA AK	57.0500	135.2300	39.0000
15092000	MAKSOUTOF R NR PT ALEXANDER AK	56.5000	134.9700	26.0000
15093400	SASHIN C NR BIG PORT WALTER AK	56.3800	134.6600	3.7200
15094000	DEER LK OUTLET NR PORT ALEXANDER AK	56.5200	134.6700	7.4100
15098000	BARANOF R NR BARANOF AK	57.0900	134.8400	32.0000
15100000	TAKATZ C NR BARANOF AK	57.1400	134.8600	17.5000
15101600	WHEELER C NR DOUGLAS AK	58.0300	134.7700	57.1000
15101800	FISHERY C NR ANGOON AK	57.7600	134.7100	54.3000
15102000	HASSELBORG C NR ANGOON AK	57.6600	134.2500	56.2000
15102350	N ARM C NR ANGOON AK	57.4000	134.3200	8.6400
15106920	KADASHAN R AB HOOK C NR TENAKEE AK	57.6600	135.1800	10.2000
15106940	HOOK C AB TR NR TENAKEE AK	57.6800	135.1300	4.4800
15106960	HOOK C NR TENAKEE AK	57.6700	135.1800	8.0000
15106980	TONALITE C NR TENAKEE AK	57.6700	135.2300	14.5000
15107000	KADASHAN R NR TENAKEE AK	57.7000	135.2200	37.7000
15108000	PAVLOF R NR TENAKEE AK	57.8400	135.0400	24.3000
15108250	GAME C NR HOONAH AK	58.0500	135.4900	42.8000
15109000	FISH C NR AUKE BAY AK	58.3300	134.5900	13.6000
15195000	DICK C NR CORDOVA AK	60.3400	144.3000	7.9500
15216000	POWER C NR CORDOVA AK	60.5900	145.6200	20.5000
15219000	WF OLSEN BAY C NR CORDOVA AK	60.7600	146.1700	4.7800
15219100	CONTROL C NR CORDOVA AK	60.7500	146.2300	4.2200
15226000	SOLOMON GULCH NR VALDEZ AK	61.0800	146.3000	19.0000
15236200	SHAKESPEARE C AT WHITTIER AK	60.7800	148.7300	3.0500
15236900	WOLVERINE C NR LAWING AK	60.3700	148.9000	9.5100
15237000	NELLIE JUAN R NR HUNTER AK	60.4200	148.7200	125.0000
15237400	CHALMERS R NR CORDOVA AK	60.2200	147.2200	6.3200
15238000	LOST C NR SEWARD AK	60.2000	149.3700	7.9600
15238600	SPRUCE C NR SEWARD AK	60.0700	149.4500	9.2600
15295600	TERROR R NR KODIAK AK	57.6500	153.0200	15.0000
15295700	TERROR R AT MOUTH NR KODIAK AK	57.7000	153.1700	46.0000
15296000	UGANIK R NR KODIAK AK	57.6900	153.4200	123.0000
15297200	MYRTLE C NR KODIAK AK	57.6000	152.4000	4.7400
15297300	KALSIN BAY TR NR KODIAK AK	57.5900	152.4300	2.3500
15297500	RED CLOUD C TR NR KODIAK AK	57.8200	152.6200	1.5100

* See definitions at end of table 2.

Table 2.--Basin characteristics of Area II gages.

Station no.	Station name	Location		Drainage area (mi ²)
		Latitude (Degrees)	Longitude	
15198500	STATION C NR MENTASTA AK	62.9300	143.6700	15.3000
15199000	COPPER R TR NR SLANA AK	62.7200	144.2400	4.3200
15200000	GAKONA R AT GAKONA AK	62.3000	145.3100	620.0000
15201000	DYI C NR GLENALLFN AK	62.1500	145.4800	11.4000
15201100	L NELCHINA R TR NR EUREKA LODGE AK	61.9900	147.0100	7.8100
15201300	MOOSE C TR NR GLENALLEN AK	62.1100	145.5200	7.1200
15206000	KLIITINA H AT COPPER CENTER AK	61.9500	145.3100	880.0000
15208000	TONSINA R AT TONSINA AK	61.6600	145.1800	420.0000
15208100	SQUIRREL C AT TONSINA AK	61.6700	145.1700	70.5000
15208200	POCK C NR TONSINA AK	61.7100	145.1500	14.3000
15211700	STRELNA C NR CHITINA AK	61.5100	144.0700	23.8000
15211900	OHKIEN C NR CHITINA AK	61.4800	144.4600	44.8000
15212000	COPPER R NR CHITINA AK	61.4700	144.4600	20600.0000
15212500	ROULDER C NR TIEKEL AK	61.3400	145.3100	9.8000
15212800	PTARMIGAN C TR NR VALDEZ AK	61.1400	144.7400	0.7200
15239000	BRADLEY R NR HOMER AK	59.7600	150.8500	54.0000
15239500	FRITZ C NR HOMER AK	59.7100	151.3400	10.4000
15239900	DIAMOND C NR HOMER AK	59.6700	151.6700	5.3500
15239900	ANCHOR R NR ANCHOR PT AK	59.7500	151.7500	133.0000
15240000	ANCHOR R AT ANCHOR POINT AK	59.7700	151.8300	226.0000
15240500	COOK INLET TR NR NINILCHIK AK	59.9800	151.7200	1.6900
15241600	NINILCHIK R AT NINILCHIK AK	60.0500	151.6600	131.0000
15242000	KASILOF R NR KASILOF AK	60.3200	151.2600	738.0000
15243950	PORCUPINE C NR PRIMROSE AK	60.3400	149.3700	16.8000
15244000	PTARMIGAN C AT LAWING AK	60.4100	149.3600	32.6000
15246000	GRANT CR NR MOOSE PASS AK	60.4600	149.3500	44.2000
15248000	TRAIL R NR LAWING AK	60.4300	149.3700	181.0000
15250000	FALLS C NR LAWING AK	60.4300	149.3700	11.8000
15251800	QUARTZ C AT GILPATRICKS AK	60.6000	149.5400	9.4100
15254000	CRESCENT C NR COOPER LANDING AK	60.5000	149.6800	31.7000
15258000	KENAI R AT COOPER LANDING AK	60.4900	149.8100	634.0000
15260000	COOPER C NR COOPER LANDING AK	60.4300	149.8200	31.8000
15260500	STETSON C NR COOPER LANDING AK	60.4400	149.8500	8.6000
15261000	COOPER C AT MOUTH NR COOPER LANDING AK	60.4700	149.8700	48.0000
15264000	RUSSIAN P NR COOPER LANDING AK	60.4500	149.9800	61.8000
15266300	KENAI R AT SOLDOTNA AK	60.4800	151.0800	2010.0000
15266500	BEAVER C NR KENAI AK	60.5600	151.1200	51.0000
15267900	RESURRECTION C NR HOPE AK	60.8900	149.6400	149.0000
15269500	GRANITE C NR PORTAGE AK	60.7300	149.2800	28.2000
15270100	FRESNO C AT SHIELD AK	60.6700	149.4800	6.0300
15270400	DONALDSON C NR WIREL AK	60.7600	149.4600	4.0700
15271900	CUB C NR SUNRISE AK	60.8700	149.4300	1.8000
15272530	CALIFORNIA C AT GIRDWOOD AK	60.9600	149.1300	6.9600
15272550	GLACIER C AT GIRWOOD AK	60.9400	149.1600	62.0000
15273900	SF CAMPBELL C AT CANYON MTH NR ANCHORAGE AK	61.1500	149.7200	25.2000
15274000	S F CAMPBELL C NR ANCHORAGE AK	61.1700	149.7700	30.4000
15274300	NF CAMPBELL C NR ANCHORAGE AK	61.1700	149.7600	13.4000
15274600	CAMPBELL C NR SPENARD AK	61.1400	149.9200	69.7000
15274800	SB SF CHESTER C NR ANCHORAGE AK	61.2100	149.7300	10.8000
15275000	CHESTER C AT ANCHORAGE AK	61.2000	149.8400	20.0000
15275100	CHESTER C AT ARCTIC BLVD AT ANCH AK	61.2100	145.9000	27.2000
15276000	SHIP C NR ANCHORAGE AK	61.2200	149.6300	90.5000
15276500	SHIP C AT ELMENDORF AFB AK	61.2400	149.7900	113.0000
15277100	EAGLE R AT EAGLE RIVER AK	61.3100	149.5600	192.0000
15277200	MEADOW C AT EAGLE RIVER AK	61.3200	149.5400	7.4300
15280000	EKLUTNA C NR PALMER AK	61.4000	149.1500	119.0000
15281000	KNIK R NR PALMER AK	61.5100	149.0300	1180.0000
15282000	CAIROU C NR SUTTON AK	61.8000	147.6800	289.0000
15282300	PINOCHELE C NR SUTTON AK	61.7900	147.9300	7.9900
15282400	PURITAN C NR SUTTON AK	61.8100	148.1300	8.5100
15283500	ESKA C NR SUTTON AK	61.7300	148.9100	13.4000
15284000	MATANUSKA R AT PALMER AK	61.6100	149.0700	2070.0000
15286000	COTTONWOOD C NR WASILLA AK	61.5700	149.4100	28.5000
15290000	LITTLE SUSITNA R NR PALMER AK	61.7100	149.2300	61.9000
15291000	SUSITNA R NR DENALI AK	63.1000	147.5200	950.0000
15291100	RAFT C NR DENALI AK	63.0500	147.2700	4.3300
15291200	MACLAREN R NR PAXSON AK	63.1200	146.5300	280.0000
15291500	SUSITNA P NR CANTWELL AK	62.7000	147.5400	4140.0000
15292000	SUSITNA P AT GOLD CR AK	62.7700	149.6900	6160.0000
15292400	CHULITNA R NR TALKKEETNA AK	62.5600	150.2300	2570.0000
15292700	TALKKEETNA R NR TALKKEETNA AK	62.3500	150.0200	2006.0000
15292800	MONTANA C NR MONTANA AK	62.1100	150.0500	164.0000
15292900	GOOSE C NR MONTANA AK	62.0600	150.0600	14.5000
15293000	CASWELL C NR CASWELL AK	61.9500	150.0500	19.6000
15294300	SKWENTNA R NR SKWENTNA AK	61.8700	151.3700	2250.0000
15294500	CHAKACHATNA R NR TYONEK AK	61.2100	152.3600	1120.0000
15297655	CLFVENGEP C ON AMCHITKA ISLAND AK	51.4100	179.1800	0.2800
15297680	BRIDGE C AT AMCHITKA ISLAND AK	51.4500	179.1800	3.0300
15297690	WHITE ALICE C ON AMCHITKA ISLAND AK	51.4800	179.1200	0.7900
15297900	ESKIMO C AT KING SALMON AK	58.6900	156.6700	16.1000
15298000	TANALIAN R NR PT ALSWORTH AK	60.1900	154.2600	200.0000
15300000	NEWHALEN R NR ILIAMNA AK	59.8600	154.8700	3478.0000
15300500	KVICHAK R AT IGIUGIG AK	59.3300	155.9000	6500.0000
15302000	NUYAKUK R NR DILLINGHAM AK	59.9300	158.1800	1490.0000
15302800	GRANT LK OUTLET NR ALEKNAGIK AK	59.8000	158.5500	34.3000
15302900	MOODY C AT ALEGNAGIK AK	59.2800	158.6000	1.2800
15303000	WOOD R NR ALEKNAGIK AK	59.2700	158.5900	1110.0000
15303010	SILVER SALMON C NR ALEKNAGIK AK	59.2300	158.6700	4.4600
15303600	KUSKOKWIM R AT MCGRATH AK	62.9500	155.5900	11700.0000
15304000	KUSKOKWIM R AT CROOKED CR AK	61.8700	158.1100	31100.0000
15305900	DENNISON FK NR TETLIN JUNCTION, AK	63.4200	142.4800	2.9300
15305920	WF TR NR TETLIN JUNCTION AK	63.6700	142.2700	1.0200
15305950	TAYLOR C NR CHICKEN AK	63.9100	142.2200	38.4000
15356000	YUKON R AT EAGLE AK	64.7900	141.2000	113500.0000
15365000	DISCOVERY F AMERICAN C NR FAGLE AK	64.6600	141.3000	5.5300
15367500	BLUFF C NR EAGLE AK	64.7500	141.2300	3.3800
15389000	PORCUPINE R NR FORT YUKON AK	66.9900	143.1400	29500.0000
15389500	CHANDALAR R NR VENETIE AK	67.1000	147.1800	9330.0000
15438500	BEDHOCK C NR MILLAR HOUSE AK	65.5600	145.0900	9.9400
15439800	ROULDER C NR CFNTRAL AK	65.5700	144.8900	31.3000

Table 2.--Basin characteristics of Area II gages--Continued.

Station no.	Station name	Location		Drainage area (mi ²)
		Latitude (Degrees)	Longitude (Degrees)	
15442500	QUARTZ C NR CENTRAL AK	65.6200	144.4900	17.2000
15457400	HESS C NR LIVENG000 AK	65.6700	149.0900	662.0000
15468000	YUKON R AT RAMPART AK	65.5100	150.1700	199400.0000
15469900	SILVER C NR NORTHWAY JUNCTION AK	62.9800	141.6700	11.7000
15470000	CHISANA R AT NORTHWAY JCT AK	63.0100	141.8000	3280.0000
15471000	HITCHE C NR NORTHWAY JUNCTION AK	63.1600	142.0400	15.4000
15471500	TANANA R TR NR FTLIN JUNCTION AK	63.2800	142.5100	7.4300
15473600	LOG CAHIN C NR LOG CAHIN INN AK	63.0200	143.3400	10.7000
15473950	CLEARWATER C NR TOR AK	63.1600	143.1400	36.4000
15476000	TANANA R AT TANACROSS AK	63.3900	143.7500	4550.0000
15476050	TANANA R TR NR TANACROSS AK	63.4100	143.8000	3.3200
15476200	TANANA R TR NR DOT LAKE AK	63.6900	144.2900	11.0000
15476300	BERRY C NR DOT LK AK	63.6900	144.3600	65.1000
15476400	DWY C NR DOT LK AK	63.6900	144.5700	57.6000
15478000	TANANA R AT BIG DELTA AK	64.1600	145.8500	13500.0000
15478010	ROCK C NR PAXSON AK	63.0700	146.1000	50.3000
15478040	PHLAN C NR PAXSON AK	63.2400	145.4600	17.2000
15478050	MCCALLUM C NR PAXSON AK	63.2200	145.6500	15.5000
15478500	PURY C NR DONNELLY AK	63.6300	145.8800	5.3200
15480000	RANNEW C AT RICHARDSON AK	64.2900	146.3500	20.2000
15484000	SALCHA P NR SALCHARET AK	64.4700	146.9200	2170.0000
15490000	MONUMENT C AT CHENA HOT SPRINGS AK	65.0500	146.0500	25.7000
15493000	CHENA R NR TWO RIVERS AK	64.9000	146.4100	941.0000
15511000	L CHENA R NR FAIRBANKS AK	64.8900	147.2500	372.0000
15511500	STEELE R NR FAIRBANKS AK	64.8900	147.4900	10.7000
15514000	CHENA R AT FAIRBANKS AK	64.8500	147.7000	1980.0000
15514500	WOOD R NR FAIRBANKS AK	64.4400	148.2100	855.0000
15515500	TANANA R AT NENANA AK	64.5700	149.0900	25600.0000
15515800	SEATTLE C NR CANTWELL AK	63.3300	148.2500	36.2000
15515900	LILY C NR CANTWELL AK	63.3300	148.2700	5.6300
15516000	NENANA R NR WINDY AK	63.4600	148.8000	710.0000
15516200	SLIME C NR CANTWELL AK	63.5100	148.8100	6.9000
15518000	NENANA R NR HEALY AK	63.8500	148.9400	1910.0000
15518100	L PANGUINGUE C NR LIGNITE AK	63.9300	149.1000	3.4400
15518200	POCK C NR FERRY AK	64.0300	149.1400	8.1700
15518250	RITCH C NR REX AK	64.1800	149.2900	4.1000
15518350	TEKLANIKA R NR LIGNITE AK	63.9200	149.5000	490.0000
15519000	BRIDGE C NR LIVENG000 AK	65.4600	148.2500	12.6000
15519200	PROOKS C TR NR LIVENG000 AK	65.3800	148.9400	7.8100
15520000	IDAHO C NR MILLAR HOUSE AK	65.3500	146.1700	5.3100
15530000	FAITH C NR CHENA HOT SPRINGS AK	65.2900	146.3800	61.1000
15535000	CARIBOU C NR CHATANIKA AK	65.1500	147.5500	9.1900
15541600	GLOBE C NR LIVENG000 AK	65.2800	148.1400	23.0000
15541650	GLOBE C TR NR LIVENG000 AK	65.2800	148.1200	9.0100
15541800	WASHINGTON C NR FOX AK	65.1500	147.8600	46.7000
15546600	MELOZITNA R NR RUHY AK	64.7900	155.5600	2693.0000
15546800	YUKON R AT RUHY AK	64.7400	155.4900	259000.0000
15546875	MF KOYUKUK R NR WISEMAN AK	67.4300	150.0800	1426.0000
15546877	WISEMAN C AT WISEMAN AK	67.4100	150.1100	49.2000
15546885	JIM R NR HETTLES AK	66.7800	150.8700	465.0000
15546900	KOYUKUK P AT HUGHES AK	66.0500	154.2600	18700.0000
15546920	YUKON R NR KALTAG AK	64.3300	158.7200	296000.0000
15621000	SNAKE R NR NOME AK	64.5600	165.5100	85.7000
15625000	ARTIC C NR NOME AK	64.6400	165.7100	1.7600
15633000	WASHINGTON C NR NOME AK	64.7100	165.8200	6.3400
15668100	STAR C NR NOME AK	64.9300	164.9600	3.7800
15668200	CHATER C NR NOME AK	64.9300	164.8700	21.9000
15712000	KUZITRIN R NR NOME AK	65.2200	164.6200	1720.0000
15744000	KUHK R AT AMBLER AK	67.0900	157.8500	6570.0000
15746000	NOATAK R AT NOATAK AK	67.5700	162.9400	12000.0000
15748000	OGOTORUK R NR POINT HOPE AK	68.1100	165.7500	34.9000
15896000	KUPAPUK R NR DEADHORSE AK	70.2800	148.9600	3130.0000
15910000	SAGAVANIRKOK R NR SAGWON AK	69.0900	148.7500	2208.0000

Drainage Basin Characteristics

Precipitation and topographic characteristics of drainage basins at the gaging stations are tabulated above. Precipitation characteristics were determined from National Weather Service publications. Topographic characteristics were computed from the latest U.S. Geological Survey topographic maps. Basin characteristics are defined as follows:

Drainage area: in square miles, is the total drainage area upstream from the gaging station or measurement site. The area is measured in a horizontal plane and is enclosed by a drainage divide.

Main-channel slope: in feet per mile, is the average slope between points 10 percent and 85 percent of the distance along the main stream from the gaging site to the basin divide.

Stream length: in miles, is the length of the main channel between the gaging station and the basin divide measured along the channel that drains the largest basin.

Mean basin elevation: in feet above mean sea level, is the mean elevation of the drainage basin measured by the grid-sampling method from topographic maps.

Area of lakes and ponds: in percent, is the percentage of the total drainage area occupied by lakes and ponds. This is measured by the grid-sampling method from topographic maps having a blue overprint which indicates lakes and ponds.

Table 2.--Basin characteristics of Area II gages--Continued.

Station no.	Main-channel slope (ft/mi)	Stream length (mi)	Mean basin elevation (ft)	Area of lakes and ponds (percent)	Area of forests (percent)	Area of glacier (percent)	Mean annual precipitation (in)	Precipitation intensity (in)	Mean annual snowfall (in)	Mean minimum January temperature (°F)
15442500	96.0000	8.5000	1270.0000	0.0	98.0000	0.0	14.0000	1.0000	50.0000	-24.0000
15457800	23.8000	44.8000	1400.0000	0.0	49.0000	0.0	15.0000	1.0000	50.0000	-16.0000
15468000	2.1000	1160.0000	2910.0000	3.0000	69.0000	2.0000	13.0000	1.0000	55.0000	-16.0000
15469900	305.0000	4.8000	2400.0000	1.0000	94.0000	0.0	12.0000	1.5000	40.0000	-24.0000
15470000	2.5400	12.1000	3730.0000	2.0000	50.0000	5.0000	15.0000	1.3000	60.0000	-23.0000
15471000	123.0000	5.4000	2430.0000	0.0	99.0000	0.0	10.0000	1.5000	30.0000	-24.0000
15471500	428.0000	2.8000	2600.0000	0.0	100.0000	0.0	10.0000	1.5000	30.0000	-24.0000
15473600	543.0000	5.4000	3730.0000	0.0	58.0000	0.0	15.0000	2.0000	40.0000	-16.0000
15473950	225.0000	12.6000	4300.0000	0.0	31.0000	0.0	12.0000	3.0000	30.0000	-20.0000
15476000	8.9300	230.0000	3860.0000	2.0000	45.0000	7.0000	18.0000	1.5000	55.0000	-22.0000
15476050	828.0000	4.2000	3300.0000	0.0	63.0000	0.0	12.0000	3.0000	30.0000	-16.0000
15476200	169.0000	7.1000	2000.0000	1.0000	82.0000	0.0	15.0000	3.0000	30.0000	-14.0000
15476300	223.0000	19.1000	3200.0000	1.0000	40.0000	5.0000	18.0000	2.0000	30.0000	-14.0000
15476400	185.0000	12.9000	3100.0000	1.0000	35.0000	0.0	18.0000	2.0000	30.0000	-13.0000
15478000	3.8600	346.0000	3440.0000	2.0000	50.0000	6.0000	22.0000	1.5000	60.0000	-20.0000
15478010	74.0000	12.8000	4200.0000	7.0000	0.0	0.0	25.0000	2.0000	200.0000	-8.0000
15478040	552.0000	4.6000	5800.0000	0.0	0.0	69.0000	80.0000	1.5000	200.0000	-8.0000
15478050	356.0000	9.0000	4880.0000	0.0	0.0	19.0000	80.0000	1.5000	200.0000	-6.0000
15478500	351.0000	5.7000	3300.0000	0.0	12.0000	0.0	30.0000	1.5000	100.0000	-8.0000
15480000	217.0000	8.0000	1730.0000	0.0	95.0000	0.0	14.0000	1.5000	60.0000	-16.0000
15484000	19.4000	124.0000	2520.0000	0.0	59.0000	0.0	16.0000	1.6000	90.0000	-19.0000
15490000	192.0000	10.4000	2660.0000	0.0	44.0000	0.0	18.0000	1.2000	100.0000	-20.0000
15493000	23.4000	63.0000	2270.0000	0.0	54.0000	0.0	18.0000	1.2000	100.0000	-19.0000
15511000	17.0000	55.0000	1480.0000	0.0	94.0000	0.0	15.0000	1.4000	100.0000	-18.0000
15511500	109.0000	4.6000	1400.0000	0.0	82.0000	0.0	12.0000	1.2500	80.0000	-16.0000
15514000	126.0000	119.0000	1770.0000	2.0000	80.0000	0.0	15.0000	1.3000	90.0000	-18.0000
15514500	39.8000	83.0000	2720.0000	0.0	28.0000	2.0000	14.0000	1.3000	60.0000	-12.0000
15515500	4.1200	449.0000	3920.0000	4.0000	56.0000	6.0000	17.0000	1.4000	70.0000	-18.0000
15515800	164.0000	10.2000	3400.0000	2.0000	6.0000	0.0	20.0000	1.5000	300.0000	-6.0000
15515900	397.0000	5.7000	3590.0000	0.0	13.0000	0.0	20.0000	1.5000	300.0000	-6.0000
15516000	48.7000	52.0000	3470.0000	2.0000	5.0000	2.0000	35.0000	2.0000	200.0000	-7.0000
15516200	586.0000	5.8000	3950.0000	0.0	4.0000	0.0	40.0000	1.5000	100.0000	-8.0000
15518000	21.2000	88.0000	3500.0000	1.0000	9.0000	4.0000	40.0000	1.5000	140.0000	-8.0000
15518100	222.0000	3.3000	1960.0000	0.0	36.0000	0.0	18.0000	1.2000	70.0000	-10.0000
15518200	337.0000	7.5000	2450.0000	0.0	40.0000	0.0	16.0000	1.2000	60.0000	-12.0000
15518250	200.0000	5.0000	1490.0000	0.0	100.0000	0.0	16.0000	1.2000	50.0000	-14.0000
15518350	490.0000	36.7000	3420.0000	0.0	65.0000	2.0000	30.0000	1.2000	90.0000	-8.0000
15519000	88.0000	5.9000	1000.0000	0.0	14.0000	0.0	20.0000	1.0000	55.0000	-16.0000
15519200	230.0000	5.5000	1410.0000	0.0	98.0000	0.0	20.0000	1.0000	60.0000	-16.0000
15520000	333.0000	4.0000	2920.0000	0.0	28.0000	0.0	20.0000	1.2000	80.0000	-20.0000
15530000	95.2000	16.8000	2800.0000	0.0	48.0000	0.0	20.0000	1.2000	90.0000	-20.0000
15535000	229.0000	3.5000	1640.0000	0.0	97.0000	0.0	18.0000	1.2000	90.0000	-18.0000
15541600	127.6000	7.5000	1590.0000	0.0	90.0000	0.0	20.0000	1.2000	80.0000	-16.0000
15541650	356.0000	6.0000	1710.0000	0.0	100.0000	0.0	20.0000	1.2000	80.0000	-16.0000
15541800	53.0000	13.8000	1500.0000	0.0	94.0000	0.0	16.0000	1.2000	90.0000	-16.0000
15564600	2.9000	184.0000	1410.0000	2.0000	57.0000	0.0	16.0000	1.3000	90.0000	-17.0000
15564800	1.8000	1350.0000	2640.0000	4.0000	62.0000	1.0000	14.0000	1.0000	60.0000	-16.0000
15564875	41.2000	55.0000	3390.0000	0.0000	4.0000	0.0	20.0000	1.5000	80.0000	-16.0000
15564877	171.0000	14.0000	2930.0000	0.0	3.0000	0.0	18.0000	1.5000	75.0000	-17.0000
15564885	38.7000	44.0000	2080.0000	0.0	10.0000	0.0	15.0000	1.5000	60.0000	-16.0000
15564900	18.8000	262.0000	2200.0000	1.0000	36.0000	0.0	18.0000	1.5000	75.0000	-17.0000
15565700	1.7000	1476.0000	2490.0000	4.0000	59.0000	1.0000	15.0000	1.0000	60.0000	-15.0000
15621000	19.6000	19.5000	632.0000	0.0	4.0000	0.0	30.0000	1.5000	70.0000	-6.0000
15625000	429.0000	1.4000	820.0000	0.0	2.0000	0.0	25.0000	1.5000	60.0000	-5.0000
15633000	121.0000	4.3000	860.0000	0.0	3.0000	0.0	25.0000	1.5000	60.0000	-6.0000
15668100	522.0000	3.7000	1500.0000	0.0	1.0000	0.0	40.0000	1.5000	100.0000	-6.0000
15668200	145.0000	9.2000	1620.0000	1.0000	3.0000	0.0	40.0000	1.5000	100.0000	-7.0000
15712000	20.2000	68.0000	700.0000	1.0000	2.0000	0.0	20.0000	1.4000	70.0000	-8.0000
15744000	4.9600	188.0000	1610.0000	1.0000	34.0000	0.0	20.0000	1.5000	70.0000	-16.0000
15746000	5.6000	366.0000	1800.0000	1.0000	2.0000	0.0	20.0000	1.5000	75.0000	-16.0000
15748000	47.8000	10.5000	380.0000	0.0	0.0	0.0	16.0000	1.0000	38.0000	-16.0000
15896000	12.0000	140.0000	900.0000	2.0000	0.0	0.0	9.0000	0.7000	40.0000	-18.0000
15910000	30.4000	79.0000	3220.0000	0.0	0.0	0.0	20.0000	1.2000	60.0000	-16.0000

Area of forests: in percent, is the percentage of the total drainage area shown as forested on the topographic maps. This is measured by the grid-sampling method from topographic maps having a green overprint which indicates forest cover.

Area of glacier: in percent, is the percentage of the total drainage area shown as glacier on the topographic maps. This is measured by the grid-sampling method from topographic maps.

Mean annual precipitation: in inches, as determined from an isohyetal map (NWS, 1972) using the grid-sampling method.

Precipitation intensity: in inches, is the maximum rainfall expected in 24 hours each 2 years as determined from U.S. Weather Bureau Technical Paper 47.

Mean annual snowfall: in inches, as determined from an isohyetal map (NWS, 1972) using the grid-sampling method.

Mean minimum January temperature: in degrees F, as determined from an isothermal map (Johnson and Hartman, 1969) using grid-sampling method.

The grid-method of sampling involves the use of transparent grids to different map scales. The grids can be used in several ways. For determining area, as of ponds, a grid can be laid over a pond and the number of squares and partial squares covering the pond can be totaled and converted to an area, or the number of grid intersections within the area can be multiplied by the area in each square. For determining elevations, temperatures, etc., from a contour map, a reading is taken under each of several grid intersections and the readings are averaged. For determining percentages, as of forested area or perhaps small ponds if very numerous, the number of grid intersections occurring over forest or over water within the basin are counted, and these, multiplied by 100 and divided by the total number of grid intersections within the basin, give the desired percentage.

Table 4.--Flood magnitudes and statistics for Area II gages--Continued.

Station no.	P1.25	P2	P5	P10	P25	P50	P100	SKREW	MFAN	SD
15442500	67.0000	156.0000	285.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15457800	2200.0000	4560.0000	7860.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15468000	446000.0000	591000.0000	740000.0000	842000.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15469900	13.0000	31.0000	89.0000	169.0000	0.0 R	0.0 R	0.0 R	0.0 R	1.5460	0.5110
15470000	6870.0000	7650.0000	8830.0000	9670.0000	10800.0000	11700.0000	12600.0000	1.0000	3.8950	0.0680
15471000	49.0000	93.0000	228.0000	400.0000	0.0 R	0.0 R	0.0 R	0.0 R	2.0420	0.4170
15471500	9.0000	15.0000	25.0000	34.0000	0.0 R	0.0 R	0.0 R	0.0 R	1.1820	0.2670
15473600	47.0000	106.0000	243.0000	376.0000	0.0 R	0.0 R	0.0 R	0.0 R	2.0290	0.4250
15473950	231.0000	431.0000	769.0000	1020.0000	0.0 R	0.0 R	0.0 R	0.0 R	2.6210	0.3110
15476000	26500.0000	29400.0000	33100.0000	35500.0000	38300.0000	40400.0000	42400.0000	0.4310	4.4730	0.0580
15476050	30.0000	103.0000	231.0000	304.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15476200	49.0000	75.0000	109.0000	131.0000	0.0 R	0.0 R	0.0 R	0.0 R	1.8620	0.2070
15476300	415.0000	698.0000	1240.0000	1720.0000	0.0 R	0.0 R	0.0 R	0.0 R	2.8610	0.2840
15476400	566.0000	943.0000	1430.0000	1720.0000	0.0 R	0.0 R	0.0 R	0.0 R	2.9460	0.2440
15478000	42900.0000	48900.0000	55800.0000	59900.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15478010	394.0000	726.0000	1190.0000	1470.0000	1790.0000	0.0 R	0.0 R	0.0 R	2.8250	0.2920
15478040	633.0000	900.0000	1370.0000	1770.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15478050	328.0000	456.0000	694.0000	902.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15478500	48.0000	105.0000	190.0000	241.0000	297.0000	0.0 R	0.0 R	0.0 R	1.9630	0.3710
15480000	50.0000	156.0000	416.0000	658.0000	0.0 B	0.0 R	0.0 R	0.0 R	2.1460	0.5520
15484000	12300.0000	18300.0000	27400.0000	34000.0000	42900.0000	50000.0000	57300.0000	0.0770	4.2650	0.2070
15490000	207.0000	594.0000	1140.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 B	0.0 R
15493000	4450.0000	7210.0000	12800.0000	18000.0000	26700.0000	35000.0000	0.0 R	0.0 R	3.8860	0.5540
15511000	1330.0000	1790.0000	2700.0000	3530.0000	4880.0000	0.0 R	0.0 R	0.0 R	3.2880	0.1940
15511500	9.7000	27.0000	103.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15514000	6740.0000	9920.0000	15600.0000	20300.0000	27400.0000	33800.0000	41000.0000	0.5560	4.0170	0.2190
15514500	3640.0000	4210.0000	4860.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15515500	69200.0000	80600.0000	97800.0000	110000.0000	127000.0000	0.0 R	0.0 R	0.0 R	4.9190	0.0920
15515800	345.0000	596.0000	1200.0000	1840.0000	0.0 B	0.0 R	0.0 R	0.0 B	2.8220	0.3320
15515900	46.0000	90.0000	153.0000	193.0000	0.0 R	0.0 B	0.0 B	0.0 R	1.9110	0.3210
15516000	5480.0000	6710.0000	8380.0000	9480.0000	10900.0000	11900.0000	13000.0000	0.3150	3.8330	0.1100
15516200	93.0000	156.0000	301.0000	451.0000	0.0 B	0.0 R	0.0 R	0.0 B	0.0 B	0.0 R
15518000	17400.0000	21200.0000	27600.0000	32500.0000	39400.0000	45100.0000	51300.0000	0.8740	4.3450	0.1240
15518100	11.0000	45.0000	118.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 B	0.0 R
15518200	71.0000	194.0000	542.0000	933.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15518250	37.0000	87.0000	201.0000	309.0000	0.0 R	0.0 R	0.0 R	0.0 R	1.9320	0.4400
15518350	3300.0000	4950.0000	9970.0000	16500.0000	0.0 B	0.0 R	0.0 R	0.0 B	3.7830	0.3280
15519000	89.0000	175.0000	411.0000	692.0000	0.0 R	0.0 B	0.0 R	0.0 B	2.2960	0.4070
15519200	14.0000	56.0000	130.0000	171.0000	0.0 R	0.0 B	0.0 R	0.0 R	1.5940	0.6320
15520000	64.0000	136.0000	313.0000	500.0000	0.0 R	0.0 R	0.0 B	0.0 B	2.1580	0.4120
15530000	867.0000	1210.0000	2050.0000	2940.0000	0.0 R	0.0 R	0.0 R	0.0 B	3.1410	0.2450
15535000	59.0000	82.0000	112.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15541600	124.0000	250.0000	535.0000	817.0000	0.0 R	0.0 B	0.0 R	0.0 R	2.4160	0.3800
15541650	67.0000	119.0000	228.0000	331.0000	0.0 R	0.0 R	0.0 R	0.0 B	2.0990	0.3190
15541800	306.0000	623.0000	1310.0000	1940.0000	0.0 R	0.0 R	0.0 R	0.0 R	2.8030	0.3750
15564600	13200.0000	21100.0000	27800.0000	30300.0000	0.0 R	0.0 R	0.0 R	0.0 R	4.2670	0.2180
15564800	481000.0000	625000.0000	777000.0000	857000.0000	939000.0000	991000.0000	0.0 R	0.0 R	5.7820	0.1260
15564875	6150.0000	9110.0000	14100.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15564877	358.0000	485.0000	633.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15564885	6500.0000	8570.0000	9860.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15564900	92300.0000	130000.0000	184000.0000	220000.0000	267000.0000	0.0 R	0.0 R	0.0 B	5.1150	0.1770
15565200	583000.0000	744000.0000	936000.0000	1050000.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15621000	2350.0000	2930.0000	3670.0000	4130.0000	0.0 R	0.0 R	0.0 R	0.0 B	0.0 B	0.0 R
15625000	19.0000	69.0000	153.0000	0.0 B	0.0 B	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15633000	51.0000	117.0000	262.0000	397.0000	0.0 R	0.0 R	0.0 R	0.0 B	2.0600	0.4250
15668100	25.0000	70.0000	140.0000	179.0000	0.0 R	0.0 R	0.0 R	0.0 B	1.7410	0.4820
15668200	389.0000	873.0000	1660.0000	2190.0000	0.0 R	0.0 R	0.0 R	0.0 B	2.8910	0.3850
15712000	9140.0000	14100.0000	23100.0000	36100.0000	0.0 B	0.0 B	0.0 R	0.0 R	0.0 B	0.0 R
15744000	54400.0000	72700.0000	89700.0000	97400.0000	0.0 B	0.0 B	0.0 B	0.0 B	0.0 B	0.0 R
15746000	136000.0000	165000.0000	208000.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 B	0.0 R
15748000	613.0000	1000.0000	1380.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R	0.0 R
15896000	26000.0000	44000.0000	73300.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R
15910000	13900.0000	21800.0000	28300.0000	0.0 R	0.0 R	0.0 R	0.0 R	0.0 R	0.0 B	0.0 R

Table 5.--Maximum known floods in Alaska.

Station no.	Stream	Location		Drainage area (mi ²)	Period of record (years/dates)	Date	Maximum known flood		
		Latitude	Longitude				Gage height (ft)	Discharge	
SOUTHEAST									
15008000	Salmon R nr Hyder	56°01'34"	130°03'55"	94.0	10(1963-73)	Aug. 30, 1971	28.9	*140,000	1,490
15010000	Davis R nr Hyder	55°45'00"	130°12'00"	80	10(1930-40)	Nov. 12, 1936	13.30	19,500	244
15010500	Halibut Bay Tr nr Hyder	55°15'00"	130°06'00"	8.58	8(1963-71)	Oct. 19, 1964	14.48	3,400	396
15011500	Red R nr Metlakatla	55°08'29"	130°31'50"	45.3	13(1963-76)	Dec. 31, 1963	10.66	11,700	258
15011900	Cabin C nr Ketchikan	55°19'19"	130°47'00"	8.80	6(1964-71)	Sept. 23, 1967	11.41	1,400	159
15012000	Winstanley C nr Ketchikan	55°25'00"	130°52'05"	15.5	30(1936-38, 1947-75)	Jan. 30, 1962	6.65	4,120	266
15014000	Punchbowl L O nr Ketchikan	55°31'00"	130°44'00"	12	6(1923-30)	Dec. 7, 1925	-	710	59.1
15015600	Klahini R nr Bell Island	56°03'15"	131°02'55"	58.0	6(1967-73)	Nov. 1, 1969	8.95	12,400	214
15016000	Short C nr Bell Island	56°01'00"	131°32'00"	20	1(1922-25)	Sept. 5, 1924	-	1,000	50.0
15018000	Shelokum L O nr Bell Island	55°59'00"	131°39'00"	18	6(1915-25)	Dec. 18, 1919	-	3,100	172
15019000	Black Bear C nr Meyers Chuck	55°43'30"	132°09'48"	16.5	8(1963-71)	Mar. 29, 1966	16.76	3,470	210
15020000	Tyee C nr Wrangell	56°12'00"	131°31'00"	14	1(1921-22, 1924-27)	Oct. 5, 1926	-	1,060	75.8
15020100	Tyee C at mouth nr Wrangell	56°12'54"	131°30'25"	16.1	7(1963-69)	Oct. 23, 1965	4.46	2,440	152
15022000	Harding R nr Wrangell	56°12'48"	131°38'12"	67.4	25(1951-76)	Oct. 14, 1961	16.22	15,000	223
15024000	Mill C nr Wrangell	56°28'00"	132°12'00"	37	3(1915-17, 1923-25, 1927-28)	Oct. 16, 1915	-	3,310	89.4
15026000	Cascade C nr Petersburg	57°00'21"	132°46'45"	23.0	35(1917-28, 1946-73)	Sept. 11, 1947	10.0	3,280	143
15028000	Scenery C nr Petersburg	57°05'00"	132°47'00"	30.0	4(1949-52, 1953-54)	Sept. 23, 1949	5.82	4,300	143
15030000	Sweetheart Falls C nr Juneau	57°57'00"	133°41'00"	27	5(1915-17, 1918-27)	Sept. 26, 1918	-	2,880	106
15031000	Long R ab Long L nr Juneau	58°10'56"	133°53'06"	8.29	10(1965-75)	Sept. 28, 1968	15.05	3,530	426
15032000	Long L O nr Juneau	58°10'00"	133°43'30"	30.2	1(1913-15)	Oct. 20, 1913	-	4,250	141
15034000	Long R nr Juneau	58°10'00"	133°41'50"	32.5	28(1915-24, 1926-33, 1951-73)	Sept. 10, 1927	10.2	6,000	185
15036000	Speel R nr Juneau	58°12'10"	133°36'40"	226	17(1916-18, 1960-75)	Sept. 27, 1918	-	35,600	158
15038000	Crater C near Juneau	58°08'15"	133°46'15"	11.4	9(1913-21, 1922-24, 1927-32)	Sept. 9, 1927	-	3,100	272
15040000	Dorothy C nr Juneau	58°13'40"	134°02'25"	15.2	37(1929-67)	Nov. 3, 1949	5.85	1,780	117
15042000	Carlson C at Sunny Cove nr Juneau	58°19'00"	134°11'00"	22.3	5(1914-20)	Sept. 26, 1918	-	6,200	278
15044000	Carlson C nr Juneau	58°18'25"	134°08'43"	24.3	10(1951-61)	Aug. 12, 1961	10.5	5,100	210
15046000	Grindstone C nr Juneau	58°12'31"	134°10'34"	3.6	3(1916-20)	Sept. 26, 1918	-	700	194
15048000	Sheep C nr Juneau	58°16'30"	134°18'50"	4.57	30(1911-13, 1916-20, 1946-73)	Sept. 8, 1948	3.60	840	184
15050000	Gold C at Juneau	58°18'25"	134°24'05"	9.76	33(1916-20, 1946-48, 1949-76)	Aug. 12, 1961	6.57	2,650	272
15052000	Lemon C nr Juneau	58°23'15"	134°25'15"	12.1	22(1951-73)	Aug. 13, 1961	5.31	3,370	279
15052500	Mendenhall R nr Auke Bay	58°25'05"	134°32'40"	85.1	11(1965-76)	Sept. 28, 1976	8.67	9,820	115
15052800	Montana C nr Auke Bay	58°23'53"	134°36'34"	15.5	10(1965-76)	Aug. 23, 1966	16.77	1,920	124
15053800	Lake C at Auke Bay	58°23'40"	134°37'50"	2.50	10(1963-73)	Aug. 23, 1966	5.20	980	391
15054000	Auke C at Auke Bay	58°22'56"	134°38'10"	3.96	16(1947-50, 1962-75)	Nov. 2, 1949	4.85	348	92.7
15054200	Herbert R nr Auke Bay	58°31'26"	134°47'40"	56.9	5(1966-71)	Sept. 18, 1967	22.40	6,280	110
15054500	Bessie C nr Auke Bay	58°35'30"	134°54'00"	1.35	10(1966-76)	Nov. 2, 1974	7.51	300	222
15054600	Bridget Cove Tr nr Auke Bay	58°37'14"	134°56'08"	0.95	3(1970-73)	May 20, 1972	2.97	108	114
15054900	Davies C nr Auke Bay	58°39'06"	134°53'07"	15.2	3(1969-72)	Aug. 8, 1972	7.85	1,560	103
15056000	Sherman C at Comet	58°52'05"	135°07'05"	3.65	2(1914-16)	Oct. 15, 1915	-	208	57.0
15056100	William Henry C nr Auke Bay	59°27'27"	135°19'23"	145	12(1963-75)	Sept. 15, 1967	8.50	13,600	93.7
15056200	West C nr Skagway	59°31'35"	135°21'10"	43.2	15(1962-76)	Sept. 15, 1967	7.75	9,800	226
15056210	Taiya R nr Skagway	59°30'44"	135°20'40"	179	7(1969-76)	Sept. 1967	-	25,000+	140+
15056500	Chilkat R at gorge nr Klukwan	59°37'40"	135°55'55"	190	6(1962-68)	Sept. 15, 1967	14.59	22,000	116
15056500	Chilkat R nr Klukwan	59°24'55"	135°55'45"	760	3(1959-61)	Aug. 14, 1961	27.40	20,600	27.1
15057500	William Henry C nr Auke Bay	58°44'46"	135°14'25"	1.58	8(1966-76)	Sept. 15, 1967	13.70	663	419
15058000	Purple L O nr Metlakatla	55°06'00"	131°26'00"	6.8	8(1947-56)	Apr. 27, 1949	5.15	716	105
15059500	Whipple C nr Ward Cove	55°26'30"	131°47'38"	5.29	8(1968-76)	Nov. 19, 1968	8.73	2,830	535
15060000	Perseverance C nr Wacker	55°24'40"	131°40'05"	2.81	26(1931-39, 1946-69)	Oct. 18, 1964	5.68	682	243
15062000	Ward C nr Wacker	55°25'50"	131°40'00"	14.0	4(1948-58)	Apr. 16, 1952	6.83	2,600	186
15064000	Ketchikan C nr Ketchikan	55°20'40"	131°38'05"	13.5	9(1909-12, 1915-19, 1964-67)	Nov. 18, 1917	-	4,400	325
15066000	Beaver Falls C nr Ketchikan	55°22'55"	131°28'25"	5.8	5(1917, 1920-25, 1927-32)	Nov. 7, 1929	-	2,180	376
15068000	Mahoney C nr Ketchikan	55°25'30"	131°30'45"	5.70	18(1920-33, 1947-58)	Feb. 2, 1954	4.66	2,530	444
15070000	Falls C nr Ketchikan	55°36'50"	131°20'55"	36.5	25(1916-26, 1927-33, 1946-59)	Nov. 1, 1917	-	5,500	150
15072000	Fish C nr Ketchikan	55°23'30"	131°11'40"	32.1	55(1915-35, 1938-76)	Oct. 15, 1961	5.85	5,400	168
15072200	Sea Level C nr Ketchikan	55°22'05"	131°11'03"	18.6	8(1963-71)	Oct. 19, 1964	13.50	4,000	215
15074000	Ella C nr Ketchikan	55°30'20"	131°01'25"	19.7	22(1927-38, 1947-58)	Dec. 7, 1930	-	1,720	87.3
15076000	Manzanita C nr Ketchikan	55°35'45"	130°58'40"	33.9	30(1927-37, 1947-67)	Oct. 14, 1961	10.27	5,820	171
15078000	Grace C nr Ketchikan	55°39'28"	130°58'14"	30.2	16(1927-37, 1963-69)	Sept. 4, 1966	6.22	3,990	132
15079800	Klu C nr Bell Island	55°50'30"	131°25'20"	5.97	6(1963-68)	Feb. 10, 1965	13.20	1,180	198
15080000	Orchard C nr Bell Island	55°50'00"	131°27'00"	59	7(1915-27)	Nov. 1, 1917	-	7,100	120
15080500	Traitors R nr Bell Island	55°43'59"	131°30'00"	20.8	4(1964-68)	Oct. 18, 1964	6.10	2,200	110
15081490	Yatuk C nr Klawock	55°53'57"	133°08'42"	5.80	6(1971-76)	Oct. 8, 1974	18.69	1,150	198
15081500	Staney C nr Craig	55°48'57"	133°07'58"	51.6	12(1964-76)	Oct. 18, 1964	13.1	15,600	302
15081800	N B Trocadero C nr Hyدابurg	55°21'41"	132°52'20"	17.4	7(1967-73)	Sept. 29, 1972	7.75	5,900	339
15081890	Natzuhini C nr Hyدابurg	55°17'08"	132°49'18"	9.10	5(1971-76)	Aug. 19, 1971	21.17	2,520	277
15082000	Reynolds C nr Hyدابurg	55°12'50"	132°36'10"	5.7	6(1951-56)	Feb. 2, 1954	3.35	475	83.4

Table 5.--Maximum known floods in Alaska--Continued.

Station no.	Stream	Location		Drainage area (mi ²)	Period of record (years/dates)	Date	Maximum known flood			
		Latitude	Longitude				Gage height (ft)	Discharge		
							(ft ³ /s)	[(ft ³ /s)/mi ²]		
NORTHWEST										
15585000	Goldengate C nr Nome	64°26'03"	165°02'46"	1.55	1(1965-67)	Sept. 8, 1965	11.70	63	40.6	
15621000	Snake R nr Nome	64°33'51"	165°30'26"	85.7	10(1965-76)	June 2, 1966	11.90	4,200	49.0	
15625000	Arctic C nr Nome	64°38'15"	165°42'46"	1.76	8(1967-76)	July 10, 1975	-	199	113	
15633000	Washington C nr Nome	64°42'52"	165°49'13"	6.34	11(1964-76)	July 10, 1975	19.35	620	97.8	
15668000	Kruzgamepa R nr Iron C	64°55'00"	164°57'20"	84	2(1908-10)	Sept. 8, 1910	-	4,300	51.2	
15668100	Star C nr Nome	64°55'40"	164°57'39"	3.78	12(1964-76)	July 30, 1972	13.30	152	40.2	
15668200	Crater C nr Nome	64°55'48"	164°52'12"	21.9	12(1964-76)	July 10, 1975	19.71	2,540	116	
15712000	Kuzitrin R nr Nome	65°13'17"	164°37'15"	1,720	11(1908-10)	June 3, 1971	-	40,000	23.3	
15743000	June C nr Kotzebue	66°51'37"	162°36'13"	10.9	3(1965-67)	June 8, 1966	6.72	209	19.2	
15744000	Kobuk R at Ambler	67°05'13"	157°50'51"	6,570	11(1965-76)	May 29, 1971	-	95,000	14.6	
15746000	Noatak R at Noatak	67°34'18"	162°56'38"	12,000	5(1965-71)	June 14, 1968	28.7	242,000	20.2	
15748000	Ogotoruk R nr Point Hope	68°06'40"	165°45'10"	35	5(1958-62)	Sept. 4, 1961	4.36	1,450	41.4	
ARCTIC SLOPE										
15798700	Nunavak C nr Barrow	71°15'35"	156°46'57"	2.79	5(1972-76)	June 23, 1974	2.92	66	23.7	
15799000	Esatkuat C nr Barrow	71°16'30"	156°43'44"	1.46	2(1972-73)	June 13, 1972	2.90	67	45.9	
15799300	Esatkuat Lagoon O at Barrow	71°17'40"	156°46'06"	3.52	2(1972-73)	June 12, 1973	1.46	101	28.7	
-	Colville R nr Nuiqsut	70°09'56"	150°55'00"	20,670	Max. Evident	--	-	600,000	29.0	
15875000	Colville R at mouth	70°30'00"	150°30'00"	23,300	Miscellaneous	June 14, 1962	-	216,000	9.3	
15896000	Kuparuk R nr Deadhorse	70°16'54"	148°57'35"	3,130	6(1971-76)	June 6, 1973	36.7	82,000	26.2	
15896000	Kuparuk R nr Deadhorse	70°16'54"	148°57'35"	3,130	Max. Evident	--	-	100,000	31.9	
15896700	Putuligayuk R nr Deadhorse	70°16'04"	148°37'36"	176	7(1970-76)	June 6, 1971	24.50	4,980	28.3	
-	Atigun R nr Galbraith Lake	68°22'08"	149°20'12"	173	Max. Evident	--	-	12,000	69.4	
15904900	Atigun R Tr nr Pump Sta 4	68°22'25"	149°18'48"	32.6	1(1976-)	July 29, 1976	-	1,000	30.7	
15905000	Galbraith Lk Tr nr Galbraith Camp	68°29'30"	149°30'36"	7.55	2(1975-76)	June 1976	29.8	38	5.0	
15910000	Sagavanirktok R nr Sagwon	69°05'24"	147°45'34"	2,208	8(1969-76)	Aug. 1969	18.4	34,900	15.8	
15910000	Sagavanirktok R nr Sagwon	69°05'24"	147°45'34"	2,208	Max. Evident	--	-	62,000	28.1	
15910200	Happy C nr Happy Valley	69°08'50"	148°49'50"	34.5	5(1972-76)	June 6, 1976	18.51	1,390	40.3	
-	Kadleroshilik R nr Deadhorse	69°56'06"	147°51'15"	451	Max. Evident	--	-	23,000	51.0	
-	Shaviovik R (Upper site)	69°52'21"	147°38'44"	660	Max. Evident	--	-	21,000	31.8	
-	Shaviovik R nr Deadhorse	70°05'07"	147°16'30"	1,580	Max. Evident	--	-	22,000	13.9	
-	Kavik R nr Deadhorse	69°32'10"	146°39'44"	237	Max. Evident	--	-	13,000	54.9	
-	Marsh Fk Canning R nr Arctic Village	69°09'53"	145°53'30"	588	Max. Evident	--	-	18,000	30.6	
-	Canning R nr Arctic Village	69°21'10"	146°02'31"	1,326	Max. Evident	--	-	22,000	16.6	
-	Canning R nr Deadhorse	69°50'38"	146°27'10"	1,871	Max. Evident	--	-	53,000	28.3	
-	Katakaturuk R nr Kaktovik	69°52'25"	145°27'10"	228	Max. Evident	--	-	10,000	43.9	
-	Marsh C nr Kaktovik	69°47'32"	144°49'00"	261	Max. Evident	--	-	500	1.9	
15975000	Chamberlin C nr Barter Island	69°17'30"	144°57'50"	1.46	Miscellaneous	July 5, 1958	-	88	60.3	
15976000	Neruokpukkoonga C nr Barter Island	69°18'30"	145°01'30"	123	Miscellaneous	June 23, 1958	-	706	5.7	
-	Sadlerochit R nr Kaktovik	69°39'13"	144°12'10"	529	Max. Evident	--	-	11,000	20.8	
-	Hulahula R nr Kaktovik	69°41'47"	144°12'10"	682	Max. Evident	--	-	10,000	14.7	
-	Jago R nr Kaktovik	69°37'02"	143°41'06"	321	Max. Evident	--	-	14,000	43.6	
-	Okerokovik R nr Kaktovik	69°42'07"	143°14'23"	169	Max. Evident	--	-	2,300	13.6	
-	Aichilik R nr Kaktovik	69°35'23"	142°58'03"	563	Max. Evident	--	-	27,000	48.0	
-	Egaksrak R nr Kaktovik	69°32'05"	142°41'05"	215	Max. Evident	--	-	9,000	41.9	
-	Ekaluakat R nr Kaktovik	69°34'35"	142°18'38"	146	Max. Evident	--	-	27,000	185	
-	Kongakut R nr Kaktovik	69°30'54"	142°42'34"	1,240	Max. Evident	--	-	98,000	79.0	
-	Turner B nr Kaktovik	69°35'56"	141°24'10"	51	Max. Evident	--	-	1,500	29.4	

Footnote explanation

* Glacier-dammed lake breakout.

+ Augmented by release of stored water from unnamed lake after embankment was breached.

f Flood from Sheep Creek overflow August 10, 1971, 19.69 ft., 3,270 ft³/s.

Table 6.--First version of prediction equations for flood magnitude and frequency.

Formulas for computing flood discharges for a given recurrence interval are given below. These formulas were superseded. If these formulas are used, be aware that for some combinations of basin characteristics Q50 might be lower than Q25, Q25 lower than Q10, and Q10 lower than Q5. However, these equations have a lower standard error than the equations in the text. The difference is shown in the table.

Recurrence interval	Exceedance probability in percent	Formulas	Percent standard error	Difference in percent standard error	Number of sites
<u>Area I</u>					
1.25	80	7.62 A ^{0.819} p ^{0.556} (St+1) ^{-0.175} (T+1) ^{0.120}	54	2	97
2	50	12.2 A ^{0.813} p ^{0.500} (St+1) ^{-0.201} (T+1) ^{0.162}	49	1	97
5	20	21.9 A ^{0.812} p ^{0.442} (St+1) ^{-0.218} (T+1) ^{0.163}	48	0	97
10	10	20.6 A ^{0.824} p ^{0.482} (St+1) ^{-0.266} (T+1) ^{0.172}	45	0	64
25	4	14.9 A ^{0.827} p ^{0.660} (St+1) ^{-0.324} (T+1) ^{0.058}	47	1	33
50	2	42.8 A ^{0.894} p ^{0.546} (St+1) ^{-0.185} (T+1) ^{-0.161}	39	3	21
100	1	-Not Shown-	--	-	15
<u>Area II</u>					
1.25	80	1.59 A ^{0.980} p ^{0.816} (St+1) ^{-0.127} (T+30) ^{-0.095} (F+1) ^{-0.258}	79	4	163
2	50	5.73 A ^{0.925} p ^{0.735} (St+1) ^{-0.171} (T+30) ^{-0.189} (F+1) ^{-0.252}	73	4	163
5	20	16.5 A ^{0.877} p ^{0.692} (St+1) ^{-0.205} (T+30) ^{-0.287} (F+1) ^{-0.224}	75	3	163
10	10	19.8 A ^{0.856} p ^{0.709} (St+1) ^{-0.218} (T+30) ^{-0.318} (F+1) ^{-0.157}	78	1	132
25	4	13.1 A ^{0.837} p ^{0.758} (St+1) ^{-0.193} (T+30) ^{-0.244} (F+1) ^{-0.104}	58	1	50
50	2	6.44 A ^{0.816} p ^{0.477} (St+1) ^{-0.315} (T+30) ^{0.268} (F+1) ^{0.084}	58	10	26
100	1	-Not Shown-	--	--	19

EXPLANATION OF SYMBOLS USED IN FIGURES 4-1
THROUGH 4-18.

2580

▲ Active stations used in analysis

2610

△ Discontinued stations used in analysis
Station numbers are without state prefix 15

—40— Mean annual precipitation (inches) from
National Weather Service (1972)

—8°— Mean minimum January temperature (°F)
from Johnson and Hartman (1969)

Area boundary

Base for following figures from U.S. Geological
Survey map E (scale 1:2,500,000) of Alaska

MAP INDEX

ARCTIC

1. West Arctic
2. Colville
3. East Arctic

NORTHWEST

4. Kotzebue Sound
5. Norton Sound

YUKON

6. Lower Yukon
7. Central Yukon
8. Koyukuk
9. Upper Yukon
10. Tanana
11. Upper Yukon-Canada

SOUTHWEST

12. Kuskokwim Bay
13. Bristol Bay
14. Aleutian

SOUTH-CENTRAL

15. Kodiak-Shelikof
16. Cook Inlet
17. Gulf of Alaska

SOUTHEAST

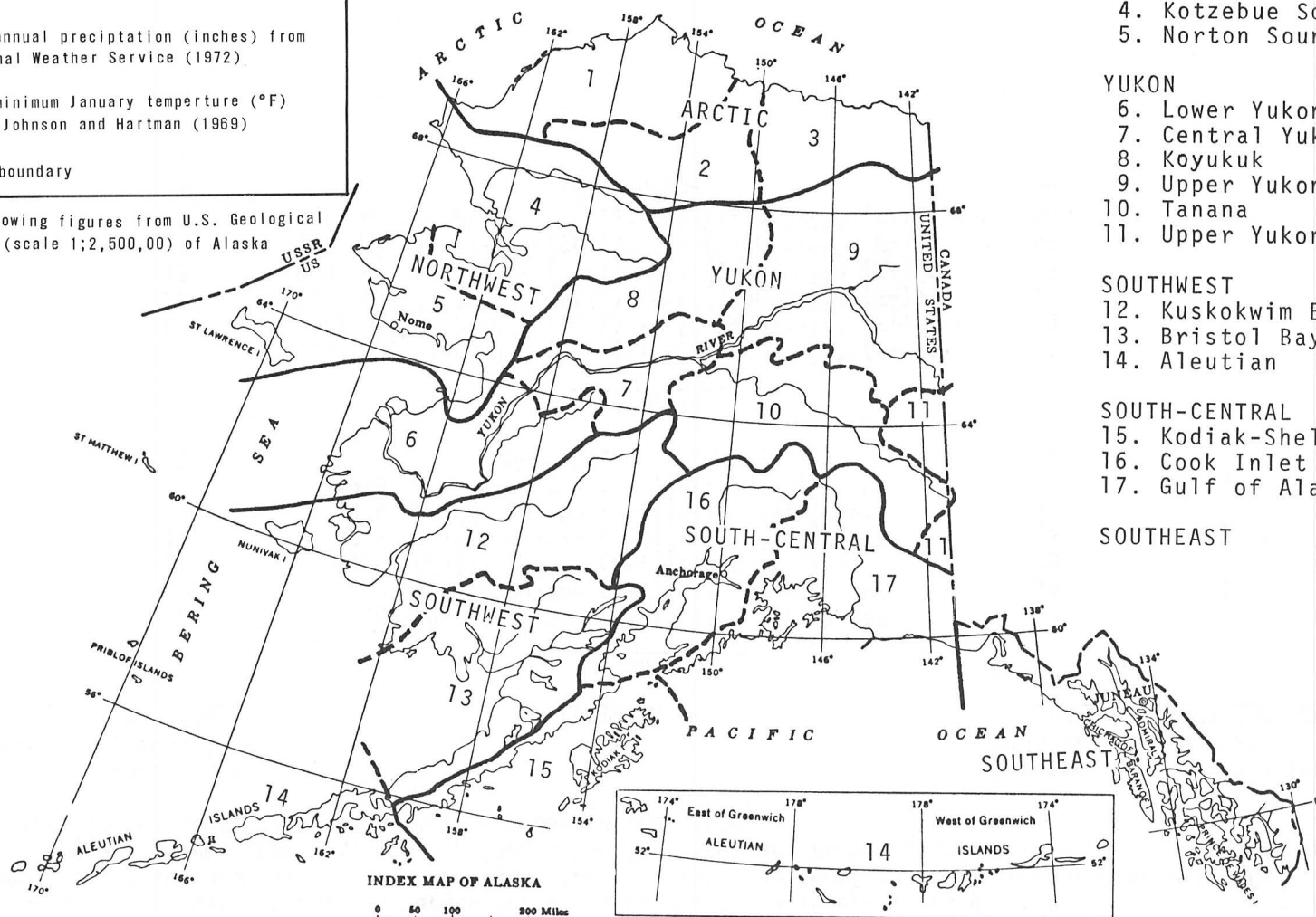


Figure 3.--Map index and symbols used in figures 4-1 through 4-18.

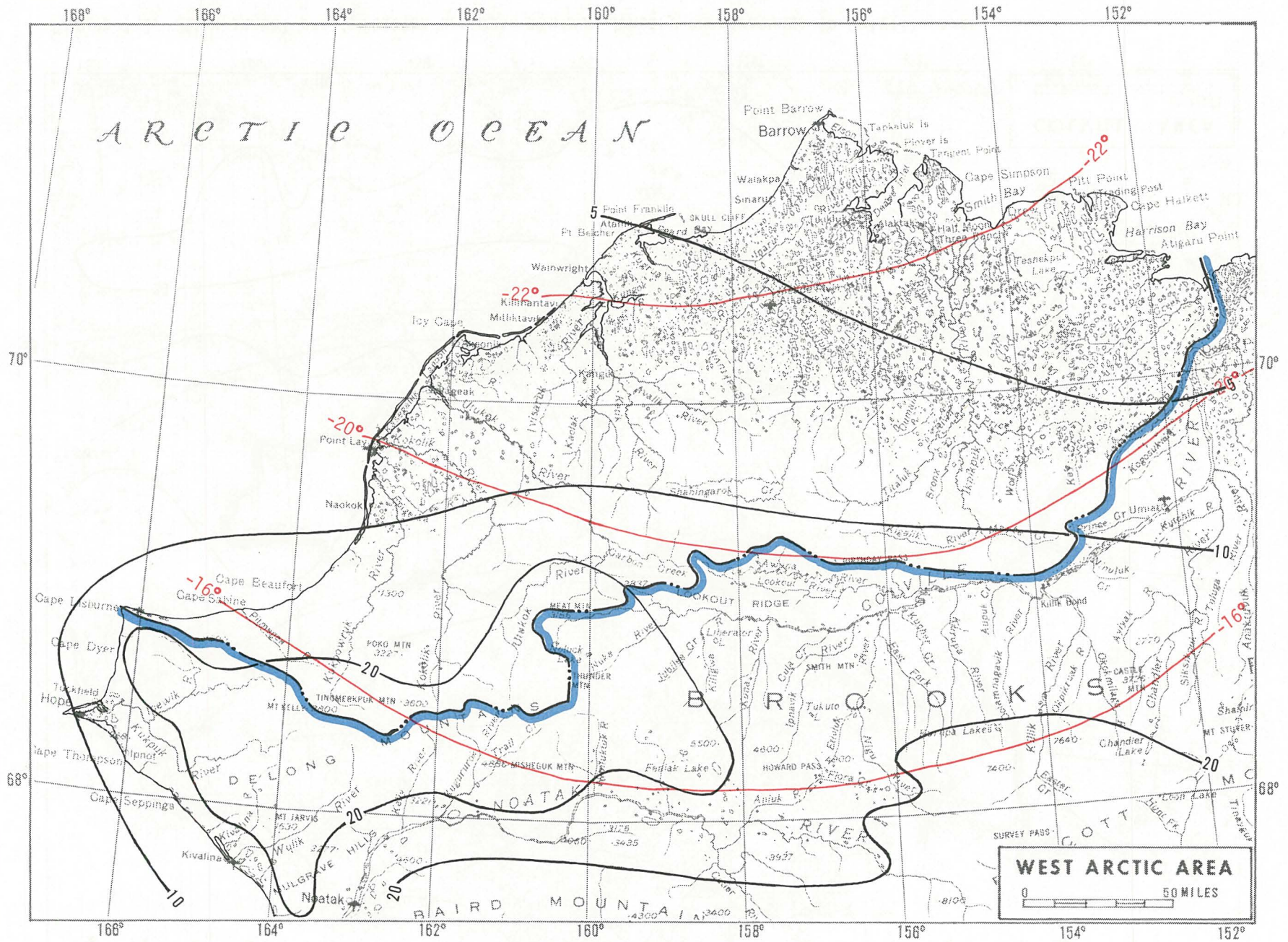


Figure 4-1.--Mean annual precipitation and mean minimum January temperatures in west Arctic area.

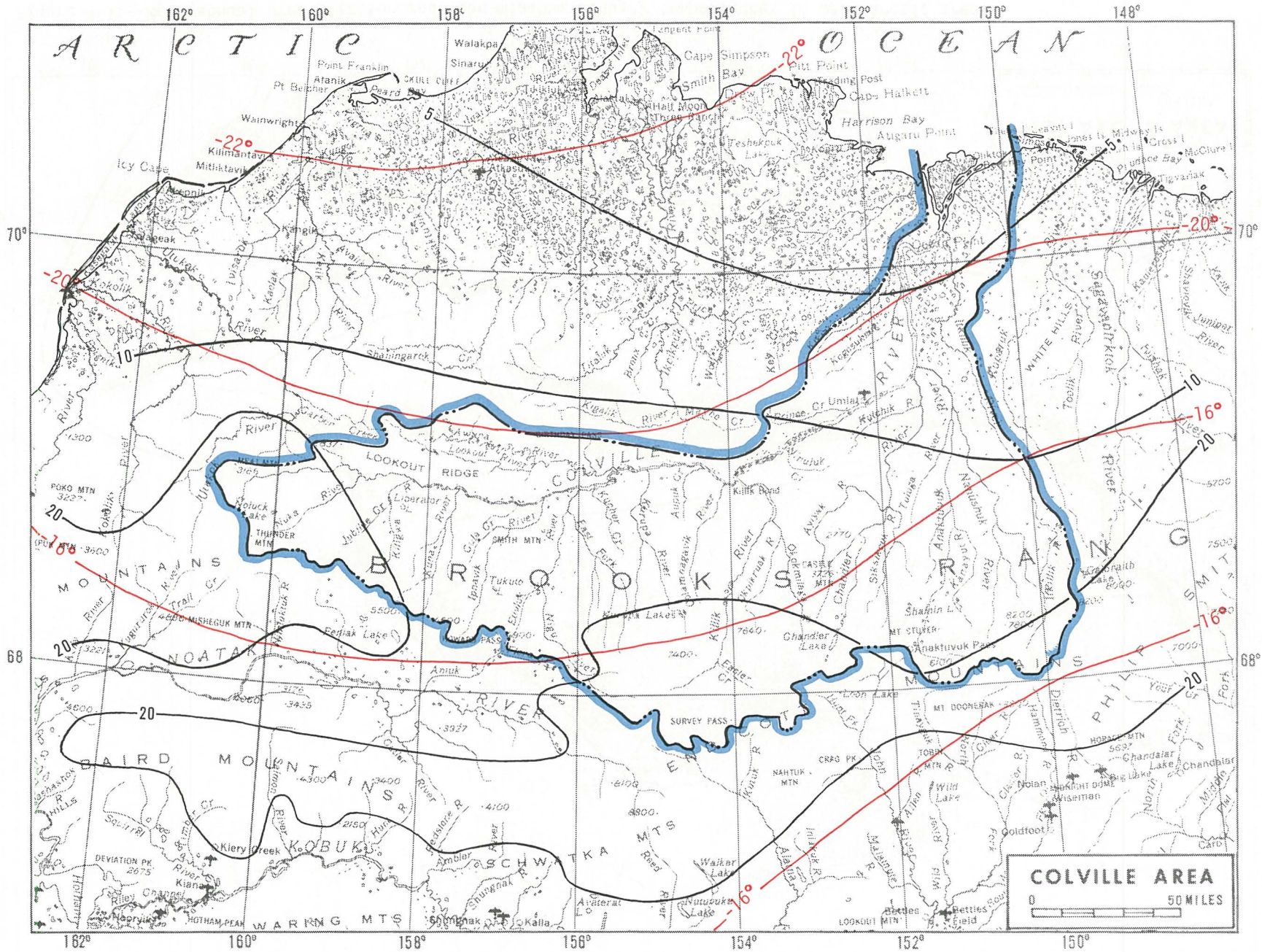


Figure 4-2.--Mean annual precipitation and mean minimum January temperatures in Colville area.

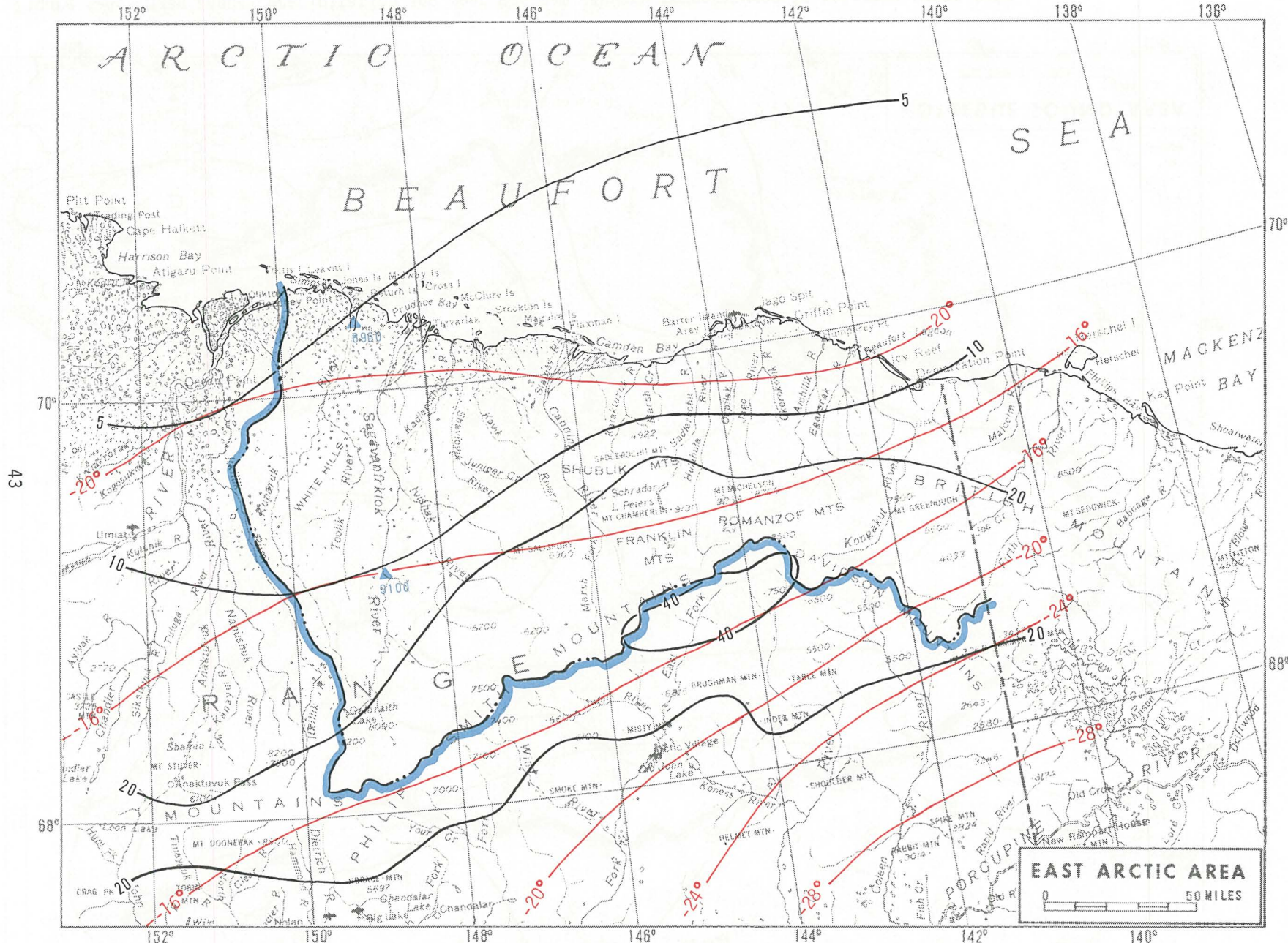


Figure 4-3.--Mean annual precipitation and mean minimum January temperatures in east Arctic area.

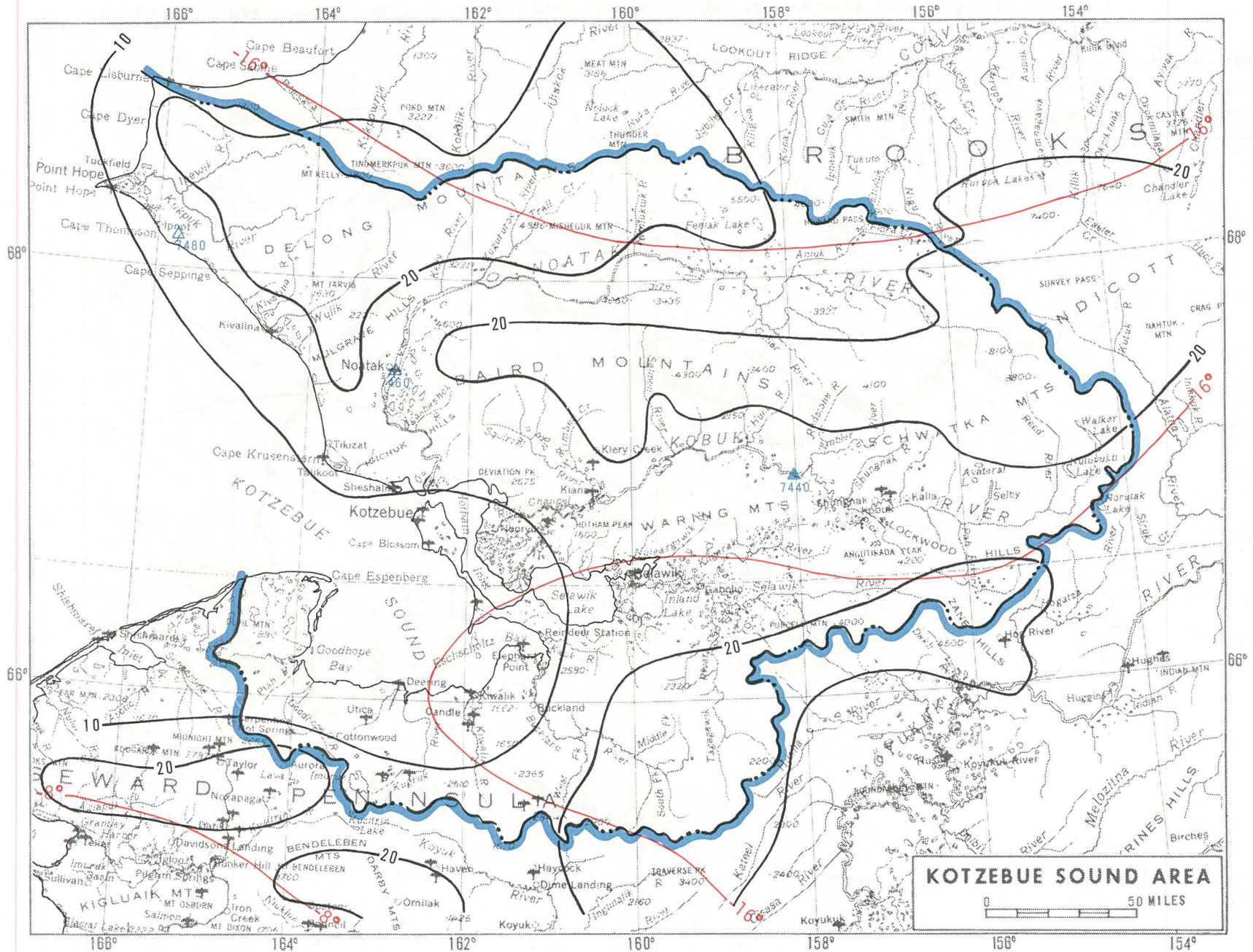


Figure 4-4.--Mean annual precipitation and mean minimum January temperatures in Kotzebue Sound area.

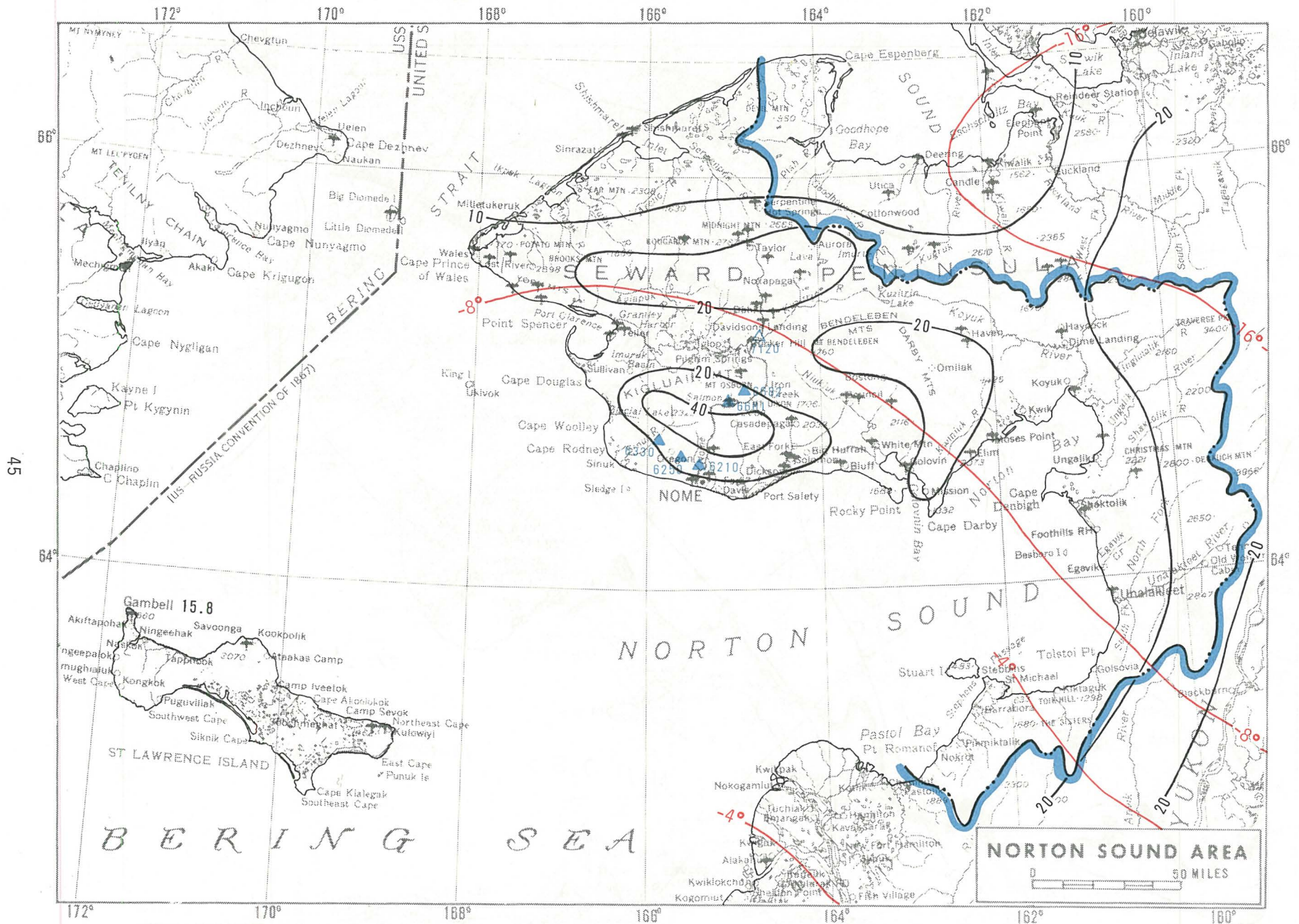


Figure 4-5.--Mean annual precipitation and mean minimum January temperatures in Norton Sound area.

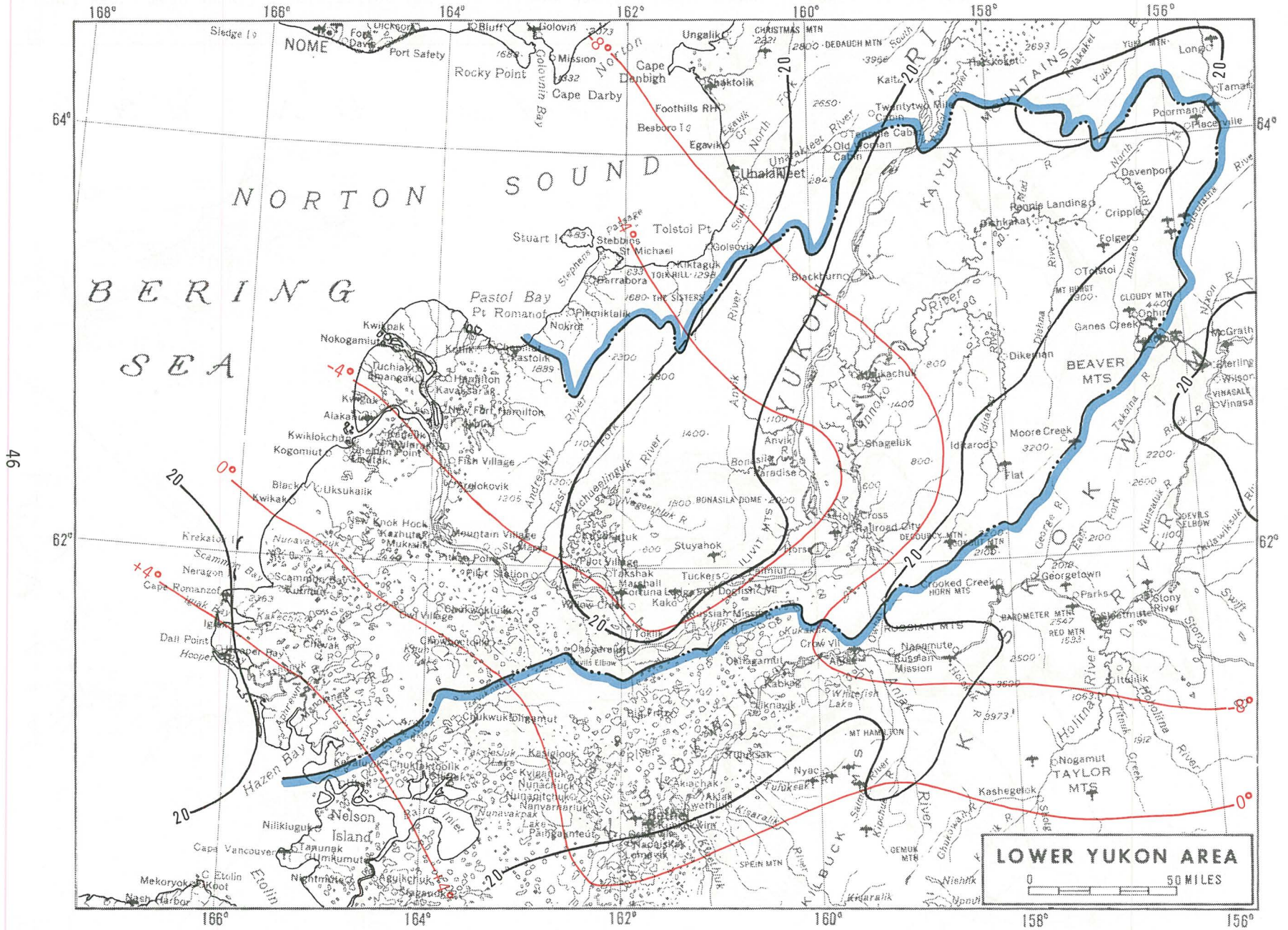


Figure 4-6.--Mean annual precipitation and mean minimum January temperatures in lower Yukon area.

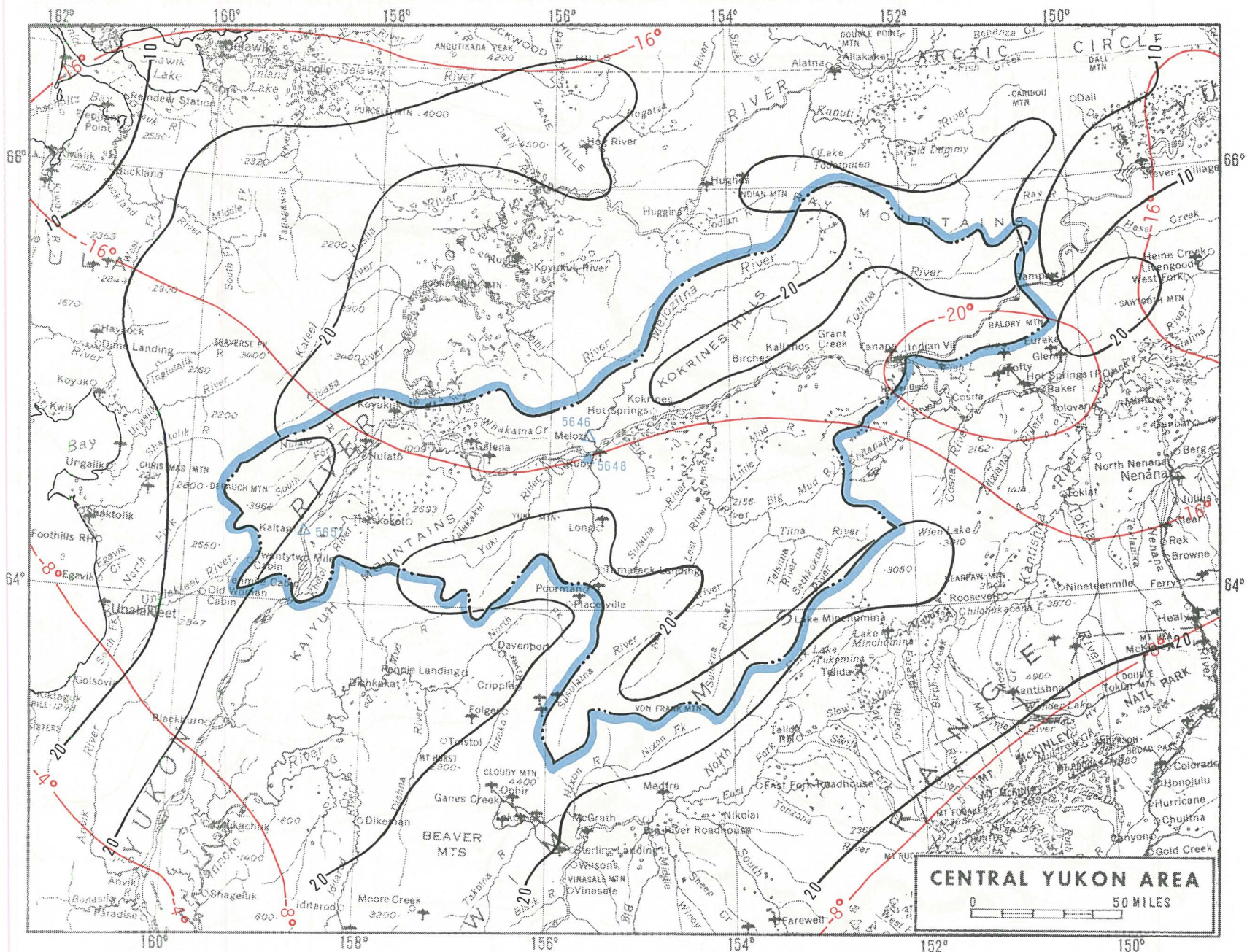


Figure 4-7.--Mean annual precipitation and mean minimum January temperatures in central Yukon area.

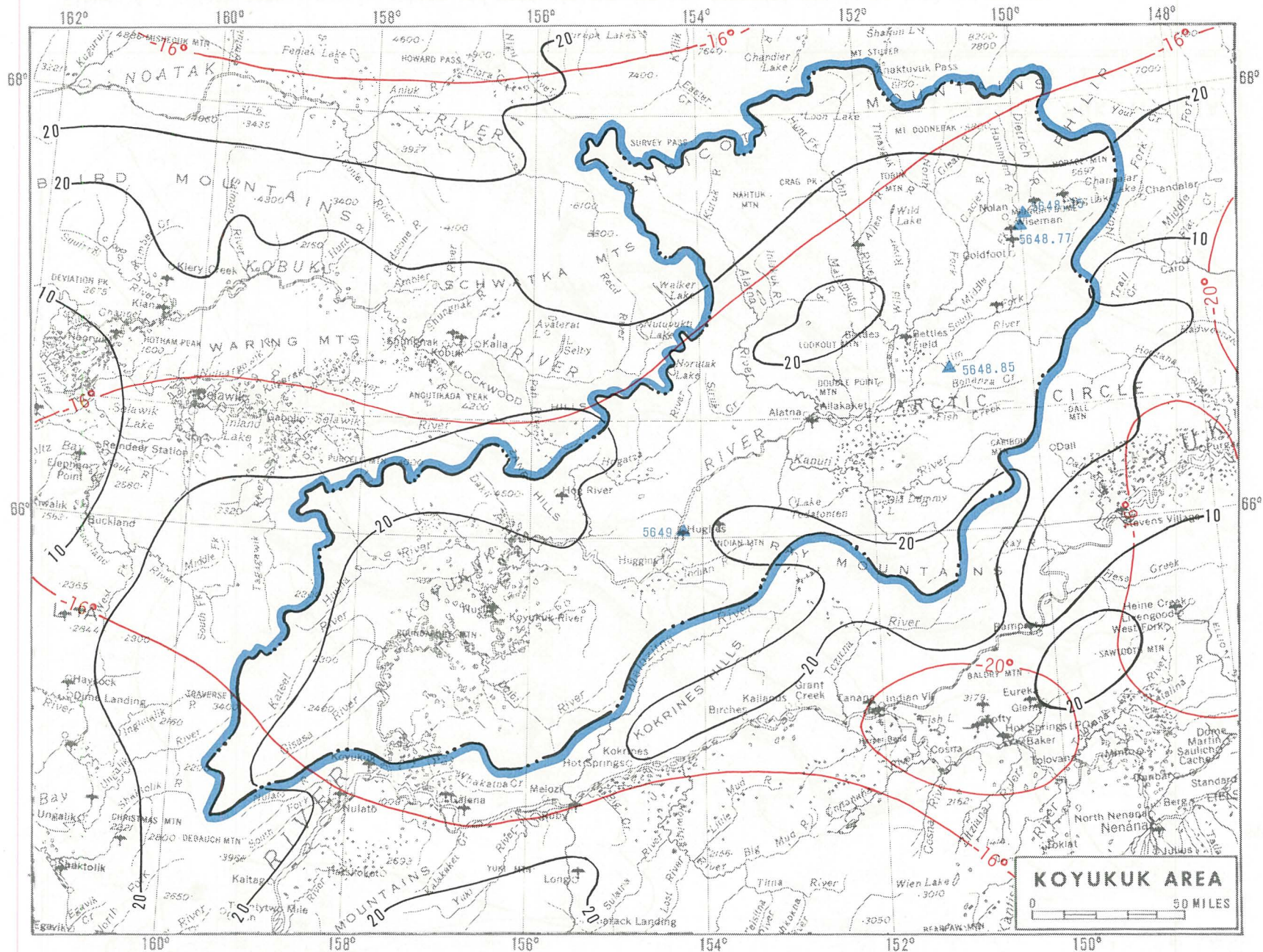


Figure 4-8.--Mean annual precipitation and mean minimum January temperatures in Koyukuk area.

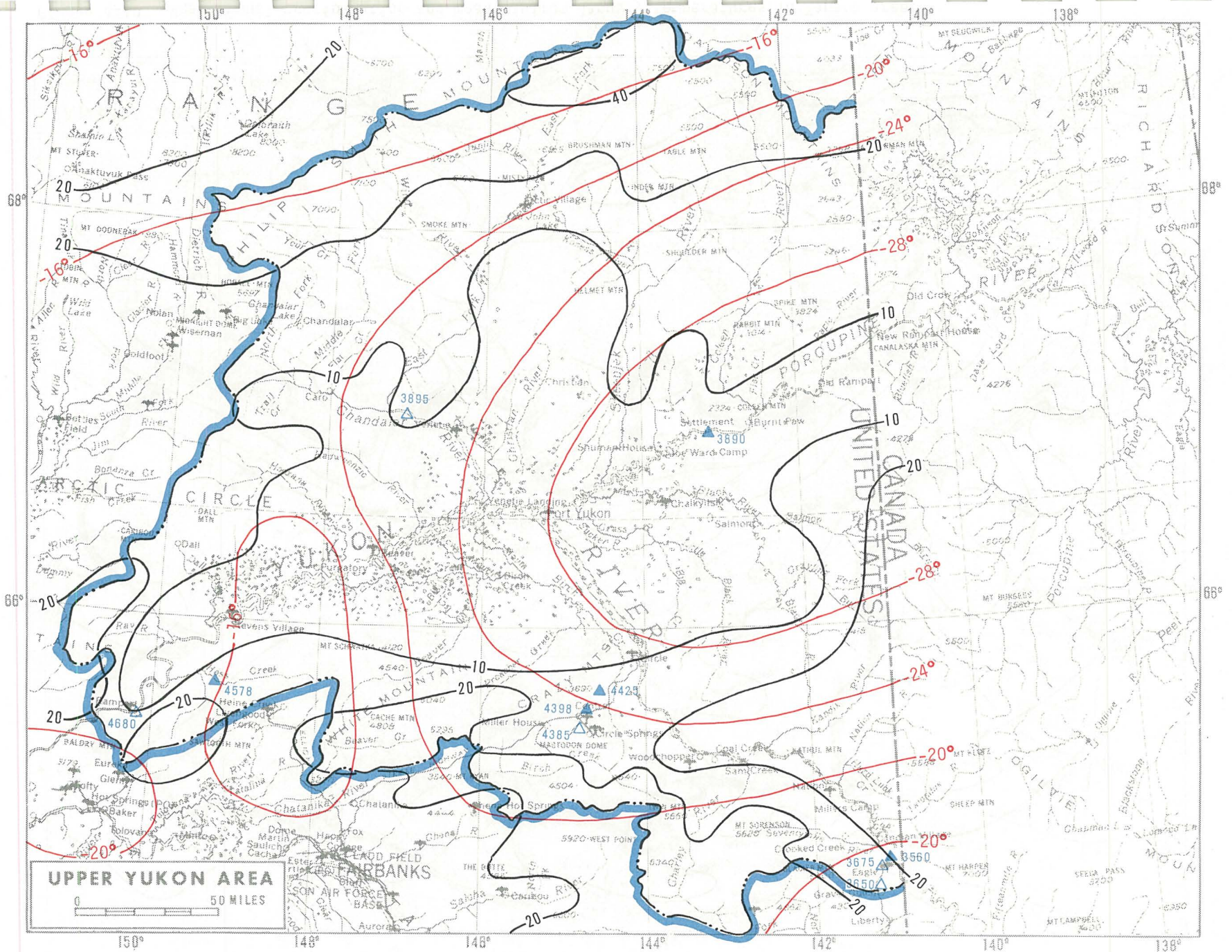


Figure 4-9.--Mean annual precipitation and mean minimum January temperatures in upper Yukon area.

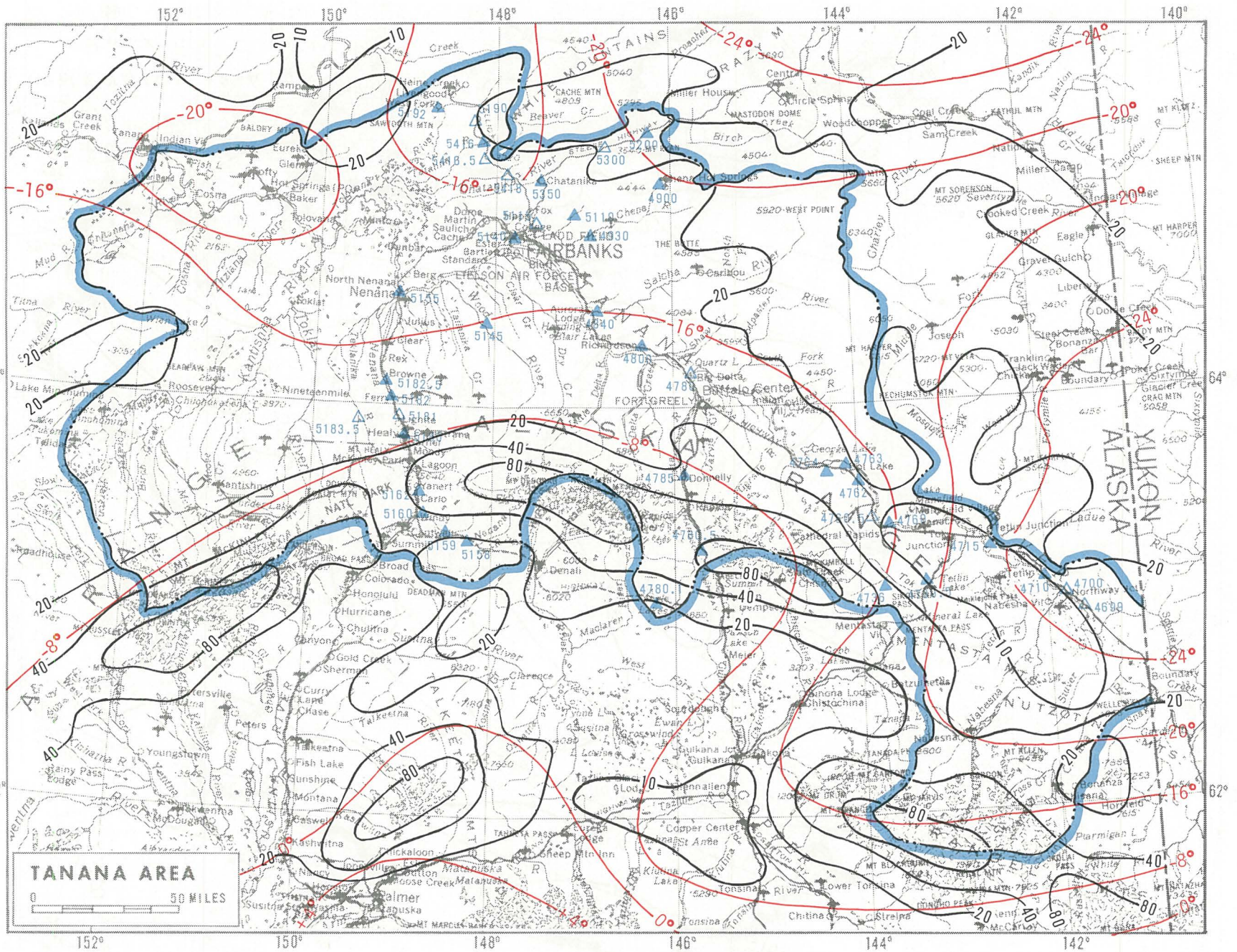


Figure 4-10 Mean annual precipitation and mean minimum January temperatures in Tanana area.

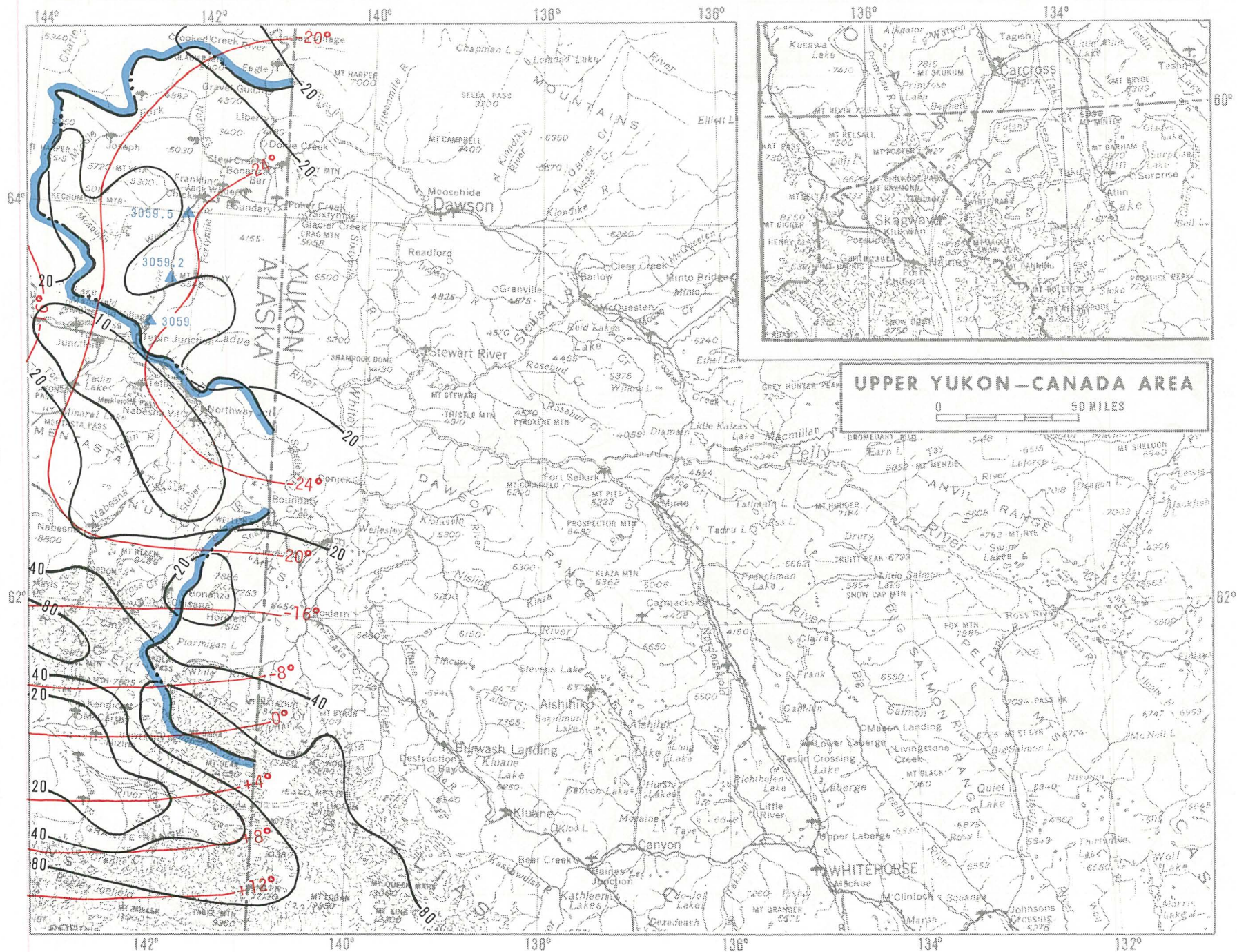


Figure 4-11.--Mean annual precipitation and mean minimum January temperatures in upper Yukon-Canada area.

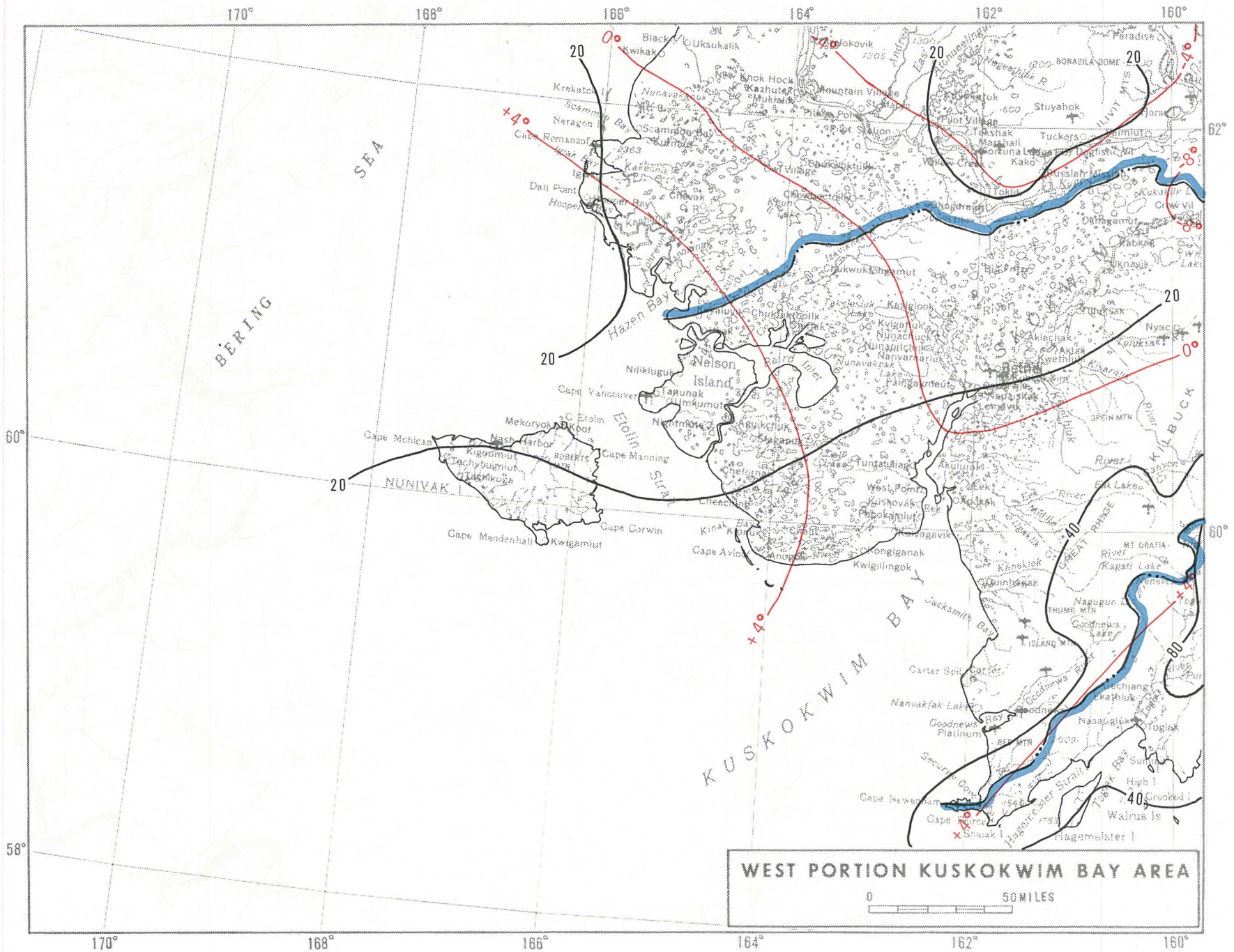


Figure 4-12a.--Mean annual precipitation and mean minimum January temperatures in west portion kuskokwim bay area.

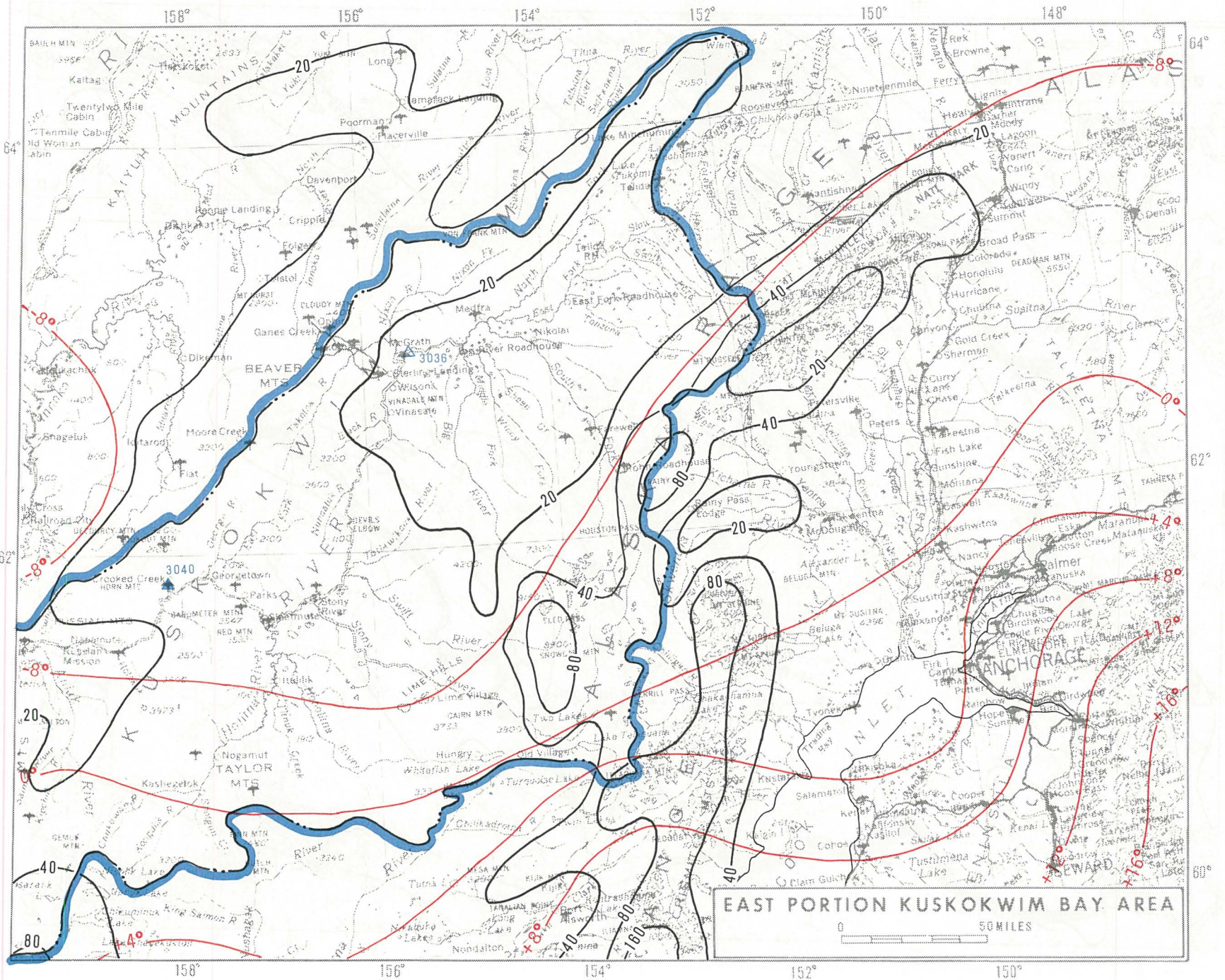


Figure 4-12b.--Mean annual precipitation and mean minimum January temperatures in east portion Kuskokwim Bay area.

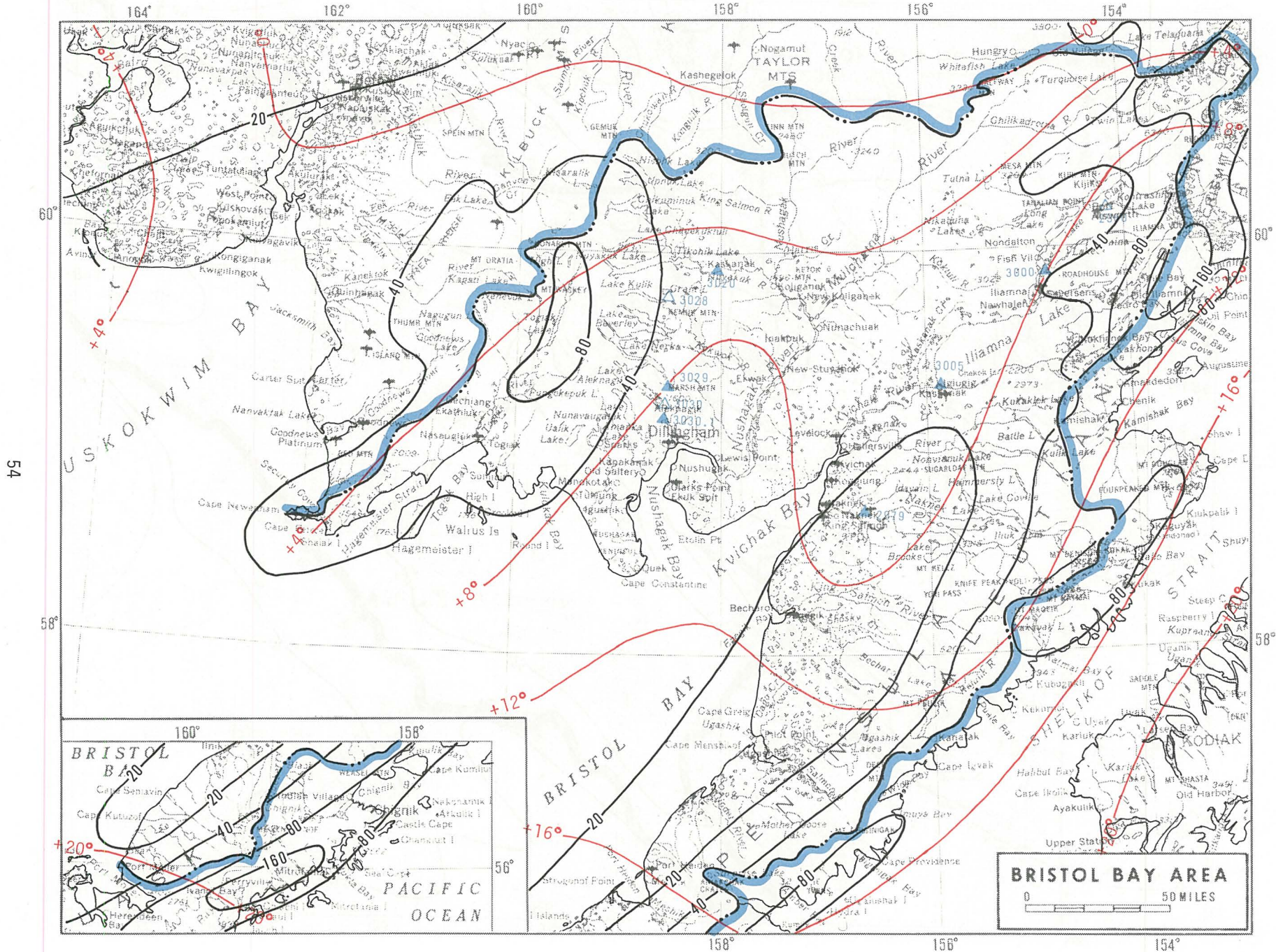


Figure 4-10. Mean annual precipitation on a mean annual maximum temperature isotherm in the Bristol Bay area.

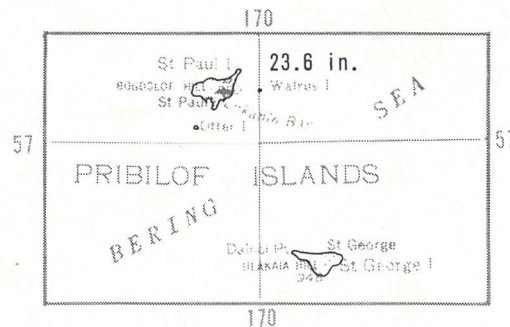
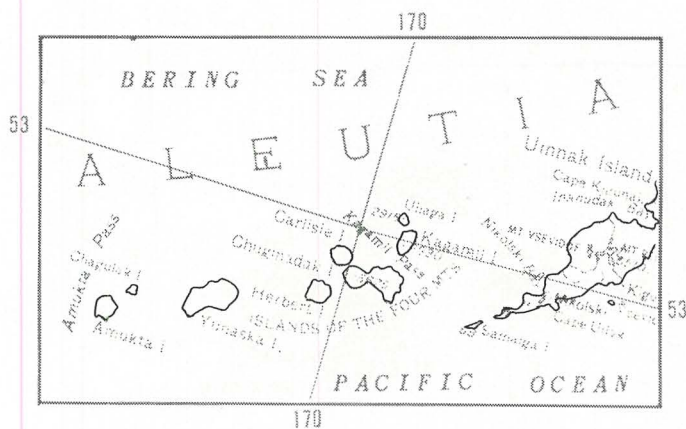
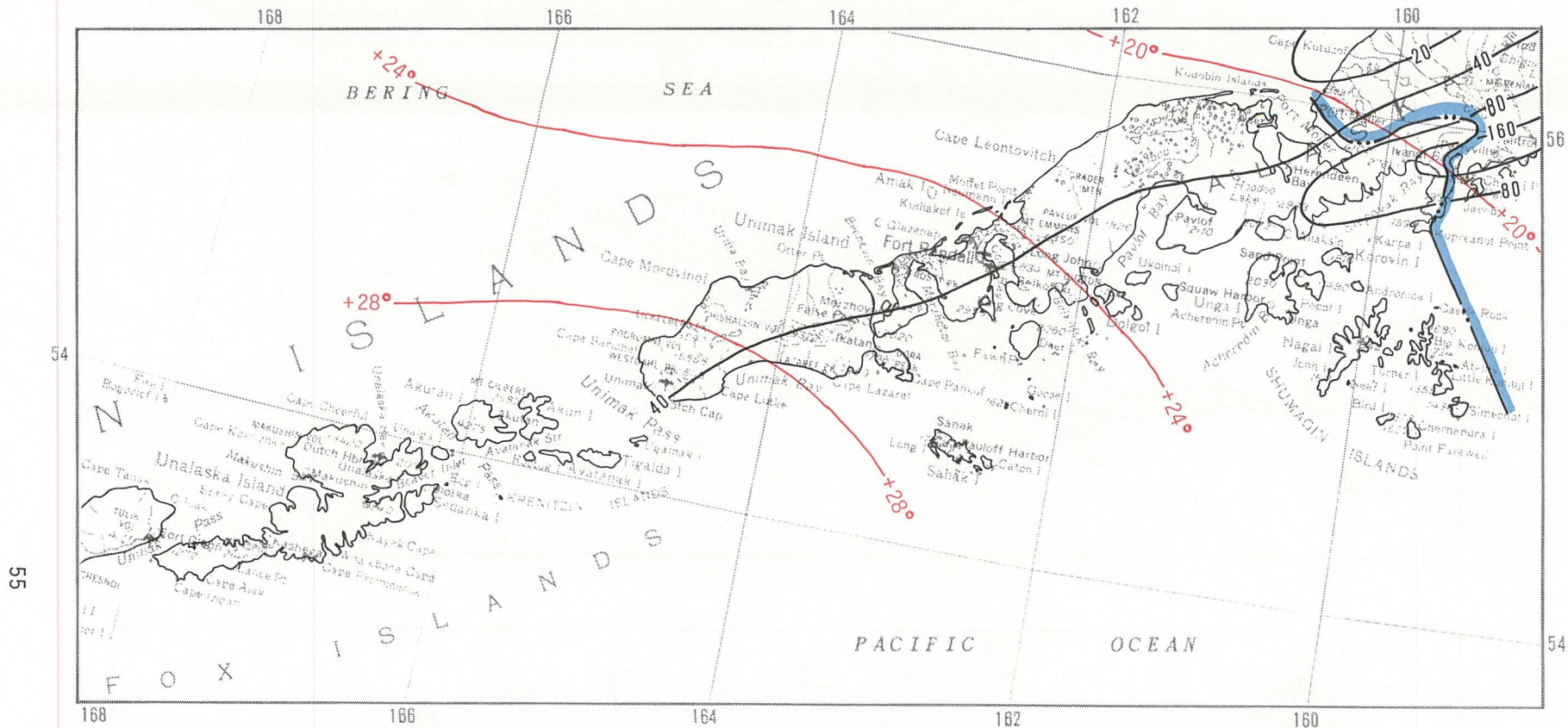


Figure 4-14a.--Mean annual precipitation and mean minimum January temperatures in east portion Aleutian area.

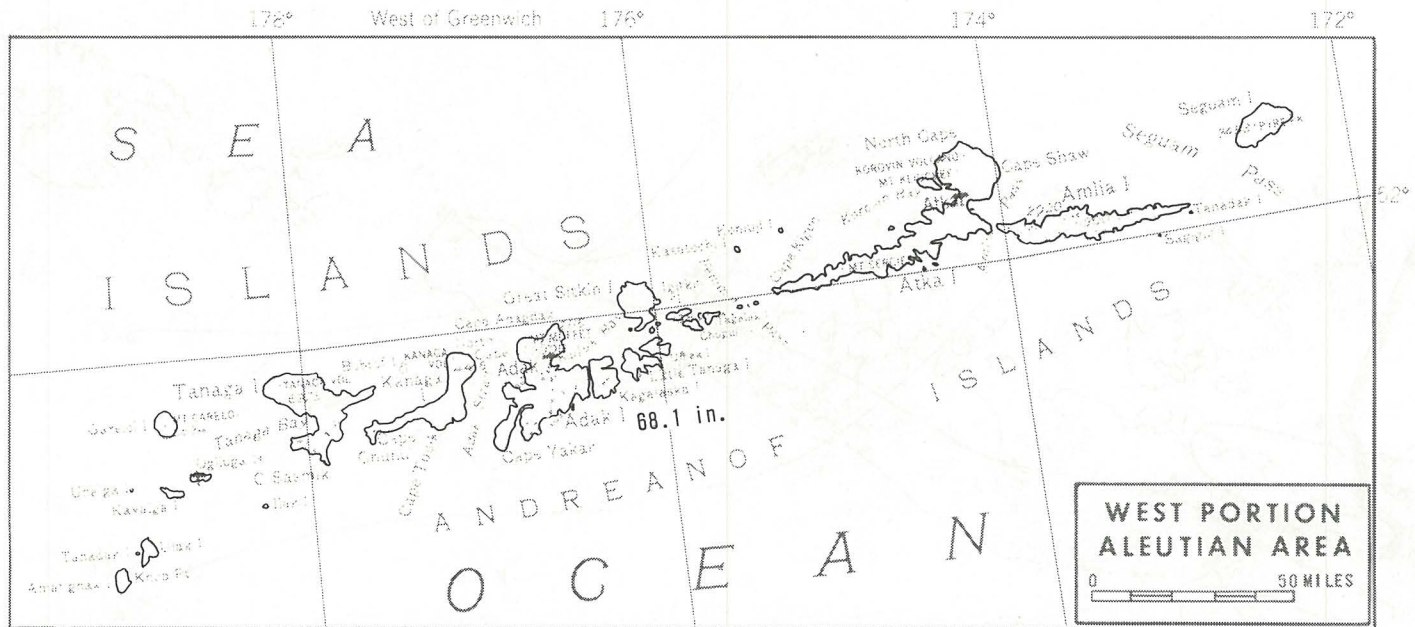
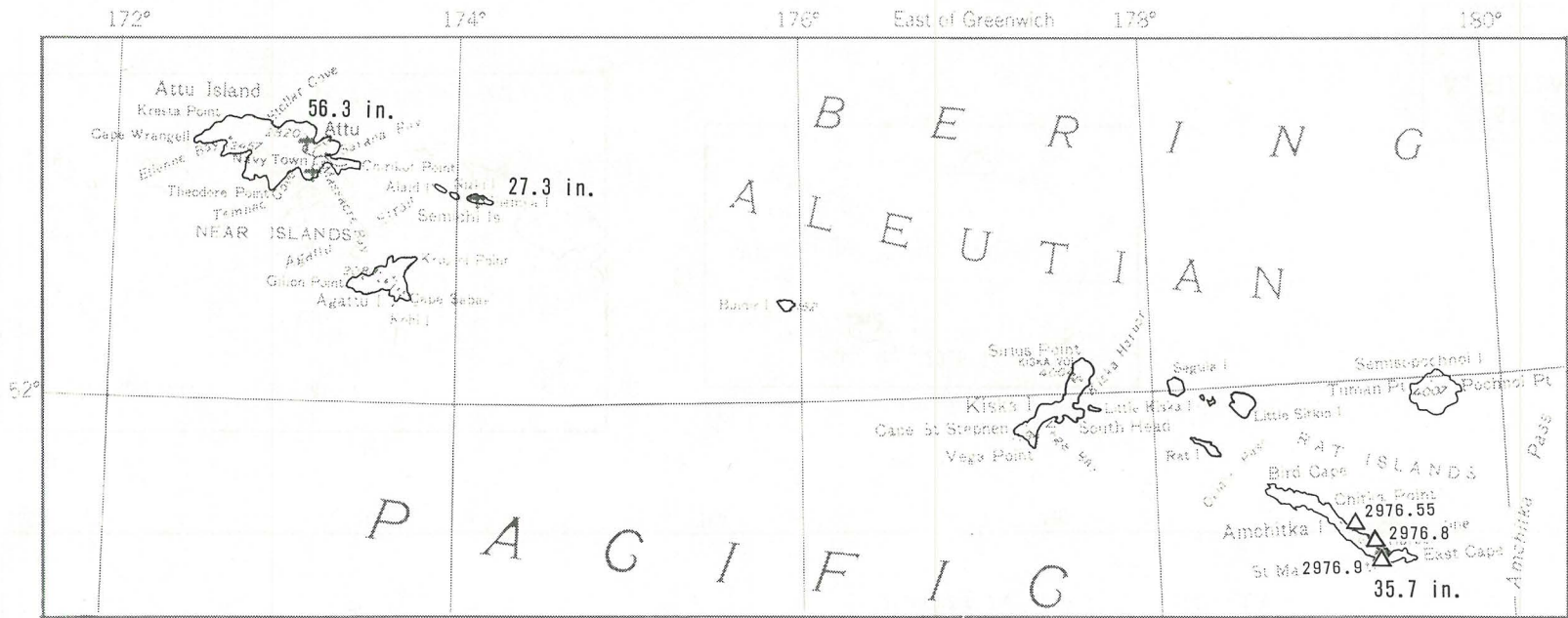


Figure 4-14b.--Mean annual precipitation and mean minimum January temperatures in west portion Aleutian area.

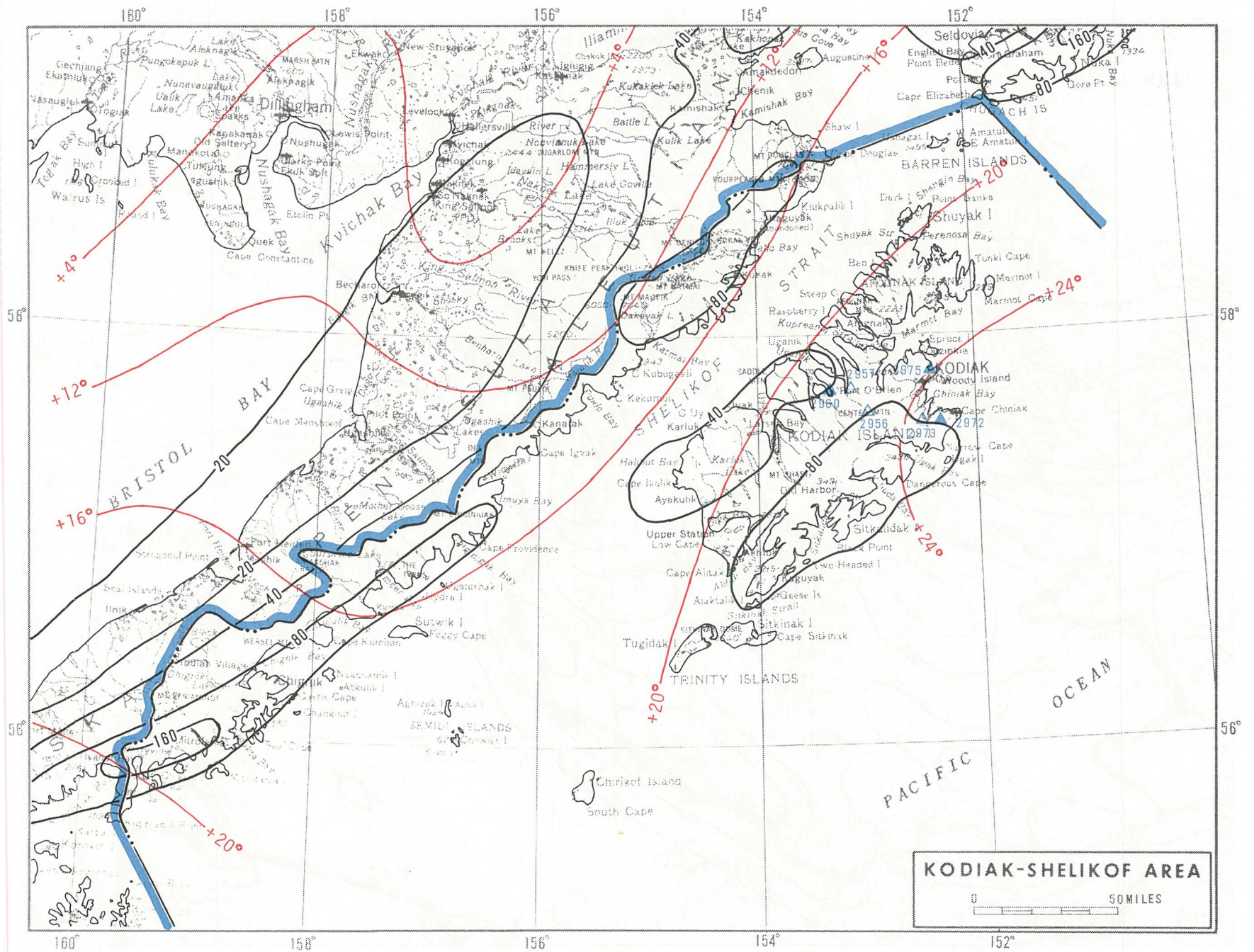


Figure 4-15.--Mean annual precipitation and mean minimum January temperatures in Kodiak-Shelikof area.

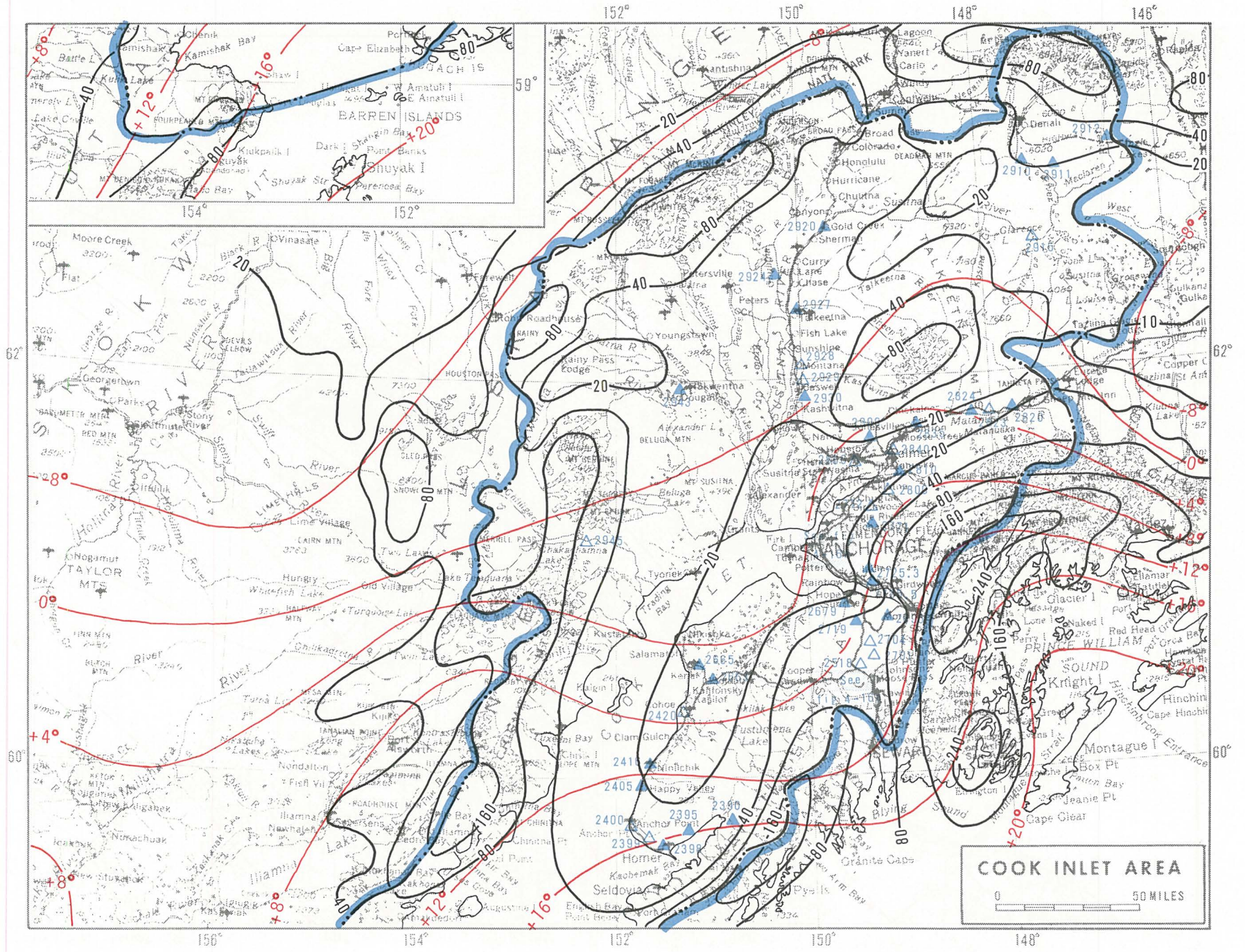


Figure 4-16.--Mean annual precipitation and mean minimum January temperatures in Cook Inlet area.

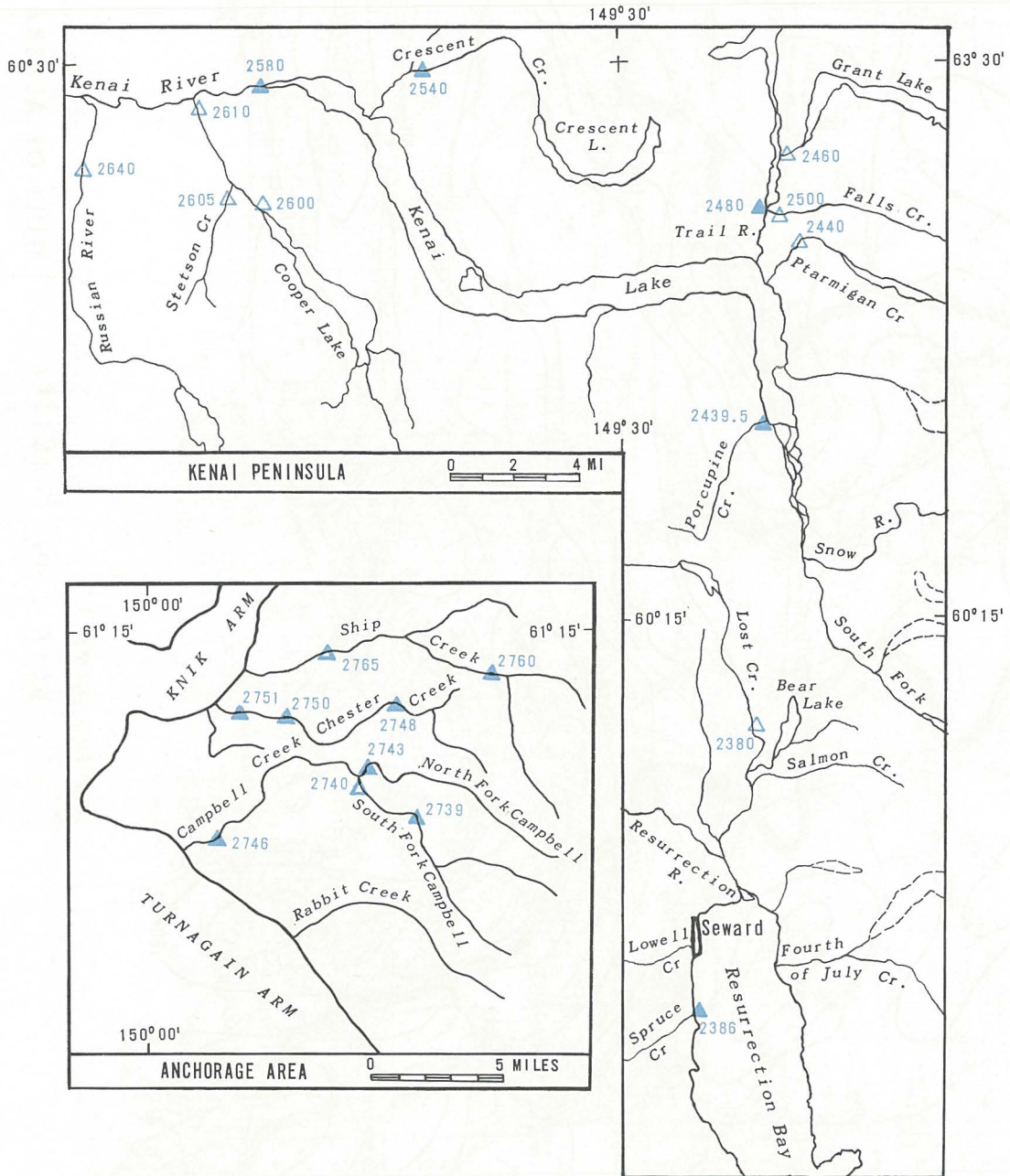


Figure 4-16a.--Details for figure 4-16.

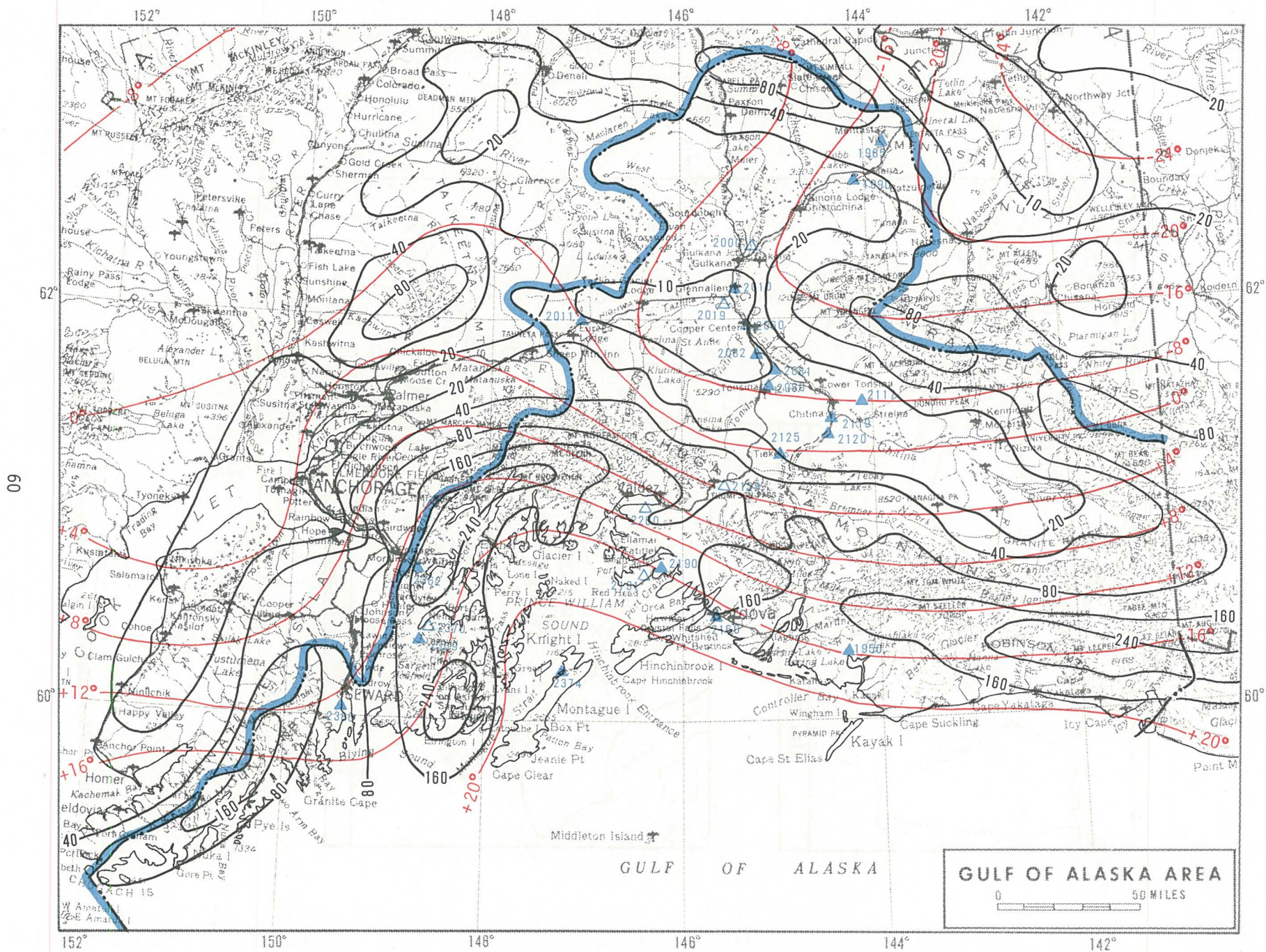


Figure 4-17 Mean annual precipitation and mean minimum January temperatures in Gulf of Alaska area.

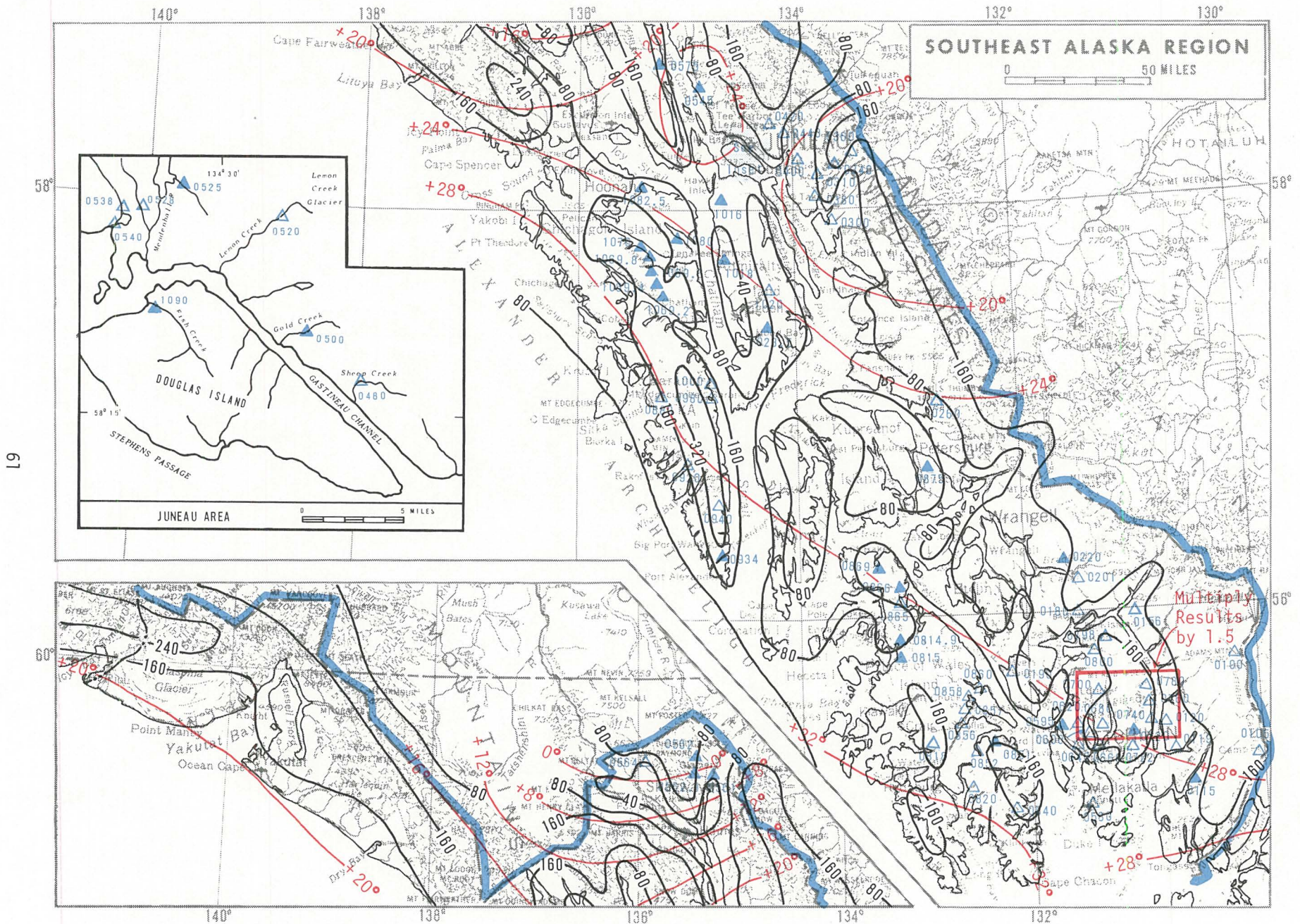


Figure 4-18.--Mean annual precipitation and mean minimum January temperatures in southeast Alaska. Anomalous peak discharge area outlined in red.